



## **Assignment ELC3050**

NAME ***Omar Amr Mahmoud Hafz***

GROUP ***A***

SEC ***3***

BENCH NUM. ***3***

STUDENT ID ***9202967***

EMAIL ***eng.omar.amr@gmail.com***

DATE ***22-12-2022***

Supervised by: **Dr. Mohamed A. Nasr**

**ELC3050**

### Resonance frequency calculation:

Adding walls to the guide forces boundary conditions in z direction:

$$\beta = \frac{l\pi}{d}, l = 0, 1, 2, \dots \quad \therefore \beta^2 = k^2 - k_c^2 \quad \therefore \left(\frac{l\pi}{d}\right)^2 = \left(\frac{w}{c}\right)^2 - \left(\frac{m\pi}{a}\right)^2 - \left(\frac{n\pi}{b}\right)^2$$
$$\therefore f_{res} = \frac{c}{2\sqrt{\mu_r \epsilon_r}} \sqrt{\left(\frac{m}{a}\right)^2 + \left(\frac{n}{b}\right)^2 + \left(\frac{l}{d}\right)^2}$$

Hence, there's a unique resonant frequency for each value of  $m, n, l$ . and for each resonant mode  $TE_{m,n,l}$ . The dominant TE resonant mode is always  $TE_{101}$ . there are four possibilities for the next resonance mode:  $TE_{102}$ ,  $TE_{011}$ ,  $TE_{201}$ ,  $TE_{110}$ .

### Which mode is the next mode?:

$$TE_{102} \rightarrow \omega_{m,n,l} \propto \left(\frac{1}{a}\right)^2 + \left(\frac{2}{d}\right)^2 \quad TM_{110} \rightarrow \omega_{m,n,l} \propto \left(\frac{1}{a}\right)^2 + \left(\frac{1}{b}\right)^2$$
$$TE_{011} \rightarrow \omega_{m,n,l} \propto \left(\frac{1}{b}\right)^2 + \left(\frac{1}{d}\right)^2 \quad TE_{201} \rightarrow \omega_{m,n,l} \propto \left(\frac{2}{a}\right)^2 + \left(\frac{1}{d}\right)^2$$

We know that the given guide dimensions will be  $d > a > b$ :

$$\therefore d > a \quad \therefore TE_{011} \rightarrow TM_{110} \quad \text{if } a \geq 2b \text{ \& } \therefore d > a \quad \therefore TE_{102} \rightarrow TE_{201} \rightarrow TE_{011}$$

if  $a < 2b$ ,  $TE_{011} \rightarrow TE_{201}$ , now the next mode is either  $TE_{102}$  or  $TE_{011}$ :

if  $\left(\frac{1}{a}\right)^2 + \left(\frac{2}{d}\right)^2 < \left(\frac{1}{b}\right)^2 + \left(\frac{1}{d}\right)^2$  then the next mode is  $TE_{102}$  (i.e,  $TE_{102} \rightarrow TE_{011}$ )

$$\frac{3}{d^2} > \frac{a^2 - b^2}{a^2 b^2} \quad \therefore d > \sqrt{\frac{3a^2 b^2}{a^2 - b^2}} \quad \text{put } r = \sqrt{\frac{3a^2 b^2}{a^2 - b^2}}$$

Generally, if  $d > r$ , the next mode is  $TE_{102}$ , otherwise the next mode is  $TE_{011}$ .

### Quality factor calculations:

$$Q_{die} = \frac{1}{\tan \delta} \quad Q_{cond} = \frac{w_{res} E_{stored}}{P_{loss}} \quad \therefore E_{stored} = W_e + W_m,$$

$$\text{at resonance: } W_e = W_m \quad \therefore E_{stored} = 2W_e = 2W_m \quad \therefore Q_{cond} = \frac{2 w_{res} W_e}{P_{loss}} = \frac{2 w_{res} W_m}{P_{loss}}$$

to calculate the quality factor, we need to calculate the power loss ( $P_{loss}$ ), the stored energy ( $E_{stored}$ ) and the resonance frequency (calculated via the above-stated relation).

### Given that:

$$H_z = A \cos(k_{xm}x) \cos(k_{yn}y) e^{-j\beta z} \quad E_y = \frac{-j\omega\mu k_{xm}}{k_c^2} A \sin(k_{xm}x) \cos(k_{yn}y) e^{-j\beta z} = -Z_{TE} H_x$$

$$E_x = \frac{j\omega\mu k_{yn}}{k_c^2} A \cos(k_{xm}x) \sin(k_{yn}y) e^{-j\beta z} = Z_{TE} H_y$$

### **For $TE_{10}$ mode:**

$$H_z = A \cos\left(\frac{\pi}{a}x\right) e^{-j\beta z} \quad E_y = \frac{-j\omega\mu}{k_c} A \sin\left(\frac{\pi}{a}x\right) e^{-j\beta z} = -Z_{TE} H_x \quad E_x = H_y = 0$$

$$k_c = \frac{\pi}{a}$$

$$\text{generally: } \beta = \frac{\omega\mu}{Z_{TE}}$$

Due to the two walls closing the resonator, the wave is reflected, it must satisfy the boundary conditions:

$$E_t = 0$$

$$H_n = 0$$

$$\therefore H_z^+ = -H_z^-$$

$$H_x^+ = H_x^-$$

$$E_y^+ = -E_y^-$$

**For  $TE_{10l}$  modes:**

$$H_z = H_z^+ + H_z^- = A(-2j)\cos\left(\frac{\pi}{a}x\right)\sin(\beta z)$$

$$E_y = E_y^+ + E_y^- = \frac{-2\omega\mu}{k_c} A \sin\left(\frac{\pi}{a}x\right)\sin(\beta z)$$

$$H_x = H_x^+ + H_x^- = \frac{(2j)\omega\mu}{k_c Z_{TE}} A \sin\left(\frac{\pi}{a}x\right)\cos(\beta z) = \frac{(2j)\beta}{k_c} A \sin\left(\frac{\pi}{a}x\right)\cos(\beta z)$$

$$\text{Where } k_c = \frac{\pi}{a}, \beta = \frac{l\pi}{d}.$$

**Energy stored calculation:**

$$W_e = \frac{\epsilon}{4} \int |E|^2 dv = \frac{\epsilon}{4} \int_{z=0}^d \int_{y=0}^b \int_{x=0}^a \left(\frac{2\omega\mu a}{\pi} A\right)^2 \sin^2\left(\frac{\pi}{a}x\right) \sin^2\left(\frac{l\pi}{d}z\right) dx dy dz = \frac{\epsilon abd}{4} \left(\frac{\omega\mu}{k_c} A\right)^2$$

$$\therefore E_{stored} = 2W_e = \frac{\epsilon abd}{2} \left(\frac{\omega\mu}{k_c} A\right)^2$$

**Power loss calculations:**

$$P_{loss} = \frac{R_s}{2} \oint |H|^2 dS = \frac{R_s}{2} (2I_1 + 2I_2 + 2I_3), \text{ where } I_1, I_2, I_3 \text{ are for the lateral, top and front faces, respectively.}$$

$$I_1 = \int_{y=0}^b \int_{x=0}^a |H|^2_{z=0,d} dx dy = \int_{y=0}^b \int_{x=0}^a \left(\frac{2\beta}{k_c} A\right)^2 \sin^2\left(\frac{\pi}{a}x\right) dx dy = \left(\frac{2al}{d} A\right)^2 \frac{ab}{2}$$

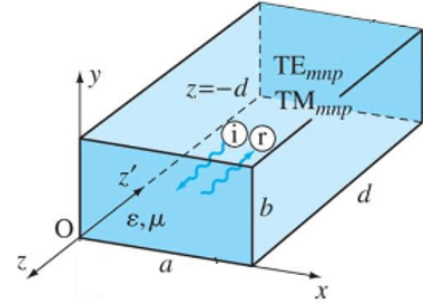
$$I_2 = \int_{z=0}^d \int_{x=0}^a |H|^2_{y=0,b} dx dz = \int_{z=0}^d \int_{x=0}^a \left(\frac{2al}{d} A\right)^2 \sin^2\left(\frac{\pi}{a}x\right) \cos^2(\beta z) + (2A)^2 \cos^2\left(\frac{\pi}{a}x\right) \sin^2(\beta z) dx dz$$

$$= (2A)^2 \frac{ad}{4} \left(1 + \left(\frac{al}{d}\right)^2\right)$$

$$I_3 = \int_{z=0}^d \int_{y=0}^b |H|^2_{x=0,a} dy dz = \int_{z=0}^d \int_{y=0}^b (2A)^2 \sin^2(\beta z) dy dz = (2A)^2 \frac{db}{2}$$

$$\therefore P_{loss} = R_s (A)^2 \left[ 2 \left(\frac{al}{d}\right)^2 ab + 2db + ad + \left(\frac{al}{d}\right)^2 ad \right]$$

$$\therefore Q_{cond,10l} = \omega_{res} \frac{\frac{\epsilon}{2} \left(\frac{\omega\mu a}{\pi}\right)^2 abd}{R_s \left[ 2 \left(\frac{al}{d}\right)^2 ab + 2db + ad + \left(\frac{al}{d}\right)^2 ad \right]}$$



Thus far we have derived a formula for calculating  $Q_{cond}$  for  $TE_{10l}$  modes which includes the dominant mode  $TE_{101}$  and the next mode if it was  $TE_{102}$  (depending on the dimensions). Now we derive a general formula for  $TE_{01l}$  mode to calculate the quality factor if the next mode was  $TE_{011}$  (the other possibility). We'll basically go through the same steps.

**For  $TE_{10}$  mode :**

$$H_z = A \cos\left(\frac{\pi}{b}y\right) e^{-j\beta z}$$

$$E_x = \frac{j\omega\mu}{\pi/b} A \sin\left(\frac{\pi}{b}y\right) e^{-j\beta z} = Z_{TE} H_y$$

$$E_y = H_x = 0$$

$$k_c = \frac{\pi}{b}$$

$$\text{generally: } \beta = \frac{\omega\mu}{Z_{TE}}$$

boundary conditions:

$$E_t = 0$$

$$H_n = 0$$

$$\therefore H_z^+ = -H_z^-$$

$$E_x^+ = -E_x^-$$

$$H_y^+ = H_y^-$$

**For  $TE_{01l}$  modes:**

$$H_z = H_z^+ + H_z^- = A(-2j) \cos\left(\frac{\pi}{b}y\right) \sin(\beta z)$$

$$E_x = E_x^+ + E_x^- = \frac{2\omega\mu}{k_c} A \sin\left(\frac{\pi}{b}y\right) \sin\left(\frac{l\pi}{d}z\right)$$

$$H_y = H_y^+ + H_y^- = \frac{(2j)\omega\mu}{k_c Z_{TE}} A \sin\left(\frac{\pi}{b}y\right) \cos(\beta z) = \frac{(2j)\beta}{k_c} A \sin\left(\frac{\pi}{b}y\right) \cos(\beta z)$$

$$\text{Where } k_c = \frac{\pi}{b}, \beta = \frac{l\pi}{d}.$$

**Energy stored calculation:**

$$W_e = \frac{\epsilon}{4} \int |E|^2 dv = \frac{\epsilon}{4} \int_{z=0}^d \int_{y=0}^b \int_{x=0}^a \left(\frac{2\omega\mu b}{\pi} A\right)^2 \sin^2\left(\frac{\pi}{b}y\right) \sin^2\left(\frac{l\pi}{d}z\right) dx dy dz = \frac{\epsilon abd}{4} \left(\frac{\omega\mu}{k_c} A\right)^2$$

$$\therefore E_{stored} = 2W_e = \frac{\epsilon abd}{2} \left(\frac{\omega\mu}{k_c} A\right)^2$$

**Power loss calculations:**

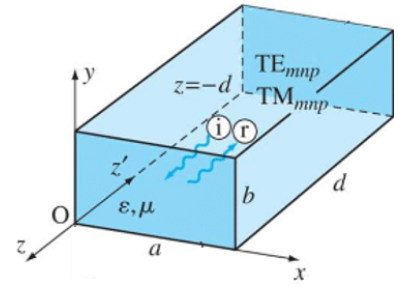
$$P_{loss} = \frac{R_s}{2} \oint |H|^2 dS = \frac{R_s}{2} (2I_1 + 2I_2 + 2I_3), \text{ where } I_1, I_2, I_3 \text{ are for the lateral, top and front faces, respectively.}$$

$$I_1 = \int_{y=0}^b \int_{x=0}^a |H|^2_{z=0,d} dx dy = \int_{y=0}^b \int_{x=0}^a \left(\frac{2\beta}{k_c} A\right)^2 \sin^2\left(\frac{\pi}{b}y\right) dx dy = \left(\frac{2bl}{d} A\right)^2 \frac{ab}{2}$$

$$I_2 = \int_{z=0}^d \int_{x=0}^a |H|^2_{y=0,b} dx dz = \int_{z=0}^d \int_{x=0}^a (2A)^2 \sin^2(\beta z) dx dz = (2A)^2 \frac{ad}{2}$$

$$\begin{aligned} I_3 &= \int_{z=0}^d \int_{y=0}^b |H|^2_{x=0,a} dy dz = \int_{z=0}^d \int_{y=0}^b \left(\frac{2\beta}{k_c} A\right)^2 \sin^2\left(\frac{\pi}{b}y\right) \cos^2(\beta z) + (2A)^2 \cos^2\left(\frac{\pi}{b}y\right) \sin^2(\beta z) dy dz \\ &= (2A)^2 \frac{bd}{4} \left(1 + \left(\frac{bl}{d}\right)^2\right) \end{aligned}$$

$$\therefore P_{loss} = R_s (A)^2 \left[ 2 \left(\frac{bl}{d}\right)^2 ab + bd + 2ad + \left(\frac{bl}{d}\right)^2 bd \right]$$



$$\therefore Q_{cond,01l} = \omega_{res} \frac{\frac{\epsilon}{2} \left( \frac{\omega \mu b}{\pi} A \right)^2 abd}{R_s \left[ 2 \left( \frac{bl}{d} \right)^2 ab + bd + 2ad + \left( \frac{bl}{d} \right)^2 bd \right]}$$

$$\therefore \frac{1}{Q_{total}} = \frac{1}{Q_{die}} + \frac{1}{Q_{cond}}$$

The fractional bandwidth is given by:

$$BW_{fractional} = \frac{\omega_2 - \omega_1}{\omega_o} = \frac{1}{Q_{total}}$$

**Program code:** (I used MATLAB R2021)

Run the “main” function via command window.

```
function main
clc;
clear;
close all;
format compact;

% cavity resonator dimensions in cm
global a;
global b;
global d;

% other cavity parameters
global epsilon_r; % relative permittivity
global sigma; % metal conductivity
global Q_die; % loss tangent at specific freq.

% epsilon_r = 2.5;
% sigma = 5.8*10^7;
% loss_tanget = 0.00004;
% Q_die = 1/loss_tanget;
% a = 0.05;
% b = 0.04;
% d = 0.07;

% get inputs from user
a = input("a (in cm)= ") * 10^-2;
b = input("b (in cm)= ") * 10^-2;
d = input("d (in cm)= ") * 10^-2;
epsilon_r = input("relative permeability e_r = ");
sigma = input("metal conductivity sigma = ");
Q_die = 1/input("loss_tanget tan(delta) = ");

% constants
global c_0;
global epsilon_0;
global u_0;

c_0 = 3*10^8;
epsilon_0 = 8.8542* 10^-12;
u_0 = 4*pi*10^-7;

f_res_dominant = resonance_freq(1,0,1); % ok<*NOPRT,*NASGU>
Q_dominant = Q_total_10l(1,2*pi*f_res_dominant);

r = sqrt( (3*(a^2)*(b^2))/(a^2-b^2));

if d > r % next mode is TE102
    f_res_next = resonance_freq(1,0,2);
    Q_next = Q_total_10l(2,2*pi*f_res_next);
else
    f_res_next = resonance_freq(0,1,1);
    Q_next = Q_total_01l(1,2*pi*f_res_next);
end

print_output(f_res_dominant,Q_dominant,f_res_next,Q_next,r);
end

function [f_resonance] = resonance_freq(m,n,l)

global a;
global b;
global d;
global epsilon_r;

c_0 = 3*10^8;
c = c_0/sqrt(epsilon_r);
kx = m*pi/a;
ky = n*pi/b;
beta = l*pi/d;
f_resonance = (c/(2*pi)) * sqrt(kx^2 + ky^2 +beta^2);
end
```

```
% TE101 , TE102
function [Q_10l] = Q_total_10l(1,w_res)
global a;
global b;
global d;
global epsilon_r;
global epsilon_0;
global u_0;
global sigma;
global Q_die;

k_c = pi/a;
R_s = sqrt( (w_res * u_0)/(2*sigma));
Q_num = w_res * (((epsilon_r*epsilon_0*a*b*d)/2) * ((w_res*u_0)/k_c)^2);
Q_den = R_s * (2*(((a^1)/d)^2)*a*b + 2*d*b + a*d + (((a^1)/d)^2)*a*d);

Q_cond_10l = Q_num/Q_den;
dummy = 1/Q_cond_10l + 1/Q_die;
Q_10l = 1/dummy;
end

% TE011
function [Q_01l] = Q_total_01l(1,w_res)

global a;
global b;
global d;
global epsilon_r;
global epsilon_0;
global u_0;
global sigma;
global Q_die;

R_s = sqrt( (w_res * u_0)/(2*sigma));
k_c = pi/b;

Q_num = w_res * (((epsilon_r*epsilon_0*a*b*d)/2) * ((w_res*u_0)/k_c)^2);
Q_den = R_s * (2*(((b^1)/d)^2)*a*b + 2*a*d + b*d + (((b^1)/d)^2)*b*d);
Q_cond_01l = Q_num/Q_den;

dummy = 1/Q_cond_01l + 1/Q_die;
Q_01l = 1/dummy;
end

function print_output(f_res_dominant,Q_dominant,f_res_next,Q_next,r)
global d;
if d > r
    next_mode = "TE102";
else
    next_mode = "TE011";
end

BW_dominant = 1/Q_dominant;
BW_next = 1/Q_next;

fprintf("\n===== \n");
fprintf("The dominant mode: TE101 \n");
fprintf("the 1st resonance frequency = %f GHz \n",f_res_dominant*10^-9);
fprintf("the quality factor Q (TE101) = %f \n",Q_dominant);
fprintf("the fractional bandwidth (TE101) = %e \n",BW_dominant);
fprintf("===== \n");
fprintf("The next mode: %s \n",next_mode);
fprintf("the 2nd resonance frequency = %f GHz \n",f_res_next*10^-9);
fprintf("the quality factor Q(%) = %f \n",next_mode,Q_next);
fprintf("the fractional bandwidth (%) = %e \n",next_mode,BW_next);
fprintf("===== \n");
end
```