

Control Systems

G V V Sharma*

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Abstract—This manual is an introduction to control systems in feedback circuits. Links to sample Python codes are available in the text.

Download python codes using

svn co <https://github.com/gadepall/school/trunk/control/feedback/codes>

1 FEEDBACK VOLTAGE AMPLIFIER: SERIES-SHUNT

2 FEEDBACK CURRENT AMPLIFIER: SHUNT-SERIES

2.1 Ideal Case

2.2 Practical Case

3 FEEDBACK CURRENT AMPLIFIER: EXAMPLE

3.1. Fig. 3.1.1 shows a feedback current amplifier. Draw the equivalent control system.

Solution: See fig 3.1.2

3.2. Refer table 3.2 for the parameters and draw the small signal equivalent model of the fig 3.1.1

Solution: See fig 3.2

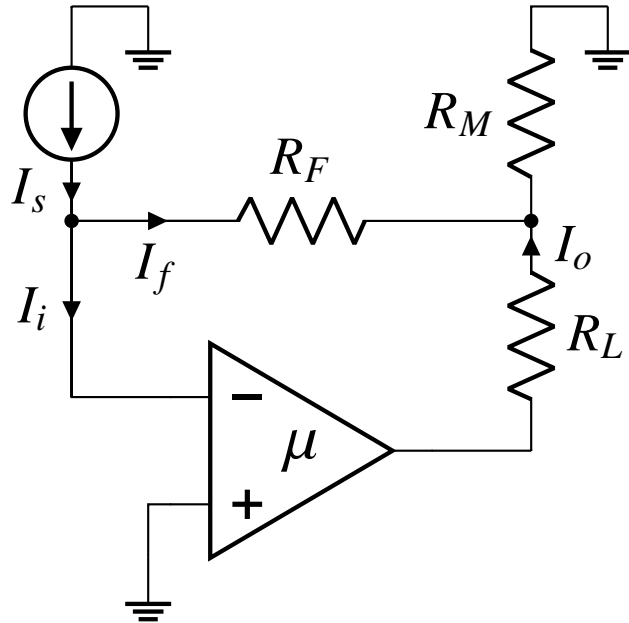


Fig. 3.1.1

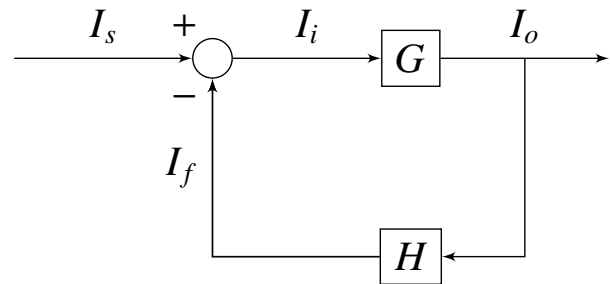


Fig. 3.1.2

Component	Description
R_{id}	Input Resistance of Op Amp
R_{out}	Output Resistance of Op Amp
I_s	Input Current
I_o	Output Current
R_M, R_F	Feedback Resistances
R_L	Load Resistance

TABLE 3.2

*The author is with the Department of Electrical Engineering, Indian Institute of Technology, Hyderabad 502285 India e-mail: gadepall@iith.ac.in. All content in this manual is released under GNU GPL. Free and open source.

3.3. Given G (open-loop gain), H (feedback gain)

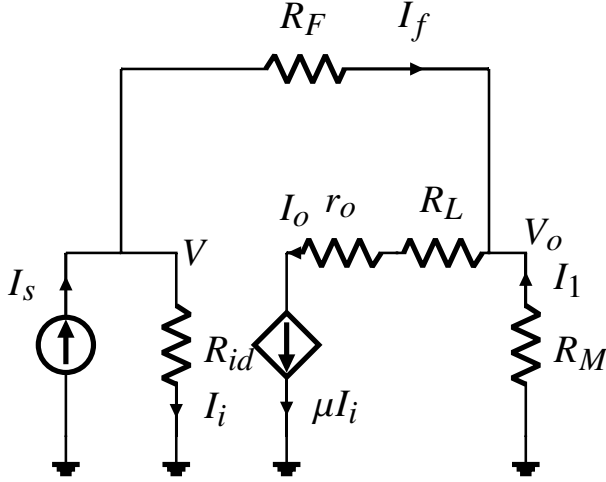


Fig. 3.2

and T (closed-loop gain) as

$$G = \frac{I_o}{I_i} \quad (3.3.1)$$

$$H = \frac{I_f}{I_o} \quad (3.3.2)$$

$$T = \frac{I_o}{I_f} \quad (3.3.3)$$

Find G and H as a function of the resistances.

Solution: Refer fig. 3.2,

We get,

$$I_o = \mu I_i \quad (3.3.4)$$

$$\Rightarrow G = \frac{I_o}{I_i} = \mu \quad (3.3.5)$$

And,

$$I_i = I_s - I_f \quad (3.3.6)$$

Using eq. 3.3.5, we get,

$$I_o = \mu (I_s - I_f) \quad (3.3.7)$$

Assuming virtual ground at V_1 , we get,

$$V_o = -I_f R_F \quad (3.3.8)$$

Therefore,

$$I_1 = -\frac{V_o}{R_M} \quad (3.3.9)$$

$$\Rightarrow I_1 = I_f \frac{R_F}{R_M} \quad (3.3.10)$$

The output current is also expressed as,

$$I_o = I_f + I_1 \quad (3.3.11)$$

$$\Rightarrow \frac{I_o}{1 + \frac{R_F}{R_M}} = I_f \quad (3.3.12)$$

Now substituting I_f in eq. 3.3.7 we get,

$$I_o = \mu \left(I_s - \frac{I_o}{1 + \frac{R_F}{R_M}} \right) \quad (3.3.13)$$

$$(3.3.14)$$

$$\Rightarrow T = \frac{I_o}{I_s} = \frac{\mu}{1 + \frac{\mu}{1 + \frac{R_F}{R_M}}} \quad (3.3.15)$$

Therefore,

$$\Rightarrow H = \frac{I_f}{I_o} = \frac{1}{1 + \frac{R_F}{R_M}} \quad (3.3.16)$$

3.4. What will be closed-loop gain(T) if $\mu \rightarrow \infty$

Solution: From eq. 3.3.15 we get,

$$T = \frac{\mu}{1 + \frac{\mu}{1 + \frac{R_F}{R_M}}} \quad (3.4.1)$$

$$T = \frac{1}{\frac{1}{\mu} + \frac{1}{1 + \frac{R_F}{R_M}}} \quad (3.4.2)$$

Applying the limit, we get,

$$\Rightarrow T = 1 + \frac{R_F}{R_M} \quad (3.4.3)$$

3.5. Refer table 3.5 and find G, H and T

Component	Value
μ	10^4
R_{id}	$1\text{ M}\Omega$
r_o	$100\ \Omega$
R_L	$10\text{ k}\Omega$
R_M	$100\ \Omega$
R_F	$10\text{ k}\Omega$

TABLE 3.5

Solution: Using eqs. 3.3.5, 3.3.16 and 3.3.15
We get,

$$G = \mu = 10^4 \quad (3.5.1)$$

$$H = \frac{1}{1 + \frac{R_F}{R_M}} = 9.9 \times 10^{-3} \quad (3.5.2)$$

$$T = \frac{\mu}{1 + \frac{\mu}{1 + \frac{R_F}{R_M}}} = 100 \quad (3.5.3)$$

3.6. Tabulate your results.

Solution: Refer table 3.6,

Gain	Value
G	10^4
H	9.9×10^{-3}
T	100

TABLE 3.6

4 FEEDBACK TRANSCONDUCTANCE AMPLIFIER: SERIES-SERIES