

TÜRKİYE CUMHURİYETİ
KOCAELİ ÜNİVERSİTESİ
MÜHENDİSLİK FAKÜLTESİ
HARİTA MÜHENDİSLİĞİ



TASARIM PROJESİ ÖDEV I

GitHub ile ödevin dosyalarına [buradan](#) ulaşabilirsiniz.

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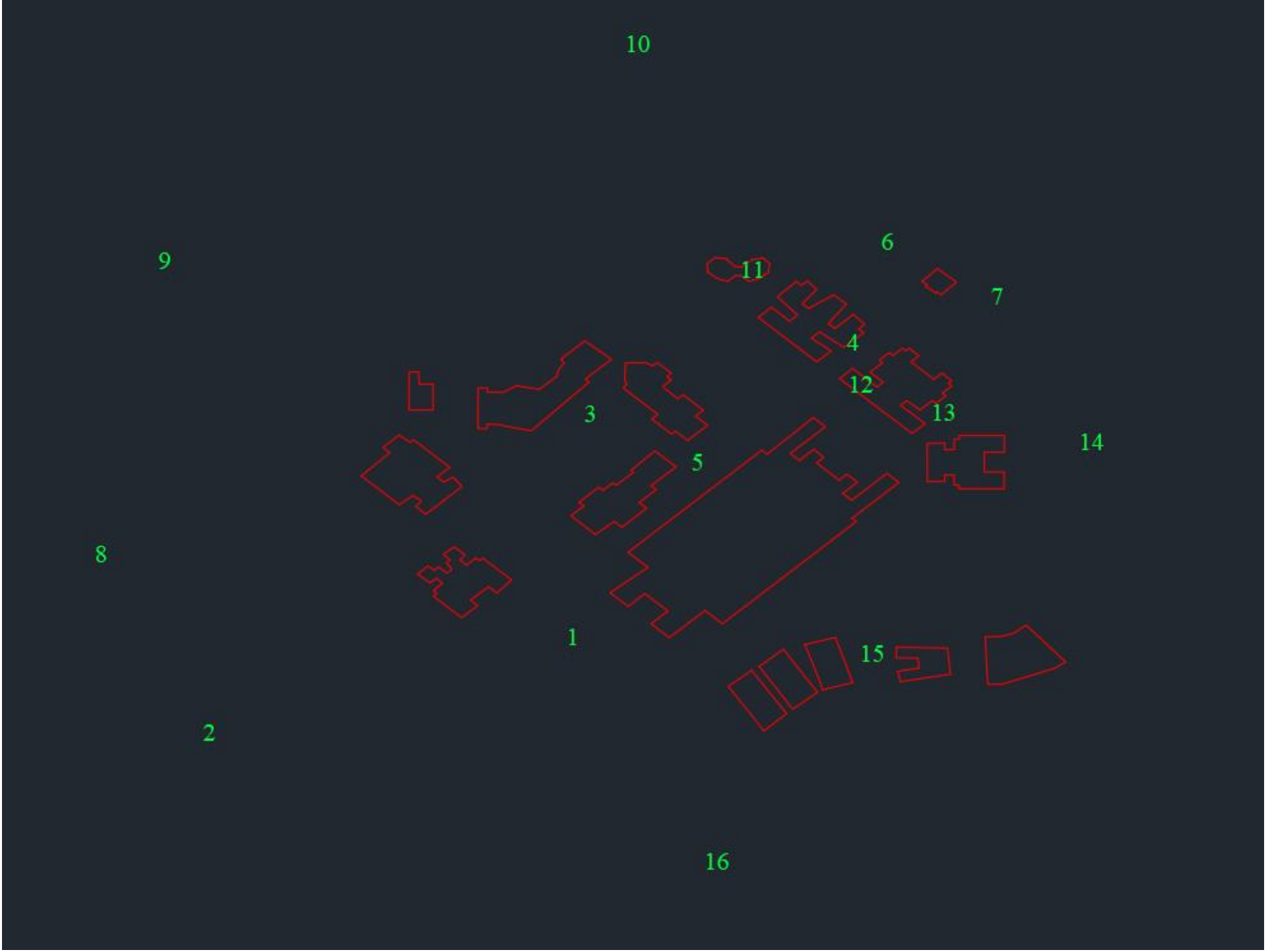
5- Çağatay Kırılı 180227030

6- Erkan Akça 180227047

Mayıs 2021, Kocaeli

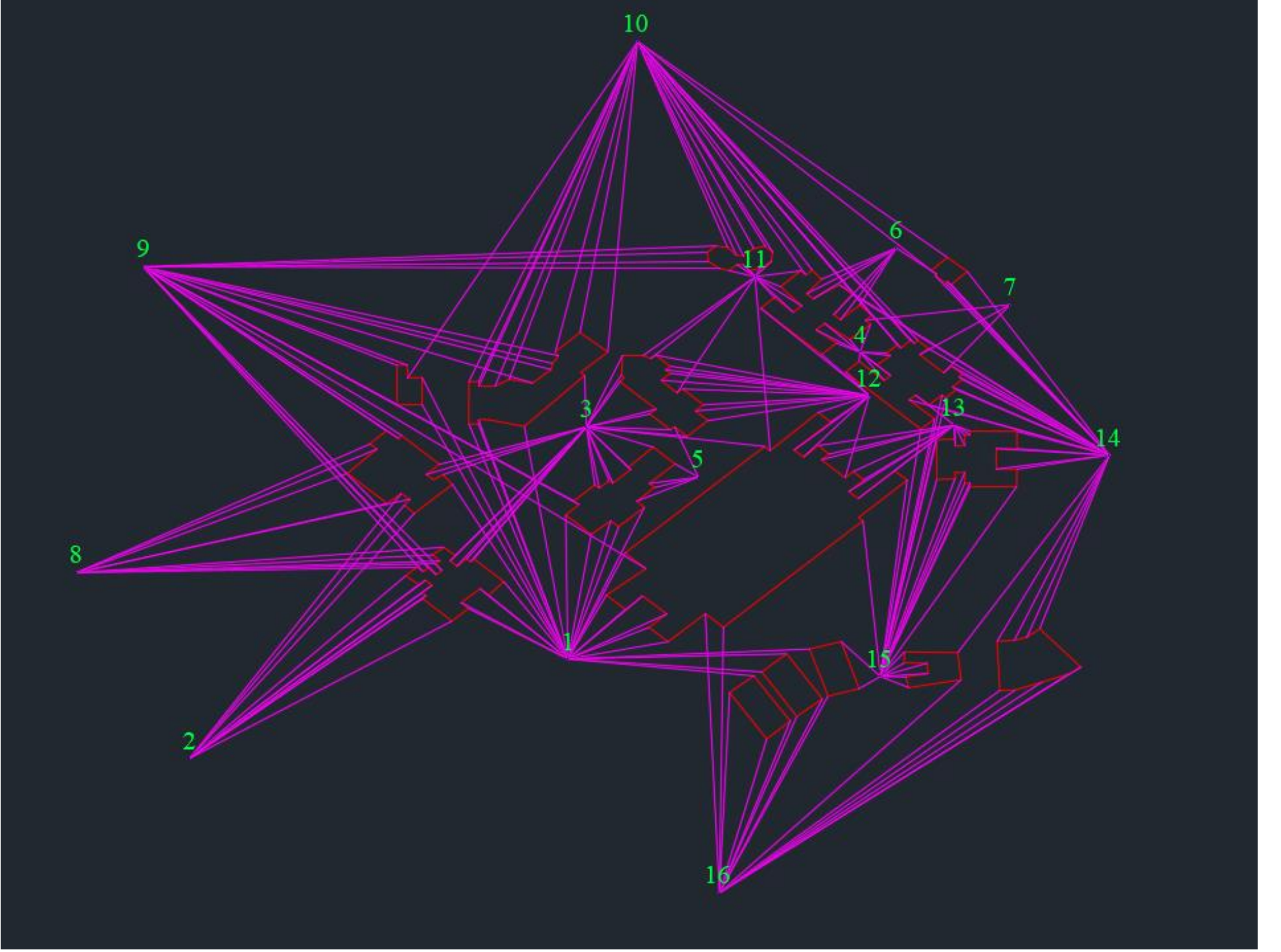
1-a)

Çalışmaya ilk olarak şekil-1’deki bina detaylarını Civil 3d programında çizerek işe başladık, Ardından tüm detay noktalarını görecektir şekilde bir poligon ağı tasarladık. Poligon ağı tasarlarken olabildiğince az nokta atmaya ve gereksiz, birbirine çok yakın noktalar atmamaya özen gösterdik.



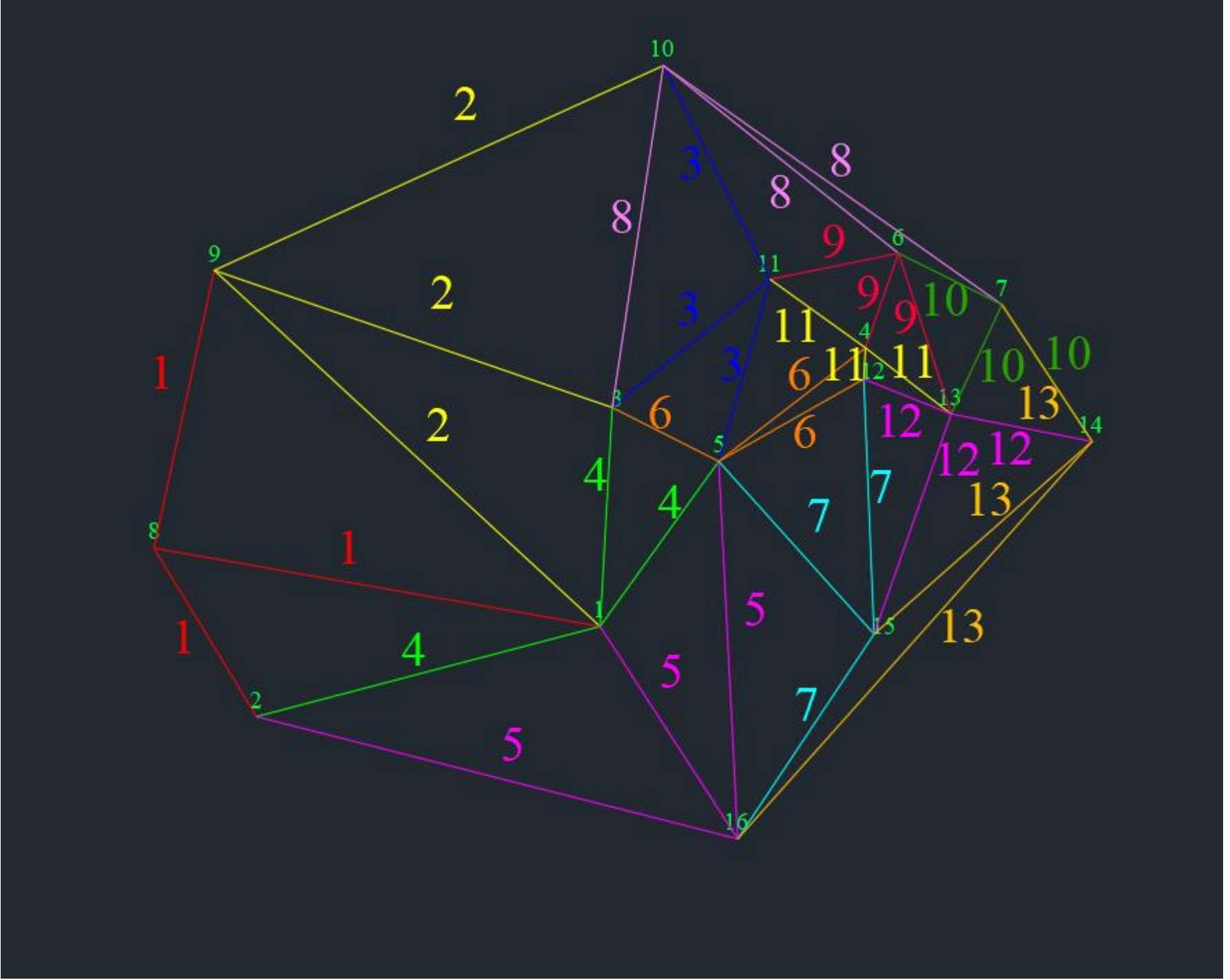
1-b)

Uygulamada poligon ağı tasarlama işleminin ardından poligon noktalarının bina köşelerini gördüğünü Civil 3D programı ile durum görüş krokisi oluşturarak kanıtladık.



1-c)

Tasarladığımız ağı uygun bir şekilde GNSS ölçü planı oluşturduk. (4 adet GNSS alıcımız var.)



Durulan 8 -> 9, 1, 2

Durulan 9 -> 10, 3, 1

Durulan 11 -> 5, 3, 10

Durulan 1 -> 2, 3, 5

Durulan 16 -> 2, 1, 5

Durulan 5 -> 3, 4, 12

Durulan 15 -> 16, 5, 12

Durulan 10 -> 7, 6, 3

Durulan 6 -> 13, 4, 11

Durulan 7 -> 14, 13, 6

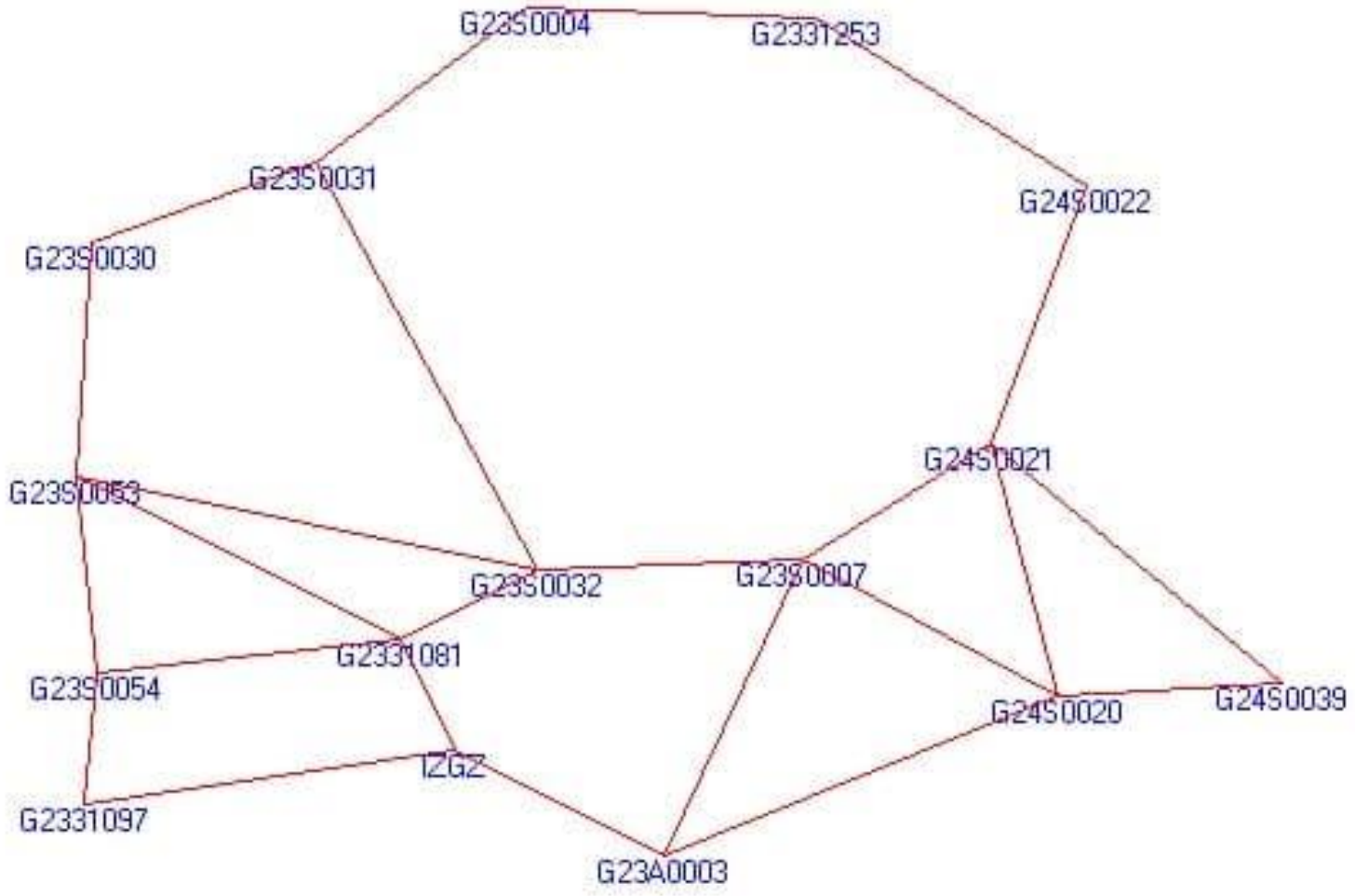
Durulan 4 -> 13, 12, 11

Durulan 13 -> 12, 14, 15

Durulan 14 -> 16, 15, 7

2-a)

1. soruda 16 nokta attığımızdan dolayı, IZDOGAP ağından 16 nokta seçerek ağ bir ağ oluşturduk. Seçtiğimiz noktaları NetCad Gis programında çizim yaparak ağıımızı görselleştirerek işe başladık.



Uygulamanın en başında coğrafi koordinatlardan kartezyen koordinatlara dönüşüm işlemi yaptık.

	A	B	C	D	E	F	G	H	I	J	K	L	M	N
1	COĞRAFİ KOORDİNATLAR [GRS80]													
2	Nokta No	Nokta Adı	Ø0	λ0	h [m]	H [m]		Ør	λr		N(m)	a(m)	e2	e'2
3	41	G2331081	40.798224	29.873423	405.4971	369.456		0.712063338	0.52138959		6387270.996	6378137	0.00669438	0.006739497
4	43	G2331097	40.743739	29.794323	36.8425	0.6469		0.711112395	0.520009035		6387250.829			
5	44	G2331253	40.982187	29.975213	286.6603	251.0183		0.715274098	0.523166161		6387339.13			
6	46	G23A0003	40.732093	29.941499	39.5141	3.5407		0.710909134	0.522577741		6387246.519			
7	51	G23S0004	40.985149	29.90182	401.452	365.5921		0.715325794	0.521885211		6387340.228			
8	52	G23S0007	40.82352	29.975195	301.7789	265.8313		0.712504836	0.523165847		6387280.361			
9	63	G23S0030	40.911933	29.792909	307.4099	271.3494		0.714047934	0.519984356		6387313.103			
10	64	G23S0031	40.937457	29.849182	351.7663	315.7638		0.714493412	0.520966505		6387322.558			
11	65	G23S0032	40.821244	29.907949	528.9837	492.9266		0.712465113	0.521992183		6387279.518			
12	75	G23S0053	40.844296	29.789868	427.6489	391.4413		0.712867446	0.51993128		6387288.053			
13	76	G23S0054	40.783893	29.7966	229.5995	193.3845		0.711813215	0.520048776		6387265.691			
14	86	G24S0020	40.782799	30.040476	141.4262	105.5062		0.711794121	0.524305215		6387265.286			
15	87	G24S0021	40.86023	30.022062	474.9719	439.1387		0.713145547	0.52398383		6387293.954			
16	88	G24S0022	40.935391	30.045051	303.5153	267.7433		0.714457354	0.524385064		6387321.792			
17	92	G24S0039	40.788228	30.097271	148.2174	112.3935		0.711888875	0.525296475		6387267.295			
18	105	IZGZ	40.76203	29.887933	49.1155	13.0769		0.711431633	0.521642837		6387257.598			
19														
20														
21	KARTEZYEN KOORDİNATLAR [GRS80]													
22	Nokta No	Nokta Adı	X(m)	Y(m)	Z(m)									
23	41	G2331081	4193056.61683	2408527.09372	4145751.05451									
24	43	G2331097	4199564.48559	2404560.70884	4140927.92639									
25	44	G2331253	4177108.09868	2409245.64855	4161118.03008									
26	46	G23A0003	4194107.13526	2415762.47153	4139949.74623									
27	51	G23S0004	4180078.88759	2403828.65578	4161441.64517									
28	52	G23S0007	4187113.38065	2415014.67796	4147809.53324									
29	63	G23S0030	4189203.75959	2398491.15119	4155238.45123									
30	64	G23S0031	4185264.58470	2401696.89144	4157409.28722									
31	65	G23S0032	4190237.18310	2410266.86825	4147766.78159									
32	75	G23S0053	4193676.32080	2400756.34091	4149637.57413									
33	76	G23S0054	4197068.96182	2403353.32126	4144431.19368									
34	86	G24S0020	4186812.14906	2421202.37022	4144281.60696									
35	87	G24S0021	4182941.49725	2417170.42456	4151007.06161									
36	88	G24S0022	4177128.38751	2416047.42492	4157204.33963									
37	92	G24S0039	4184073.76554	2425156.48130	4144742.53727									
38	105	IZGZ	4194488.74538	2410762.65062	4142474.64760									

$$\Phi r = \Phi 0 * \frac{pi}{180}$$

$$\lambda r = \lambda 0 * \frac{pi}{180}$$

$$N(m) = \frac{a}{\sqrt{1 - e^2 * (\sin \Phi r)^2}}$$

$$X = (N + h) * (\cos \Phi r) * (\cos \lambda r)$$

$$Y = (N + h) * (\cos \Phi r) * (\sin \lambda r)$$

$$Z = \left(\frac{N}{1 + e'^2 + h}\right) * \sin \Phi r$$

Bize verilen EK_1 ve EK_2 bilgilerinden çalışmada kullanacağımız verileri çektik

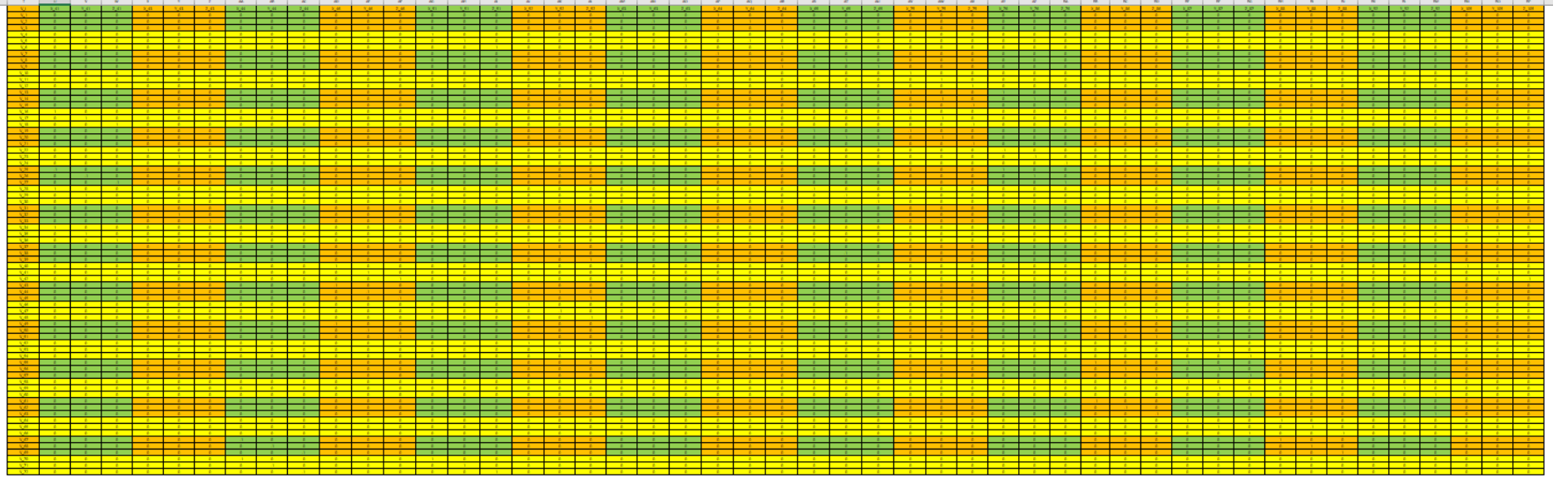
	A	B	C	D	E	F	G	H	I	J	K	L	M	N	O	P
1	KARTEZYEN KOORDİNATLAR [GRS80]						Noktalar arası baz vektörleri, standart sapma ve korelasyon değerleri									
2	Nokta No	Nokta Adı	X(m)	Y(m)	Z(m)		Baz (DN-BN)	dx [m]	dy [m]	dz [m]	sigma _x [m]	sigma _y [m]	sigma _z [m]	corr _{XY}	corr _{XZ}	corr _{YZ}
3	41	G2331081	4193056.61683	2408527.09372	4145751.05451	63-64	G23S0030-G23S0031	-3939.1327	3205.7534	2170.7706	0.003	0.002	0.003	0.5	0.65	0.06
4	43	G2331097	4199564.48559	2404560.70884	4140927.92639	64-51	G23S0031-G23S0004	-5185.7415	2131.7103	4032.4205	0.004	0.003	0.004	0.52	0.49	0.64
5	44	G2331253	4177108.09868	2409245.64855	4161118.03008	64-65	G23S0031-G23S0032	4972.5996	8569.9617	-9642.4821	0.007	0.005	0.007	0.52	0.67	0.11
6	46	G23A0003	4194107.13526	2415762.47153	4139949.74623	63-75	G23S0030-G23S0053	4472.6332	2265.152	-5600.9311	0.004	0.002	0.004	0.4	0.65	-0.04
7	51	G23S0004	4180078.88759	2403828.65578	4161441.64517	75-76	G23S0053-G23S0054	3392.6228	2596.9818	-5206.3477	0.004	0.003	0.004	0.78	0.84	0.71
8	52	G23S0007	4187113.38065	2415014.67796	4147809.53324	75-41	G23S0053-G2331081	-619.7746	7770.7473	-3886.4651	0.006	0.004	0.006	0.77	0.9	0.75
9	63	G23S0030	4189203.75959	2398491.15119	4155238.45123	75-65	G23S0053-G23S0032	-3439.1815	9510.5594	-1870.7795	0.006	0.004	0.006	0.75	0.87	0.75
10	64	G23S0031	4185264.58470	2401696.89144	4157409.28722	76-43	G23S0054-G2331097	2495.5009	1207.4084	-3503.2524	0.002	0.002	0.002	0.72	0.82	0.49
11	65	G23S0032	4190237.18310	2410266.86825	4147766.78159	41-76	G2331081-G23S0054	4012.3689	-5173.7761	-1319.9004	0.004	0.003	0.003	0.75	0.83	0.55
12	75	G23S0053	4193676.32080	2400756.34091	4149637.57413	65-41	G23S0032-G2331081	2819.422	-1739.8003	-2015.6997	0.003	0.002	0.003	0.59	0.72	0.23
13	76	G23S0054	4197068.96182	2403353.32126	4144431.19368	105-43	IZGZ-G2331097	5075.703	-6201.9855	-1546.6628	0.004	0.003	0.004	0.76	0.79	0.48
14	86	G24S0020	4186812.14906	2421202.37022	4144281.60696	105-41	IZGZ-G2331081	-1432.1702	-2235.6151	3276.4847	0.002	0.002	0.002	0.66	0.78	0.37
15	87	G24S0021	4182941.49725	2417170.42456	4151007.06161	65-52	G23S0032-G23S0007	-3123.7484	4747.8031	42.6965	0.006	0.004	0.005	0.85	0.84	0.73
16	88	G24S0022	4177128.38751	2416047.42492	4157204.33963	105-46	IZGZ-G23A0003	-381.6609	4999.7902	-2524.8337	0.003	0.002	0.003	0.66	0.73	0.41
17	92	G24S0039	4184073.76554	2425156.48130	4144742.53727	46-52	G23A0003-G23S0007	-6993.6805	-747.797	7859.7283	0.009	0.007	0.008	0.87	0.83	0.76
18	105	IZGZ	4194488.74538	2410762.65062	4142474.64760	52-86	G23S0007-G24S0020	-301.3012	6187.6865	-3527.8693	0.004	0.002	0.004	0.6	0.61	0.3
19						46-86	G23A0003-G24S0020	-7284.9811	5439.885	4331.8835	0.009	0.004	0.008	0.59	0.73	0.29
20						87-52	G24S0021-G23S0007	4171.9319	-2155.7224	-3197.6071	0.003	0.003	0.002	0.77	0.88	0.56
21						87-86	G24S0021-G24S0020	3870.6402	4031.9636	-6725.4678	0.004	0.003	0.004	0.56	0.59	0.46
22						87-92	G24S0021-G24S0039	1132.3057	7986.1178	-6264.5775	0.006	0.005	0.005	0.62	0.66	0.47
23						86-92	G24S0020-G24S0039	-2738.3426	3954.1355	460.8897	0.003	0.002	0.003	0.43	0.75	0.15
24						88-87	G24S0022-G24S0021	5813.0467	1122.9059	-6197.2178	0.005	0.003	0.005	0.66	0.55	0.4
25						44-88	G2331253-G24S0022	20.2528	6801.8252	-3913.6905	0.004	0.002	0.004	0.72	0.71	0.46
26						44-51	G2331253-G23S0004	2970.7275	-5416.9977	323.6836	0.004	0.003	0.003	0.65	0.75	0.42

Sırasıyla K_{11} , O_{11} , P_{11} ve I matrislerini hesapladık

$$K_{ll} = \begin{bmatrix} \sigma_x^2 & r_{xy}\sigma_x\sigma_y & r_{xz}\sigma_x\sigma_z \\ r_{yx}\sigma_y\sigma_x & \sigma_y^2 & r_{yz}\sigma_y\sigma_z \\ r_{zx}\sigma_z\sigma_x & r_{zy}\sigma_z\sigma_y & \sigma_z^2 \end{bmatrix} \quad \begin{aligned} lx_{DN,BN} &= [\Delta X_{DN,BN} - (X_{BN} - X_{DN})] * 100 \\ ly_{DN,BN} &= [\Delta Y_{DN,BN} - (Y_{BN} - Y_{DN})] * 100 \\ lz_{DN,BN} &= [\Delta Z_{DN,BN} - (Z_{BN} - Z_{DN})] * 100 \end{aligned}$$

[illegible]

Daha sonra 16 nokta için $16 \times 3 = 48$ sütunlu 24 baz gözlemi için $24 \times 3 = 72$ satırlı bir A katsayılar matrisi oluşturduk



G dönüşüm matrisi köşegen elemanları $1/p$ (p =nokta sayısı) olacak şekilde $16 \times 3 = 48$ satır ve 3 sütun şeklinde oluşmuştur. Her bir gözlem için elde edilen P_{ll} matrisleri köşegen şeklinde yazılarak tüm ağ için P_{ll} ağırlık matrisi elde edilir. Burada 24 gözlem için 72×72 boyutunda bir matris kare matris oluşmuştur.

107	P(nokta sayısı) =	16		
108				
109		0.25	0	0
110		0	0.25	0
111		0	0	0.25
112		0.25	0	0
113		0	0.25	0
114		0	0	0.25
115		0.25	0	0
116		0	0.25	0
117		0	0	0.25
118		0.25	0	0
119		0	0.25	0
120		0	0	0.25
121		0.25	0	0
122		0	0.25	0
123		0	0	0.25
124		0.25	0	0
125		0	0.25	0
126		0	0	0.25
127	G	0.25	0	0
128		0	0.25	0
129		0	0	0.25
130		0.25	0	0
131		0	0.25	0
132		0	0	0.25
133		0.25	0	0
134		0	0.25	0
135		0	0	0.25
136		0.25	0	0
137		0	0.25	0
138		0	0	0.25
139		0.25	0	0
140		0	0.25	0
141		0	0	0.25
142		0.25	0	0
143		0	0.25	0
144		0	0	0.25
145		0.25	0	0
146		0	0.25	0
147		0	0	0.25
148		0.25	0	0
149		0	0.25	0
150		0	0	0.25
151		0.25	0	0
152		0	0.25	0
153		0	0	0.25
154		0.25	0	0
155		0	0.25	0
156		0	0	0.25

A large grid of graph paper. A thick horizontal line runs across the middle of the page, and a thick vertical line runs down the left side, creating a header area and a left margin. The rest of the page is filled with a standard grid of small squares.

Burada N matrisinin MoorePenrose tersi alınarak Q_xx matrisine ulaşılır.

$$N = A^T P_{ll} A$$

$$Q_{xx} = N^+ = (N + GG^T)^{-1} - GG^T$$

0	1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19	20	21	22	23	24	25	26	27	28	29	30	31	32	33	34	35	36	37	38	39	40	41	42	43	44	45	46	47	48	49	50	51	52	53	54	55	56	57	58	59	60	61	62	63	64	65	66	67	68	69	70	71	72	73	74	75	76	77	78	79	80	81	82	83	84	85	86	87	88	89	90	91	92	93	94	95	96	97	98	99	100	101	102	103	104	105	106	107	108	109	110	111	112	113	114	115	116	117	118	119	120	121	122	123	124	125	126	127	128	129	130	131	132	133	134	135	136	137	138	139	140	141	142	143	144	145	146	147	148	149	150	151	152	153	154	155	156	157	158	159	160	161	162	163	164	165	166	167	168	169	170	171	172	173	174	175	176	177	178	179	180	181	182	183	184	185	186	187	188	189	190	191	192	193	194	195	196	197	198	199	200	201	202	203	204	205	206	207	208	209	210	211	212	213	214	215	216	217	218	219	220	221	222	223	224	225	226	227	228	229	230	231	232	233	234	235	236	237	238	239	240	241	242	243	244	245	246	247	248	249	250	251	252	253	254	255	256	257	258	259	260	261	262	263	264	265	266	267	268	269	270	271	272	273	274	275	276	277	278	279	280	281	282	283	284	285	286	287	288	289	290	291	292	293	294	295	296	297	298	299	300	301	302	303	304	305	306	307	308	309	310	311	312	313	314	315	316	317	318	319	320	321	322	323	324	325	326	327	328	329	330	331	332	333	334	335	336	337	338	339	340	341	342	343	344	345	346	347	348	349	350	351	352	353	354	355	356	357	358	359	360	361	362	363	364	365	366	367	368	369	370	371	372	373	374	375	376	377	378	379	380	381	382	383	384	385	386	387	388	389	390	391	392	393	394	395	396	397	398	399	400	401	402	403	404	405	406	407	408	409	410	411	412	413	414	415	416	417	418	419	420	421	422	423	424	425	426	427	428	429	430	431	432	433	434	435	436	437	438	439	440	441	442	443	444	445	446	447	448	449	450	451	452	453	454	455	456	457	458	459	460	461	462	463	464	465	466	467	468	469	470	471	472	473	474	475	476	477	478	479	480	481	482	483	484	485	486	487	488	489	490	491	492	493	494	495	496	497	498	499	500	501	502	503	504	505	506	507	508	509	510	511	512	513	514	515	516	517	518	519	520	521	522	523	524	525	526	527	528	529	530	531	532	533	534	535	536	537	538	539	540	541	542	543	544	545	546	547	548	549	550	551	552	553	554	555	556	557	558	559	560	561	562	563	564	565	566	567	568	569	570	571	572	573	574	575	576	577	578	579	580	581	582	583	584	585	586	587	588	589	590	591	592	593	594	595	596	597	598	599	600	601	602	603	604	605	606	607	608	609	610	611	612	613	614	615	616	617	618	619	620	621	622	623	624	625	626	627	628	629	630	631	632	633	634	635	636	637	638	639	640	641	642	643	644	645	646	647	648	649	650	651	652	653	654	655	656	657	658	659	660	661	662	663	664	665	666	667	668	669	670	671	672	673	674	675	676	677	678	679	680	681	682	683	684	685	686	687	688	689	690	691	692	693	694	695	696	697	698	699	700	701	702	703	704	705	706	707	708	709	710	711	712	713	714	715	716	717	718	719	720	721	722	723	724	725	726	727	728	729	730	731	732	733	734	735	736	737	738	739	740	741	742	743	744	745	746	747	748	749	750	751	752	753	754	755	756	757	758	759	760	761	762	763	764	765	766	767	768	769	770	771	772	773	774	775	776	777	778	779	780	781	782	783	784	785	786	787	788	789	790	791	792	793	794	795	796	797	798	799	800	801	802	803	804	805	806	807	808	809	810	811	812	813	814	815	816	817	818	819	820	821	822	823	824	825	826	827	828	829	830	831	832	833	834	835	836	837	838	839	840	841	842	843	844	845	846	847	848	849	850	851	852	853	854	855	856	857	858	859	860	861	862	863	864	865	866	867	868	869	870	871	872	873	874	875	876	877	878	879	880	881	882	883	884	885	886	887	888	889	890	891	892	893	894	895	896	897	898	899	900	901	902	903	904	905	906	907	908	909	910	911	912	913	914	915	916	917	918	919	920	921	922	923	924	925	926	927	928	929	930	931	932	933	934	935	936	937	938	939	940	941	942	943	944	945	946	947	948	949	950	951	952	953	954	955	956	957	958	959	960	961	962	963	964	965	966	967	968	969	970	971	972	973	974	975	976	977	978	979	980	981	982	983	984	985	986	987	988	989	990	991	992	993	994	995	996	997	998	999	1000	1001	1002	1003	1004	1005	1006	1007	1008	1009	1010	1011	1012	1013	1014	1015	1016	1017	1018	1019	1020	1021	1022	1023	1024	1025	1026	1027	1028	1029	1030	1031	1032	1033	1034	1035	1036	1037	1038	1039	1040	1041	1042	1043	1044	1045	1046	1047	1048	1049	1050	1051	1052	1053	1054	1055	1056	1057	1058	1059	1060	1061	1062	1063	1064	1065	1066	1067	1068	1069	1070	1071	1072	1073	1074	1075	1076	1077	1078	1079	1080	1081	1082	1083	1084	1085	1086	1087	1088	1089	1090	1091	1092	1093	1094	1095	1096	1097	1098	1099	1100	1101	1102	1103	1104	1105	1106	1107	1108	1109	1110	1111	1112	1113	1114	1115	1116	1117	1118	1119	1120	1121	1122	1123	1124	1125	1126	1127	1128	1129	1130	1131	1132	1133	1134	1135	1136	1137	1138	1139	1140	1141	1142	1143	1144	1145	1146	1147	1148	1149	1150	1151	1152	1153	1154	1155	1156	1157	1158	1159	1160	1161	1162	1163	1164	1165	1166	1167	1168	1169	1170	1171	1172	1173	1174	1175	1176	1177	1178	1179	1180	1181	1182	1183	1184	1185	1186	1187	1188	1189	1190	1191	1192	1193	1194	1195	1196	1197	1198	1199	1200	1201	1202	1203	1204	1205	1206	1207	1208	1209	1210	1211	1212	1213	1214	1215	1216	1217	1218	1219	1220	1221	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[illegible]

Ardından X ve m_0 değerlerini hesaplayıp test büyüklüğü ve sınır değerlerini hesapladık

$$v = Ax - l$$

$$m_0 = \sqrt{\frac{V^T P_{ll} V}{n - u}}$$

Test büyüklüğü tablo değerinden büyük ($T > q$), dengeleme modeli geçersizdir. Bu durum, ölçülerde kaba hata olması ya da fonksiyonel ve stokastik modellerin yanlış kurulması gibi nedenlerden kaynaklanabilir. Bu durumda uyuşumsuz ölçüler testi ile uyuşumsuz ölçülerin ayıklanması gerekmektedir. Test sonucunda uyuşumsuz ölçülerden arınmış ölçülerle yeni bir dengeleme işlemi yapılır ve model hipotezi testi yenilenir.

Uyuşumsuz Ölçüler Testi, Q_{vv} düzeltmeleri ters ağırlık matris değerlerini hesapladık

$$Q_{vv} = Q_{ll} - A Q_{xx} A^T$$

$$Q_{ll} = P_{ll}^{-1}$$

σ_0^2 Bilinmiyorsa (Tau-Dağılımı, Pope Testi)

$$T_i = \frac{|\underline{e}_i^T \underline{P} \underline{v}|}{m_0 \sqrt{\underline{e}_i^T \underline{P} \underline{Q}_{vv} \underline{P} \underline{e}_i}} = \frac{|(\underline{P} \underline{v})_i|}{m_0 \sqrt{(\underline{P} \underline{Q}_{vv} \underline{P})_{ii}}} \sim \tau_f \quad \text{Test büyüklüğü}$$

$$q = \tau(f, \alpha_0)$$

Sınır değeri

$$\tau_{(f, \alpha_0)} = \sqrt{\frac{f t_{(f-1, \alpha_0)}^2}{f-1 + t_{(f-1, \alpha_0)}^2}} \quad t_{(f-1, \alpha_0)}^2 = F_{(1, f-1, 2 \alpha_0)}$$

2-b)

Sonuç Denetimleri				
DN-BN	delta X,Y,Z	v = A * x - l (cm)	l.i + v.i (m)	X_BN - X_DN
	-3939.1327	0.154105045	-3939.131159	-3939.131159
63-64	3205.7534	0.197231838	3205.755372	3205.755372
	2170.7706	0.129823332	2170.771898	2170.771898
	-5185.7415	1.146434218	-5185.730036	-5185.730036
64-51	2131.7103	0.417407822	2131.714474	2131.714474
	4032.4205	-0.032406617	4032.420176	4032.420176
	4972.5996	-1.927871494	4972.580321	4972.580321
64-65	8569.9617	-1.077992696	8569.95092	8569.95092
	-9642.4821	0.936130683	-9642.472739	-9642.472739
	4472.6332	-0.142467913	4472.631775	4472.631775
63-75	2265.152	-0.176651885	2265.150233	2265.150233
	-5600.9311	-0.17162356	-5600.932816	-5600.932816
	3392.6228	-1.022439513	3392.612576	3392.612576
75-76	2596.9818	-0.525189153	2596.976548	2596.976548
	-5206.3477	-1.080386738	-5206.358504	-5206.358504
	-619.7746	1.228436613	-619.7623156	-619.7623156
75-41	7770.7473	0.463481619	7770.751935	7770.751935
	-3886.4651	0.145679464	-3886.463643	-3886.463643
	-3439.1815	-0.111298536	-3439.182613	-3439.182613
75-65	9510.5594	-0.334108973	9510.556059	9510.556059
	-1870.7795	1.147577575	-1870.768024	-1870.768024
	2495.5009	-0.082391719	2495.500076	2495.500076
76-43	1207.4084	-0.114619483	1207.407254	1207.407254
	-3503.2524	-0.056496509	-3503.252965	-3503.252965
	4012.3689	0.599123874	4012.374891	4012.374891
41-76	-5173.7761	0.071329227	-5173.775387	-5173.775387
	-1319.9004	0.553933798	-1319.894861	-1319.894861
	2819.422	-0.170264851	2819.420297	2819.420297
65-41	-1739.8003	-0.382409408	-1739.804124	-1739.804124
	-2015.6997	0.40810189	-2015.695619	-2015.695619
	5075.703	0.260304488	5075.705603	5075.705603
105-43	-6201.9855	0.257252417	-6201.982927	-6201.982927
	-1546.6628	0.166325054	-1546.661137	-1546.661137
	-1432.1702	0.083572333	-1432.169364	-1432.169364
105-41	-2235.6151	0.030542673	-2235.614795	-2235.614795
	3276.4847	0.198887766	3276.486689	3276.486689
	-3123.7484	-1.318657837	-3123.761587	-3123.761587
65-52	4747.8031	-0.697162008	4747.796128	4747.796128
	42.6965	0.214862154	42.69864862	42.69864862
	-381.6609	-0.236094158	-381.6632609	-381.6632609
105-46	4999.7902	-0.15741936	4999.788626	4999.788626
	-2524.8337	-0.534013423	-2524.83904	-2524.83904
	-6993.6805	-0.748726495	-6993.687987	-6993.687987
46-52	-747.797	-0.616790567	-747.8031679	-747.8031679
	7859.7283	-0.830338547	7859.719997	7859.719997
	-301.3012	0.28825189	-301.2983175	-301.2983175
52-86	6187.6865	0.021937778	6187.686719	6187.686719
	-3527.8693	0.794003298	-3527.86136	-3527.86136
	-7294.9811	-0.520474606	-7294.986305	-7294.986305
46-86	5439.885	-0.144852789	5439.883551	5439.883551
	4331.8835	-2.486335248	4331.858637	4331.858637
	4171.9319	0.75054149	4171.939405	4171.939405
87-52	-2155.7224	0.538710015	-2155.717013	-2155.717013
	-3197.6071	0.165824366	-3197.605442	-3197.605442
	3870.6402	0.08879338	3870.641088	3870.641088
87-86	4031.9636	0.610647793	4031.969706	4031.969706
	-6725.4678	0.099827665	-6725.466802	-6725.466802
	1132.3057	-0.694487888	1132.298755	1132.298755
87-92	7986.1178	-1.066728396	7986.107133	7986.107133
	-6264.5775	-0.091910969	-6264.578419	-6264.578419
	-2738.3426	0.026718732	-2738.342333	-2738.342333
86-92	3954.1355	0.192623811	3954.137426	3954.137426
	460.8897	-0.131738633	460.8883826	460.8883826
	5813.0467	1.700855963	5813.063709	5813.063709
88-87	1122.9059	0.845033433	1122.91435	1122.91435
	-6197.2178	-0.164476945	-6197.219445	-6197.219445
	20.2528	0.900242326	20.26180242	20.26180242
44-88	6801.8252	0.429044626	6801.82949	6801.82949
	-3913.6905	0.111662471	-3913.689383	-3913.689383
	2970.7275	-1.135396672	2970.716146	2970.716146
44-51	-5416.9977	-0.804649401	-5417.005746	-5417.005746
	323.6836	-0.360389562	323.6799961	323.6799961

589		YAKLAŞIK KOORDİNATLAR KÜMESİ			DENGELİ KOORDİNATLAR			$K = N_{+} \cdot A_{-T} \cdot P_{-II} \cdot I \text{ (cm)}$	
590	Nokta No	X(m)	Y(m)	Z(m)	X(m)	Y(m)	Z(m)	-2.117716865	Nokta No
591	41	4193056.61683	2408527.09372	4145751.05451	4193056.596	2408527.071	4145751.093	-2.308099137	41
592	43	4199564.48559	2404560.70884	4140927.92639	4199564.471	2404560.703	4140927.945	3.81877992	43
593	44	4177108.09868	2409245.64855	4161118.03008	4177108.149	2409245.644	4161118.001	-1.496984662	44
594	46	4194107.13526	2415762.47153	4139949.74623	4194107.102	2415762.474	4139949.767	-0.633389413	46
595	51	4180078.88759	2403828.65578	4161441.64517	4180078.865	2403828.638	4161441.681	1.84821721	51
596	52	4187113.38065	2415014.67796	4147809.53324	4187113.414	2415014.671	4147809.487	5.017250406	52
597	63	4189203.75959	2398491.15119	4155238.45123	4189203.726	2398491.168	4155238.489	-0.448639838	63
598	64	4185264.58470	2401696.89144	4157409.28722	4185264.595	2401696.924	4157409.261	-2.884469684	64
599	65	4190237.18310	2410266.86825	4147766.78159	4190237.175	2410266.875	4147766.788	-3.350383327	65
600	75	4193676.32080	2400756.34091	4149637.57413	4193676.358	2400756.319	4149637.556	0.252938786	75
601	76	4197068.96182	2403353.32126	4144431.19368	4197068.971	2403353.295	4144431.198	2.073878731	76
602	86	4186812.14906	2421202.37022	4144281.60696	4186812.115	2421202.358	4144281.626	-2.259146278	86
603	87	4182941.49725	2417170.42456	4151007.06161	4182941.474	2417170.388	4151007.092	-1.746289249	87
604	88	4177128.38751	2416047.42492	4157204.33963	4177128.411	2416047.474	4157204.312	3.606140755	88
605	92	4184073.76554	2425156.48130	4144742.53727	4184073.773	2425156.495	4144742.514	3.311890149	92
606	105	4194488.74538	2410762.65062	4142474.64760	4194488.765	2410762.685	4142474.606	-0.70685176	105
607								-4.627459778	
608					STANDART SAPMA			-3.339685538	
609					6874.675652	7760.674404	7043.632787	1.728071094	
610								3.792724055	
611								1.033419498	
612								3.240302952	
613								-2.616452618	
614								-0.774451998	
615								0.651310266	
616								0.672678067	
617								3.716846553	
618								-2.220580759	
619								-1.778899536	
620								0.872407042	
621								-2.600769944	
622								0.415713732	
623								-3.360857963	
624								-1.260913974	
625								1.864543499	
626								-2.288651325	
627								-3.665561794	
628								3.079715814	
629								2.314492734	
630								4.863404779	
631								-2.777807203	
632								0.757860784	
633								1.373709819	
634								-2.328195154	
635								1.963710799	
636								3.48135817	
637								-4.159107809	

Uygulamanın son kısmında sonuç denetimleri, dengeli koordinatlar ve dengeli koordinatların standart sapma değerini hesapladık.

3-a)

Çalışmaya ilk olarak matris kondisyonunu artırmak için verilen koordinatları indirgeyerek başladık. Daha sonra $N = h - H$ formülünden geoit yüksekliği değerlerimizi hesapladık.

	A	B	C	D	E	F	G	H	I	J	K	L
1	KARTEZYEN KOORDİNATLAR [GRS80]											
2	Nokta No	Nokta Adı	X(m)	Y(m)	Z(m)	h [m]	H [m]	N = h - H (m)	X(m)	Y(m)	x_0	4188245.24746
3	41	G2331081	-4811.36937	1588.10510	4145751.05451	405.4971	369.456	36.0411	4193056.61683	2408527.09372	y_0	2410115.19882
4	43	G2331097	-11319.23813	5554.48998	4140927.92639	36.8425	0.6469	36.1956	4199564.48559	2404560.70884		
5	44	G2331253	11137.14878	869.55027	4161118.03008	286.6603	251.0183	35.642	4177108.09868	2409245.64855		
6	46	G23A0003	-5861.88780	-5647.27271	4139949.74623	39.5141	3.5407	35.9734	4194107.13526	2415762.47153		
7	51	G23S0004	8166.35987	6286.54304	4161441.64517	401.452	365.5921	35.8599	4180078.88759	2403828.65578		
8	52	G23S0007	1131.86681	-4899.47914	4147809.53324	301.7789	265.8313	35.9476	4187113.38065	2415014.67796		
9	63	G23S0030	-958.51213	11624.04763	4155238.45123	307.4099	271.3494	36.0605	4189203.75959	2398491.15119		
10	64	G23S0031	2980.66276	8418.30738	4157409.28722	351.7663	315.7638	36.0025	4185264.58470	2401696.89144		
11	65	G23S0032	-1991.93564	-151.66943	4147766.78159	528.9837	492.9266	36.0571	4190237.18310	2410266.86825		
12	75	G23S0053	-5431.07334	9358.85791	4149637.57413	427.6489	391.4413	36.2076	4193676.32080	2400756.34091		
13	76	G23S0054	-8823.71436	6761.87756	4144431.19368	229.5995	193.3845	36.215	4197068.96182	2403353.32126		
14	86	G24S0020	1433.09840	-11087.17140	4144281.60696	141.4262	105.5062	35.92	4186812.14906	2421202.37022		
15	87	G24S0021	5303.75021	-7055.22574	4151007.06161	474.9719	439.1387	35.8332	4182941.49725	2417170.42456		
16	88	G24S0022	11116.85995	-5932.22610	4157204.33963	303.5153	267.7433	35.772	4177128.38751	2416047.42492		
17	92	G24S0039	4171.48192	-15041.28248	4144742.53727	148.2174	112.3935	35.8239	4184073.76554	2425156.48130		
18	105	IZGZ	-6243.49792	-647.45180	4142474.64760	49.1155	13.0769	36.0386	4194488.74538	2410762.65062		

3. derece bir yüzey polinomu oluşturduk ve bu polinoma bağlı olarak A katsayılar matrisimizi oluşturduk.

Daha sonra X matrisinin hesabı için n ve Qxx matrislerini oluşturduk. Ardından v düzeltmeler matrisimizi hesapladık.

$$\underline{n} = \underline{A}^T \underline{l}$$

$$Q_{xx} = N^{-1} = (\underline{A}^T \underline{A})^{-1}$$

$$\underline{X} = \underline{N}^{-1} \underline{n}$$

$$\underline{v} = \underline{A} \underline{X} - \underline{l}$$

19	n=3 için ;											
20	N(x,y)=a_0+a_1y+a_2x+a_3x^2+a_4xy+a_5y^2+a_6x^3+a_4x^2y+a_8xy^2+a_9y^3											
21												
22												
23	Nokta No	a_0	a_1y	a_2x	a_3x^2	a_4xy	a_5y^2	a_6x^3	a_7x^2y	a_8xy^2	a_9y^3	L (m)
24	41	1.0000	1588.1051	-4811.3694	23149275.2206	-7640960.2144	2522077.7948	-111379713748.5000	36763481937.8493	-12134647851.9997	4005324597.4082	36.0411
25	43	1.0000	5554.4900	-11319.2381	128125151.8578	-62872594.7283	30852358.8893	-1450279104400.6400	711669871619.5020	-349225197159.7070	171369118175.1220	36.1956
26	44	1.0000	869.5503	11137.1488	124036082.9339	9684310.6794	756117.6644	1381408309646.3000	107855608862.3110	8420994923.6793	657482315.9652	35.642
27	46	1.0000	-5647.2727	-5861.8878	34361728.5871	33103679.0312	31891689.1105	-201424597613.1620	-194050052268.7560	-186945503338.2990	-180101065729.2000	35.9734
28	51	1.0000	6286.5430	8166.3599	66689433.5161	51338172.7632	39520623.3388	544609913577.6170	419245993820.6950	322739632446.3930	248448099413.8750	35.8599
29	52	1.0000	-4899.4791	1131.8668	1281122.4742	-5545557.8267	24004895.8862	1450060007.2519	-6276832843.5614	27170344916.0544	-117611486757.1500	35.9476
30	63	1.0000	11624.0476	-958.5121	918745.5046	-11141790.6561	135118483.2028	-880628711.0724	10679541500.7709	-129512705221.4810	1570623683851.5500	36.0605
31	64	1.0000	8418.3074	2980.6628	8884350.4851	25092135.2915	70867899.0705	26481252632.2551	74791193216.5821	211233307594.6250	596587757440.3090	36.0025
32	65	1.0000	-151.6694	-1991.9356	3967807.5964	302115.7519	23003.6173	-7903617366.3928	-601795133.8521	-45821725.2100	-3488945.6280	36.0571
33	75	1.0000	9358.8579	-5431.0733	29496557.6312	-50828643.6699	87588221.2977	-160197967791.2400	276054091575.8920	-475698053642.5900	819723717331.5160	36.2076
34	76	1.0000	6761.8776	-8823.7144	77857935.1179	-59664876.0924	45712988.0773	-686996180188.3180	526465834000.9850	-403446586508.0350	309173246855.7750	36.215
35	86	1.0000	-11087.1714	1433.0984	2053771.0223	-15889007.5933	122925369.7500	2943255964.7289	-22770511349.4835	176164150631.2960	-1362894644364.2300	35.92
36	87	1.0000	-7055.2257	5303.7502	128129766.2834	-37419155.0189	49776210.3041	149193253815.5170	-198461851266.2380	26400585822.2370	-351182400394.8570	35.8332
37	88	1.0000	-5932.2261	11116.8599	123584575.1340	-65947726.7904	35191306.5534	1373872413668.0800	-733131642708.1780	391216826389.9980	-208762787383.3070	35.772
38	92	1.0000	-15041.2825	4171.4819	17401261.4037	-62744437.9278	226240178.7748	72589047919.7510	-261737288357.1210	943756815195.1530	-3402942438266.7200	35.8239
39	105	1.0000	-647.4518	-6243.4979	38981266.2848	4042363.9943	419193.8390	-243379454992.7720	-25238491192.9395	-2617235862.0616	-271407807.4357	36.0386
40												
41												
42												
43												
44		0.787803455	0.000133227	0.00016694	-4.49839E-09	9.30978E-10	-6.78289E-09	-1.35621E-12	-2.02674E-12	-2.42011E-12	-1.18124E-12	
45		0.000133227	4.18343E-08	4.28285E-08	-2.6586E-13	9.20889E-13	-1.22134E-12	-3.74043E-16	-6.86872E-16	-3.49671E-16	-3.49671E-16	
46		0.00016694	4.28285E-08	6.79474E-08	-2.6988E-13	1.20291E-12	-1.31504E-12	-5.78329E-16	-7.82592E-16	-9.58329E-16	-3.84797E-16	
47		-4.49839E-09	-2.6586E-13	-2.6988E-13	2.78689E-09	5.30545E-17	3.85317E-17	-8.68347E-22	-2.21795E-21	3.26514E-21	2.52823E-21	
48	Q_xx = (A.T * A)^-1	9.30978E-10	9.20889E-13	1.20291E-12	5.30545E-17	3.85317E-17	1.07732E-17	-1.3322E-20	-2.26163E-20	-2.33158E-20	-8.86449E-21	
49		-6.78289E-09	-1.22134E-12	-1.31504E-12	3.85317E-17	1.07732E-17	1.64708E-20	1.64708E-20	1.64708E-20	1.04581E-20	1.04581E-20	
50		-1.35621E-12	-3.74043E-16	-5.78329E-16	-8.68347E-22	-1.3322E-20	1.08716E-20	5.44114E-24	7.35258E-24	7.91312E-24	3.25209E-24	
51		-2.02674E-12	-6.54434E-16	-7.82592E-16	-2.21795E-21	-2.26163E-20	1.64708E-20	1.25311E-23	1.24729E-23	5.55744E-24	5.55744E-24	
52		-2.42011E-12	-6.86872E-16	-9.58329E-16	3.26514E-21	-2.33158E-20	1.69886E-20	7.91312E-24	1.24729E-23	1.6557E-23	6.49879E-24	
53		-1.18124E-12	-3.49671E-16	-3.84797E-16	2.52823E-21	-8.86449E-21	1.04581E-20	3.25209E-24	5.55744E-24	6.49879E-24	3.13464E-24	
54												
55												
56												

V = A * X - L	f = n-u	6
0.03625842	n	16
0.009485367	u	10
0.062923291	m_0 = (V.T * V / n-u)^1/2 (m)	0.053729405
-0.005583114		0.047689303
-0.04810144		1.09895E-05
-0.001349022		1.39435E-05
-0.040057791		4.74116E-10
-0.009246726	m_x=m_0 * (Q_xx)^1/2	6.30765E-10
-0.027672959		4.76833E-10
-0.027520786		1.25331E-13
-0.019603435		1.90197E-13
-0.036707461		2.18626E-13
0.042371964		9.51275E-14
-0.048133562		
0.019100362		
0.013721307		

Ardından dengeli jeoid yüksekliğinin duyarlılığını hesapladık. Bu değer mo <= -+ 1 dm olmalıdır, aksi takdirde yüzey polinomun derecesi aşamalı olarak artırılmalıdır. Bu uygulamada mo değerimiz mo <= -+ 1 dm bağıntısını sağlamaktadır. Daha sonra mx (mai) değerinin hesabını yaptık.

$$\overline{m_o} = \mp \sqrt{\frac{v^T v}{n-u}}$$

$$m_{a_i} = m_o \sqrt{Q_{xx}}$$

3-b)

Uygulamanın bu kısmında parametre anlamlılık testi uygulayarak anlamlı parametrelerin tespitini yaptık. Daha sonra a_o anlamlı parametresini düzeltme işlemleri için tekrardan uygulamasını yaptık.

Sonuç olarak en uygun polinom derecemiz (n) 3, anlamlı katsayımızın a 0 olduğu tespiti yapıldı.

[illegible]

3-c)

Uygulamanın bu kısmında IZDOĞAP ağından 5 yeni noktanın küçük h ve H değerini EK-1'den çektik. Polinomumuzun $N = a_c$ olduğu tespit edilerek, düzeltilmiş ortometrik yükseklik değerinin hesabını yaptık.

		N = (a_0)	36.00963334	
nokta adı	h (m)	H(m)	Düzeltilmiş Ortometrik Yükseklik (h-N)	FARK
1	155.9092	119.5752	119.8995667	0.324366656
2	213.8734	178.4003	177.8637667	-0.536533344
3	189.2755	153.9951	153.2658667	-0.729233344
4	79.2462	43.861	43.23656666	-0.624433344
5	136.2698	100.7859	100.2601667	-0.525733344

En son gerçek değerler ile yapmış olduğumuz fark hesabı sonucun farkların desimetre hassasiyetinde olduğunu gözlemledik. Gerçek değerler ile benzer sonuçlar çıktığı gözlemlenmiştir.

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