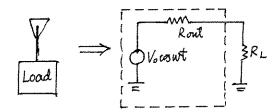
Thevenin Equivalent: Vs = Vo cos wt Rs = Rout



Average power delivered to load = (IRMS) 2RL,

$$I_{RMS} = \frac{V_{RMS}}{R_{out} + R_L}$$
,  $V_{RMS} = \frac{V_o}{\sqrt{2}} \implies I_{RMS} = \frac{V_o}{\sqrt{2} (R_{out} + R_L)}$ 

Average power = 
$$(l_{RMS})^2 R_L = \frac{V_0^2 R_L}{2(R_{out} + R_L)^2}$$
 (Eq. 1)

Plot of Average Power

When RL is small, Eq. I is small.

When RL is large, Eq. I is also small.

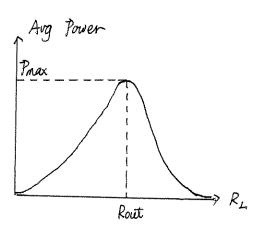
So for some RL Between zero and infinity, the average power will reach its peak. Let's take the derivative of Eq. I with respect to

$$\frac{\partial}{\partial R_L} \left[ \frac{V_o^2 R_L}{2(Rout + R_L)^2} \right] = \frac{V_o^2}{2(Rout + R_L)^2} - \frac{V_o^2 R_L}{(Rout + R_L)^3}$$

Setting it to zero and solve for  $R_L$ 

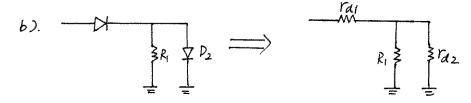
$$\frac{V_3^2}{2(\text{Rout } + R_L)^2} = \frac{V_3^2 R_L}{(\text{Rout } + R_L)^3} \Rightarrow \frac{(\text{Rout } + R_L)}{2} = R_L$$

$$\Rightarrow$$
 Rout  $\dagger R_L = 2R_L \Rightarrow R_L = Rout$ 



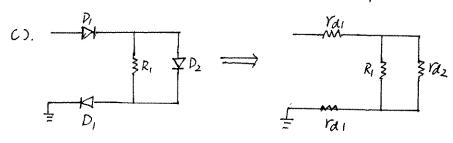
2) In small signal operation, a diode can be replaced by a linear resistor if changes are small.

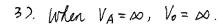


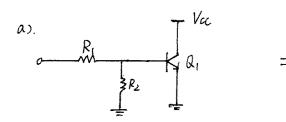


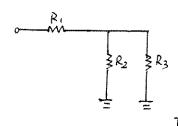
Rin = Yai + Rill Yd2

(// means in parallel)

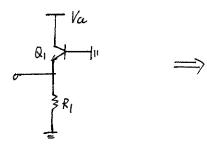


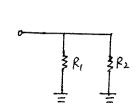






Ы.



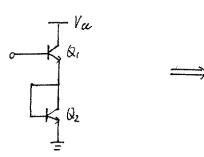


Replacing Q1 by its equivalent resistance see at emitter

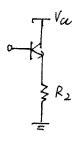
$$Q_1 = \frac{1}{2} I_{11}$$

$$Q_2 = \frac{1}{2} I_{11} I_{12}$$

c).



So  $Rin = R_1 // R_2 = Rin // (\frac{1}{g_{ms}} // r_{21})$ 

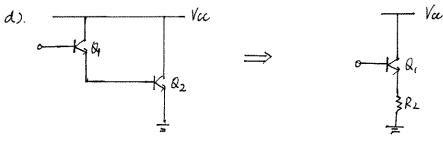


Replacing 82 by its equivalent diode-connected resistante

$$R_2 = \left(\frac{1}{g_{\text{max}}} / | Y_{\text{max}} \right)$$

$$R_2 = \left(\frac{1}{g_{\text{max}}} / | Y_{\text{max}} \right)$$

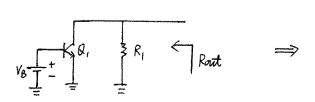


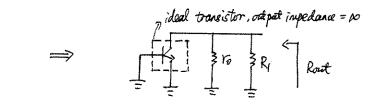


Replacing 
$$Q_2$$
 by its equivalent resistance seen at Base.  $R_2 = Y_{2.2}$ 

(Please refer to the textbook for all the equivalent resistances)

- 4). Since the problem doesn't say  $V_A = \infty$ , ro must be considered in derivation.
- a). Short VB since its a DC source, and replace Q1 with an ideal transistor with its output resistance.



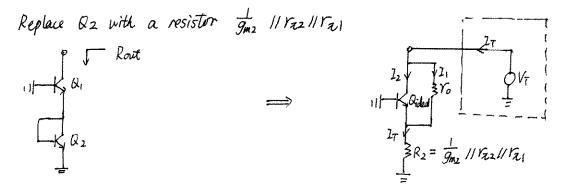


So Rout = R1/110/10 = R1/110



By drawing the small-signal model, it's easy to tell  $V_{BE} = D$  and Rout =  $Y_0$ 

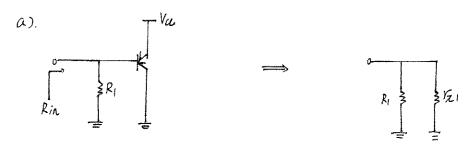
C). Replace Q1 with an ideal transistor and an output impedance Y01.

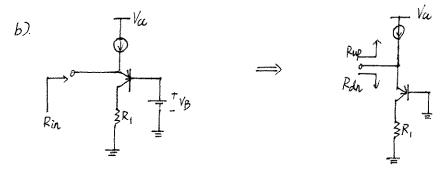


Here,  $r_{2,1}$  is included in  $R_2$  because it is also connected from emitter to ground and it accounts for the base awrent of  $R_1$ .

4) 
$$I_{1} = \frac{V_{1} - 2\tau R_{2}}{\gamma_{0}}$$
,  $I_{2} = g_{M1}(0 - 1\tau R_{2})$   
 $I_{7} = I_{1} + I_{2} = \frac{V_{7} - I_{7}R_{2}}{\gamma_{0}} - g_{M1}I_{7}R_{2}$   
 $\Rightarrow I_{7} + \frac{I_{7}R_{2}}{\gamma_{0}} + g_{M}I_{7}R_{2} = \frac{V_{7}}{\gamma_{0}}$   
 $\Rightarrow \frac{V_{7}}{I_{7}} = \gamma_{0}\left(1 + \frac{R_{2}}{\gamma_{0}} + g_{M1}R_{2}\right)$   
 $\Rightarrow Road = \frac{V_{1}}{I_{7}} = \gamma_{0}\left(1 + g_{M1}R_{2}\right) + R_{2}$   
 $= \gamma_{0}\left[1 + g_{M1}\left(\frac{1}{g_{M2}} / \gamma_{22} / \gamma_{21}\right)\right] + \frac{1}{g_{M2}} / \gamma_{22} / \gamma_{21}$   
Usually  $\frac{1}{g_{M}} < \gamma_{2}$ , and if  $Q_{1} = Q_{2}$   
 $Road \approx \frac{1}{g_{M}} + 2\gamma_{0}$ 

5). 
$$V_A = \infty$$
,  $r_0 = \infty$ 

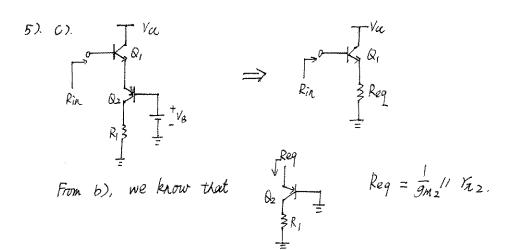


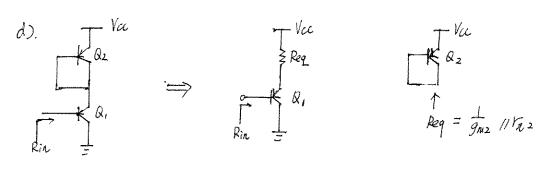


Rin = Rup 1/Rdn. Rup = 10, since a DC awrect source is open.

Finding Rdn:

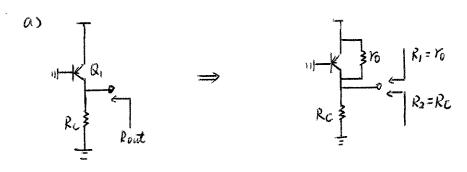
So Rin = Rup // Rdn = 10 // 9m // 2 = 9m //2

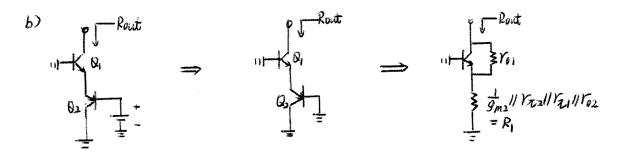




$$\begin{array}{c}
e) \\
R_{in} & \downarrow \\
\end{array}$$

Rin =  $r_{22}$ . Q<sub>1</sub> plays no role here since its connected to the collector of  $Q_2$ . It can not be seen from the Base of  $Q_2$ . 6) Since the problem doesn't state VA = 00, ro is not so.





As shown is problem 4) c).

$$Rout = R_1 + Y_{01} + g_{m2} Y_{01} R_1 = Y_{01} + (1 + g_{m1} Y_{01}) R_1$$

$$= Y_{01} + (1 + g_{m1} Y_{01}) (\frac{1}{g_{m2}} || Y_{22} || || Y_{21} || || Y_{02}).$$

7) a). 
$$I_{BE} = \frac{V_{CC} - V_{BE}}{100 \text{ K}\Omega}, I_{C} = \frac{\beta I_{B}}{100 \text{ K}\Omega}$$

$$V_{BE} = V_{T} \ln \left(\frac{I_{C}}{I_{S}}\right)$$

Guess 
$$V_{BE} = 0.7V$$
,
$$I = \beta \left( \frac{V_{CC} - V_{BE}}{100 \text{ K}\Omega} \right) = 1.8 \text{ mA}$$

$$V_{BE} = V_{T} \ln \left( \frac{I_{C}}{I_{C}} \right) = 0.747 \text{ V}, \text{ Not } 0.7V$$
, Yeiterate

$$V_{8E}=0.747\,V$$
,  $I_{c}=1.753\,\text{mA}$   
 $Verify\ V_{8E}$ ,  $V_{8E}=V_{T}\ln\left(\frac{I_{c}}{I_{s}}\right)=0.746v$ , converged

$$V_{CE} = 2.5 - (1.753)(0.5K) = 1.62V$$
 $V_{CE} > V_{SE}$ ,  $Q_1$  in forward active region.

$$I_c = 1.754 \text{ mA} \qquad V_{CE} = 1.62V$$

$$I_B = 17.54 \text{ MA} \qquad V_{BE} = 0.746V$$

$$\uparrow \qquad \qquad \uparrow \qquad \qquad \downarrow \qquad \qquad$$

$$I_{81} = 2.5V$$
 $I_{81} = 2.5 - (V_{BE1} + V_{BE2})$ 
 $I_{80}$ 

$$V_{SE_1} = V_T ln \left( \frac{I_{c_1}}{I_s} \right), V_{SE_2} = V_T ln \left( \frac{I_{c_2}}{I_s} \right)$$

$$I_{c1} = \beta \left( \frac{2.5 - 1.6}{100 \text{K}} \right) = 0.9 \text{mA}$$

$$V_{BE1} = V_T ln \left( \frac{I_c}{I_s} \right) = 0.728 V$$
, not 0.8V, reiterate

$$I_{c_1} = \beta \left( \frac{2.5 - (2)(0.728)}{100 \text{ Kg}} \right) = 1.042 \text{ mA} = I_{c_2}$$

$$V_{BE1} = V_{BE2} = V_{7} ln \left( \frac{I_{c}}{I_{s}} \right) = 0.733 V$$
, iterate one more

$$I_{c_1} = I_{c_2} = \beta \left( \frac{2.5 - (2\chi_0.753)}{100 \text{KM}} \right) = 1.034 \text{ mA}$$

$$I_{c_1} = I_2 = |.034 \text{ mA}|$$

$$V_{BE_1} = V_{BE_2} = V_T \ln \left(\frac{I_c}{I_s}\right) = 0.733$$
, Converges.

$$V_{CE_1} = 2.5 - 0.733 - (1.034)(1KR) = 0.733V$$
 $V_{CE} = V_{8E}$ ,  $A_{2}$  at the edge of active region.
 $V_{8E_2} = V_{CE_2} = 0.733V$ 

## Operating Point:

$$I_{c_1} = (.034 \text{mA})$$
  $I_{c_2} = 1.034 \text{mA}$   
 $I_{B_1} = 0.01 \text{ mA}$   $I_{B_2} = 0.01 \text{ mA}$   
 $V_{BE_1} = 0.733 \text{ V}$   $V_{CE_2} = 0.733 \text{ V}$   
 $V_{CE_3} = 0.733 \text{ V}$ 

Although, for  $A_2$   $V_{BE} = V_{CE}$ , it is at the edge of active region, the situation is not as severe as  $Q_2$ 's. Since  $Q_2$ 's configuration will always render  $V_{BE} = V_{CE}$ , whereas for  $Q_2$ ,  $V_{CE}$  may drop below  $V_{BE}$ .

$$I_{B} = \frac{V_{cc} - (V_{BE} + 0.5)}{I_{OVK}}$$

$$I_{C} = \beta I_{B}$$

$$V_{SE} = V_{T} \ln \left(\frac{I_{C}}{I_{S}}\right)$$

$$I_{B} = \frac{V_{cc} - (V_{BE} + 0.5)}{100K}$$

$$I_{c} = \beta I_{B}$$

$$V_{BE} = V_{f} \ln \left(\frac{I_{c}}{I}\right)$$

Guess 
$$V_{BE} = 0.8 \text{ V}$$
,  $I_c = \beta \left( \frac{2 \cdot 5 - 1 \cdot 3}{100 \text{ K}} \right) = 1.2 \text{ mA}$   $V_{BE} = V_T \ln \left( \frac{I_c}{I_s} \right) = 0.736 \text{ V}$ , Not 0.8, Yeiterate

$$V_{BZ} = 0.736V$$
,  $I_c = \beta \left( \frac{2.5 - (0.736 + 0.5)}{100 \text{ K}\Omega} \right) = 1.26 \text{ mA}$ 

$$V_{BE} = V_T ln \left( \frac{I_c}{I_s} \right) = 0.738 V$$
, (onverges.

VCE > VBE, QI in forward active region Operating Point

$$I_c = 1.26 \text{ mA}$$
  $V_{BE} = 0.738 \text{ V}$   
 $I_B = 0.0126 \text{ mA}$   $V_{CE} = 0.74 \text{ V}$ 

$$|V(c)| = 2.5 \text{ V.}$$

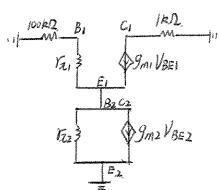
$$|OORD| = |V_{R}| = 2.5 \text{ V.}$$

$$|OORD| = |V_{R}| = |$$

$$g_{M} = \frac{1c}{V_{T}} = \frac{1.754 \text{mA}}{26 \text{mV}} = 0.0675 \text{ S}$$

$$r_{ZI} = \frac{\beta}{9m} = \frac{100}{0.0675} \Omega = 1482.3 \Omega.$$

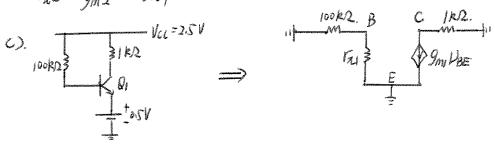
b). 
$$|C| = 25V$$
 $|C| = 25V$ 
 $|C| = 25V$ 



$$g_{m1} = \frac{1}{V_T} = \frac{1.034 mA}{2b mV} = 0.04 S$$

$$g_{n2} = \frac{1}{V_T} = \frac{1034 \text{ mA}}{26 \text{ mV}} = 0.04 \text{ S}$$

$$r_{22} = \frac{\beta}{g_{M2}} = \frac{100}{0.04} \Omega = 2500 \Omega$$



$$g_{MI} = \frac{2}{V_T} = \frac{1.26 \text{m/A}}{26 \text{mV}} = 0.048 \text{ S}$$

$$r_{21} = \frac{\beta}{g_{m1}} = \frac{100}{0.048} \Omega = 2083 \Omega$$

9). a)
$$\begin{array}{c}
V(c = 2.5)V \\
3RD
\end{array}$$

$$\begin{array}{c}
R_{th} \\
R_{th}
\end{array}$$

$$\begin{array}{c}
R_{th} \\
R_{th}
\end{array}$$

$$\begin{array}{c}
R_{th} \\
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$$\begin{array}{c}
R_{th}$$

$$\begin{array}{$$

The voin Equivalent 
$$Rth = \frac{34 \times 16}{34 + 16} k\Omega = 10.88 k \Omega$$
.  
 $Vth = \frac{2.5 V \times 16}{34 + 16} = 0.8 V$ .

$$I_c = \beta \left( \frac{0.8 - V_{BE}}{10.88K} \right)$$
,  $V_{BE} = V_T I_N \left( \frac{I_c}{I_s} \right)$ 

Assume 
$$V_{BE} = 0.7$$
,  
 $I_c = \beta \left( \frac{0.8 - 0.7}{10.88 \text{ K} \Lambda} \right) = 0.92 \text{ mA}$   
 $V_{BE} = V_T \ln \left( \frac{I_c}{T} \right) = 0.734 \text{ V}$ 

Iterate, 
$$V_{3E} = 0.734V$$
  
 $I_c = \beta \left( \frac{0.8 - 0.734}{10.88KR} \right) = 0.61 \text{ m/A}$ 

$$VBE = V_1 ln \left(\frac{I_c}{I_s}\right) = 0.724 V$$

Iterate, VBE = 0.724V

$$I_c = \beta \left( \frac{0.8 - 0.724}{10.88 \text{ K} \Omega} \right) = 0.699 \text{ mA}$$

$$I_c = \beta \left( \frac{0.8 - 0.727}{10.88 \text{ KA}} \right) = 0.67 \text{ m/s}$$

$$V_{BE} = V_{T} ln \left(\frac{I_{c}}{I_{s}}\right) = 0.726 V$$
, Converged !!

$$V_{CE} = 2.5 - (0.67)(3KM) = 0.49$$
  
 $V_{8E} - V_{CE} = 0.236V$ , Soft-saturation, Still ok.

## Operating Point:

$$I_c = 0.67 \text{mA}$$
  $V_{8E} = 0.726 \sqrt{}$   
 $I_R = 6.7 \text{MA}$   $V_{CZ} = 0.49 \text{V}$ 

9) b). 
$$\frac{25V}{9k\Omega^{\frac{3}{2}}}$$
  $Rh = \frac{9 \times 16}{9 + 16} k\Omega = 5.76 k\Omega$   
 $16k\Omega^{\frac{3}{2}}$   $Rh = 25V \times \frac{16}{9 + 16} = 1.6V$ 

$$Rm = \frac{9 \times 16}{9 + 16} kD = 5.76 kD$$

$$Wh = 250 \times \frac{16}{9 + 16} = 1.60$$

$$I_{c_1} = \beta \left( \frac{1.6 - (V_{BE_1} + V_{BE_2})}{5.76\mu\Omega} \right)$$

$$V_{BE} = V_{BE_1} = V_{BE_2} = V_{T} \ln \left( \frac{I_c}{I_s} \right)$$

$$I_{c_1} = I_{c_2} = I_{c}$$

$$I_{c_1} = I_{c_2} = I_{c}$$

$$V_{BE} = V_{BE} = V_{BE} = V_{T} ln \left( \frac{I_{c}}{I_{c}} \right)$$

$$I_{c_{1}} = I_{c_{2}} = I_{c}$$

$$I_c = \beta \left( \frac{1.6 - 1.4}{5.76 \text{ kg}} \right) = 3.47 \text{ mA}$$

$$V_{BE} = V_f \ln \left( \frac{I_c}{I_s} \right) = 0.769 \text{ V}$$

Iterate, VBE = 0.769V

$$I_c = \beta \left( \frac{1.6 - 62(0.769)}{5.76 \text{ KJ}} \right) = 1.08 \text{mA}$$

9)
$$I_{c} = 1.08 \text{ mA}$$

$$V_{8E} = V_{T} \ln \left(\frac{I_{c}}{I_{s}}\right) = 0.738 \text{ V}$$
Iterate, 
$$V_{8E} = 0.738 \text{ V}$$

$$I_{c} = \beta \left(\frac{1.6 - 2(0.738)}{5.76 \text{ KD}}\right) = 2.15 \text{ mA}$$

$$V_{8E} = V_{T} \ln \left(\frac{I_{c}}{I_{s}}\right) = 0.756 \text{ V}$$
Iterate, 
$$V_{8E} = 0.756 \text{ V}$$

$$I_{c} = \beta \left(\frac{1.6 - 2(0.756)}{5.76 \text{ KD}}\right) = 1.53 \text{ mA}$$

$$V_{8E} = V_{T} \ln \left(\frac{I_{c}}{I_{s}}\right) = 0.747 \text{ V}$$
Iterate... (For 3 more times)
$$V_{8E} = 0.757 \text{ J. } I_{c} = 1.74 \text{ mA} \text{ Converged}$$

$$V_{CE} = 2.5 - 0.75 - 1.74 \text{ (0.5)} = 0.88 \text{ V}$$
Operating Point
$$I_{c} = 1.74 \text{ mA}$$

$$I_{c} = 1.74 \text{ mA}$$

$$V_{8E} = 0.757 \text{ (Forward active)}$$

$$V_{8E} = 0.757 \text{ (Edge of forward active)}$$

V== 0.88V

VCE= 0.75V active)

9). c). 
$$V_{L} = 2.5 V$$
.

 $V_{L} = 2.5 V \times \frac{13}{12+13} = 1.3 V$ .

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$$I_c = \beta \left( \frac{1.3 - (0.743 + 0.5)}{6.24 \text{KM}} \right) = 0.913 \text{ mA}$$

$$V_{BE} = V_T ln \left( \frac{I_c}{I_s} \right) = 0.734 V$$

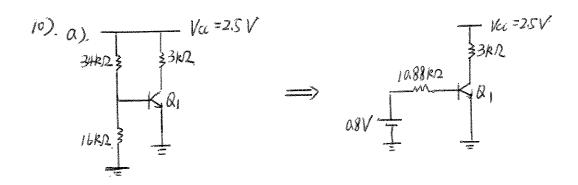
Iterate,  $V_{BE} = 0.734V$   $I_{c} = \beta \left( \frac{1.3 - (0.734 + 0.5)}{6.24 \text{K} \Omega} \right) = 1.06 \text{mA}$ 

$$V_{BE} = V_{1} ln \left( \frac{I_{c}}{I_{s}} \right) = 0.738V$$

$$I_c = \beta \left( \frac{1.3 - (0.738 + 0.5)}{6.24 \text{KN}} \right) = 0.99 \text{mA}$$

$$V_{BZ} = V_T \ln \left( \frac{I_c}{I_s} \right) = 0.736V$$

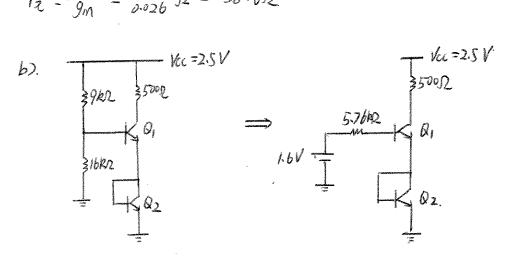
## Operating Point

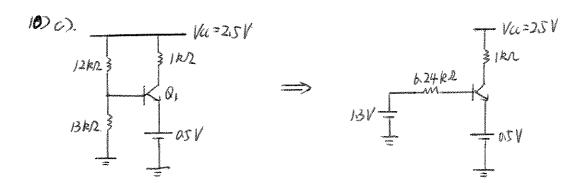


$$\Rightarrow \frac{1088k\Omega}{M} = \frac{3k\Omega}{M} =$$

$$g_{M} = \frac{2c}{V_{T}} = \frac{0.67mA}{26mV} = 0.026S$$

$$r_2 = \frac{\beta}{9m} = \frac{100}{0.026} J_2 = 3846 J_2$$

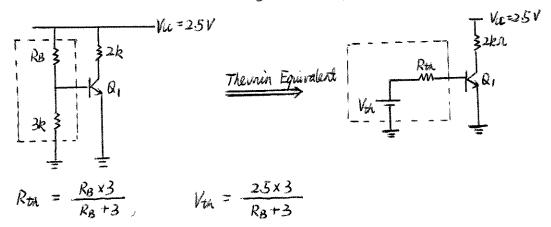




$$g_{m1} = \frac{1c}{V\tau} = \frac{0.99mA}{26mV} = 0.038 S$$

$$\gamma_{21} = \frac{\beta}{9m_1} = \frac{100}{0.038} \Omega = 2632 \Omega$$

11). a). Find the minimum RB that guarantees forward active region.



To maintain Q1 in forward-active region, 
$$V_{CE} \ge V_{BE}$$

$$V_{CE} = V_{CC} - 1_{C} \cdot 2k, \quad I_{C} = \beta I_{B}, \quad I_{B} = \frac{V_{th} - V_{BE}}{R_{th}}$$
So  $V_{CE} = V_{CC} - \beta \left( \frac{V_{th} - V_{BE}}{R_{th}} \right) \cdot 2k$ 

From &

$$V_{CC} - \beta \left( \frac{V_{th} - V_{BE}}{R_{th}} \right) \cdot 2k \geqslant V_{BE}$$
And  $V_{BE} = V_T \ln [2c/2s) = V_T \ln [\beta (V_{th} - V_{BE})/R_{th}/I_S]$ 
Find the minimum RB by iteration. Givess  $V_{BE} = 0.8$  as initial condition.

Use VBE = 0.8, and subsitute Rtn and Vtn into (1), it can be calculated

Check the validity of VBE. With RB 26.178k. from @ VBE = 0.727V.

So the initial guess of VBE is not accurate.

Restants with  $V_{BE} = 0.727$ , it can be calculated from O $R_{B} \gg 7.058 \, k$ . 11) With RB ≥ 706k, from @

Its very close to 0.727. So the results have converged. (Salisty both O&@)

The final answer is

RB > Zobk

b). β charges from 100 to 200, 50 ∂β is 100

$$\frac{\partial V_{CB}}{\partial \beta} = -\left(\frac{V_{M} - V_{BE}}{R_{M}}\right) \cdot 2k$$

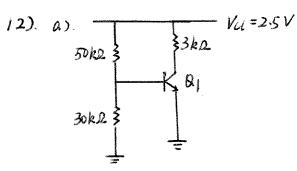
$$\partial V_{\mathcal{B}} = -\left(\frac{V_{th} - V_{BE}}{R_{th}}\right) \cdot 2k \cdot (\partial \beta) = -1.6627$$

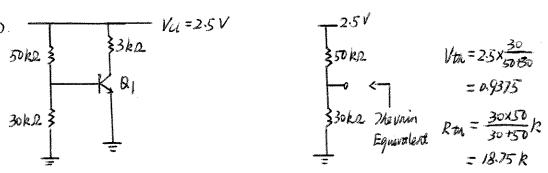
( Forward bias sustained during  $\beta$ 's rising : 1.663 V )

Original VCB = 0.01428

Total net forward bias after \beta has rose to 200:

1-16627+0.01428 = 1648 (V)





Since  $1_c = 0.5 \text{ mA}$ ,  $1_B = \frac{1_c}{B} = 0.05 \text{ mA}$ .

$$Z_B = \frac{V th - V_B E}{R th} \Rightarrow V_{BE} = V th - Z_B \cdot R th = 0.84375$$

$$I_c = I_S e^{(\frac{V_F}{P_c})} \Rightarrow I_S = \frac{I_c}{e^{(V_F/F_c)}} = 4.03 \times 10^{-15} (mA)$$

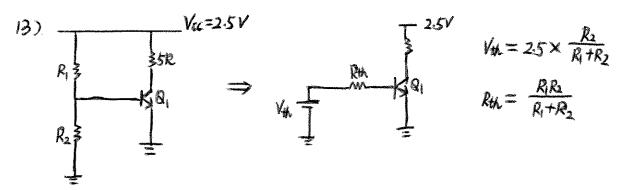
b). At the edge of saturation means  $V_{BE} - V_{CE} = 0$ .

(soft saturation not allowed)

$$V_{CE} = 2.5 - 1c \cdot (3k)$$
, in which  $I_{c} = \beta I_{B} = \beta \left( \frac{V_{m} - V_{BE}}{R_{M}} \right)$   
50  $V_{BE} = 2.5 - \beta \left( \frac{V_{m} - V_{BE}}{R_{M}} \right) \cdot (3k)$ 

Solve this equation:

$$I_S = \frac{2c}{e^{1/3\epsilon/V_T}} = \frac{\beta \left(\frac{Vm - VBE}{RM}\right)}{e^{1/4\epsilon/V_T}} = 7.84 \times 10^{-15} \text{ (mA)}$$



$$R_{in} = R_{th} / V_{in} = R_{th} / V_{fg} = R_{th} / V_{fg} / I_{C} > 10 R_{sh}$$

$$g_{m} > \frac{1}{260R} = 20038 S$$

Let's choose In to be 0.00385

$$g_m = \frac{I_c}{V_T} \Rightarrow I_c = g_m V_T = 0.104 (mA)$$

Let Rin=10 KM

$$I_B = \frac{I_c}{\beta} = \frac{V_h - V_{BE}}{\rho h} \Rightarrow V_h = V_{E} + \frac{I_c \cdot (Rh)}{\beta} = 0.78$$

It can be solved that R1 = 51.710, R2 = 23.44100

This is only one possible solution set. The thought process is more important.

14). If 
$$g_m$$
 at least  $\frac{1}{26} = 0.03848 (D^{-1})$   
Let  $g_m = 0.03848 = \frac{I_c}{V_T} \Rightarrow I_c = 0.99996 (MA)$ .  
 $V_{BE} = V_T M \left(\frac{I_c}{I_S}\right) = 0.82 \text{ V}$   
 $V_{CE} = V_{CL} - I_{CC} \cdot 5k = -2.5$ 

No solution exists because the transister is in saturation mode where  $g_m$  is essentially zero.

Whereas for problem 13),

$$V_{GE} = V_{CC} - I_{C} \cdot 5k = 2.5 - 0.104 \times 5 = 1.98 \vee V_{BE} = 0.76 \mid V_{GE} > V_{BE}$$

So Qi is still in forward-active region.

15). 
$$\frac{1}{R_2}$$
  $\frac{1}{3}$   $\frac{1}{3}$   $\frac{1}{8}$   $\frac{1}{8}$ 

$$R_{in} = \frac{R_{iR_2}}{R_{i}+R_2} / r_{in}, r_{in} = \frac{B}{g_m}$$

$$Rin = \frac{R_1 R_2}{R_1 t R_2} / \frac{B}{g_m}$$

$$Gain = A_0 = g_m R_0 \Rightarrow g_m = \frac{A_0}{R_0} = \frac{I_c}{V_r} \Rightarrow I_c = \frac{A_0}{R_0} V_r$$

$$(I_c \text{ is Set})$$

Bias point analysis:

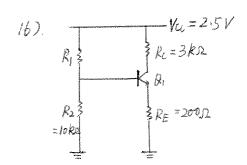
$$\frac{V_{co}R_2}{R_1+R_2} - V_{3E}$$

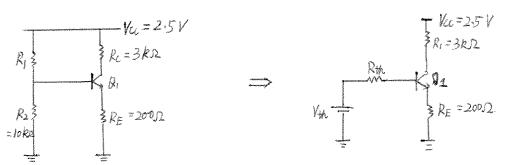
$$\frac{R_1R_2}{R_1+R_2} = \frac{A_0 V_T}{R_0}$$

$$\frac{R_1R_2}{R_1+R_2} = \frac{V_{cc}R_2}{R_1+R_2} - V_7 ln \left(\frac{A_0 V_7}{R_0 I_s}\right)$$

$$\frac{A_0 V_7}{R_0}$$

Max Rin:





a) 
$$V_{th} = V_{cc} \cdot \frac{R_2}{R_1 + R_2} = 2.5 \times \frac{10k}{10k + R_1}$$
,  
 $R_{th} = \frac{R_1 R_2}{R_1 + R_2} = \frac{R_1 \cdot (10k)}{R_1 + 10k}$ 

(F)

Since 
$$1_E = 0.25 \text{ mA}$$
,  $1_B = 0.0025 \text{ mA}$ ,  $2_E = \frac{0.25 \text{ mA}}{99} = 0.2525 \text{ mA}$   
 $V_{AE} = V_T \ln \left(\frac{1}{T_S}\right) = 0.696 \text{ V}$ 

A becomes

$$25 \times \frac{10k}{10k+R_1} = 0.0025m \times \frac{R_1 \cdot (10k)}{R_1 + 10k} + 0.696 + 0.2525 \times 0.2$$

So

$$R_1 = 22.73 k$$

b) If RE deviates by 5%, changes in RE is 1052.

$$l_{B} = \frac{V_{th} - (V_{BE} + L_{E}R_{E})}{R_{th}} \Rightarrow \frac{I_{C}}{\beta} = \frac{V_{th} - (V_{SE} + \frac{L_{C}}{\alpha}R_{E})}{R_{th}}$$

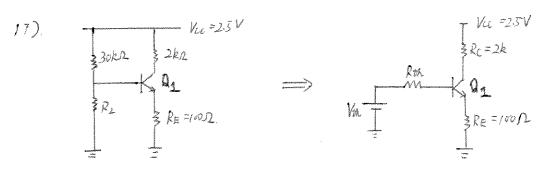
$$\Rightarrow i_c = \frac{\beta \propto (V_{th} - V_{BE})}{\alpha R_{th} + \beta R_E}$$

$$\Rightarrow \partial lc = -\frac{\beta^2 \chi (V_{th} - V_{BE})}{(\kappa R_{th} + \beta R_{E})^2} \partial R_{E}$$

16)  $\partial R_E = 10$ ,  $V_m = 0.764$ ,  $V_{BE} = 0.7465$ ,  $R_m = 8.94k$ , x = 0.99,  $\beta = 100$ .

So  $\partial I_C = -0.0024$  (mA)

The error is  $\frac{0.0024}{0.25} \times 100\% = 0.96\%$  in  $I_C$ .



$$Vth = \frac{R_2 \times 2.5}{30k + R_2} , Rth = \frac{30k \times R_2}{30k + R_2}$$

VLE 3 VBE (To be guaranteed in active mode, soft saturation is not allowed.)

$$I_{c} = \frac{\beta \times (V_{th} - V_{BE})}{\times R_{th} + \beta R_{E}} \qquad (: I_{c} = \frac{V_{th} - (V_{BE} + \frac{1}{2} R_{E})}{R_{th}})$$

So 
$$V_{CE} = V_{CC} - \left[ \frac{B\dot{X} \left( V_{th} - V_{BE} \right)}{XR_{th} + \beta R_{E}} - 2k + \frac{B \left( V_{th} - V_{BE} \right)}{XR_{th} + \beta R_{E}} \times 100 \right]$$

VCE 7 VBE MEANS

$$2.5 - \left[ \frac{99 \left( \frac{R_2 \times 2.5}{30 R + R_2} - V_{BE} \right)}{0.99 \times \frac{30 R^3 R_2}{30 R + R_2} + 100 \times 100} \times 2R + \frac{100 \left( \frac{R_2 \times 2.5}{30 R + R_2} - V_{BE} \right)}{0.99 \times \frac{30 R^3 R_2}{30 R + R_2} + 100 \times 100} \times 100 \right] \ge V_{BE} O$$

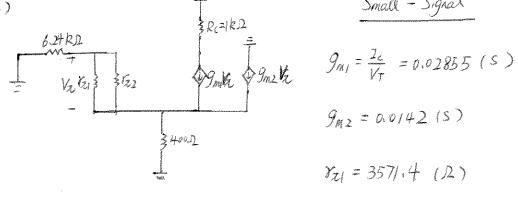
And

$$V_{BE} = V_T \ln \left(\frac{I_C}{I_S}\right) = V_{H} \ln \left[\frac{\beta x \left(V_{hh} - V_{BE}\right)}{I_S \left(\alpha R_{th} + \beta R_E\right)}\right]$$

There are two unknowns ( $R_2$  and  $V_{BE}$ ) and two equations ( $\mathcal{O}$  and  $\mathcal{O}$ )

Since  $\mathcal{O}$  is a nonlinear equation, the problem can be solved by iteration.

Maximum 
$$R_2 = 20.343k$$



$$g_{m_1} = \frac{I_c}{V_T} = 0.02855 (s)$$

18). a).

$$1_{S1} = 21_{S2} = 5 \times 10^{-16} \text{ A}$$
 $1_{SR} = 3R_1$ 
 $R_1 = R_2 = 100$ 
 $R_2 = 2.5 \times 10^{-16} \text{ A}$ 
 $R_2 = 2.5 \times 10^{-16} \text{ A}$ 

$$I_{S1} = 2I_{S2} = 5 \times 10^{-16} \text{ A}$$

$$\beta_1 = \beta_2 = 100$$

$$V_{th} = V_{ct} \times \frac{R_2}{R_1 + R_2} = 1.2 V$$

$$V_{th} = V_{cc} \times \frac{R_2}{R_1 + R_2} = 1.2 V$$

$$R_{th} = R_1 1/R_2 = 6.24 R_3 2.$$

$$\Rightarrow 1.2 V = \frac{6.24 R_3 2}{R_1 + R_2} = \frac{6.24 R_3 2}{R_2 + 6.24 R_3 2}$$

$$1_{B2} = \frac{1.2 - (V_{BE} + 3I_{E2} \cdot R_E)}{6.24k}$$
 and  $I_{B2} = \frac{I_{C2}}{B}$ 

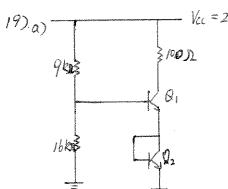
$$50 \quad \frac{I_{c2}}{\beta} = \frac{1.2 - (V_{3E} + 3I_{c2}/(x - 0.4k))}{6.24k}$$

$$\Rightarrow I_{c2} = \frac{(1.2 - V_{BE}) \cdot (\beta X)}{(X \cdot 6.24k + 3\beta \cdot 0.4k)} = \frac{(1.2 - V_{BE})(99)}{126 \cdot 1776} (mA).$$

$$V_{BE} = V_T \ln \left(\frac{1_c}{1_{S2}}\right) = 0.724$$
, not 0.8, so reiterate.

$$I_{c2} = \frac{(1.2 - 0.724)(99)}{126.1776} = 0.3735$$

$$V_{BE} = 26 \ln \left( \frac{0.3735}{2.5 \times 10^{-3}} \right) = 0.728$$
, close, iterate again



$$\beta_1 = \beta_2 = 100$$

$$V_{th} = \frac{(2.5)(16k)}{9R+16k} = 1.6(10)$$

$$2B_1 = \frac{Vth - 2(VBE)}{Rth}, \quad I_{C_1} = \beta 2B_1 = \beta \frac{Vth - 2(VBE)}{Rth}$$

$$V_{BE} = V_T \ m \left( \frac{I_{CI}}{I_{SI}} \right). \tag{2}$$

Guess VBE = 0.7,

$$0 \Rightarrow I_{c_1} = 100 \times \frac{A6 - 2 \times 0.7}{5.76} = 3.47 (mA)$$

$$\Im \Rightarrow V_{BE} = V_T \ln \left( \frac{3.47}{4 \times 10^{-15}} \right) = 0.7746$$
, not 0.7, reiterate

$$0 \Rightarrow 2c_1 = 0.88/9$$

After several iterations, VBI converges to 0.755

$$P(B) = \sqrt{B} = 0.755 \text{ (V)}.$$

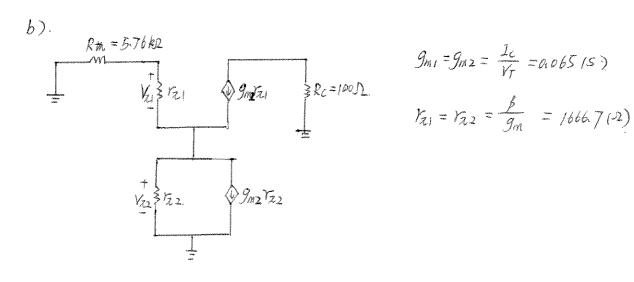
$$I_{B1} = \frac{V_{Th} - 2V_{BE}}{R_{th}} = 0.0136 \text{ (mA)}.$$

$$I_{L2} = \beta I_{B1} = \lambda 56 \text{ (mA)}.$$

$$V_{CE} = V_{CC} - \left[1c \cdot (0.1) + V_{BE}\right] = \lambda 589 \text{ (V)}.$$

$$I_{C2} = \lambda 56 \text{ (mA)}.$$

$$V_{CE2} = V_{BE} = 0.755 \text{ (V)}.$$



$$g_{m1} = g_{m2} = \frac{1c}{V_T} = 0.065 (5)$$

$$Y_{21} = Y_{22} = \frac{b}{g_m} = 16667 (2)$$

$$I_{c} = I_{mA}$$

$$V_{BE} = V_{T} l_{n} \left(\frac{I_{c}}{I_{s}}\right) = 0.750V$$

$$V_{B} = 2.5 - \left(I_{E}(I_{KR}) + I_{B}R_{B}\right) = 0.750V$$

$$I_{E} = 1.01_{MA}$$

$$I_{B} = 0.01_{MA}$$

$$V_B = 2.5 - |.0| - 0.01 R_B = 0.750$$

VCC = 2.5V

$$V_X = 1.1V$$
 $S = 1.1V$ 
 $S = 1.00$ 
 $S$ 

$$\beta = 100$$

$$I_s = 7$$

$$I_E = \frac{2.5 - 1.1}{3 = 0.00} = 4.67 \text{ mA}$$

$$I_s = I_c$$

$$\frac{1}{2} \left( \frac{V_{BE}}{V_T} \right), \quad V_{BE} = 1.1 - \frac{4.624}{100} (10K) = 0.6376V$$

$$V_{LL} = 25 V$$

$$I_{S} = 6 \times 10^{-16} A$$

$$\beta = 100$$

$$V_{X}$$

$$V_{A} = 90$$

$$A_{I}$$

$$A_{I}$$

$$\frac{V_{cc} - V_{x}}{o.5k} = I_{c} + I_{B} = I_{c} \left(1 + \frac{1}{\beta}\right) \Rightarrow V_{x} = 2.5 - o.5k \cdot \frac{I_{c}}{\alpha}$$

$$\frac{V_{\mathcal{X}} - (V_{\mathcal{B}E} + I_{E} \cdot 0.4k)}{20 k} = \frac{J_{\mathcal{C}}}{\beta} \Rightarrow V_{\mathcal{X}} = (20k)(\frac{J_{\mathcal{C}}}{\beta}) + V_{\mathcal{B}E} + \frac{J_{\mathcal{C}}}{\alpha}(0.4k)$$

Equating Vx in 10 and 3

$$2.5 - (0.5k)(\frac{1}{\alpha}) = (20k)(\frac{1}{\beta}) + V_{BE} + \frac{1}{\alpha}(0.4k)$$

$$I_{c} = \frac{2.5 - V_{BE}}{\frac{\alpha g_{k}}{\lambda} + \frac{20k}{\beta}} = \frac{2.5 - V_{BE}}{1.11k}$$

First iteration VBE = 0.8.

$$V_{B\bar{E}} = V_{f} \ln(\frac{2}{15}) = 0.743$$
, not 0.8, reterate

$$3 \Rightarrow 1c = \frac{2.5 - 0.745}{1.11} = 1.583 (mA)$$

$$V_{B\bar{c}} = V_7 \ln \left( \frac{1583}{I_5} \right) = 0.744$$
, converged.

Ic= 
$$\frac{\beta(2.5-I_E(N)-V_{BE})}{R_B}$$

$$I_c = \beta\left(\frac{2.5-I_E(N)-V_{BE}}{R_B}\right)$$

$$I_c = \frac{1}{\beta}\left(\frac{1}{R_B} - \frac{1}{2}\right)$$

$$I_c = \frac{2.5-V_{BE}}{\beta} + \frac{1}{2}$$

$$I_c = \frac{1}{\beta}\left(\frac{1}{R_B}\right)$$

$$V_{BC} \leq 0.2V$$

$$(V_X - I_B R_B) - (V_X - I_c 0.5) \leq 0.2V$$

$$I_C (0.5 - \frac{R_B}{B}) \leq 0.2V$$

$$\left(\frac{2.5 - V_{BE}}{\frac{R_B}{B} + \frac{11K}{A}}\right) (0.5 - \frac{R_B}{B}) \leq 0.2V$$

$$(2)$$
Guess  $V_{BE} = 0.75V \Rightarrow R_B \geq 34.513KA$  (From (2))

$$I_c = 1.291 \text{ mA}$$
, (From CI))  
 $V_{BE} = V_f ln \left(\frac{I_c}{I_b}\right) = 0.7564 \text{ V}$ , Not  $0.75$ , Veiterate  
 $V_{BE} = 0.7564 \text{ V}$ .  $\Rightarrow$   $R_B \ge 34.461 \text{ K}\Omega$ 

Let RB = 34.513KM

$$V_{BE} = V_T \ln \left( \frac{I_c}{I_s} \right) = 0.7563 V$$
, Converged 1!

Check 
$$V_{BC}$$
:  $V_{BC} = (1.287)(0.5) - (\frac{1.287}{100})(34.46)$ 

24). a). 
$$V_{\alpha} = 25V$$

$$I_{S} = 8 \times 10^{-16} A$$

$$\beta = 100$$

$$V_{A} = \infty$$

$$V_{A} = \infty$$

$$V_{A} = 2.5 - (\frac{1c}{\alpha} + \frac{V_{B}}{40k}) \cdot 1k$$

$$V_{x}=25-\left(\frac{1c}{\alpha}+\frac{V_{B}}{40k}\right)\cdot |k|$$

$$V_{\mathcal{X}} = \left(\frac{V_{\mathcal{B}}}{40k} + 2\mathcal{B}\right) 10k + V_{\mathcal{B}} = \left(\frac{V_{\mathcal{B}}}{40k} + \frac{1}{\beta}\right) 10k + V_{\mathcal{B}}$$

Equating 
$$Vx \Rightarrow 2.5 - (V_B + \frac{V_B \cdot |k|}{40R} + \frac{V_B \cdot 10k}{40R}) = \frac{1_C}{\alpha} \cdot |k + \frac{1_C}{\beta} \cdot |0k|$$

$$\Rightarrow 1_C = \frac{2.5 - 1.273V_B}{1R + \frac{10R}{\beta}}$$

Guess VB = 0.8

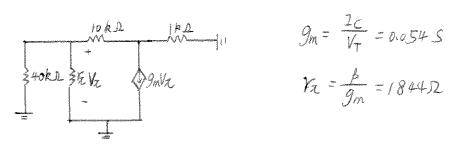
$$I_C = \frac{1.48}{\frac{1k}{0.99} + \frac{10k}{100}} = 1.33 \, m(A)$$

Then

Resterate

So Vs unwerges to 0.73 V

24 b) Small Signal



$$g_m = \frac{2c}{V_T} = 0.054 \text{ S}$$

$$R = \frac{k}{g_m} = 184452$$

$$I_{c_1} = | MA |, I_{E_1} = |.0| mA$$

$$I_{S_1} = I_{S_2} = 3 \times |0^{-16}A|$$

$$V_A = \infty$$

$$\beta = |00|$$

$$\begin{split} V_E &= \left( I_{E_1} + I_{E_2} \right) 0.5 K \; , \; \; V_{BE_1} = V_T ln \left( \frac{I_{C1}}{I_S} \right) = 0.75 V \\ V_E &= 2.5 - V_{BE_2} \\ V_B - \left( I_{\cdot} \circ I + I_{E_2} \right) 0.5 = 0.75 V . \\ Guess \; V_{BE_2} &= 0.7 V \\ V_E &= 1.8 = \rangle \; I_{E_1} + I_{E_2} = 3.6 \text{mA} = \rangle \; I_{E_2} = 2.59 \text{mA} \\ I_{C_2} &= 2.5641 \text{mA} = \rangle \; \; V_{8E_3} = V_T ln \left( \frac{I_{C2}}{I_S} \right) = 0.774 V \end{split}$$

Reiterate

VBE = 0.773V, Ic2 = 2.42mA, IE1 = 2.44mA

$$V_{8} = 0.75 + (1.01 + 2.44) 0.5 = 2.475V$$

$$V_{c} = 2.5 - (110.2) = 2.3$$
A1 in 50ft-saturation region.

6)

Small Signal Model

$$J_{m_1} = \frac{1 \text{ mA}}{2 \text{ bmV}} = 0.0385 \left(\frac{1}{10}\right) \text{ S}$$

$$V_{\pi_1} = \frac{100}{0.0385} = 2.6 \text{ KM}$$

$$g_{m2} = \frac{2.42 \text{ mA}}{26 \text{ mV}} = 0.0931 \left(\frac{1}{1.0000}\right) \text{ S}$$

$$V_{a_2} = \frac{100}{0.0931} = 1.07 \text{ KM}$$

26). 
$$\beta_{npn} = 2\beta_{pnp} = 100$$
  $1s = 9 \times 10^{-16} \text{ A}$   $V_{A}$ 

$$V_{A} = 2.5 \text{ V}$$

$$Q_{1}$$

$$\frac{3600}{2}$$

$$1(a)$$

a) 
$$I_{c} = \frac{2.5 - |V_{BE}|}{60k} \beta_{PPP}$$
,  $V_{BE} = V_{T} \ln |\frac{1}{1s}|$ .

Guess  $|V_{BE}| = 0.8 \implies I_{c} = 1.42m(A)$ 
 $|V_{BE}| = 2646^{3} \ln (\frac{1.42}{9 \times 10^{43}}) = 0.730(V)$ , not 0.8

Reiterate,  $I_{c} = \frac{2.5 - 0.75}{60R} \times 50 = 1.475m(A)$ 
 $|V_{BE}| = 2646^{3} \ln (\frac{1.42}{9 \times 10^{43}}) = 0.731(V)$ 

Perturate, 
$$I_C = \frac{2.5 - 0.731}{bok} \times 50 = 1.474 \text{ m (A)}$$

$$|V_{BE}| = 2646^3 \ln(\frac{1.474}{9\times1045}) = 0.731(V), \text{ converged.}$$

$$Q_1: |V_{BE}| = 0.731V$$
,  $I_C = 1.47mA$ ,  $I_B = 29.4uA$ .

 $|V_{EE}| = 2.206V$ .

In forward active region.

ş4:

b). 
$$I_{c2} = \frac{25 - (V_{BE1} + |V_{BE2}|)}{80k}$$

$$\frac{1_{C2} \cdot \frac{\beta_{pnp} + 1}{\beta_{pnp}} = \frac{1_{C1} (\beta_{npn} + 1)}{\beta_{npn}}}{\beta_{npn}} = \frac{1_{C1} (\beta_{npn} + 1)}{\beta_{npn}} = \frac{1_{C1} (\beta_{npn} + 1)}{\beta_{npn}} = \frac{1_{C2} (\beta_{npn} + 1)}{2\beta_{pnp} + 1} = \frac{1_{C2} (\beta_{npn} + 1)}{2\beta_{npn} + 1} = \frac{1_{C2} (\beta_$$

$$V_{BE} = V_T \ln \left( \frac{L_I}{L_S} \right)$$

$$V_{BE2} = V_T \ln \left( \frac{2c_2}{2s} \right) \tag{4}$$

GNESS VBE2 = VBE1 = 0.8

$$O \Rightarrow I_{C2} = 50 \times (\frac{25-1.6}{80 \, k}) A = 0.5625 \, \text{mA}$$

$$\bigoplus \Rightarrow V_{BE2} = V_T \ln \left( \frac{0.5625}{9 \times 10^{13}} \right) V = 0.706 V$$

Resterate,

l'enternte,

So

$$I_{C2} = 0.680 \text{ mA}$$

$$I_{B1} = 0.8 \text{ mA}$$

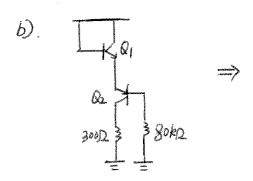
$$I_{B2} = 13.48 \text{ mA}$$

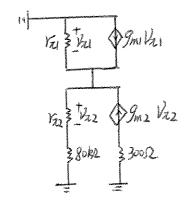
$$V_{BE1} = 0.711 \text{ V}$$

$$V_{CE1} = 0.711 \text{ V}$$

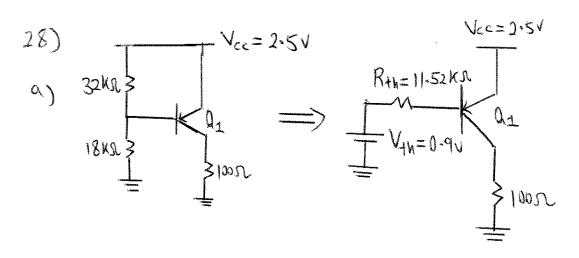
$$V_{CE2} = 2.5 \text{ V} - 0.711 \text{ V} - (0.674)(0.3) \text{ V} = 1.5868 \text{ V}$$

$$g_{m1} = \frac{I_c}{V_T} = \frac{1.47mA}{26mV} = 0.0565S$$
  
 $Y_{Z1} = \frac{B}{g_{m1}} = 884\Omega$ 





$$g_{m1} = \frac{\lambda_{c1}}{V_7} = a 02615 S$$



$$I_c = \beta_{pnp} \left( \frac{2.5 - |V_{BE}| - V_{th}}{R_{th}} \right)$$

Guess 
$$|V_{BE}| = 0.7 \text{ V}$$
,  $I_c = 3.91 \text{ mA}$   
 $|V_{BE}| = V_T \ln \left(\frac{I_c}{I_s}\right) = 0.757 \text{ V}$ 

Reiterate, 
$$|V_{BE}| = 0.757V$$
,  $I_c = 3.66mA$   
 $|V_{BE}| = V_7 ln(\frac{I_c}{I_8}) = 0.755V$ 

Reiterate, 
$$|V_{BE}| = 0.755 \text{ V}$$
,  $I_c = 3.67 \text{ mA}$   
 $|V_{BE}| = V_T \ln \left( \frac{I_c}{I_s} \right) = 0.755 \text{ V}$ , Converged!

 $V_c = (3.67 \text{ mA})(0.1 \text{ K}\Omega) = 0.367 \text{ V}, V_B = 2.5 - 0.755 = 1.745 \text{ V}$  $Q_1$  in forward active.

Bias Point =

$$I_c = 3.67 \text{ mA}$$
  $|V_{BE}| = 0.755$   
 $I_B = 73.4 \text{ mA}$   $|V_{CE}| = 2.5 - 0.367 = 2.133V$ 

28)
$$a_1$$
 $a_2$ 
 $a_1$ 
 $a_2$ 
 $a_3$ 
 $a_4$ 
 $a_4$ 
 $a_4$ 
 $a_5$ 
 $a_4$ 
 $a_5$ 
 $a_4$ 
 $a_5$ 
 $a_4$ 
 $a_5$ 
 $a_5$ 
 $a_6$ 
 $a_7$ 
 $a_8$ 
 $a_8$ 

$$I_{c_2} = \frac{2.5 - (V_{8E_1} + V_{8E_2}) - 0.9}{11.52 \text{ K}}$$

$$I_{c_1} = I_{c_2} (1.0099)$$

$$(From \beta relation)$$

$$V_{BE_1} = V_T ln(\frac{I_{c_1}}{I_s})$$

$$|V_{BE_2}| = V_T \ln \left( \frac{f_{c_2}}{I_s} \right)$$

Guess, 
$$V_{BE} = V_{BE2} = 0.7V$$
  
 $J_{C2} = 0.868 \text{ mA}, \quad J_{C1} = 0.877 \text{ mA}$   
 $V_{BE} = V_{7} \ln \left( \frac{J_{C1}}{J_{8}} \right) = 0.718V, \quad \left| V_{BE2} \right| = V_{7} \ln \left( \frac{J_{C2}}{J_{8}} \right) = 0.717$ 

Reiterate, 
$$V_{BE_1} = 0.718V$$
,  $V_{BE_2} = 0.717V$   
 $I_{c_2} = 0.716 \text{ mA}$ ,  $I_{c_1} = 0.723 \text{ mA}$   
 $V_{BE_1} = V_T ln\left(\frac{I_{c_1}}{I_S}\right) = 0.713 \text{ V}$ ,  $|V_{BE_2}| = V_T ln\left(\frac{I_{c_2}}{I_S}\right) = 0.712 \text{ V}$ 

Reiterate, 
$$V_{BE_1} = 0.713 \text{ V}$$
,  $|V_{BE_2}| = 0.712 \text{ V}$   
 $I_{c_2} = 0.760 \text{ mA}$ ,  $I_{c_1} = 0.767 \text{ mA}$   
 $V_{BE_1} = 0.714 \text{ V}$ ,  $|V_{BE_2}| = 0.714 \text{ V}$ 

Reiterate, 
$$V_{BE} = 0.714 \text{ V}$$
,  $|V_{BE}| = 0.714 \text{ V}$ 

$$I_{C_2} = 0.747 \text{ mA}, \quad I_{C_1} = 0.754 \text{ mA}$$

$$V_{BE_1} = V_{1} V_{1} = 0.714 \text{ V}$$

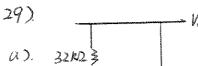
$$|V_{BE_2}| = 0.714 \text{ V}$$

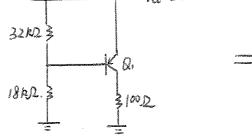
$$V_{B_2} = \frac{(0.747 \text{mA})}{50} (11.52 \text{Kr}) + 0.9 = 1.07 \text{V}$$

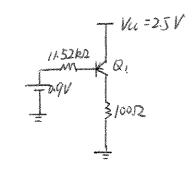
$$V_{C_2} = \frac{(0.747 \text{mA})(1 \text{Kr})}{(0.747 \text{mA})(1 \text{Kr})} = 0.747 \text{V}$$

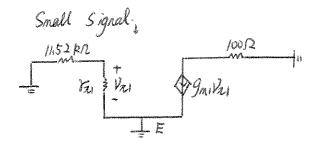
Q2 is in forward-active region. Q1 is always in forward-active region.

Bias point:





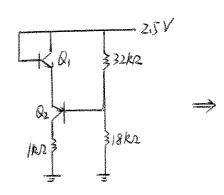


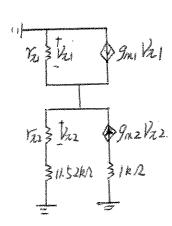


$$g_{m1} = \frac{3.67mA}{26mV} = 0.141 S$$

$$Y_2 = \frac{50}{0.141} \Omega = 354.2 \Omega$$







$$R_{M} = \frac{(R_{B})(5k\Omega)}{R_{B} + 5k\Omega}$$

$$R_{M} = \frac{(R_{B})(5k\Omega)}{R_{B} + 5k\Omega}$$

$$R_{M} = \frac{R_{B}}{R_{B} + 5k\Omega} \cdot 25V$$

$$R_{M} = \frac{R_{B}}{R_{B} + 5k\Omega} \cdot 25V$$

$$R_{M} = \frac{R_{B}}{R_{B} + 5k\Omega} \cdot 25V$$

$$R_{M} = \frac{1}{2} |k\Omega|$$

$$R_{M} = \frac{1}$$

$$\beta = 50$$
,  $I_s = 8 \times 10^{-16} A$ ,  $V_A = \infty$   
Edge of Saturation:  $|V_{BE}| = |V_{CE}|$ 

$$I_c = \frac{50(2.5 - 1V_{BE}1 - V_{th})}{R_{th}}$$
,  $|V_{CE}| = 2.5 - I_c |KR = |V_{BE}|$   
 $2.5 - \frac{50(2.5 - |V_{BE}| - V_{th})}{R_{th}} (|KR|) = |V_{BE}|$ 

Substitute in Rth and Vth and rearrange:

3°) So 
$$\pm 5\%$$
 of  $9.62 \text{KM}$ .

 $15\%$  Case:

 $9.62 \text{KM} + 5\% = |0.10| \text{KM}$ 
 $1 = 1.67 \text{ V}$ ,  $1 = 3.345 \text{ KM}$ 
 $1 = \frac{(2.5 - 0.74 - 1.64)}{3.345} = 1.3455 \text{ mA}$ 

Chech for  $1 = \frac{(2.5 - 0.74 - 1.64)}{3.345} = 0.732 \text{ V}$ , iterate once

 $1 = 1.4651 \text{ mA}$ ,  $1 = 1.4651 \text{ mA}$ 

 $|V_{BE}| \simeq 0.734$ ,  $|V_{CE}| = 2.5 - 1.4651 (1/km) = 1.0349V$  $V_{BC} = 0.3009 V$  (Reverse bias)

-5% Case:

9.62 kn - 5% = 9.139 knV<sub>th</sub> = 1.616 V,  $R_{th} = 3.23184 \text{kn}$ 

 $I_c = (2.5 - 0.74 - 1.616)$  50 = 2.228 mA,  $|V_{BE}| = V_7 |n(\frac{1}{2}) = 0.745 \text{V}$ 

reiterate: |VBE| = 0.745 V, I\_ = 2.150 mA, Verify VBE, |VBE| = V+ In(Is) = 0.744 V, Converged

NCZ = 25-2-150 (IKA) = 0.35, NBZ = 0.744V, VBC = -0.394V (Forward Bias)

$$V(L) = 2.5 V$$

$$RE$$

$$|ORD| = 2.5 V$$

$$V_{BC} = 1.25 + I_{B}R_{+h} - I_{c}5K = 0.3$$
  
 $1.25 + I_{c}5 - I_{c}5K = 0.3$   
 $\beta = 50 \implies I_{c} = 0.1939_{mA}$ 

$$I_{B} = \frac{(2.5 - I_{c}R_{E} - |V_{BE}|) - 1.25}{SK}$$

$$\alpha = 0.9804$$

$$I_{B} = 0.003878 \text{ mA}$$

NBE = 0.882V Ic = 0.1939mA

If 
$$R_E$$
 is halved =>  $R_E = 1.44 \text{K} \Lambda$ 

$$I_C = B \left( \frac{2.5 - |V_{BE}| - 1.25 - \alpha I_C R_E}{5 \text{K}} \right)$$

$$I_C = \frac{62.5 - 50 |V_{BE}|}{78.44}, \text{ Gluess } |V_{BE}| = 0.682 \text{V}$$

$$I_c = \frac{62.5 - 50(0.698)}{78.44} = 0.352 \text{ mA}$$

60 Ic= 0.352 mA, which is 1.82 times of 0.1939 mA

$$V_{BC} = 1.25 + (0.352)(5KR) - (0.352)(5KR) = -0.4748V$$

Which drive Q1 into saturation.

32). 
$$\sqrt{k} = 25V$$

$$\sqrt{k} = 80$$

$$\sqrt{k} = 80$$

$$\sqrt{k} = 80$$

$$V_{B} = (Z_{B})(20kR) + Z_{E} \cdot (16R/2)$$

$$1c = 1mA$$

$$20k2$$

$$\frac{1}{3}16kD$$

$$2B = \frac{1}{80}mA$$

$$V_{B} = (\frac{1}{80})(20)V + (10125)(1.6)V$$

$$V_{A} = 10$$

$$V_{B} = (\frac{1}{80})(20)V + (10125)(1.6)V$$

$$V_{A} = 10$$

$$V_{B} = (\frac{1}{80})(20)V + (10125)(1.6)V$$

$$V_{B} = (\frac{1}{80})(20)V + (10125)(1.6)V$$

$$V_{A} = 10$$

$$V_{B} = (\frac{1}{80})(20)V + (10125)(1.6)V$$

Is = 3x10-11 mA.

33) If Base ourset is reglected, 
$$I_c = I_E$$

$$I_1 = \frac{V_E - V_C}{R_1 + R_2}$$

$$I_1 = \frac{V_E - V_C}{R_1 + R_2}$$

$$|V_{BE}| = I_1 R_1 = \frac{|V_E - V_C|}{R_1 + R_2} R_1 = \frac{|V_{CE}|}{R_1 + R_2} R_1$$

$$|V_{BE}| = \frac{|V_{CE}|}{|V_{BE}|} = \frac{R_1 + R_2}{R_1}$$

If Base current is reglected, 
$$I_c = I_E$$

$$I_1 = \frac{V_E - V_L}{R_1 + R_2}$$

$$|V_{BE}| = I_1 R_1 = \frac{V_E - V_C}{R_1 + R_2} R_1 = \frac{|V_{CE}|}{R_1 + R_2} R_1$$

$$So \frac{|V_{OE}|}{|V_{BE}|} = \frac{R_1 + R_2}{R_1}$$

Let 
$$A = \frac{R_1 + R_2}{R_I}$$
,  $|V_{CE}| = A |V_{BE}|$ , thus  $|V_{BE}|$  is multiplied.

$$\frac{L_{c}R_{c}}{VT} = 20 \implies 2c = \frac{20V_{T}}{R_{c}}$$

$$L_{c} = 0.0/04MA$$

$$V_{A} = 10V, V_{0} = \frac{V_{A}}{I_{c}}, y_{m} = \frac{I_{c}}{V_{T}}$$

$$V_{in} = \frac{V_{A}}{I_{c}}, y_{m} = \frac{I_{c}}{V_{T}}$$

$$V_{in} = \frac{V_{A}}{I_{c}}, y_{m} = \frac{I_{c}}{V_{T}}$$

$$\left|\frac{V_{\text{out}}}{V_{\text{in}}}\right| = \int_{M} \left(\frac{R_{\text{c}}/V_{\text{o}}}{R_{\text{c}}+V_{\text{o}}}\right) = \frac{R_{\text{c}}V_{\text{A}}}{V_{\text{T}}\left(R_{\text{c}}+\frac{V_{\text{A}}}{I_{\text{c}}}\right)}$$

As the equation above shows, a large gain means a large Ic. However, a large Ic Will drive Q1 into Saturation. So a tradeoff must be made. The maximum limit for Ic is when it drives Q1 into the edge of Saturation, namely,  $V_{BE} = V_{CE}$ .

36) 
$$V_{cc}$$

$$Q_{l}$$

$$V_{in} = V_{o} = V_{o} = V_{o}$$

$$R_{out} = V_{o} = V_{o}$$

$$A_{\nu} = 50$$
 $R_{out} = Y_{o} = 10KN$ 

$$A_V = g_m R_{out} = \frac{I_c}{V_T} R_{out} = 50$$

$$I_c = 50 \left( \frac{V_r}{Rout} \right) = 0.13 \text{ mA}$$

37). 
$$I_{c} = I_{s} \exp\left(\frac{V_{RE}}{2V_{T}}\right)$$

$$V_{IA} = \frac{\partial I_{c}}{\partial V_{SE}} = \frac{I_{c}}{2V_{T}}$$

$$R_{out} = R_{c}$$

$$V_{out} = V_{out} = \frac{I_{c}R_{c}}{2V_{T}} = \frac{(I_{m}A)(I_{k}R_{t})}{(2)(0.026V_{t})} = 19.23$$

38). (Find Av, Rin, Rout)
$$V_{A} = \infty$$

$$Rout = \frac{Rup}{Rup} / \frac{Rdn}{Rdn}$$

$$Rup = \frac{1}{9m_{2}} / \frac{1}{7n_{2}}, Rdn = \infty$$

$$Vin. o = \frac{1}{9m_{2}} / \frac{1}{7n_{2}}$$

$$Rout = \frac{1}{9m_{2}} / \frac{1}{7n_{2}}$$

$$Rout = \frac{1}{9m_{2}} / \frac{1}{7n_{2}}$$

$$Rin = Y_{n_1}$$

$$A_{v} = \left| \frac{V_{out}}{V_{in}} \right| = g_{m_1} \left( \frac{1}{g_{m_2}} \right) / Y_{n_2}$$

b). The Value of the Rup = 
$$R_1 + \frac{1}{9} / Y_{\pi_2}$$
 $R_{\mu p} = R_1 + \frac{1}{9} / Y_{\pi_2}$ 
 $R_{\mu p} = R_1 + \frac{1}{9} / Y_{\pi_2}$ 

38  
C). The Var 
$$V_A = \infty$$
  
 $R_{up} = R_c + \left(\frac{1}{g} // Y_{n_2}\right), R_{dn} = \infty$   
 $R_{up} = R_c + \left(\frac{1}{g} // Y_{n_2}\right), R_{in} = Y_{n_1}$   
 $V_{ino} = V_{ino}$   
 $A_V = J_{m_1} \left(R_c + \left(\frac{1}{g} // Y_{n_2}\right)\right)$ 

$$A_{v} = g_{m_{2}} \left( Y_{n_{2}} / \frac{1}{g} \right)$$

Rup = 
$$\infty$$

Rup =  $\infty$ 

where 
$$G_m = \left| \frac{I_{out}}{V_{in}} \right|$$

$$I_{out} + I_2 = I_3 , I_3 = \frac{V_1}{R_c}$$

$$V_1 = -I_1(R_c//r_{02}) = -J_m V_{in}(R_c//r_{02})$$

a). The Rup = 
$$\frac{1}{9}$$
  $\frac{1}{72}$   $\frac{1}{702}$ ,  $\frac{1}{702}$   $\frac{1}$ 

b) 
$$\frac{Va}{|R_{0}|} = R_{1} + \frac{1}{2} \frac{1}{|R_{2}|} = \frac{1}{|R_$$

39 d)

Find Rup:

$$I_{T} = I_{1} + I_{2}$$

$$I_{Re} = V_{T} - V_{1}$$

$$V_{1} = (I_{2} - J_{m} V_{T}) V_{0}$$

$$R_{out} = \frac{V_{o1}}{R_{out}} = \frac{V_{o2}}{R_{c} + V_{o2}} \frac{1}{1 + g_{m2} V_{o2}} = \frac{I_{7} = \frac{g_{m} V_{7}}{I_{7}} + \frac{(1 + g_{m} V_{o})}{R_{c} + V_{o}}}{V_{7}} = \frac{V_{7}}{R_{c} + V_{o}}$$

$$R_{im} = V_{71} = \frac{V_{7}}{I_{7}} = \frac{V_{7}}{R_{c} + V_{o}} = \frac{I_{7}}{R_{c} + V_{o}}$$

$$|A_{1}| = \frac{V_{out}}{V_{in}}| = \frac{g_{m1} (V_{71} - \frac{(R_{c} + V_{o2})}{I_{7}})}{I_{7} + g_{m2} V_{o2}} = \frac{I_{7}}{R_{c} + V_{o}} = \frac{I_{7}}{R_{c} + V_{o}}$$

$$|A_{1}| = \frac{V_{out}}{V_{in}}| = \frac{g_{m1} (V_{71} - \frac{(R_{c} + V_{o2})}{I_{7}})}{I_{7} + g_{m2} V_{o2}} = \frac{I_{7}}{R_{c} + V_{o}} = \frac{I_{7}}{I_{7} + g_{m2} V_{o2}}$$

$$|A_{1}| = \frac{V_{out}}{V_{in}}| = \frac{g_{m1} (V_{71} - \frac{(R_{c} + V_{o2})}{I_{7} + g_{m2} V_{o2}})}{I_{7} + g_{m2} V_{o2}}$$

$$|A_{1}| = \frac{V_{out}}{V_{in}}| = \frac{g_{m1} (V_{71} - \frac{(R_{c} + V_{o2})}{I_{7} + g_{m2} V_{o2}})}{I_{7} + g_{m2} V_{o2}}$$

$$|A_{1}| = \frac{V_{out}}{V_{in}}| = \frac{g_{m1} (V_{71} - \frac{(R_{c} + V_{o2})}{I_{7} + g_{o2}})}{I_{7} + g_{m2} V_{o2}}$$

$$|A_{1}| = \frac{V_{out}}{V_{in}}| = \frac{g_{m2} (V_{71} - \frac{(R_{c} + V_{o2})}{I_{7} + g_{o2}})}{I_{7} + g_{m2} V_{o2}}$$

$$|A_{1}| = \frac{V_{out}}{V_{in}}| = \frac{g_{m2} (V_{71} - \frac{(R_{c} + V_{o2})}{I_{7} + g_{o2}})}{I_{7} + g_{m2} V_{o2}}$$

$$|A_{1}| = \frac{V_{out}}{V_{in}}| = \frac{g_{m2} (V_{71} - \frac{(R_{c} + V_{o2})}{I_{7} + g_{o2}})$$

$$I_{T} = I_{1} + I_{2}$$
 $I_{2} = \frac{V_{1} - V_{1}}{R_{c}}$ ,  $I_{1} = \frac{J_{m} V_{1}}{B}$ 

$$R_{up} = \frac{V_{1} = (I_{2} - g_{m}V_{T})V_{0}}{I_{2}}$$

$$I_{2} = \frac{V_{7} - (I_{2} - g_{m}V_{T})V_{0}}{R_{c}}$$

$$I_{3} = \frac{V_{7} - (I_{2} - g_{m}V_{T})V_{0}}{R_{c}}$$

$$I_{4} = \frac{V_{1} - (I_{2} - g_{m}V_{T})V_{0}}{R_{c}}$$

$$I_{5} = \frac{(I + g_{m}V_{0})}{R_{c} + V_{0}}$$

$$I_{6} = \frac{V_{1} - (I_{2} - g_{m}V_{T})V_{0}}{R_{c} + V_{0}}$$

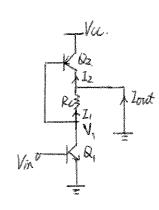
$$I_2 = \frac{(1+J_m V_0)}{R_c + V_0} V_T$$

$$I_7 = \frac{g_m V_T}{\beta} + \frac{(1 + g_m Y_0)}{R_c + Y_0} V_T$$

$$\frac{V_{\tau}}{I_{\tau}} = R_{up} = \frac{1}{g_{m} + \frac{(1+g_{m}V_{0})}{R_{c}+Y_{0}}}$$

39 e). The Rup = 
$$r_{02}$$
.

Rup =  $r_{02}$ .



$$G_{m} = \left| \frac{2 \operatorname{out}}{\sqrt{m}} \right|$$

$$I_{2}$$

$$I_{3}$$

$$I_{4}$$

$$I_{5}$$

$$I_{7}$$

$$I_{7}$$

$$I_{8}$$

$$I_{1} = \frac{V_{1}}{R_{c}}$$

$$I_{2} = V_{1} \cdot g_{m} \cdot 2$$

$$V_{1} = -\left( \frac{g_{m} \cdot V_{m}}{R_{c}} \right) \left( \frac{r_{0}}{R_{c}} \right) \left( \frac{r_{0}}{R_{c}} \right) \left( \frac{r_{0}}{R_{c}} \right)$$

$$lout = V_1 I g_{m2} - \frac{1}{Rc} ) = -g_{m1} V_{in} (Y_0 I I Rc I I Y_{22}) (g_{m2} - \frac{1}{Rc})$$

$$G_m = \left| \frac{2uxt}{V_{in}} \right| = g_m (Y_0 I I Rc I I Y_{22}) (g_{m2} - \frac{1}{Rc})$$

$$A_{V} = \frac{-R_{c}}{\frac{1}{g_{m}} + R_{E}} = \frac{-R_{c}g_{m}}{1 + R_{E}g_{m}}$$

$$\frac{\partial A_{V}}{\partial I_{c}} = R_{c} \left( \frac{g_{m}R_{E}}{(1+R_{E}g_{m})^{2}} \frac{\partial g_{m}}{\partial I_{c}} - \frac{\partial g_{m}/\partial I_{c}}{1+g_{m}R_{E}} \right)$$

$$\frac{\partial g_{m}}{\partial I_{c}} = \frac{1}{V_{T}} = \frac{1}{26mV} = 38.46 \left( \frac{1}{V} \right)$$

$$\frac{\partial A_{V}}{\partial I_{c}} = R_{c} \left(-2.404\right) \qquad \partial I_{c} = 0.1 I_{c}$$

$$\frac{\partial A_{V}}{\partial I_{c}} = -R_{c} I_{c} \left(0.24\right)$$

Relative Change in gain = 
$$\frac{\partial A_{V}}{A_{V}} = \frac{-0.24 (R_{c}I_{c})}{R_{c}I_{c}} = 2.5\%$$

$$\frac{R_{c}I_{c}}{V_{T}(1+R_{E}g_{m})}$$

$$\frac{\partial A_{V}}{\partial I_{c}} = -R_{c} \cdot 0.6$$

Relative Change in gain

$$\frac{\partial A_{V}}{A_{V}} = \frac{-0.06 (R_{c}I_{c})}{-R_{c}I_{c}} = 1.25\%$$

$$\frac{\partial A_{V}}{\nabla_{T} (1+R_{E}J_{m})} = 1.25\%$$

Vin 
$$V_{cc}$$
 $V_{A} = \infty$ 
 $R_{c}$ 
 $R$ 

$$|A_{V}| = \frac{R_{c}}{R_{E} + \frac{1}{J_{m}}} = \frac{R_{c}}{R_{E} + \frac{V_{T}}{I_{c}}} = \frac{R_{c}I_{c}}{R_{E}I_{c} + V_{T}}$$

Assume B is large, so Ic = Iz.

$$|A_V| = \frac{20V_T}{5V_T + V_T} = \frac{20V_T}{6V_T} = 3.33$$

Vin
$$V_{cc} = 2.5V$$

$$V_{in}$$

$$V_{out}$$

$$V_{out}$$

$$V_{out}$$

$$V_{out}$$

$$R_{e}I_{c} + V_{r}$$

$$Edge of Saturation$$

$$V_{cE} = V_{BE} = 2.5 - I_{c}(R_{c} + R_{E})$$

$$|A_{V}| = \frac{R_{c}L_{c}}{R_{E}L_{c} + V_{T}} = 10$$

Edge of Saturation  

$$V_{CE} = V_{8E} = 2.5 - I_c (R_c + R_E)$$

Equating the two equations above => 1.7-0.2Ic = 2Ic+0.26 => Ic= 0.655mA Check for VBE = VI ln (Ic) = 0.725, Not 0.8, Reiterate

$$I_cR_c = 1.775 - I_c0.2$$
 (operating point)  
 $I_cR_c = 2I_c + 0.26$  (Goin equation)

Equating the two equations => Ic = 0.689 mA Check for VBE = V In (Ic) = 0.7274, iterate I more time

$$I_{c}R_{c} = 1.773 - I_{c}0.2$$
 (operating point)  
 $I_{c}R_{c} = 2I_{c} + 0.26$  (Gain equation)

Check for 
$$V_{BE} \Rightarrow V_{BE} = V_7 ln(\frac{I_c}{I_s}) = 0.727 V$$
, converged

$$R_c = \frac{2I_c + 0.26}{I_c} = \frac{(200-688) + 0.26}{0.688}$$

$$R_c = 2.38K \Omega$$

$$Rin = \frac{\beta}{3} + 4013(0.2) = 240KM$$

$$V_{cc} = 2.5V$$

$$V_{n} = 100$$

$$V_{n} = 100$$

$$V_{out} = 100$$

$$|A_{N}| = |00|$$
 =>  $R_{c}I_{c} = |00|(R_{E}I_{c} + V_{T})$   
 $R_{c}I_{c} = 20I_{c} + 2.6$  (1)  
 $R_{c}I_{c} = |0.7| - I_{c}0.2$  (2) (Assume  $V_{3E} = 0.8$ )

Equating (1) and (2) field

1.7-Ic 0.2 = 2ºIc+2.6 => Ic= -0.04455mA

A negative Ic in forward active region is impossible, therefore, a solution does Not exist. The reason is because RcIc is too large to produce a gain of 100 that drive Q1 into saturation region.

Maximum Jain achievable:

$$\frac{R_{c}I_{c}}{R_{E}I_{c}+V_{T}}=|A_{v}| \qquad (Gain Equation)$$

2.5 = RcIc + VCB + RcIc (Operating Point Equation)

Let A = Maximum gain

$$=) I_c = \frac{1.7 - A0.026}{A0.2 + 0.2}$$

Since I cannot be zero, set

$$\frac{1.7 - A0.026}{A0.2 + 0.2} > 0$$

$$A < \frac{1.7}{0.026} = 65.4$$
 (Maximum gain achievable)

44) 
$$V_A = \infty$$

Vin RB

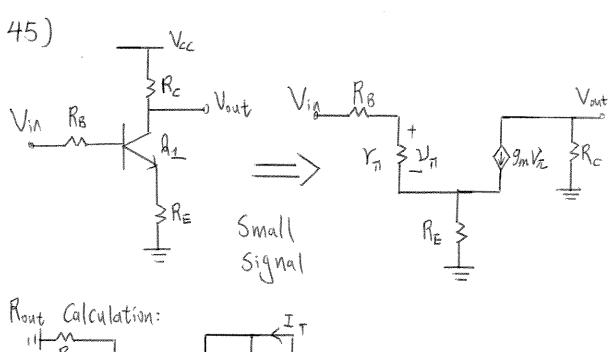
Small Signal:  $V_{ino} = \frac{RB}{RE}$ 

Voiat =  $-9m V_A Rc$ 

$$V_{\pi} = \frac{V_{A} R}{R_{B} + R + (\beta + 1) R_{E}}$$

$$V_{ord} = \frac{-g_{m} r_{a} R_{c} V_{in}}{R_{B} + r_{a} + (\beta + 1) R_{E}} = \frac{-\beta R_{c} V_{in}}{R_{B} + r_{a} + (\beta + 1) R_{E}} = \frac{-R_{c} V_{in}}{R_{B} + r_{a} + (\beta + 1) R_{E}} = \frac{-R_{c} V_{in}}{R_{B} + r_{a} + (\beta + 1) R_{E}}$$

$$\frac{V_{out}}{V_{in}} \approx \frac{-R_{c}}{\frac{R_{B}}{\beta+1} + \frac{1}{g_{m}} + R_{E}}$$

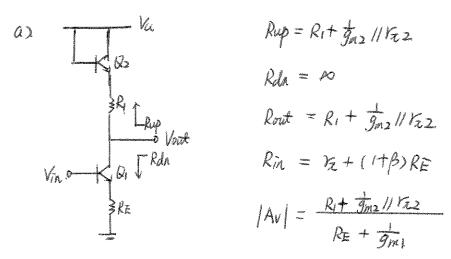


$$V_{A} = \int_{M} V_{\pi} (R_{E} // R_{B} + V_{\pi}) \qquad (1)$$

$$V_{A} = -\frac{V_{A} V_{\pi}}{V_{\pi} + R_{B}} \implies V_{A} = -\frac{V_{\pi} (V_{\pi} + R_{B})}{V_{\pi}} \qquad (2)$$

The only possible solution for 1) and 2) is  $Y_A = V_A = 0$ , Sing 1) is positive and 2) is negative.  $Y_A = 0 \Rightarrow J_m Y_A \Rightarrow 0 \Rightarrow Y_A = R_C$ 

Therefore, Rout = Rc



$$Rup = R_1 + \frac{1}{2}m_2 1/R_2$$

$$Rdn = 80$$

$$Rout = R_1 + \frac{1}{2}m_2 1/R_2$$

$$Rin = 72 + (1+\beta)RE$$

$$|Av| = \frac{R_1 + \frac{1}{2}m_2 1/R_2}{|Av|}$$

Vin a Vec. 
$$Rup = Rc$$

$$Vin a Vin Rup = Rc$$

$$Vin a Vin Rup = Rc$$

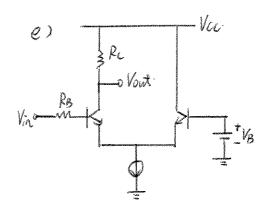
$$Rout = Rc$$

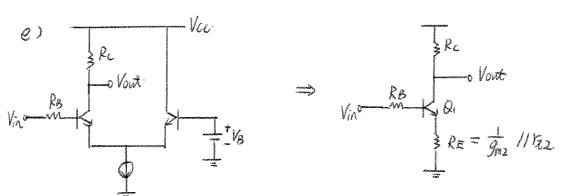
$$Rin = \frac{1}{2} + \frac{1}{2} + \frac{1}{2}$$

$$|Av| = \frac{Rc}{\frac{1}{2}m_2} ||F_{22}||^2$$

$$V_{ino} = V_{ci} + V_{ci} +$$

46). 
$$R_{B}$$
  $R_{C}$   $R_{C}$ 





$$R_{out} = R_{c}$$

$$R_{in} = R_{B} + r_{21} + (\beta + 1)(\frac{1}{g_{m2}} / r_{22})$$

$$|Av| = \frac{R_{c}}{\frac{1}{g_{m2}} / r_{22} + \frac{1}{g_{m1}} + \frac{R_{B}}{B + 1}}$$

Rout = 
$$Rc + \frac{1}{g_{m3}} 11 \frac{\pi}{2}$$
  
Vino Rin =  $\frac{\pi}{4} + (1+\beta)RE$   
 $\frac{\pi}{4} + \frac{1}{2} \frac{\pi}{4} = \frac$ 

b). Rout = 
$$\frac{1}{g_{m2}} / R_{2}$$
.

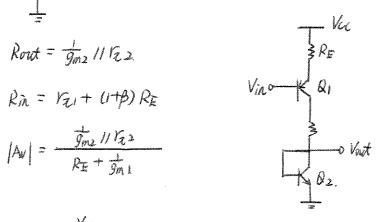
 $R_{in} = R_{2} + U + \beta R_{E}$ 
 $|A_{W}| = \frac{\frac{1}{g_{m2}} / R_{2}}{R_{E} + \frac{1}{g_{m1}}}$ 

d) Rout = Rc // Pa 2

$$R_{in} = r_{2i} + (\beta + 1)R_{E}$$

$$|A_{i}| = \frac{R_{C} // r_{2} 2}{R_{E} + \frac{1}{q_{in}}}$$

Rout = 
$$Rc + \frac{1}{g_{m3}} 11 \frac{\pi}{2}$$
  
 $Rin = \frac{1}{4} + (1+\beta) R_E$   
 $|Av| = \frac{Rc + \frac{1}{2m_3} 11 \frac{\pi}{2}}{R_E + \frac{1}{2m_3}}$ 



C). 
$$Roat = Rc + \frac{1}{9m_2} II r_{22}$$

$$Vin = Val \qquad Rin = r_{21} + (1+\beta) \left(\frac{1}{9m_3} II r_{23}\right)$$

$$Roat = Rc + \frac{1}{9m_2} II r_{23}$$

$$Roat = Rc + \frac{1}{9m_2} II r_{23}$$

$$Roat = Rc + \frac{1}{9m_3} II r_{23}$$

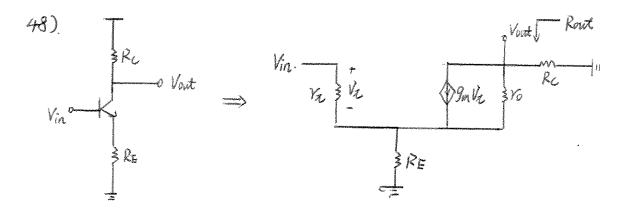
$$Re$$

$$Roat = Rc + \frac{1}{9m_3} II r_{23}$$

$$Re$$

$$Roat = Rc + \frac{1}{9m_3} II r_{23}$$

$$Re$$



Solve for Reg.

$$I_{T} = \int_{M} V_{T} + \frac{(V_{T} + V_{T})}{Y_{o}}$$

$$V_{T} = -I_{T} (Y_{T} / | R_{E})$$

$$I_{T} = -g_{m}I_{T}(Y_{T}//R_{E}) + (V_{T} - I_{T}(Y_{T}//R_{E}))$$

$$\frac{V_{T}}{I_{T}} = Y_{o}(1 + (Y_{T}//R_{E})) + g_{m}(Y_{T}//R_{E}))$$

$$\frac{V_{T}}{I_{T}} = Y_{o} + (1 + g_{m}Y_{o})(Y_{T}//R_{E})$$

$$Reg = Y_{o} + (1 + g_{m}Y_{o})(Y_{T}//R_{E})$$

$$Rout = R_{c}//Y_{o} + (1 + g_{m}Y_{o})(Y_{T}//R_{E})$$

49).  $\beta \gg 1$  and  $V_A < \infty$  to have meaningful result.

b). 
$$Rad Va$$

$$Q_1 \qquad RB$$

$$Q_1 \qquad Reg = \frac{1}{g_{n,2}} + RB$$

b). 
$$Road = roit (1+g_{m1}roi) \left[ \left( \frac{1}{g_{m2}} + \frac{R_B}{B+1} \right) / r_{Zi} \right]$$

$$\approx roit + (1+g_{m1}roi) \left( \frac{1}{g_{m2}} + \frac{R_B}{B+1} \right) / r_{Zi}$$

$$\approx roit + (1+g_{m1}roi) \left( \frac{1}{g_{m2}} + \frac{R_B}{B} \right)$$

$$\approx roit + (1+g_{m1}roi) \left( \frac{1}{g_{m2}} + \frac{R_B}{B} \right)$$

$$\approx roit + (1+g_{m1}roi) \left( \frac{1}{g_{m2}} + \frac{R_B}{B} \right)$$

C). Prost 
$$Q_2$$
  $Q_2$ 

C). Rout = 
$$r_0 + (1+g_{n1}r_0)(R_1/R_{n2}/R_{n1})$$
  
 $R_1/R_1/R_{n2} \approx R_1$ , since  $\beta >> 1$ .  
 $R_1/R_1/R_{n1} \approx r_0(1+g_{n1}R_1)$ 

$$50 > \beta >> 1$$
,  $V_A > M$ , for meaningful results

Rout = 
$$62 + (1 + g_{m2} r_{02}) (r_{01} / r_{22})$$
  
 $\approx r_{02} [1 + g_{m2} (r_{01} / r_{22})]$ 

The output impedance in b) is larger than a) because  $O_2$ 's connected for a high impedance load, whereas in a) it's womented to a low impedance load.

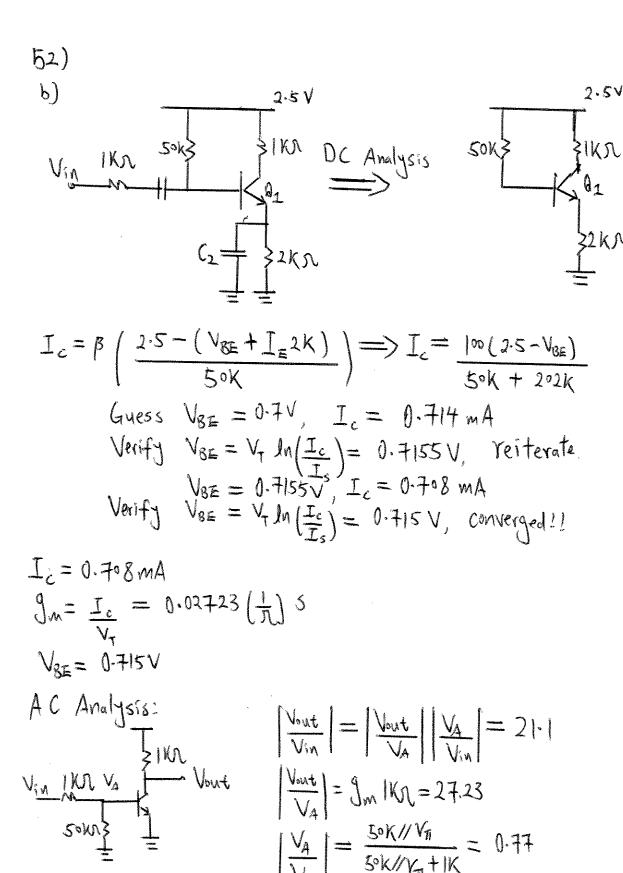
$$R_{in} = \frac{\gamma_{n}}{I/R_{B}} = \frac{\frac{\beta V_{T}}{I_{L}} R_{B}}{\frac{\beta V_{T}}{I_{C}} + R_{B}} = \frac{V_{T} R_{B}}{V_{T} + \frac{1}{\beta} R_{B}} = \frac{V_{T} R_{B}}{V_{T} + 2 \beta R_{B}}$$

Since 
$$L_B R_B >> V_f \Rightarrow R_{in} \approx \frac{V_f R_B}{L_B R_B} = \frac{V_f}{L_B} = \frac{V_f}{R} = \frac{\beta V_f}{L_c} \approx \gamma_c$$

52) 
$$L_S = 8 \times 10^{-6} A$$
,  $\beta = 100$ ,  $V_A = 80$ 

a)

 $V_{in} = \frac{100 \text{ Mpc}}{100 \text{ Mpc}} = \frac{1000 \text{ Mpc}}{10$ 



Verify 
$$V_{BE} = \frac{V_1}{M(\frac{V_2}{V_3})} = 0.676 \, \text{V}$$
, not  $0.7 \, \text{V}$ , reiterate  $V_{BE} = 0.676 \, \text{V}$ ,  $I_c = 0.164 \, \text{mA}$ 

Verify 
$$V_{BZ} = V_T \ln \left( \frac{I_c}{I_s} \right) = 0.677 V$$
, Converged 1!  
 $I_c = 0.164 \text{ mA}$ ,  $V_{BZ} = 0.677 V$ ,  $g_m = 0.00631 ( \frac{1}{12} ) S$ ,  $V_{AI} = 15.85 k$ 

AC Analysis: 
$$\frac{|V_{out}|}{|V_{in}|} = \frac{|V_{out}|}{|V_{in}|} = \frac{|V_{out}|}{|V_{in}|} = \frac{|V_{out}|}{|V_{out}|} = \frac{|V_{$$

53). 
$$V_{\alpha} = 25 V$$
  $R_{B} = 25 K \Lambda$   $R_{C} = 250 \Lambda$   $R_{C} = 250 \Lambda$   $R_{C} = 5 \times 10^{-4} A$   $V_{A} = 0$ 

DC Analysis: Assume collector bias voltage is still 1.5 V. So 1 V across Rc => Ic = 4mA.

$$V_{8E} = V_T J_n \left(\frac{I_c}{I_s}\right) = 0.832$$

$$I_B = \frac{2.5 - V_{BE}}{25K} = 0.06673 \text{ mA}$$

$$\beta = \frac{I_c}{I_B} = \frac{0.832 \text{ mA}}{0.06673 \text{ mA}} = 60$$

$$A_{v} = \left| \frac{V_{out}}{V_{in}} \right| = g_{m}(250\pi/18\pi) = 1-2$$
, (Greater than unity)

$$g_{m} = \frac{4mA}{26mV} = 0.1538 \left(\frac{1}{5}\right) S$$

Rout = 500 N

b) Since  $|A_1| = g_m R_c$ , and  $g_m$  is fixed by  $I_c$ . The only way to maximize  $|A_1|$  is to maximize  $R_c$ . However a large  $R_c$  Will Push  $g_m$  into saturation, losing its gain altogether. Therefore,  $g_m$  has to be as small as possible to provide enough room for  $g_m$  to drop  $g_m$  large  $g_m$  large  $g_m$ 

55) 
$$V_A = \infty$$

$$|A_V| = \frac{R_C + \frac{1}{9m_2} / |Y_{R2}|}{\frac{1}{9m_1}}$$
  
=  $9m_1(R_C + \frac{1}{9m_2} / |Y_{R2}|)$ 

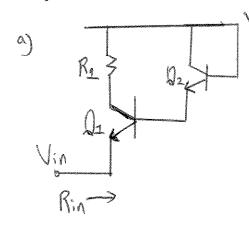
$$|Av| = \frac{V_{22}}{\frac{1}{g_{m_1}}} = g_{m_1} V_{22}$$

$$|AV| = \frac{Rc + \frac{1}{9m_3} 1/r_{23}}{\frac{1}{9m_1}}$$
  
=  $9m_1(Rc + \frac{1}{9m_3} 1/r_{23})$ 

55). 
$$|Av| = \left| \frac{V_{out}}{V_A} \right| \frac{V_A}{V_{in}}$$

$$= \left[ g_{mi} \left( R_C + \frac{1}{g_{m3}} \frac{1}{3} \right) \right] \left( \frac{R_E / \frac{1}{g_{mi}}}{R_E / \frac{1}{g_{mi}} + R_S} \right)$$

$$= V_{out}$$



$$R_{in} = \frac{1}{9} \sqrt{v_{n_1}} + \frac{1}{9} \sqrt{v_{n_2}}$$

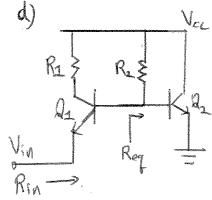
$$\frac{1}{8} + 1$$

Since B is usually very large

$$R_{in} \approx \frac{1}{J_{m_1}} + \frac{1}{J_{m_1}(\beta_1+1)}$$

Reg = 
$$R_2/100 = R_2$$
 $R_{13}$ 
 $R_{14}$ 
 $R_{15}$ 
 $R$ 

$$R_{in} = \frac{1}{J_{m_1}} \frac{1}{V_{m_2}} + \frac{R_2}{R_2 + 1}$$

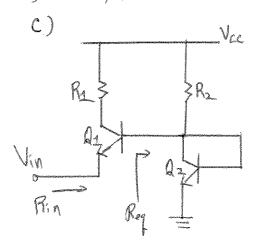


$$\frac{1}{R_{1}} = \frac{1}{3} \frac{1}{1} \frac{Y_{01}}{R_{1}} + \frac{R_{2} \frac{1}{1} Y_{02}}{R_{1} + 1}$$

Since B is usually very large

$$R_{in} \approx \frac{1}{J_{m_2}} + \frac{R_2 / \gamma_{n_2}}{\beta_1 + 1}$$

56) \* Note, part c) and d) have swapped places



Vcc 
$$R_{eq} = R_2 // \frac{1}{9} // Y_{n_2}$$
 $R_2$ 
 $R_{in} = \frac{1}{9} // Y_{n_2} + R_2 // \frac{1}{9} // Y_{n_2}$ 
 $R_3$ 
 $R_{in} = \frac{1}{9} // Y_{n_2} + R_2 // \frac{1}{9} // Y_{n_2}$ 
 $R_3$ 
 $R_4$ 
 $R$ 

$$\begin{array}{c} R_{in} \approx \frac{1}{J_{m_1}} + \frac{R_2 J_{ij}}{g_{m_2}} \\ \\ \frac{R}{1} + 1 \end{array}$$

Since an ideal current source is an open circuit, the signal current produced by the transistor has no where to go but Yo.

So Vout = 
$$-(g_m(o-V_{in}))v_o + V_{in}$$
  
 $V_{out} = g_m v_o V_{in} + V_{in}$   
 $V_{out} = V_{in}(g_m v_o + 1)$   
 $\frac{V_{out}}{V_{in}} = 1 + g_m v_o$   
 $V_{in}$ 

b) AC Analysis

Vout 
$$|X| = |V_{out}| = g_{m}|X|$$
 $|Y_{in}| = |Y_{out}| = g_{m}|X|$ 
 $|Y_{in}| = |Y_{out}| = |Y_{out$ 

$$A_{v} = \left| \frac{V_{out}}{V_{in}} \right| = g_{m} |K|$$

58) 
$$\frac{1}{2} | V_{cc} = 2.5$$

O) DC Analysis:
$$I_{c} = \beta \left( \frac{1 \cdot 2 - (V_{8E} + I_{E} 0.4)}{6 \cdot 24} \right) \Rightarrow \frac{\beta (1 \cdot 2 - V_{8E})}{6 \cdot 24 + 0.4B}$$
Guess  $V_{8E} = 0.7 \Rightarrow I_{c} = 1.072 \text{ mA}$ 

$$Verify  $V_{8E}: V_{8E} = V_{7} \ln \left( \frac{I_{c}}{I_{s}} \right) = 0.726 \text{ V}, \text{ Not } 0.7\text{ V}, \text{ reiterate}$$$

$$V_{BE} = 0.726 \text{ V}; I_c = 1.0163 \text{ mA}$$
  
Verify  $V_{BE}$ :  $V_{BE} = V_T J_n(\frac{I_c}{I_s}) = 0.725 \text{ V}, \text{ Converged!}$ 

$$V_{BE} = 0.725$$
,  $V_{CE} = 2.5 - [0.0163)(1K) + 0.4(\frac{1.0163}{0.99})$   
 $V_{CE} = 1.07$   
 $I_{c} = 1.0163 \text{ MA}$ 

$$C_8 = 0$$

a) Since C8 Was Not considered during DC analysis, it has no effect on operating point analysis. So it is still the same as 58).

$$V_{8E} = 0.725 V$$
 $I_c = 1.0163 \text{ mA}$ 
 $I_3 = 10.163 \text{ MA}$ 
 $V_{GE} = 1.07 V$ 

b) Since capacitor is frequency dependent, the circuit's AC analysis will be different.

Vant 
$$\frac{1}{3}$$
 |  $A_{1} = \frac{1}{1}$  |  $A_{1} = \frac{1}{1}$  |  $A_{2} = \frac{11.4}{1}$  |  $A_{3} = \frac{1}{1}$  |  $A_{4} = \frac{1}{1}$  |  $A_{5} = \frac{11.4}{1}$  |  $A_{5} = \frac{11.4}$ 

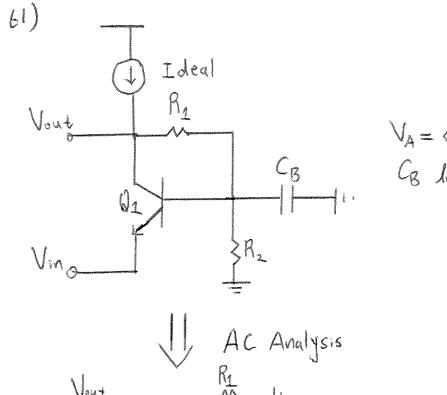
$$|A_{1}| = \frac{1k}{\frac{1}{3} + \frac{6.24 \, \text{K} \Omega}{\beta + 1}} = 11.4$$

Note: 6.24 KM is RTHEN of 13 Ks and 12 Ks Combination.

$$R_{\text{out}} = \frac{1}{J_{\text{M2}}} / R_{1} \approx \frac{1}{J_{\text{M2}}} / R_{1}$$

$$A_{\text{N}} = \left| \frac{V_{\text{out}}}{V_{\text{in}}} \right| = g_{\text{M1}} \left( \frac{1}{J_{\text{M2}}} / Y_{\text{M2}} / R_{1} \right) \approx g_{\text{M2}} \left( \frac{1}{J_{\text{M2}}} / R_{2} \right)$$

$$V_{\text{in}} = \frac{1}{J_{\text{M2}}} / \frac{1}{J_{\text{M2}}} = \frac{1}{J_{\text{M2}}} \left( \frac{1}{J_{\text{M2}}} / \frac{1}{J_{\text{M2}}} \right) \approx g_{\text{M2}} \left( \frac{1}{J_{\text{M2}}} / \frac{1}{J_{\text{M2}}} \right)$$



$$R_{\text{out}} = R_{1}$$

$$R_{\text{in}} = \frac{1}{J_{m_{1}}} / V_{\pi_{1}} \approx \frac{1}{J_{m_{1}}}$$

$$\frac{V_{\text{out}}}{V_{i\dot{n}}} = -g_{m}(-V_{i\dot{n}})Y_{o} + V_{i\dot{n}} = V_{\text{out}} = V_{\text{out}} = (g_{m}V_{o} + 1)$$

$$\dot{A}_{V} = (g_{m}V_{o} + 1) \left( \frac{V_{\pi}}{V_{\pi} + R_{S}} \right).$$

$$V_{cc}$$

$$V_{de}$$

$$V_{ee}$$

$$V$$

$$\Rightarrow \int_{M_1} \frac{J_{M_2}}{2} \Rightarrow \left| \frac{V_{\text{out}_2}}{V_{\text{in}}} \right| = \frac{1}{2} \left| \frac{V_{\text{out}_2}}{V_{\text{in}}} \right|$$

( V8E1 = V8E2 = V8E)

$$\begin{array}{c} \text{Vout} \\ \text{Vout} \\ \text{Re} \\ \text{Vin} \end{array} \Rightarrow \begin{array}{c} \text{Re} \\ \text{Vin} \\ \text{Vin} \\ \end{array}$$

$$V_{out} = -\left(I_{1} + J_{m}V_{\pi}\right)R_{c}, \quad I_{1} = \frac{V_{out} - V_{E}}{Y_{o}}$$

$$V_{out} = -\left(\frac{V_{out} - V_{E}}{Y_{o}} + J_{m}V_{\pi}\right)R_{c}, \quad V_{E} = -\frac{J_{m}V_{\pi}}{\beta}(Y_{\pi} + R_{B})$$

$$V_{out} = -\left(\frac{V_{out} + J_{m}V_{\pi}(Y_{\pi} + R_{B})}{\beta} + J_{m}V_{\pi}\right)R_{c}$$

$$V_{out} = -\left(\frac{V_{out} + J_{m}V_{\pi}(Y_{\pi} + R_{B})}{\gamma_{o}} + J_{m}V_{\pi}\right)R_{c}$$

Re arranging

$$V_{\pi} = -\frac{\left(1 + \frac{R_c}{Y_0}\right)}{\frac{g_m(Y_n + R_B)R_c}{\beta Y_0}} \quad V_{out} = AV_{out}$$

Summing the voltage at Node E. 
$$V_E - \left( (1 + \frac{1}{\beta}) g_m L_n + \frac{(V_{out} - V_E)}{V_o} \right) R_E = V_{in}$$
 (1)

substituting A into equation

$$V_{cc} = 2.5V$$

$$V_{out}$$

$$R_{E} = 100 \Omega$$

$$R_E = 100\Omega$$

$$V_A = \infty$$

$$|A_J| = 0.8$$

$$|A_1| = \frac{R_E}{R_E + \frac{1}{3}m} = \frac{R_E I_c}{R_E I_c + V_T} = 0.8$$

$$\Rightarrow R_{E}I_{c} = 0.8(R_{E}I_{c} + V_{T}), R_{E} = 1000$$

$$\Rightarrow 0.1I_{c} = 0.08I_{c} + 0.0208 \Rightarrow 0.02I_{c} = 0.0208$$

$$\Rightarrow I_{c} = 1.04mA$$

$$|A_{1}| = \frac{R_{E}I_{c}}{R_{E}I_{c} + V_{T}} > 0.9 \Rightarrow R_{E}I_{c} > 0.9[R_{E}I_{c} + V_{T}]$$

$$R_{in} = Y_{\pi} + (1+\beta)R_{E} > 10K \Rightarrow 100V_{\pi} + (101)R_{E}I_{c} > 10K\Pi I_{c}$$
  
Substituting  $R_{E}I_{c} = 240 \,\text{mV} \Rightarrow I_{c} < 2.684 \,\text{mA}$ 

To Verify:

$$R_{in} = \frac{100 (0.026)}{2.5} + (101) 0.096 = 10.74 K \Lambda$$

$$|A_{1}| = \frac{(0.096)(2.5)}{(0.096)(2.5) + 0.026} = 0.902$$

Vin Rs Volt 
$$R_s$$
  $R_s$   $R_s$ 

$$R_{out} = \frac{1}{9} + \frac{R_s}{(B+1)} \le 5 \pi \quad (Assuming Y_n >> \frac{1}{9})$$

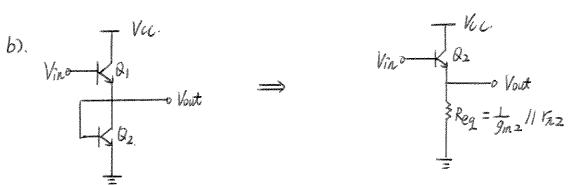
$$R_{out} = 0.026 + \frac{200\pi I_c}{101} \le 5\pi I_c$$

$$=> I_c \ge 0.0086A$$

$$Pick I_c = 0.009 A$$

$$R_{\text{out}} = \frac{0.026V}{0.009A} + \frac{200}{101} = 4.87 \Omega$$

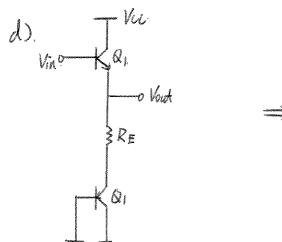
$$|A_V| = \frac{\gamma_0}{\gamma_0 + \frac{1}{q_m}}$$
, Since  $\gamma_0 = \infty$ 



$$|Av| = \frac{\frac{1}{9m^2} 1/722}{\frac{1}{9m^2} 1/722 + \frac{1}{9m^2}}$$
 Rin =  $\frac{1}{12m^2} + \frac{1}{9m^2} 1/722 + \frac{1}{9m^2} 1/722$ 

$$Rin = \frac{1}{2} + (1+\beta) \frac{1}{9m^2} 11 \frac{1}{2}$$

$$|A_V| = \frac{\frac{1}{g_{m2}} + \frac{R_S}{\beta + 1}}{\frac{1}{g_{m2}} + \frac{R_S}{\beta + 1} + \frac{1}{g_{m1}}}$$



$$|Av| = \frac{R_E + (g_{m_1} / |G_1|)}{R_E + (g_{m_1} / |G_1|) + g_{m_1}}$$
  $R_{in} = \frac{R_E + (1/p) \left[ R_E + (g_{m_1} / |G_1|) \right]}{R_{in}}$ 

Vin a Ka,

Voit

Req = 
$$\frac{1}{g_{m2}} + \frac{Rs}{\beta+1}$$

(Assuming  $Y_{T1} >> \frac{1}{g_{m1}}$ )

$$Rin = r_2 + (1t\beta) \left( \frac{1}{9m^2} + \frac{Rc}{\beta+1} \right)$$

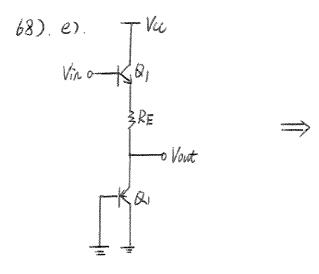
Rout = 
$$(\frac{1}{9m_2} + \frac{R_s}{\beta+1}) / (\frac{1}{9m_1} / k_2)$$
.  
Rout  $\approx (\frac{1}{9m_2} + \frac{R_s}{\beta+1}) / (\frac{1}{9m_1} / k_2)$ .  
 $= \sqrt{\frac{1}{9m_2}} + \frac{R_s}{\beta+1} = \sqrt{\frac{1}{9m_2}} + \sqrt{\frac{1}{9m_2}}$ 

$$Rout = (\frac{g_{m2}}{g_{m2}} + \frac{1}{\beta+1}) / (\frac{1}{g_{m1}} / \frac{1}{2}).$$

$$Rout \approx (\frac{1}{g_{m2}} + \frac{R_s}{\beta+1}) / (\frac{1}{g_{m1}} / \frac{1}{2}).$$

$$V_{in} = \frac{1}{2} Reg = R_E + (\frac{1}{g_{m1}} / \frac{1}{2}).$$

$$Reg = R_E + (\frac{1}{g_{m1}} / \frac{1}{2}).$$



Vin o 
$$RE$$

Reg =  $\frac{1}{g_{mi}} / r_{Zi}$ 

$$|Av| = \frac{\frac{1}{g_{mi}}/|Y_{2i}|}{\frac{1}{g_{mi}}/|Y_{2i}| + R_E + \frac{1}{g_{mi}}}$$

$$R_{in} = Y_{\pi_{1}} + (1+\beta)Y_{\pi_{2}}$$

Rin=
$$\frac{1}{9}$$
 +  $\frac{1}{9}$  (Assume  $\frac{1}{1}$ )

Rin= $\frac{1}{9}$  +  $\frac{1}{9}$  ( $\frac{1}{1}$ )

Rin= $\frac{1}{1}$  +  $\frac{1}{9}$  ( $\frac{1}{1}$ )

C) Current Gain = 
$$\frac{\left(I_{c1} + I_{c2}\right)}{I_{B1}} = \frac{\beta + \frac{I_{c2}}{I_{B1}}}{I_{B1}} = \frac{\beta + \frac{\beta I_{B2}}{I_{B1}}}{I_{B1}}$$
  
Since  $I_{B2} = I_{c2} = \beta I_{B1}$ 

Current Gain = 
$$\beta + \beta^2 = \beta(\beta + 1)$$
, (Assuming  $\beta_1 = \beta_2 = \beta$ )

") 
$$R_{cs} = V_{o_2} + (1 + g_{w_2} V_{o_3})(R_E / V_{n_2})$$

Vin 
$$O$$
  $A_N = \frac{R_{es} // Y_{o1}}{R_{es} // Y_{o1} + \frac{1}{J_{m_1}}}$ 

$$A_{J} = (Y_{o2} + (I + g_{M_2} Y_{o2})(R_E / Y_{n_2})) / Y_{o1}$$

$$= (Y_{o2} + (I + g_{M_2} Y_{o2})(R_E / Y_{n_2})) / Y_{o1} + \frac{1}{g_{M_1}}$$

71). 
$$V\alpha = 2.5V$$

$$I_{3} = 7 \times 10^{-16} A$$

$$V_{in} = 100$$

$$V_{10} = 100$$

$$V_{10} = 5V$$

$$V_{10} = 5V$$

$$I_{s} = 7 \times 10^{-16} A$$

$$\beta = 100$$

$$V_{A} = 5 V$$

## DC Analysis:

(Ignore Vo's effect)

$$I_{c} = \beta \left( \frac{2.5 \cdot \left( V_{BE} + \frac{I_{c}}{\alpha} I K \Omega \right)}{10 K \Omega} \right)$$

$$= \frac{1.5 V}{10 K \Omega}$$

$$Veavrange = \frac{2.5 - V_{BE}}{10 K \Omega}$$

$$I_{c} = \frac{2.5 - V_{BE}}{10 K \Omega}$$

$$= \frac{10 K \Omega}{\beta} + \frac{1 K \Omega}{\alpha}$$

Guess: VBE = 0.7V, Ic=1.621mA

check for VBE: VBE = 4 M(=) = 0.740V, not 0.7, reiterate

Var = 0.740V, I = 1.59 mA

Check for Vai: VBE = 4 M (=) = 0.740V, Converged.

So I = 1.59 mA, Jm = 0.0612 (1)5, = 16.34 s. V. = 3.14KA

AC Analysis: (Include 
$$V_0$$
)

Vin  $V_{cc} = 2.5 \text{ V}$ 

Vin  $V_{cc} = 2.5 \text{ V}$ 

Vin  $V_{cc} = 2.5 \text{ V}$ 

(Assume  $C_1$  and  $C_2$  are large)

$$= \frac{V_{cc} = 2.5 \text{ V}}{V_0 + V_0}$$

$$= \frac{V_0 + V_0}{V_0 + V_0} = \frac{V_0 + V_0}{V_0} = \frac{V_0 + V_0}{V_0}$$

$$= \frac{V_0 + V_0}{V_0} = \frac{V_0 + V_0$$

a) 
$$R_{in} = Y_{n_1} + (1+\beta)(R_E // Y_{n_2} // Y_{0_1})$$
  
 $R_{out} = R_c // Y_{0_2}$ 

b) 
$$\left| \frac{V_{out}}{V_{in}} \right| = \left| \frac{V_x}{V_{in}} \right| \left| \frac{V_{out}}{V_x} \right|$$

$$\left| \frac{V_x}{V_{in}} \right| = \frac{\left( R_E // Y_{n_2} // Y_{01} \right)}{\frac{1}{S_{m_1}} + R_E // Y_{n_2} // Y_{01}}, \quad \left| \frac{V_{out}}{V_x} \right| = S_{m_2} R_c$$

73).

Vin 0 + 
$$Q_1$$
 $Q_1$ 
 $Q_2$ 
 $Q_3$ 
 $Q_4$ 
 $Q_4$ 
 $Q_4$ 
 $Q_4$ 
 $Q_5$ 
 $Q_6$ 
 $Q_6$ 

a) 
$$R_{eq} = R_E / |Y_{n_1}| / \frac{1}{g}$$

$$R_{in} = Y_{n_1} + (1+\beta) [R_E / |Y_{n_2}| / \frac{1}{g}]$$

$$R_{out} = R_c$$

b) 
$$\left| \frac{V_{\text{out}}}{V_{\text{in}}} \right| = \left| \frac{V_{\text{x}}}{V_{\text{in}}} \right| \frac{V_{\text{out}}}{V_{\text{x}}}$$

$$\left| \frac{V_{\text{x}}}{V_{\text{in}}} \right| = \frac{R_{\text{E}} / \frac{1}{2} / |Y_{\text{fin}}|}{\frac{1}{2} / |Y_{\text{fin}}|}, \quad \left| \frac{V_{\text{out}}}{V_{\text{x}}} \right| = \int_{m_{\text{E}}} R_{\text{c}}$$

$$\left| \frac{V_{\text{x}}}{V_{\text{in}}} \right| = \frac{1}{2} \frac{V_{\text{out}}}{V_{\text{x}}} + R_{\text{E}} / \frac{1}{2} / |Y_{\text{fin}}|}, \quad \left| \frac{V_{\text{out}}}{V_{\text{x}}} \right| = \int_{m_{\text{E}}} R_{\text{c}}$$

74). 
$$V_{CB} = 2.5V$$

$$R_{CB} = 10$$

$$R_{CB} = 1 \text{K.} \quad R_{C} = 1 \text{K.}$$

$$R_{CB} = 1 \text{K.} \quad R_{C} = 1 \text{K.}$$

$$A_V = 10$$
  
 $R_{in} > 5KN$   
 $R_{out} = 1K$ ,  $R_c = 1KN$ 

$$Av = \frac{R_c}{\frac{1}{3m}} = \frac{10}{10} = \frac{I_c R_c}{V_T} \Rightarrow I_c = 0.26mA$$

$$V_{E} = V_T ln \left(\frac{I_c}{I_s}\right) = 0.697V.$$

$$I_c = 100 \left( \frac{2.5 - 0.697}{R_B} \right) \Rightarrow R_B = 693 \text{KN}, \ Y_A = \beta \frac{V_T}{I_c} = 10 \text{KN}$$

$$R_{in} = 693 \, \text{K// lok} = 9.86 \, \text{K} \, \text{N}$$

$$\frac{1}{2\pi (200) \, C_B} = \frac{1}{10} \, \frac{1}{9} = 10 \, \text{A} = 7 \, \text{C}_B = 80 \, \text{M} \, \text{G}$$

$$(To avoid gain degradation).$$

$$R_c = 1 \text{ KR}$$
 $R_B = 693 \text{ K}$ 
 $C_B = 80 \text{ M}$ 
 $R_{in} = 9.86 \text{ KR}$ 

75). 
$$\sqrt{Vac} = 2.5 \text{ V}$$

Vin o  $\sqrt{Q_1}$ 

$$A_V = Maximum$$
  
 $R_{out} \le 500\Lambda$   
 $V_{BC} \le 400 \, \text{mV}$ 

$$A_{\nu} = g_{m}R_{c} = \frac{I_{c}R_{c}}{V_{T}}$$
, gain is maximized by maximize  $I_{c}R_{c}$ 

$$R_{\text{out}} = R_c \leq 500\text{N}$$
, Choose  $R_c = 450\text{N}$ ,  $R_{\text{out}} = 450\text{N}$   
 $V_{\text{RC}} = V_{\text{RE}} - (2.5 - I_c R_c) \leq 400 \text{ mV}$ 

Guess 
$$V_{8E} = 0.7$$
, and let  $V_{8C} = 400 \,\text{mV}$  to maximize  $I_{c}R_{c}$ .  $0.7 - (2.5 - I_{c}0.450) = 0.4$   $I_{c} = 4.89 \,\text{mA}$ ,  $V_{3E} = V_{7} \, ln \left(\frac{I_{c}}{I_{c}}\right) = 0.773$ 

Not 0.7, Veiterate.

$$0.773-2.5+I_{c}0.450=0.4$$
  
 $I_{c}=4.73$  mA,  $V_{8e}=0.772$  (onverged!]

$$A_{V} = \left(\frac{I_{c}}{V_{T}}\right)\left(R_{c}\right) = \left(\frac{4.73}{26}\right)\left(450\right) = 81.9$$

$$R_8 = 100 \left( \frac{2.5 - 0.772}{4.73} \right) = 36.5 \text{K}$$

$$R_B = 36.5k$$
 =>  $A_V = 81.9$   
 $R_c = 450\Lambda$   $V_{BC} = 0.4V$   
 $R_{out} = 450\Lambda$ 

$$V_{ino} = 2.5V$$

$$V_{ino} = 2.5V$$

$$Q_{1}$$

$$Rin: Maximum$$
 $Av \ge 20$ 
 $Rout = Rc = 1K$ 

$$A_v = g_m R_c = \frac{I_c R_c}{V_T} \ge 20 \implies I_c \ge 0.52 \text{ mA}$$

$$R_{in} = R_B / r_n = \frac{\beta R_B V_T}{R_B I_c + V_T \beta} ), \quad I_c = \beta \left( \frac{2.5 - V_{BE}}{R_B} \right)^2$$

As We can see from 1), higher Ic means lower Rin. So set Ic as low as possible,  $I_c = 0.52 \, \text{mA}$ .  $V_{BE} = V_T \ln \left(\frac{I_c}{T}\right) = 0.715 \, \text{V}$ 

From 2), 
$$R_B = \frac{100(2.5 - 0.715)}{0.52} = 343.3 \text{Ke}, V_n = 5 \text{Ke}$$

$$R_c = 1K\Lambda$$
 =>  $A_v = 20$   
 $R_B = 343.3K\Lambda$   $R_{out} = 1K\Lambda$ 

77). 
$$Vac$$
 $Re$ 
 $Re$ 

$$A_{V} = \int_{m} R_{c} = \frac{I_{c}}{V_{T}} R_{c} = 15$$

$$A_{v} = J_{on}R_{c} = \frac{I_{c}R_{c}}{V_{T}} = 15 \Rightarrow I_{c} = 0.195 \text{mA}$$

$$V_{8c} = V_{T} \ln \left(\frac{I_{c}}{I_{c}}\right) = 0.689$$

$$V_{8c} = V_{8E} - (V_{cc} - I_c R_c) \le 0.4 \text{V}$$
,  $I_c R_c = 0.39 \text{V}$   
 $V_{cc} \ge 0.689 + 0.39 - 0.4 = 0.679 \text{V}$ 

Since the problem is concerned with minimum power supply, let  $V_{cc} = 0.69 \, \text{V}$ , Since  $V_{BE} = 0.679 \, \text{V} \, (\text{V}_{cc} > \text{V}_{SE})$ 

$$I_c = B\left(\frac{V_{cc} - 0.689}{R_B}\right) = R_B = 100\left(\frac{0.69 - 0.689}{0.195}\right) = 512.8 \text{ R}$$

$$R_c = 2KR$$
 $R_B = 512.8R => A_V = 15$ 
 $V_{cc} = 0.69V$ 
 $R_{out} = 2KR$ 

78). 
$$V_{cc} = 2.5 V$$
 $A_0 = g_m R_c$ 
 $V_{in} = g_m R_c$ 

$$A_0 = \frac{I_c R_c}{V_T}$$
, Power Dissipation =  $I_c V_{cc}$   
 $R_{out} = R_c = \frac{A_0 V_T}{I_c}$ 

For large Rout, Ic has to be small, which decreases power. So small power dissipation and small output impedance cannot be satisfied simultaneously.

79). 
$$\sqrt{\frac{1}{R_{B}^{3}}} \sqrt{\frac{1}{R_{C}}} \sqrt{\frac{1}{R_{$$

$$A_{V} = g_{m}R_{c} = \frac{I_{c}R_{c}}{V_{T}} = 20, \quad V_{cc}I_{c} = I_{m}W$$

$$I_{c} = 0.4 \text{ mA}, \quad R_{c} = 1.3K$$

$$V_{8E} = V_{T} \ln\left(\frac{I_{c}}{I_{s}}\right) = 0.708V, \quad I_{c} = \beta\left(\frac{V_{cc} - V_{8E}}{R_{B}}\right) = \frac{100\left(\frac{2.5 - 0.708}{R_{B}}\right)}{R_{B}}$$

=> 
$$R_B = 448K$$
,  $R_{in} = 448/(100)(\frac{26}{0.4}) = 6.4K$ 

$$R_8 = 448K$$
 =>  $A_v = 20$   
 $R_c = 1.3K$  Power Budget =  $ImW$   
 $R_{out} = 1.3K\Lambda$   
 $R_{in} = 6.4K$ 

80) 
$$\frac{3R_{c}}{3R_{c}} = \frac{3R_{c}}{3R_{c}}$$
Vin of Rout =  $R_{c} = 500$ N
$$R_{E}I_{c} \approx 300 \text{ mV}$$

$$A_V = 5$$
  
 $R_{out} = R_c = 500$   
 $R_{E}I_c = 300$  mV

$$A_V = \frac{R_c I_c}{R_E I_c + V_T} = \frac{R_c I_c}{300 + 26} \Rightarrow \begin{array}{l} R_c I_c = 1.63V \Rightarrow I_c = 3.26 \text{ mA} \\ R_E I_c \approx 300 \text{ mV} \Rightarrow R_E = 92 \text{ }\Omega \end{array}$$

$$R_{1} = 2.5 - (V_{BE} + 0.3), V_{BE} = V_{T} ln \left(\frac{I_{c}}{I_{s}}\right) = 0.7624$$

$$10 I_{B} = 0.326 \text{ mA}$$

$$R_1 = \frac{2.5 - (0.7624 + 0.3)}{0.326} = 4.41K$$

$$R_2 = \frac{(0.7624 + 0.3)}{(940.0326)} = 3.62 K$$

De is in soft saturation region, so active region characteristics Still apply.

$$R_{c} = 500 \Lambda$$
 $R_{1} = 441 K \Lambda$ 
 $R_{2} = 3.64 K \Lambda$ 
 $R_{5} = 92 \Lambda$ 
 $R_{6} = 92 \Lambda$ 

81) 
$$\frac{V_{CC} = 2.5V}{R_{1}}$$

$$V_{ino} = \frac{V_{CC}}{V_{ino}}$$

$$R_{2} = \frac{V_{CC}}{V_{out}}$$

$$R_{2} = \frac{V_{CC}}{V_{out}}$$

$$R_{2} = \frac{V_{CC}}{V_{out}}$$

$$R_{3} = \frac{V_{CC}}{V_{out}}$$

$$R_{2} = \frac{V_{CC}}{V_{out}}$$

$$R_{3} = \frac{V_{CC}}{V_{out}}$$

$$R_{4} = \frac{V_{CC}}{V_{out}}$$

$$R_{5} = \frac{V_{CC}}{V_{out}}$$

$$R_{6} = \frac{V_{CC}}{V_{out}}$$

$$R_{7} = \frac{V_{CC}}{V_{out}}$$

$$R_{8} = \frac{V_{CC}}{V_{out}}$$

$$R_{8} = \frac{V_{CC}}{V_{out}}$$

$$R_{8} = \frac{V_{CC}}{V_{out}}$$

$$A_V = M_{aximum}$$
 $R_{out} = R_c \le 1 K \Omega$ 
 $V_{BC} = 0.4 V$ 
 $R_E I_c \approx 200 \text{ mV}$ 

$$V_{BC} = (V_{BE} + 0.2) - (2.5 - I_c R_c) = 0.4 i)$$

$$A_{V} = \frac{R_c I_c}{R_E I_c + V_T} = \frac{R_c I_c}{0.226}$$

Rearrange, 1) becomes 
$$I_cR_c = 0.4+2.5-(V_{8z}+0.2)$$
  
Guess  $V_{RE} = 0.7 \Rightarrow I_cR_c = 2V$   
Let  $R_c = 1K \Rightarrow I_c = 2mA$ 

Check for VBE: VBE = VT In (Ic) = 0.750, Not 0.7, reiterate

Check for VBE: VBE = VT IN(=) = 0.750, Converged!

$$I_c = 1.95 \text{ mA}$$
,  $R_E I_c = 200 \text{ mA} = 7 R_E = 103 \Omega$   
 $I_B = 0.0195 \text{ mA}$ 

$$R_1 = \frac{2.5 - (0.750 + 0.2)}{(19)(0.0195)} = 7.95 \text{ K}$$

$$R_2 = \frac{(0.750 + 0.2)}{(9)(0.0195)} = 5.41K$$

$$A_{V} = \frac{R_{c}I_{c}}{R_{E}I_{c} + V_{T}} = \frac{1.95}{0.226} = 8.63$$

This is the maximum gain We would get when Rout is IKA and VBC is at 0.4 V. Since anything larger Will Violate either requirement.

$$R_c = 1K\Omega$$
 $R_E = 103\Omega$ 
 $R_1 = 7.95K\Omega$ 
 $R_2 = 5.41K\Omega$ 

82). 
$$R_1 | 101_B > R_C$$
 Power budget = 5

 $R_1 | 101_B > R_C$ 
 $R_2 > R_3$ 
 $R_4 = 5$ 
 $R_4 = 5$ 

$$V_{cc} (I_c + I_c) = 5 \text{ mW} \Rightarrow I_c = 1.82 \text{ mA}, I_B = 0.0182 \text{ mA}$$
 $V_{cc} = V_T \ln(I_c) = 0.747$ 

$$A_{V} = \frac{R_{c}I_{c}}{R_{c}I_{c}+V_{T}} = \frac{R_{c}I_{c}}{0.226} = 5 \implies R_{c}I_{c} = 1.13V \implies R_{c} = 621 \Omega$$

$$R_1 = \frac{2.5 - (0.747 + 0.2)}{(10 \times 0.0182)} = 8.53 \text{K}\Omega$$

$$R_2 = \frac{(0.747 + 0.2)}{(9)(0.0182)} = 5.78K \mathcal{R}$$

$$R_c = 621 \Omega$$
 $R_E = 110 \Omega$ 
 $R_1 = 8.53 \text{ KD}$ 
 $R_1 = 5.78 \text{ KD}$ 
 $R_2 = 5.78 \text{ KD}$ 

83). 
$$R_{E} = 20$$

$$R_{I} = 80$$

$$R_{I} = 50$$

$$R_{E} I_{C} \approx 10$$

$$R_{E} I_{C} \approx 10$$

$$R_{E} I_{C} \approx 10$$

$$R_{E} I_{C} \approx 10$$

$$A_V = 20$$

$$R_{in} = 50 \Omega$$

$$R_E I_c \approx 10 V_T = 260 \text{ mV}$$

$$R_{in} = \frac{1}{g_m} = 50$$
 , Since  $R_E$  doesn't affect input impedance.

$$\frac{V_{1}}{I_{c}} = 50\pi \implies I_{c} = \frac{V_{1}}{50\pi} = 0.52 \text{ mA}, I_{8} = 0.0052 \text{ mA}$$

$$A_{V} = \frac{R_{c}}{1/9_{m}} = \frac{I_{c}R_{c}}{V_{T}} = 20 \implies R_{c} = 1KR$$

$$R_1 = \frac{2.5 - (0.715 + 0.260)}{(10)(0.0052)} = 29.3K$$

$$R_2 = \frac{(0.715 + 0.260)}{(9)(0.0052)} = 20.83K$$

$$\frac{R_{E}I_{c} \approx 260 \text{ mV} \Rightarrow R_{E} \approx 500 \text{ N}}{C_{B}(2\pi)(2^{\circ})} = \frac{1}{10} \frac{1}{9} = 50 \Rightarrow C_{B} = 159.1 \text{ mf}}$$

$$R_c = 1K\Omega$$
,  $R_E = 500\Omega$ ,  $R_A = 29.3K\Omega$ ,  $R_a = 20.83K$ ,  $C_B = 159.1 \text{ M}$   
=>  $A_V = 20$ ,  $R_{in} = 50\Omega$ 

$$R_1$$
 $R_2$ 
 $R_2$ 
 $R_3$ 
 $R_4$ 
 $R_5$ 
 $R_6$ 
 $R_6$ 

$$A_{\nu} = 8$$

$$R_{out} = 500 \Omega$$

$$R_{\text{out}} = R_c = 500 \Omega$$

$$A_{V} = I_{c} R_{c} = 8 = 7$$
  $I_{c} = 0.416 \text{ mA}, I_{B} = 0.00416 \text{ mA}$   
 $V_{BE} = V_{T} In \left(\frac{I_{c}}{I_{s}}\right) = 0.709$ 

$$R_{\rm E} \approx \frac{260\,{\rm mV}}{{
m I}_{c}} = 625\,{
m T}_{c}$$
,  $R_{\rm I} = \frac{2.5-\left(0.709+0.260\right)}{\left(10\right)\left(0.00416\right)} = 36.8 {
m K}{
m T}_{c}$ 

$$R_2 = \frac{(0.709 + 0.260)}{(9)(0.00416)} = 25.9 \text{KM}$$

$$\frac{1}{9_m} = \frac{V_7}{I_c} = 62.5 \, \text{T}, \frac{1}{C_B 200 (2\pi)} = \frac{62.5}{10} \Rightarrow C_B = 127.3 \, \text{Mf}$$

$$C_{B} = 127.3Mf$$
 $R_{1} = 36.8 K$ 
 $R_{2} = 25.9 K$ 
 $R_{c} = 500 \pi$ 
 $R_{c} = 625 \pi$ 
 $R_{c} = 625 \pi$ 
 $R_{c} = 625 \pi$ 

$$A_{V} = 20$$

$$R_{c} = 2000$$

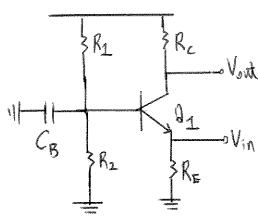
$$(R_{c} = R_{out})$$

$$A_{V} = \frac{I_{c}R_{c}}{V_{T}} = 20 \Rightarrow I_{c} = 2.6 \text{ mA}$$

$$I_{B} = 0.026 \text{ mA}, 10I_{B} = 0.26 \text{ mA}$$

Power = Vec (Ic+ 10 IB) = 2.5 (0.26 mA + 2.6 mA) = 7.15 mW

This is the minimum power dissipation, Since anything lower Will lower the Voltage gain.

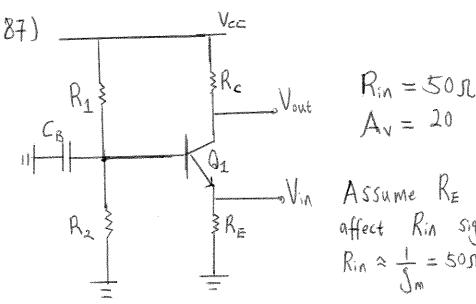


$$A_{V} = g_{m}R_{c} = \frac{I_{c}R_{c}}{V_{T}} = 10 \Rightarrow R_{c} = 0.143KR$$

$$R_{1} = \frac{2.5 - (0.747 + 0.260)}{(10)(0.0182)} = 8.2K, R_{2} = \frac{(0.747 + 0.260)}{(9)(0.0182)} = 6.15K$$

$$\frac{1}{g_{m}} = \frac{V_{1}}{I_{c}} = \frac{14.3 \, \Pi}{C_{B} \, 2\pi (200)} = \frac{14.3}{10} \implies C_{B} = 556.5 \, \text{Mf}$$

$$R_c = 143 \, \text{N}$$
,  $R_E = 143 \, \text{N}$ ,  $R_A = 8.2 \, \text{K}$ ,  $R_A = 6.15 \, \text{K}$ ,  $C_B = 556.5 \, \text{M}$ .



$$R_{in} = 50 \Omega$$

$$A_{v} = 20$$

Assume  $R_{E}$  doesn't affect  $R_{in}$  significantly,  $R_{in} \approx \frac{1}{5} = 50$  s.

$$A_{\nu} = \frac{R_{c}}{I/J_{m}} = 20 \implies R_{c} = IK\Omega, \quad \frac{1}{J_{m}} = \frac{V_{f}}{I_{c}} \Rightarrow I_{c} = \frac{26mV}{50\Omega} = 0.52$$

$$\frac{1}{J_{m}} = \frac{V_{f}}{I_{c}} \Rightarrow I_{c} = \frac{26mV}{50\Omega} = 0.52$$

 $V_{RE} = V_{T} \ln \left( \frac{I_{c}}{I_{c}} \right) = 0.715 V_{r} R_{E} I_{c} = 260 \text{ mV} \Rightarrow R_{E} = 500 \Omega$ 

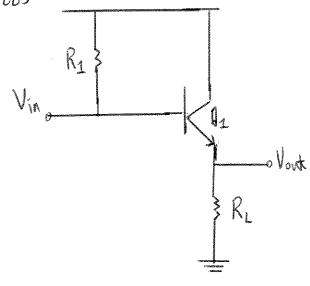
$$V_{cc} = I_c R_c + V_{cE} + I_c R_E = 0.52 + V_{cE} + 0.260$$

VBc is forward biased to 0.4V, VCE = VBE - 0.4 = 0.315 V Vcc = 0.52 + 0.315 + 0.260 = 1.1V. (Mirlimum Supply Voltage)

$$R_1 = \frac{1 \cdot 1 - (0.715 + 0.260)}{0.052} = 2.4 \text{ K}, R_2 = \frac{(0.715 + 0.260)}{(1)(0.0052)} = 20.83 \text{ K}$$

$$\frac{1}{C_{B}21/200} = \frac{1}{10}\frac{1}{J_{m}} = 5 \implies C_{B} = 159.2 \text{ Mf}$$

Vcc=1.1V, R1=2.4K, R2=20.83K, Rc=1K, RE=500D, CB=159.2Mf => Rin = 50 A. Av=20



$$A_V = \frac{R_L}{R_L + \frac{1}{J_m}} = 0.85 \Rightarrow \frac{200}{200 + \frac{1}{J_m}} = 0.85$$

$$\Rightarrow 200 = 0.85 (200 + \frac{1}{J_m}) \Rightarrow \frac{1}{J_m} = 35.294 \Omega$$

$$= \sum_{k=0}^{\infty} \frac{26 \, \text{mV}}{35 \cdot \lambda 94 \, \text{n}} = 0.737 \, \text{mA}, \quad V_{BE} = V_{T} \ln \left( \frac{0.737}{6 \times 10^{78}} \right) = 0.724 \, \text{V}$$

$$R_{in} = R_1 / (Y_{\pi} + (1+\beta)(200 \text{ n}))$$

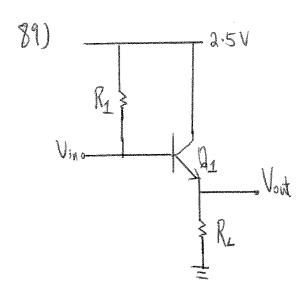
$$R_{1} = \frac{R_{1} 23.73K}{R_{1} + 23.73K} > 10K \Rightarrow R_{1} > 17.28K (Input Impedance Vequire ment)$$

To support an Ic of 0.737, Re must be determined.

$$R_1 = \frac{2.5 - (0.724 + (0.737)(0.2)/0.99)}{0.737/100}$$

$$R_1 = 220.77 \text{K} \Omega => R_{in} = 220.77 \text{K} \Omega // 23.73 \text{K} \Omega$$
  
 $R_{in} = 21.43 \text{K} \Omega > 10 \text{K} \Omega$ 

$$R_1 = 220.77 \text{K}\Omega = A_1 = 0.85$$
 $R_1 = 200 \Omega$ 
 $R_{in} = 21.43 \text{K}\Omega$ 



Power = 
$$5 \text{ mW}$$

$$A_{V} = 0.9$$

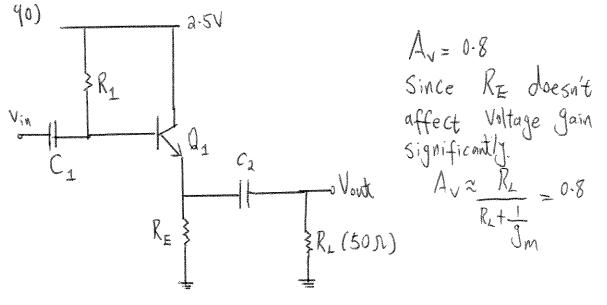
$$A_{N} = \frac{R_{L}}{R_{L} + \frac{1}{J_{m}}} = 0.9 \implies R_{L} = 0.9(R_{L} + \frac{1}{J_{m}})$$

$$R_{L} = 9 \frac{1}{J_{m}}$$

Power = 2.5 (I<sub>c</sub>+ I<sub>c</sub>) 
$$\Rightarrow$$
 I<sub>c</sub> = 1.98 m A  

$$\frac{1}{9m} = \frac{V_T}{I_c} = \frac{26mV}{1.98mA} = 13.13 \text{ J}$$

This is the minimum lood resistance, since anything lower Will lower the Voltage gain.



$$A_V = 0.8$$
  
Since  $R_E$  doesn't  
affect Voltage gain  
significantly.  
 $A_V \approx \frac{R_L}{R_L + \frac{1}{3}} = 0.8$ 

$$R_{L} = 0.8 (R_{L} + \frac{1}{J_{m}})$$

$$0.2R_{L} = 0.8 \frac{1}{J_{m}}$$

$$R_{L} = \frac{1}{J_{m}} = 0.8 \frac{1}{J_{m}}$$

$$R_{L} = \frac{1}{J_{m}} = \frac{12.5}{J_{m}} = \frac{1}{I_{c}}$$

$$I_{c} = \frac{26mV}{12.5N} = 2.08 \text{ mA}$$

$$V_{RE} = V_{f} \ln \left(\frac{I_{c}}{I_{c}}\right) = 0.751 \text{ V}$$

$$Let R_{E}I_{c} = 20 V_{f}, R_{E} = \frac{20}{J_{m}} = 250 \Omega$$

$$(0.52V)$$

$$R_1 = \frac{2.5 - (0.751 + 0.52)}{0.0208 \text{mA}} = 59.1 \text{ K}$$

$$\frac{1}{(2\pi)(100\times10^{6})C_{1}} = \frac{1}{10} \frac{1}{9m} \Rightarrow C_{1} = 1.27nf$$

$$\frac{1}{(2\pi)(100\times10^{6})C_{2}} = \frac{1}{10}50 \implies C_{2} = 0.32nf$$
(50 C2 Will Not Joad 11).

$$C_1 = 1.27 \text{ nf}$$
 $C_2 = 0.32 \text{ nf}$ 
 $R_1 = 591 \text{ K}_1$   $\Longrightarrow$   $A_v = 0.8$ 
 $R_{E} = 250 \text{ n}$ 
 $R_{E} = 50 \text{ n}$