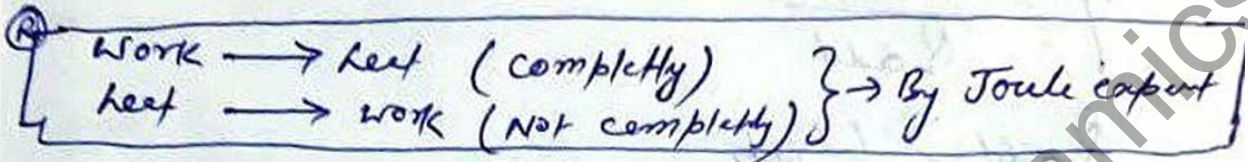


Limitation of 1st L.T.

- (i) It does not tell about feasibility of process in cycle.
- (ii) It also does not tell about direction of heat flow.
exp → Natural process occurs in one direction.

Second Law of Thermodynamics.

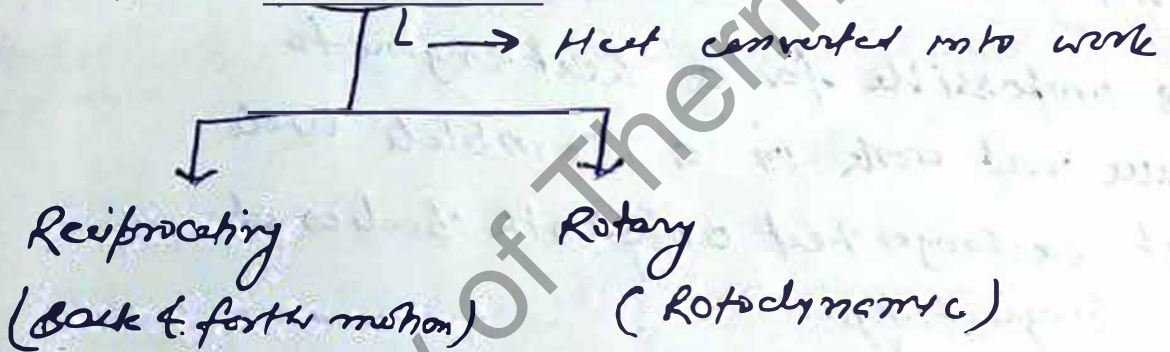
↓
direction of heat flow



Statement of Second Law

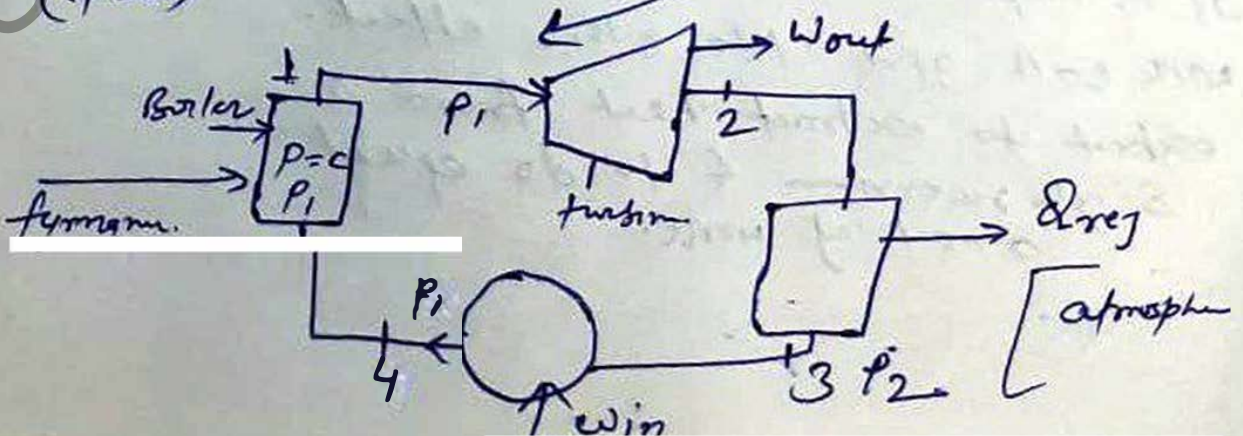
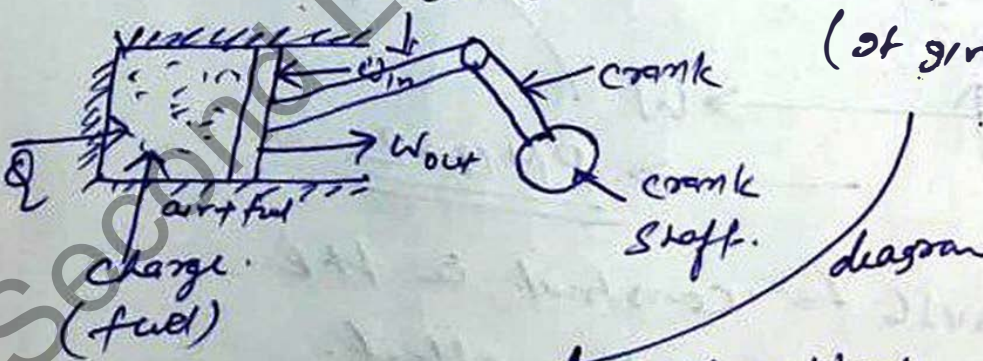
(1) Kelvin-Planck's statement.

Cyclic Heat engine.



exp. car, bike

exp. gas turbine
steam turbine
(it gives true work)



$$Q_{\text{net}} = W_{\text{net}} \text{ (for complete cycle)}$$

2

$$Q_{\text{add}} - Q_{\text{rej}} = W_{\text{out}} - W_{\text{in}}$$

$$Q_{\text{add}} = Q_{\text{rej}} + W_{\text{net}}$$

* Thermal Efficiency

It measures the performance of any heat engine.

$$\eta = \frac{W_{\text{net}}}{Q_{\text{add}}}$$

$$Q_{\text{add}} > W_{\text{net}}$$

$$\eta < 100\%$$

$$\eta < 1$$

* Kelvin-Planck's Statement

It is impossible for a heat engine to produce net work in a complete cycle if it exchanges heat only with bodies at single temp.



Perpetual motion machine

It is impossible to construct a H.E. which will give no other effect except to extract heat from a single reservoir & to do equal amount of work.

In case of PMM-2

$$Q_{rej} = 0$$

$$\eta = \frac{W}{Q_{in}} \neq 1 \text{ or } 100\%$$

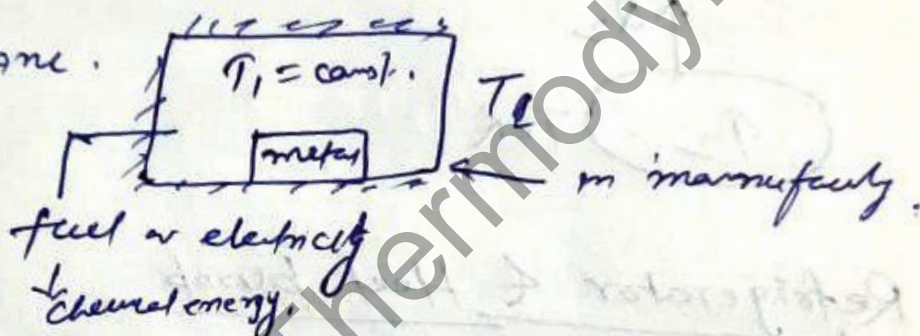
↓
This is violation of Kelvin-Planck statement.

TER

Thermal Energy Reservoir.

→ are the bodies of infinite heat capacity

ex: furnace.



Part of TER

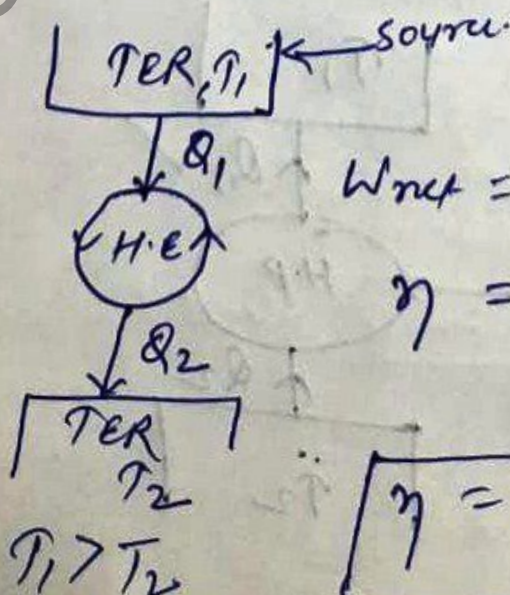
← (Thermal energy Reservoir)

Source

Sink
rejet

Supply

TER → T - not changed.



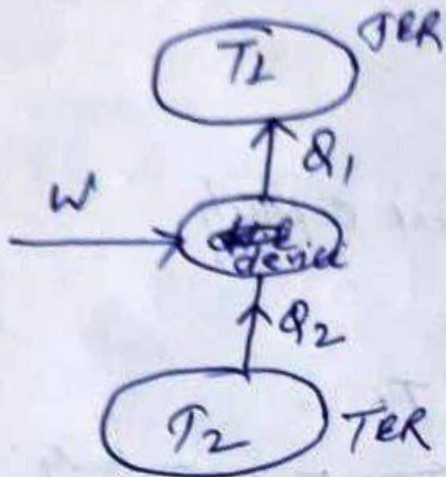
$$W_{net} = Q_1 - Q_2$$

$$\eta = \frac{Q_1 - Q_2}{Q_1}$$

$$\eta = 1 - \frac{Q_2}{Q_1}$$

Clausius Statement

It is impossible to construct a device which, while operating in a cycle will produce no other effect other than the transfer of heat from cooler to hotter body.

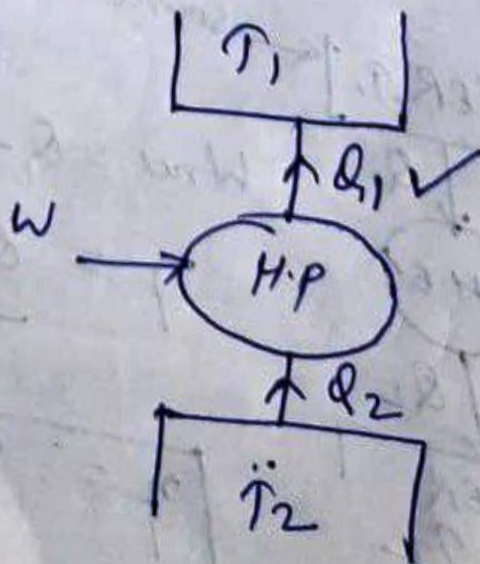
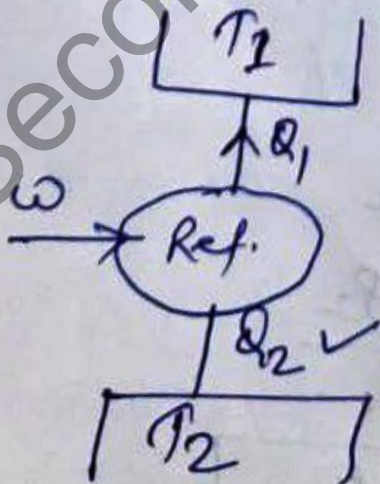


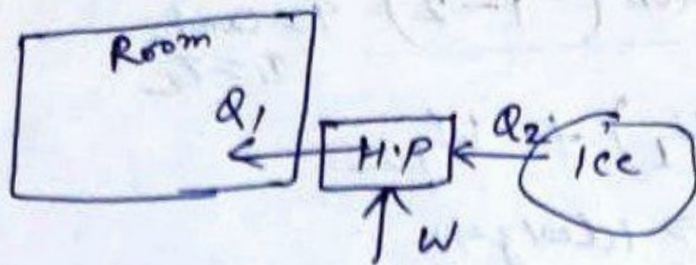
Refrigerator & Heat pump

Maintain the temp. of any body at particular temp.

Co-efficient of Performance.

$$[COP] = \frac{\text{Desired effect}}{\text{Work input}}$$





$$[COP]_{Ref} = \frac{Q_2}{W} = \frac{Q_2}{Q_1 - Q_2}$$

$$[COP]_{H.P.} = \frac{Q_1}{W} = \frac{Q_1}{Q_1 - Q_2}$$

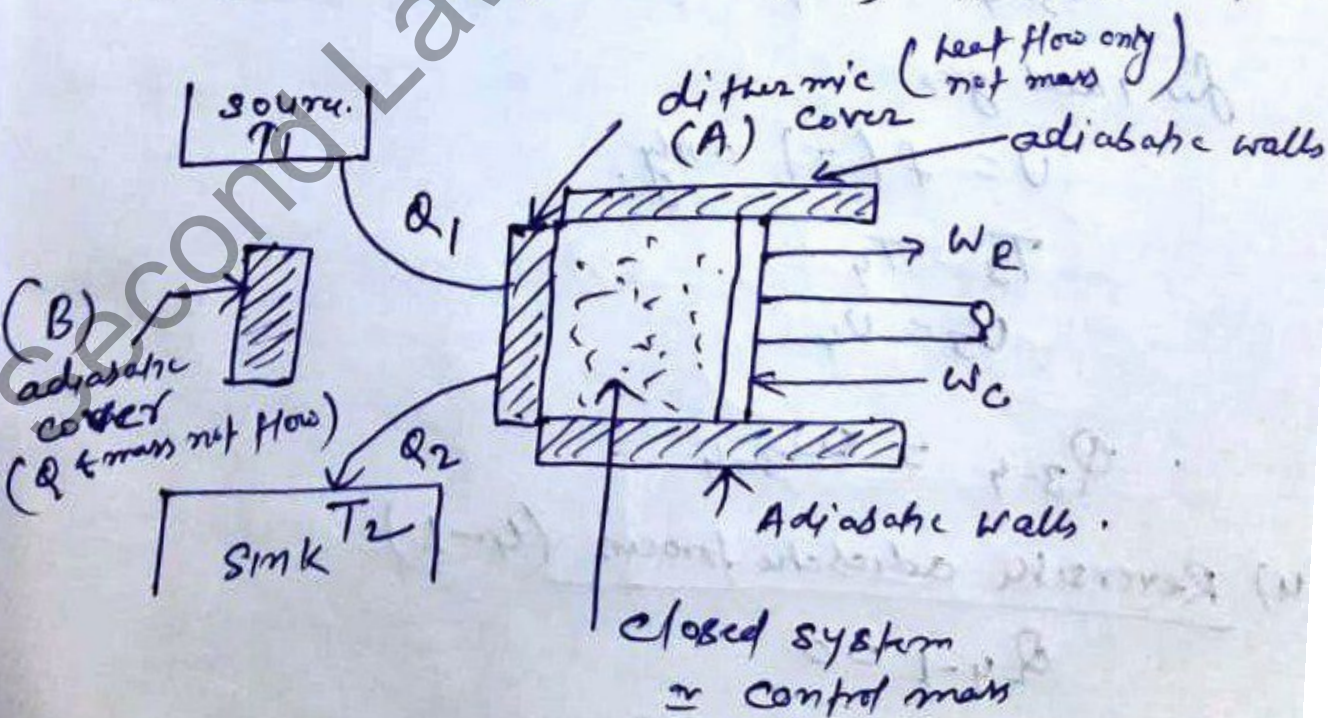
Relation b/w Both. [COP]

$$[COP]_{H.P.} = [COP]_{Ref} + 1$$

∴ $[COP]_{H.P.} > [COP]_{Ref}$ by unity.

Carnot Cycle

It is a ideal cycle & completely hypothetical cycle.



(1) Isothermal process (1-2) $T = \text{const.}$
 $T_1 = T_2$

Heat added
 $Q_{1-2} = (U_2 - U_1) + W_{1-2}$
of working fluid \rightarrow ideal gas

$$U_2 = U_1$$

$$\therefore \boxed{Q_{1-2} = W_{1-2}}$$

(2) Reversible adiabatic process (2-3)

$$Q_{2-3} = 0$$

$$Q_{2-3} = (U_3 - U_2) + W_{2-3}$$

$$\therefore \boxed{W_{2-3} = U_2 - U_3}$$

(3) Isothermal process (3-4)

$$Q_{3-4} = U_4 - U_3 + W_{3-4}$$

for ideal gas,

$$U = f(T) \text{ only.}$$

$$T_3 = T_4$$

$$U_3 = U_4$$

$$\therefore Q_{3-4} = W_{3-4}$$

(4) Reversible adiabatic process (4-1)

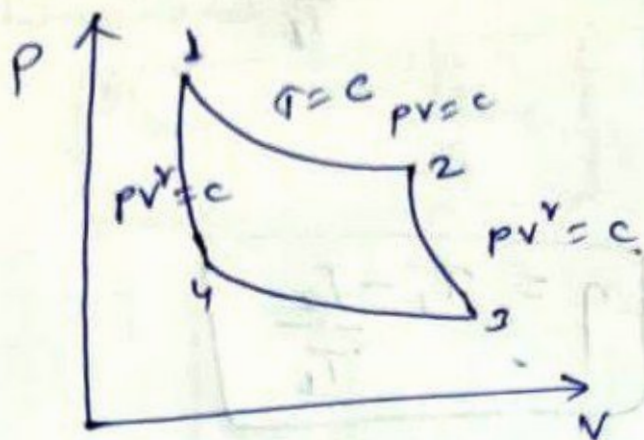
$$Q_{4-1} = 0$$

$$Q_{4-1} = U_1 - U_4 + W_{4-1}$$

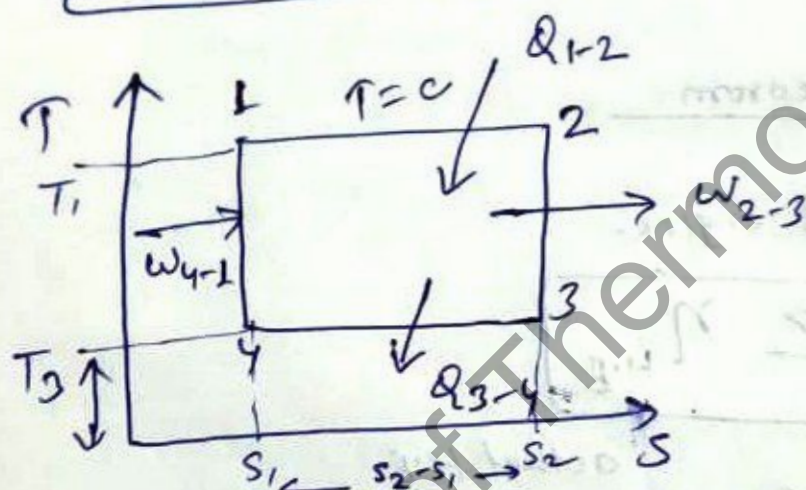
$$\boxed{U_4 - U_1 = W_{4-1}}$$

PV-diagram: Carnot cycle.

7



$$\oint dQ = \oint W$$



$$\therefore Q_{1-2} - Q_{3-4} = W_{2-3} - W_{4-1}$$

→ $Q_{12} = \text{Area under process 1-2 in } T-S \text{ plot}$

$$Q_{1-2} = T_1 \Delta S = T_1 (S_2 - S_1) \checkmark$$

→ $Q_{3-4} = \text{Area under process 3-4 in } T-S \text{ plot}$

$$Q_{34} = T_3 (S_2 - S_1) \checkmark$$

$$\therefore W_{\text{net}} = Q_{12} - Q_{34}$$

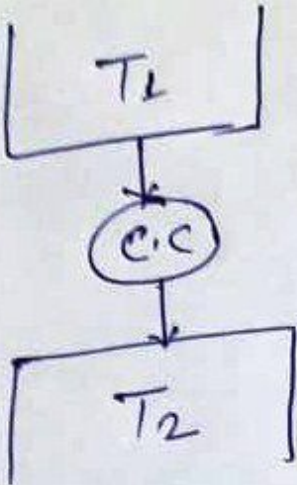
for Carnot engine

$$\eta = \frac{W_{\text{net}}}{Q_{1-2}} = \frac{Q_{12} - Q_{34}}{Q_{12}}$$

$$= \frac{T_1 (S_2 - S_1) - T_3 (S_2 - S_1)}{T_1 (S_2 - S_1)}$$

$$\eta = \frac{T_1 - T_3}{T_1} = \frac{T_1 - T_2}{T_1}$$

8



$$\eta = \frac{T_1 - T_2}{T_L}$$

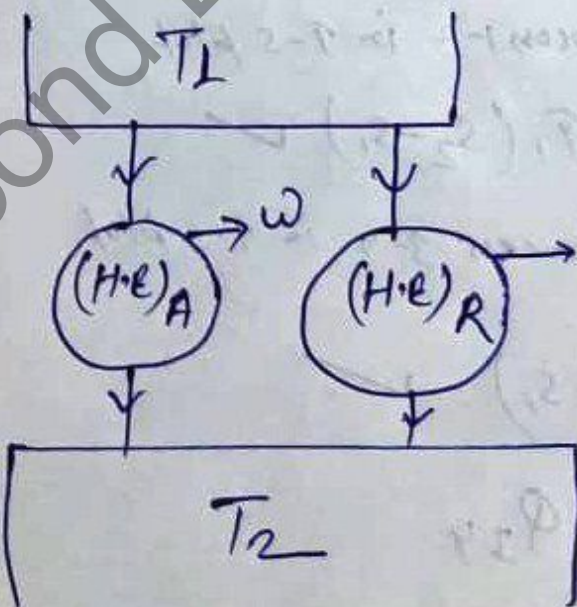
$$W = p \Delta V$$

Carnot's theorem
 ↓
 for all heat engine.

$$\eta_{\text{rev H.E}} \geq \eta_{\text{H.E}}$$

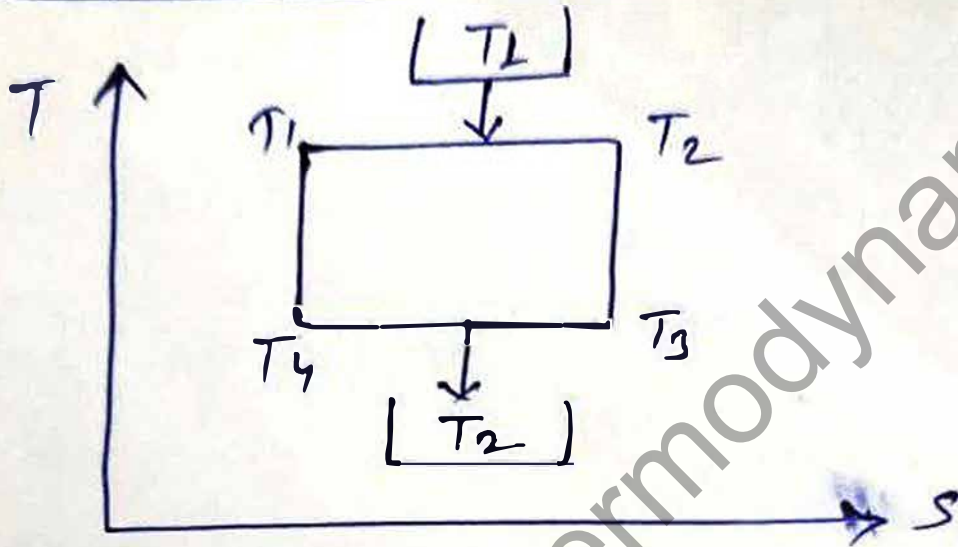
Reversible H.E

actual H.E



$$\eta_{\max} = \eta_{\text{Rev}}$$

$$\eta_{\text{Rev}} = 1 - \frac{T_2}{T_1}$$



$$T_3 = T_4 = T_2 \quad (\text{Sink})$$

$$T_1 = T_2 = T_1 \quad (\text{Source})$$