

Why the missing 1/L in the relaxation function does not cause problem in our viscoelastic simulation? Because the error pointed out by Peter Moczo is not an error.

1 Boltzmann principle

For a linear isotropic viscoelastic material, the stress-strain relation is given by Boltzmann principle. In scalar notation, we have:

$$\sigma(t) = \int_{-\infty}^t \psi(t-t') \dot{\varepsilon}(t') dt' \quad (1)$$

where $\sigma(t)$ is stress, $\dot{\varepsilon}(t)$ time derivative of strain, and $\psi(t)$ stress relaxation function defined as a stress response to Heaviside unit step function in strain. The stress at a given time t is determined by the entire history of the strain until t .

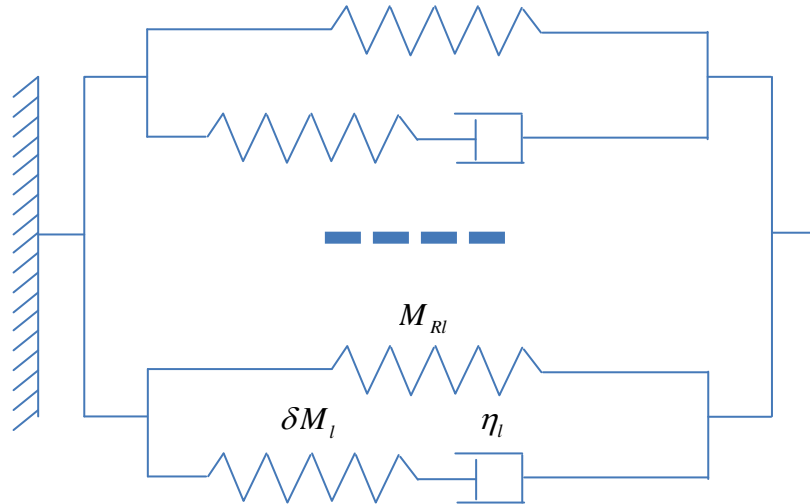
Using symbol $*$ for the convolution and applying the convolution's property, we have:

$$\sigma(t) = \psi(t) * \dot{\varepsilon}(t) = \dot{\psi}(t) * \varepsilon(t) \quad (2)$$

In following, we set $\dot{\psi}(t) = M(t)$.

2 Representation of $M(t)$ by a set of standard linear solid

In seismology, we typically encounter viscoelastic material with attenuation is observed to be relatively constant over a broad frequency range. For this kind of material, we could approximate the $M(t)$ by a set of standard linear solid:



For viscoelastic material described by N standard linear solids, we have:

$$M(\omega) = \sum_{l=1}^N M_{Rl} \frac{1 + i\tau_{el}\omega}{1 + i\tau_{ol}\omega} \quad (3)$$

Where $\tau_{el} = \frac{\eta_l}{\delta M_l} \frac{M_{Ul}}{M_{Rl}}$, $\tau_{ol} = \frac{\eta_l}{\delta M_l}$, $\frac{\tau_{el}}{\tau_{ol}} = \frac{M_{Ul}}{M_{Rl}}$. M_R is the total relaxed modulu.

Correspondingly, for $M_{Rl} = \frac{M_R}{N}$ we have:

$$\psi(t) = M_R \left[1 - \frac{1}{N} \sum_{l=1}^N \left(1 - \frac{\tau_{el}}{\tau_{ol}} \right) e^{-t/\tau_{ol}} \right] H(t) \quad (4)$$

3 Error pointed out by Peter Moczo

In his 2005 paper : “On the rheological models used for time-domain methods of seismic wave

See also a more precise analysis in Changhua Zhang, Zhinan Xie, Dimitri Komatitsch, Paul Cristini and René Matzen, Revisiting the 1/L problem in rheological models for time-domain seismic wave propagation, Proceedings of the 86th annual meeting of the Society of Exploration Geophysics (SEG'2016), p. 1-3 (2016). Available at http://komatitsch.free.fr/preprints/Zhang_SEG_2016.pdf

propagation”, Moczo pointed out that the $\frac{1}{N}$ is missing in Liu’s paper: “Velocity dispersion due to anelasticity: Implications for seismology and mantle composition”. That Liu use (4) wrongly as:

$$\psi(t) = M_R \left[1 - \sum_{l=1}^N \left(1 - \frac{\tau_{\varepsilon l}}{\tau_{\sigma l}} \right) e^{-t/\tau_{\sigma l}} \right] H(t) \quad (5)$$

Taking into account that the SPEC-FEM2D and SPEC-FEM3D are based on (5), that means the two codes would give wrong results in case for viscoelastic simulation.

4 Error pointed out by Peter Moczo is not an error.

First by setting $M_{Rl} = \frac{M_R}{N}$, (3) can be rewritten as:

$$\begin{aligned} M(\omega) &= \sum_{l=1}^N M_{Rl} \frac{1 + \mathbf{i}\tau_{\varepsilon l}\omega}{1 + \mathbf{i}\tau_{\sigma l}\omega} = \frac{M_R}{N} \sum_{l=1}^N \frac{1 + \mathbf{i}\tau_{\varepsilon l}\omega}{1 + \mathbf{i}\tau_{\sigma l}\omega} = \frac{M_R}{N} \sum_{l=1}^N \left(1 + \frac{\mathbf{i}\omega(\tau_{\varepsilon l} - \tau_{\sigma l})}{1 + \mathbf{i}\tau_{\sigma l}\omega} \right) \\ &= \frac{M_R}{N} \sum_{l=1}^N \left(1 + \frac{\mathbf{i}\omega(\tau_{\varepsilon l} - \tau_{\sigma l})(1 - \mathbf{i}\tau_{\sigma l}\omega)}{1 + \omega^2\tau_{\sigma l}^2} \right) = M_R + \frac{M_R}{N} \sum_{l=1}^N \left(\frac{\mathbf{i}\omega(\tau_{\varepsilon l} - \tau_{\sigma l})(1 - \mathbf{i}\tau_{\sigma l}\omega)}{1 + \omega^2\tau_{\sigma l}^2} \right) \quad (4) \\ &= M_R \left[1 + \sum_{l=1}^N \frac{\omega^2\tau_{\sigma l}^2}{1 + \omega^2\tau_{\sigma l}^2} \left(\frac{1}{N} \frac{(\tau_{\varepsilon l} - \tau_{\sigma l})}{\tau_{\sigma l}} \right) + \sum_{l=1}^N \frac{\mathbf{i}\omega\tau_{\sigma l}}{1 + \omega^2\tau_{\sigma l}^2} \left(\frac{1}{N} \frac{(\tau_{\varepsilon l} - \tau_{\sigma l})}{\tau_{\sigma l}} \right) \right] \end{aligned}$$

Introducing $\frac{\tau'_{\varepsilon l} - \tau_{\sigma l}}{\tau_{\sigma l}} = \frac{1}{N} \frac{(\tau_{\varepsilon l} - \tau_{\sigma l})}{\tau_{\sigma l}}$ that is:

$$\tau'_{\varepsilon l} = \frac{1}{N} (\tau_{\varepsilon l} - \tau_{\sigma l}) + \tau_{\sigma l} \quad (5)$$

then the (4) reduces to

$$M(\omega) = M_R \left[1 + \sum_{l=1}^N \frac{\omega\tau_{\sigma l}(\tau'_{\varepsilon l} - \tau_{\sigma l})}{1 + \omega^2\tau_{\sigma l}^2} + \sum_{l=1}^N \frac{\mathbf{i}\omega\tau_{\sigma l}(\tau'_{\varepsilon l} - \tau_{\sigma l})}{1 + \omega^2\tau_{\sigma l}^2} \right] \quad (6)$$

(6) corresponds exactly as

$$\psi(t) = M_R \left[1 - \sum_{l=1}^N \left(1 - \frac{\tau'_{\varepsilon l}}{\tau_{\sigma l}} \right) e^{-t/\tau_{\sigma l}} \right] H(t) \quad (7)$$

Thus if in frequency domain we use (6) to obtain the value of M_R , $\tau'_{\varepsilon l}$ and $\tau_{\sigma l}$, no error exists. In our codes SPEC-FEM3D and SPEC-FEM2D, we use (6) together with (7). Thus, no modification has to be made in our code.

It worth note here, $\tau'_{\varepsilon l}$ do not share the same physical meaning as $\tau_{\varepsilon l}$.

Appendix A: For constant τ method, relationship between M_R , $\tau_{\varepsilon l}$ and $\tau_{\sigma l}$ determined by (3) and that by (6)

Considering using one standard linear solid, for both (3) and (6), we have

$$M(\omega) = M_R \left(1 - \frac{\omega^2\tau_{\sigma 1}(\tau_{\sigma 1} - \tau_{\varepsilon 1})}{1 + \omega^2\tau_{\sigma 1}^2} + \mathbf{i} \frac{\omega(\tau_{\varepsilon 1} - \tau_{\sigma 1})}{1 + \omega^2\tau_{\sigma 1}^2} \right) \quad (A-1)$$

Thus

$$Q^{-1} = \frac{\text{Im}[M(\omega)]}{\text{Re}[M(\omega)]} = \frac{\frac{\omega(\tau_{\varepsilon l} - \tau_{\sigma l})}{1 + \omega^2 \tau_{\sigma l}^2}}{1 - \frac{\omega^2 \tau_{\sigma l}(\tau_{\sigma l} - \tau_{\varepsilon l})}{1 + \omega^2 \tau_{\sigma l}^2}} = \frac{\omega(\tau_{\varepsilon l} - \tau_{\sigma l})}{1 + \omega^2 \tau_{\sigma l} \tau_{\varepsilon l}} \quad (\text{A-2})$$

Introducing $\tau = \frac{\tau_{\varepsilon l} - \tau_{\sigma l}}{\tau_{\sigma l}}$, we can rewritten (A-2) as:

$$Q^{-1} = \frac{\omega \tau \tau_{\sigma l}}{1 + \omega^2 \tau_{\sigma l}^2 (1 + \tau)} \quad (\text{A-3})$$

In paper: “Modeling of a constant Q: Methodology and algorithm for an efficient and optimally inexpensive viscoelastic technique”, Blanch, Robertsson and Symes observed the L2 approximation of constant Q near the interesting band $[\omega_0 - \Delta\omega, \omega_0 + \Delta\omega]$ with (A-3) gives $\tau \ll 1$ for bigger Q ($Q > 20$). Moreover, by setting a constant τ , the change of $\tau_{\sigma l}$ is enough to give good approximation if ω_0 changes. Thus they prosper to use constant τ in approximation of constant Q in wide frequency band.

Thus, in general case, for $\tau \ll 1$, with (3) we have:

$$Q^{-1} = \frac{\frac{1}{N} \sum_{l=1}^N \frac{\omega \tau_{(3)} \tau_{\sigma l}}{1 + \omega^2 \tau_{\sigma l}^2}}{1 - \tau_{(3)} \frac{1}{N} \sum_{l=1}^N \frac{\omega^2 \tau_{\sigma l} \tau_{\sigma l}}{1 + \omega^2 \tau_{\sigma l}^2}} \approx \frac{1}{N} \sum_{l=1}^N \frac{\omega \tau_{(3)} \tau_{\sigma l}}{1 + \omega^2 \tau_{\sigma l}^2} \quad (\text{A-4})$$

While (6) we have

$$Q^{-1} = \frac{\sum_{l=1}^N \frac{\omega \tau_{(6)} \tau_{\sigma l}}{1 + \omega^2 \tau_{\sigma l}^2}}{1 - \tau_{(6)} \sum_{l=1}^N \frac{\omega^2 \tau_{\sigma l} \tau_{\sigma l}}{1 + \omega^2 \tau_{\sigma l}^2}} \approx \sum_{l=1}^N \frac{\omega \tau_{(6)} \tau_{\sigma l}}{1 + \omega^2 \tau_{\sigma l}^2} \quad (\text{A-5})$$

If we use same set of $\tau_{\sigma l}$. Different value of τ will be obtained by (3) compared that obtained by (6) denoted as $\tau_{(6)}$, which gives that

$$\tau_{(3)} / N = \tau_{(6)} \quad (\text{A-6})$$

That is

$$\tau'_{\varepsilon l} = (\tau_{\varepsilon l} - \tau_{\sigma l}) \frac{1}{N} + \tau_{\sigma l} \quad (\text{A-6})$$