# Differential Equations Coursework Aeroplane Landing Modelling

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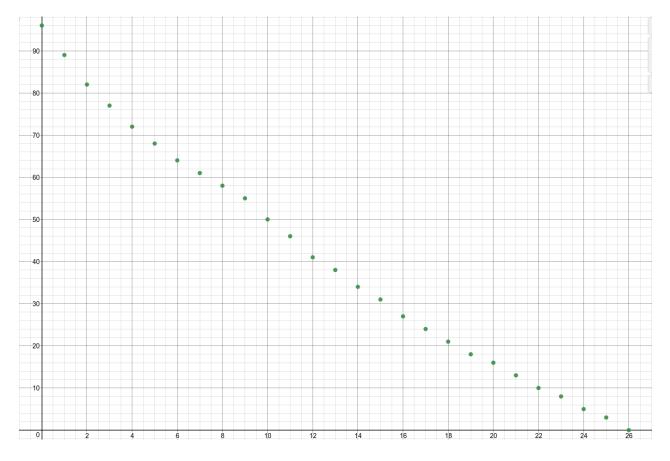
## 1 Simplifying situation and setting up the model

#### 1.1 Given data

I've been given data about a landing aeroplane after touchdown. The mass of the aeroplane is 120000 kg. Initially air resistance slows the aeroplane and then, when it is slow enough, wheel brakes add a constant force to fully stop the aeroplane. The table below shows the aeroplane's speed, v ms<sup>-1</sup>, t seconds after touchdown.

| t  | V  | t  | v  |
|----|----|----|----|
| 0  | 96 | 14 | 34 |
| 1  | 89 | 15 | 31 |
| 2  | 82 | 16 | 27 |
| 3  | 77 | 17 | 24 |
| 4  | 72 | 18 | 21 |
| 5  | 68 | 19 | 18 |
| 6  | 64 | 20 | 16 |
| 7  | 61 | 21 | 13 |
| 8  | 58 | 22 | 10 |
| 9  | 55 | 23 | 8  |
| 10 | 50 | 24 | 5  |
| 11 | 46 | 25 | 3  |
| 12 | 41 | 26 | 0  |
| 13 | 38 |    |    |

The image below shows a chart of the original data.



#### 1.2 Modeling assumptions

- The aeroplane can be modeled as a point particle. This assumption allows us to negate any complex resistances that would occur. Modeling this way is appropriate because we are not given velocity (only speed) of the aeroplane at different points in time, so we are not interested in any rotations of the plane.
- The runway can be modeled as a plane. Without this assumption we would need to consider the possibility that the runway has a complex shape, for example it can have hills and/or pits.
- The runway is horizontal. Without this assumption we would need to include components of the weight and the reaction force in the model which would increase the complexity of the model and affect the calculations.
- The aeroplane is moving in the horizontal plane. This assumption allows us to negate any vertical forces
- The constant force from the wheel brakes (after the brakes are applied) and the air resistance are the only forces acting on the aeroplane in the horizontal plane. This assumption allows us to say that any other resistance is negligible and there are no other forces, alternatively we can say that the air resistance model is a model of the total resistance force.
- The given values for speed are rounded to the nearest integer. This assumption allows the model of speed to have an error  $\pm 0.5$ . It's very unlikely that the values of speed are exactly integers, so it's a reasonable assumption.
- Brakes are applied at t = 9. The table below shows differences between consecutive speed values,  $\Delta v$ , and differences between consecutive differences,  $\Delta(\Delta v)$ .  $\Delta(\Delta v)$  is the lowest when t = 10. This means that the highest decrease of acceleration occurred between t = 9 and t = 10, hence we will assume that the brakes were applied during that time. We will model this as if the brakes were applied at t = 9.

| t  | V  | $\Delta$ v | $\Delta (\Delta v)$ | t  | V  | $\Delta$ v | $\Delta (\Delta v)$ |
|----|----|------------|---------------------|----|----|------------|---------------------|
| 0  | 96 |            |                     | 14 | 34 | -4         | -1                  |
| 1  | 89 | -7         |                     | 15 | 31 | -3         | 1                   |
| 2  | 82 | -7         | 0                   | 16 | 27 | -4         | -1                  |
| 3  | 77 | -5         | 2                   | 17 | 24 | -3         | 1                   |
| 4  | 72 | -5         | 0                   | 18 | 21 | -3         | 0                   |
| 5  | 68 | -4         | 1                   | 19 | 18 | -3         | 0                   |
| 6  | 64 | -4         | 0                   | 20 | 16 | -2         | 1                   |
| 7  | 61 | -3         | 1                   | 21 | 13 | -3         | -1                  |
| 8  | 58 | -3         | 0                   | 22 | 10 | -3         | 0                   |
| 9  | 55 | -3         | 0                   | 23 | 8  | -2         | 1                   |
| 10 | 50 | -5         | -2                  | 24 | 5  | -3         | -1                  |
| 11 | 46 | -4         | 1                   | 25 | 3  | -2         | 1                   |
| 12 | 41 | -5         | -1                  | 26 | 0  | -3         | -1                  |
| 13 | 38 | -3         | 2                   |    |    |            |                     |

- Braking force starts working instantly. This assumption makes acceleration not continuous and simplifies the calculations.
- There is no wind. This allows us to assume that if the plane is not moving then there is no air resistance.

#### 1.3 Derivation of the initial model

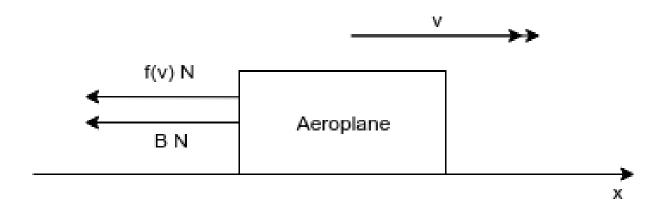


Figure 1: Forces diagram

The diagram shows the x-axis, direction of velocity, v, the air resistance, f(v), and the constant braking force (when brakes are used), B.

$$F = ma \text{ (Newton's second law)}$$

$$F = \begin{cases} -f(v), & 0 \le t < 9 \\ -f(v) - B, & 9 \le t \le 26 \end{cases}$$

$$a = \dot{v}$$

$$\Rightarrow \begin{cases} m\dot{v} = -f(v), & t < 9 \\ m\dot{v} = -f(v) - B, & t \ge 9 \end{cases}$$
where  $m = 120000$ 

#### 2 Model 1

#### 2.1 Defining f(v)

As you can see in the table with the differences, speed for  $t \in (0,9)$  clearly isn't decreasing linearly. And you can see that, as speed decreases (in that interval), the rate at which it decreases also decreases. So it's reasonable to suggest that

$$f(v) \propto v^{2}$$

$$\Rightarrow f(v) = kv^{2}$$

$$\Rightarrow m\dot{v} = \begin{cases} -kv^{2}, & 0 \le t < 9\\ -kv^{2} - B, & 9 \le t \le 26 \end{cases}$$

To make v continuous I will assume that both models are valid for t = 9.

$$m\dot{v} = \begin{cases} -kv^2, & 0 \le t \le 9\\ -kv^2 - B, & 9 \le t \le 26 \end{cases}$$

#### 2.2 General solution

## **2.2.1** $0 \le t \le 9$

$$m\dot{v} = -kv^{2}$$

$$\Rightarrow m\frac{\dot{v}}{v^{2}} = -k$$

$$\Rightarrow m\int \frac{\dot{v}}{v^{2}}dt = -k\int dt$$

$$\Rightarrow m\int v^{-2}dv = -kt + c_{1}$$

$$\Rightarrow m\frac{v^{-1}}{-1} = -kt + c_{1}$$

$$\Rightarrow \frac{-m}{v} = -kt + c_{1}$$

$$\Rightarrow v = \frac{m}{kt - c_{1}}$$

#### $\textbf{2.2.2} \quad 9 \leq t \leq \textbf{26}$

$$m\dot{v} = -kv^2 - B$$

$$m\frac{\dot{v}}{kv^2 + B} = -1$$

$$m\int \frac{\dot{v}}{kv^2 + B}dt = -\int dt$$

$$m\int \frac{1}{kv^2 + B}dv = -\int dt$$

$$\arctan'(\psi) = \frac{1}{\psi^2 + 1}$$

$$\Rightarrow \arctan'(\frac{a}{b}\psi) = \frac{a}{b} \times \frac{1}{(\frac{a}{b}\psi)^2 + 1} = \frac{a}{b} \times \frac{b^2}{a^2\psi^2 + b^2} = \frac{ab}{a^2\psi^2 + b^2}$$

$$\Rightarrow \arctan'(\sqrt{\frac{a}{b}}\psi) = \frac{\sqrt{ab}}{a\psi^2 + b}$$

$$\Rightarrow \int \frac{1}{kv^2 + B}dv = \frac{1}{\sqrt{kB}}\int \frac{\sqrt{kB}}{kv^2 + B} = \frac{\arctan(\sqrt{\frac{k}{B}}v)}{\sqrt{kB}} + c$$

$$\Rightarrow \frac{m\arctan(\sqrt{\frac{k}{B}}v)}{\sqrt{kB}} = -t + c$$

$$\Rightarrow \sqrt{\frac{k}{B}}v = \tan\frac{\sqrt{kB}(-t + c)}{m}$$

$$\Rightarrow v = \sqrt{\frac{B}{k}}\tan\frac{\sqrt{kB}(-t + c)}{m}$$
Let  $c_2 = \sqrt{kB}c$ 

$$\Rightarrow v = \sqrt{\frac{B}{k}} \tan(\frac{c_2 - \sqrt{kB}t}{m})$$

$$\Rightarrow v = \begin{cases} \frac{m}{kt - c_1}, & 0 \le t \le 9\\ \sqrt{\frac{B}{k}} \tan(\frac{c_2 - \sqrt{kB}t}{m}), & 9 \le t \le 26 \end{cases}$$

#### 2.3 Particular solution

The general solution has 4 unknown constants: the constant braking force, B, the coefficient from the air resistance model, k, and 2 constants of integration from solving the 2 differential equations,  $c_1$  and  $c_2$ . To make v continuous I will use point (t = 9, v = 55).

$$\begin{cases} \frac{m}{9k - c_1} = 55\\ \sqrt{\frac{B}{k}} \tan \frac{c_2 - 9\sqrt{kB}}{m} = 55 \end{cases}$$
$$\Rightarrow 9k - c_1 = \frac{m}{55}$$
$$\Rightarrow k = \frac{c_1 + \frac{m}{55}}{9}$$

S is the set of given data.

$$(t_1, v_1), (t_2, v_2) \in S; t_1, t_2 \leq 9, t_1 \neq t_2$$

$$\begin{cases} v_1 = \frac{m}{t_1 k - c_1} \\ v_2 = \frac{m}{t_2 k - c_1} \end{cases}$$

$$\Rightarrow \begin{cases} v_1 v_2 t_2 t_1 k - v_1 v_2 t_2 c_1 = m v_2 t_2 \\ v_1 v_2 t_1 t_2 k - v_1 v_2 t_1 c_1 = m v_1 t_1 \end{cases}$$

$$\Rightarrow c_1 v_1 v_2 (t_2 - t_1) = m(v_1 t_1 - v_2 t_2)$$

$$\Rightarrow c_1 = \frac{m(v_1 t_1 - v_2 t_2)}{v_1 v_2 (t_2 - t_1)}$$

$$\sqrt{\frac{B}{k}} \tan \frac{c_2 - 9\sqrt{kB}}{m} = 55$$

$$\Rightarrow c_2(B) = m \arctan(\frac{55k\sqrt{\frac{B}{k}}}{B}) + 9\sqrt{Bk}$$

$$(t_3, v_3) \in S; t_3 > 9$$

$$\Rightarrow v_3 = \sqrt{\frac{B}{k}} \tan \frac{c_2(B) - \sqrt{kB}t_3}{m}$$

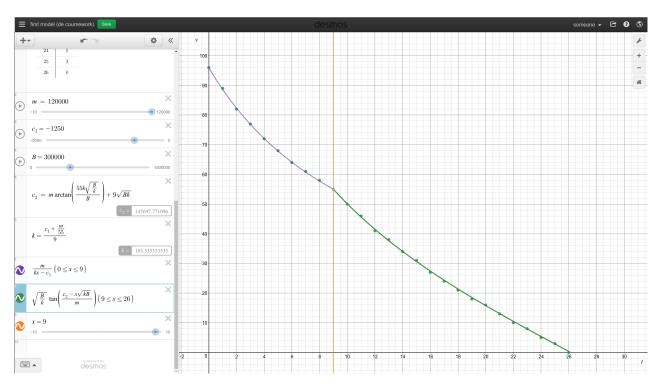
$$\Rightarrow \arctan(v_3\sqrt{\frac{k}{B}}) = \frac{c_2(B) - \sqrt{kB}t_3}{m}$$

$$\Rightarrow \arctan(v_3\sqrt{\frac{k}{B}}) = \frac{c_2(B) - \sqrt{kB}t_3}{m}$$
Let  $\lambda(B) = \frac{c_2(B) - \sqrt{kB}t_3}{m} - \arctan(v_3\sqrt{\frac{k}{B}})$ 
Newton-Raphson's rule:  $B_{n+1} = B_n + \frac{\lambda'(B_n)}{\lambda(B_n)}$ 

$$\begin{cases} c_{1} = \frac{m(v_{1}t_{1} - v_{2}t_{2})}{v_{1}v_{2}(t_{2} - t_{1})} \\ k = \frac{c_{1} + \frac{m}{55}}{9} \end{cases} \\ c_{2}(B) = m \arctan(\frac{55k\sqrt{\frac{B}{k}}}{B}) + 9\sqrt{Bk} \\ \lambda(B) = \frac{c_{2}(B) - \sqrt{kB}t_{3}}{m} - \arctan(v_{3}\sqrt{\frac{k}{B}}) \\ B_{n+1} = B_{n} - \frac{\lambda(B_{n})}{\lambda'(B_{n})}B_{0} = 300000 \end{cases}$$

$$(1)$$

To find  $B_0$  I used a graphing web app. First I put in all the formulas and given data points.  $v(0) = \frac{m}{-c_1} > 0$ , hence  $c_1 < 0$ . I started decreasing  $c_1$  until it roughly matched first 10 points. B > 0, so for this value of  $c_1$  I started increasing B until I found that  $B \approx 300,000$ .



Now I can use programming to find the parameters. To do this I wrote 5 modules in Haskell. The first module is a module for automatic differentiation using dual numbers and Newton-Raphson method.

```
module AutoDiff where
import Data.Matrix
import Data.Vector (Vector)
import qualified Data.Vector as V

data Dual a =
    Dual { val :: a
        , diff :: a
        , deriving (Eq, Show)

constDual :: Num a => a -> Dual a
    constDual x = Dual x 0

-- to use we put Dual (f x) (f' x). Eg if using "x", then write Dual x 1, cause dx/dx = 1
```

```
instance Num a => Num (Dual a) where
    (Dual u u') + (Dual v v') = Dual (u + v) (u' + v')
    (Dual u u') - (Dual v v') = Dual (u - v) (u' - v')
    (Dual \ u \ u') * (Dual \ v \ v') = Dual \ (u * v) \ (u' * v + u * v')
    abs (Dual u u') = Dual (abs u) (u' * signum u)
    signum (Dual u u') = Dual (signum u) 0
    fromInteger n = Dual (fromInteger n) 0
instance Fractional a => Fractional (Dual a) where
    (Dual \ u \ u') / (Dual \ v \ v') = Dual \ (u / v) ((u' * v - u * v') / v^2)
    fromRational q = Dual (fromRational q) 0
instance (Eq a, Floating a) => Floating (Dual a) where
                      = Dual pi
    рi
          (Dual u u') = Dual (exp u)
                                       (u' * exp u)
    exp
          (Dual u u') = Dual (log u)
                                       (u' / u)
    log
    sqrt (Dual u u') = Dual (sqrt u)
                                       (u' / (2 * sqrt u))
          (Dual u u') = Dual (sin u)
                                        (u' * cos u)
    sin
          (Dual u u') = Dual (cos u)
                                       (-1 * u' * \sin u)
    COS
          (Dual u u') = Dual (tan u)
                                       (u' / (cos u ** 2))
    tan
    asin (Dual u u') = Dual (asin u) (u' / sqrt(1 - (u ** 2)))
    acos (Dual u u') = Dual (acos u)
                                       ((-1) * u' / sqrt(1 - (u ** 2)))
                                       (u' / (1 + (u ** 2)))
    atan (Dual u u') = Dual (atan u)
    sinh (Dual u u') = Dual (sinh u)
                                       (u' * cosh u)
    cosh (Dual u u') = Dual (cosh u) (u' * sinh u)
    tanh (Dual u u') = Dual (tanh u) (u' * (1 - (tanh u ** 2)))
    asinh (Dual u u') = Dual (asinh u) (u' / sqrt(1 + (u ** 2)))
    acosh (Dual u u') = Dual (acosh u) (u' / (sqrt((u ** 2) - 1)))
    atanh (Dual u u') = Dual (atanh u) (u' / (1 - (u ** 2)))
    (Dual u u') ** (Dual n 0)
                                    = Dual (u ** n) (u' * n * u ** (n - 1))
    (Dual a 0) ** (Dual v v')
                                    = Dual (a ** v) (v' * log a * a ** v)
    (Dual \ u \ u') ** (Dual \ v \ v') = Dual (u ** v) ((u ** v) * (v' * log u + (v * u' / u)))
    logBase (Dual u u') (Dual v v') =
        Dual (logBase u v) ((log v * u' / u - log u * v' / v) / (log u ** 2))
instance Ord a => Ord (Dual a) where
    (Dual x _) \le (Dual y _) = x \le y
instance (Enum a, Num a) => Enum (Dual a) where
    toEnum n = constDual \$ toEnum n
    fromEnum (Dual x _) = fromEnum x
d :: (Num a, Num c) => (Dual a -> Dual c) -> a -> c
d f x = diff . f $ Dual x 1
toNormalF :: (Num a, Num b) => (Dual a -> Dual b) -> a -> b
toNormalF f = val . f . constDual
```

```
newton :: (Fractional a, Ord a) => (Dual a -> Dual a) -> Either Integer (a -> Bool) -> a -> a
newton f stop y = newtonHelper stop y y
  where newtonHelper stopCond minX x
          | either (== 0) ($ x) stopCond = if minCheck then x else minX
          | otherwise = newtonHelper (either (Left . (n \rightarrow n - 1)) (const stopCond) stopCond)
                                      (if minCheck then x else minX)
                                      nextX
          where nextX = x - toNormalF f x / d f x
                minCheck = abs (toNormalF f x) < abs (toNormalF f minX)</pre>
   The second module contains the given data.
{-# LANGUAGE RecordWildCards #-}
module GivenData where
import
                 AutoDiff
import
                 Data.Vector (Vector)
import qualified Data. Vector as V
vs :: Num a => [a]
vs = [96,89,82,77,72,68,64,61,58,55,50,46,41,38,34,31,27,24,21,18,16,13,10,8,5,3,0]
data Point a =
    Point { pTime :: a
          , pSpeed :: a
          } deriving (Show, Eq)
points :: (Num a, Enum a) => [Point a]
points = zipWith Point [0..26] vs
vectorPoints :: (Num a, Enum a) => Vector (Point a)
vectorPoints = V.fromList points
m :: Num a => a
m = 120000
toDualPoint :: Num a => Point a -> Point (Dual a)
toDualPoint Point{..} = Point (constDual pTime) (constDual pSpeed)
```

Then I defined a general interface for models.

```
{-# LANGUAGE TypeFamilies #-}
module Solution. Model where
import
                 Data.Proxy
class ModelParams f where
    type SolutionGen f :: * -> *
    predict :: f Double -> Double -> Double
    findParams :: (Floating a, Ord a, Enum a) => SolutionGen f a -> f a
    combinations :: (Num a, Enum a, Eq a) => Proxy f -> [SolutionGen f a]
   The fourth module is for the first model and finding parameters.
{-# LANGUAGE RecordWildCards #-}
{-# LANGUAGE TypeFamilies
module Solution.First (Parameters, SolutionGen) where
import
                 Data.Proxy
import
                 AutoDiff
import
                 GivenData
import qualified Solution. Model as M
data Parameters a =
   Parameters { pC1 :: a
               , pK :: a
               , pC2 :: a
               , pB :: a
               , pGen :: SolutionGen a
data SolutionGen a =
    SolutionGen { sgPoint1 :: Point a
                , sgPoint2 :: Point a
                , sgPoint3 :: Point a
                }
instance Show a => Show (SolutionGen a) where
    show SolutionGen{..} =
         ", p1 = (" ++ show (pTime sgPoint1) ++ ", " ++ show (pSpeed sgPoint1) ++ ")"
     ++ ", p2 = (" ++ show (pTime sgPoint2) ++ ", " ++ show (pSpeed sgPoint2) ++ ")"
     ++ ", p3 = (" ++ show (pTime sgPoint3) ++ ", " ++ show (pSpeed sgPoint3) ++ ")"
```

```
instance Show a => Show (Parameters a) where
    show Parameters{..} = "c1 = " ++ show pC1
                       ++ ", k = " ++ show pK
                       ++ ", c2 = " ++ show pC2
                       ++ ", b = " ++ show pB
                       ++ show pGen
                       ++ "\n"
c1F :: Fractional a => Point a -> Point a -> a
c1F (Point t1 v1) (Point t2 v2) = m * (v1 * t1 - v2 * t2) / (v1 * v2 * (t2 - t1))
kF :: Fractional a => a -> a
kF c1 = (c1 + m / 55) / 9
c2F :: Floating a \Rightarrow a \rightarrow a \rightarrow a
c2F \ k \ b = m * atan (55 * k * sqrt (b / k) / b) + 9 * sqrt (b * k)
lambda :: Floating a => Point a -> a -> a
lambda (Point t3 v3) k b = (c2F k b - sqrt (k * b) * t3) / m - atan (v3 * sqrt (k / b))
findParams :: (Floating a, Ord a) => SolutionGen a -> Parameters a
findParams gen@SolutionGen{..} = parameters
  where parameters =
          Parameters { pC1 = c1F sgPoint1 sgPoint2
                     , pK = kF \  pC1 parameters
                      , pC2 = c2F (pK parameters) (pB parameters)
                      , pB = newton (lambda (toDualPoint sgPoint3) (constDual $ pK parameters))
                                     (Right $ (<= 0.0001) . abs . lambda sgPoint3 (pK parameters))
                                     300000
                      , pGen = gen
predict :: Parameters Double -> Double -> Double
predict Parameters{..} t
  | 0 \le t \&\& t \le 9 = m / (pK * t - pC1)
  | 9 < t \&\& t <= 26 = sqrt (pB / pK) * tan ((pC2 - sqrt (pK * pB) * t) / m)
  | otherwise = error "Invalid time!"
combinations :: (Enum a, Num a, Eq a) => [SolutionGen a]
combinations = zipWith (flip $ uncurry SolutionGen) (drop 10 points)
             $ filter (uncurry (/=))
             $ (\l -> [ (p1, p2) | p1 <- 1, p2 <- 1 ])
             $ take 10 points
instance M.ModelParams Parameters where
    type SolutionGen Parameters = SolutionGen
    predict = predict
    findParams = findParams
    combinations Proxy = combinations
```

And finally the main module, which runs this code to find the parameters.

```
import
                Data.List
                               (sort, sortOn)
import
                Data.Proxy
import
                GivenData
import qualified Solution. First as Sol
                Solution. Model as Model
import
adjustLength :: (a -> String) -> (a -> String -> b) -> [a] -> [b]
adjustLength g s l =
  (\x -> let str = g x in s x $ str ++ replicate (longest - length str) ' ') <$> 1
  where longest = maximum $ length . g <$> 1
showPredictions :: (ModelParams f, Show (f Double)) => f Double -> String
showPredictions params =
  foldMap ((x, y, z, w) \rightarrow "| " ++ x ++ " | " ++ y ++ " | " ++ z ++ " | " ++ w ++ " | n")
     $ adjustLength (\(_, _, z, _) -> z) (\(x, y, _, w) z -> (x, y, z, w))
    \ adjustLength (\(x, _, _, _) -> x) (\(_, y, z, w) x -> (x, y, z, w))
    $ (("Time", "Predicted Speed", "Rounded predicted speed", "Observed Speed"):)
    (\ensuremath{(Point\ t\ v)} \rightarrow let\ v' = predict\ params\ t\ in\ (show\ t,\ show\ v',\ rounded\ v')
    <$> points
  where rounded = show . round
maxErr :: (a -> Double -> Double) -> a -> Double
maxErr predict params =
  maximum $ abs . (\(Point t v) -> predict params t - v) <$> points
  where n = fromIntegral (length points)
avrErr :: (a -> Double -> Double) -> a -> Double
avrErr predict params =
  (/ n)  sum   abs . ((Point t v) -> predict params t - v) < points 
  where n = fromIntegral (length points)
rms :: (a -> Double -> Double) -> a -> Double
rms predict params =
  (/ n)  sqrt   (^2)  . ((Point t v) -> predict params t - v) <> points )
  where n = fromIntegral (length points)
showErrors :: (ModelParams f, Show (f Double)) => f Double -> String
showErrors params =
  foldMap (\(x, y, z) -> "| " ++ x ++ " | " ++ y ++ " | " ++ z ++ " |\n")
  \ adjustLength (\((_, _, z) -> z) (\((x, y, _) z -> (x, y, z))
  \ adjustLength (\(\(\(\)\_\, \, \) -> \(\)\ (\(\(\)\, \, \, \, z) \(\) y -> \(\(\)\, \(\)\, \(\)\)
  $ adjustLength (\(x, _, _) \rightarrow x) (\(_, y, z) x \rightarrow (x, y, z)) 
  [ ("Maximum Error", "Average Error", "Root mean square")
  , (show $ maxErr predict params, show $ avrErr predict params, show $ rms predict params)
  ٦
```

Here is the result. It shows the best and the worst parameters found using the derived formulas and for both of the configurations it shows sums of squares of errors, and predictions for each of the given point with rounded versions.

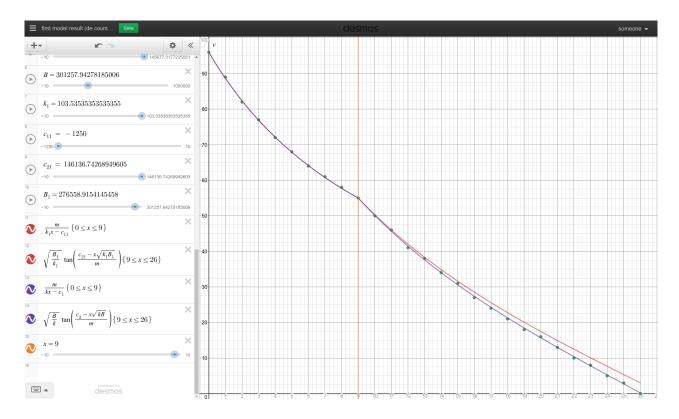
```
:h ⇒ optimizer → stack exec optimizer-exe
c1 = -1250.0, k = 103.535353535353555, c2 = 145677.3177225051, b = 301257.94278185006, p1 = (0.0, 96.0), p2 = (5.0, 68.0), p3 = (14.0, 34.0)
 Maximum Error | Average Error | Root mean square | 0.47598886269637575 | 0.23822424753496707 | 0.2776875104911393 |
                                    | Rounded predicted speed | Observed Speed
          Predicted Speed
          96.0
88.65671641791045
                                                                     89
82
77
72
68
64
61
58
55
50
46
41
38
31
1 27
21
1 18
1 16
1 18
1 5
1 10
1 8
                                      89
           82.35701906412478
           76.89320388349515
                                      77
72
           72.1092564491654
          67.88571428571429
64.12955465587045
           60.767263427109974
           57.739975698663415
                                      58
           50.10816658852111
                                      50
           45.62206303621237
          41.475988862696376
37.61659930730753
           34.00002062308155
           30.589724513917773
           27.35493651754378
           24.269426053394415
           18.45863841578133
           15.696183121094782
           13.00760227741885
           10.378741615250261
           7.796577949697343
5.248946558956161
          0.2115083630415522 | 0
The worst result:
c1 = -1250.0, k = 103.53535353535355, c2 = 146136.74268949605, b = 276558.9154145458, p1 = (0.0, 96.0), p2 = (2.0, 82.0), p3 = (11.0, 46.0)
  Maximum Error | Average Error | Root mean square
3.0224756774093864 | 1.0279882781712646 | 1.4042237215181517
  Maximum Error
```

## 2.4 Graphs and Analysis

| Speed   Speed   Predicted   Speed   Speed | Time                    | Predicted               | Rounded | Observed |
|---|-------------------------|-------------------------|---------|----------|
| 0.0         96.0         96         96           1.0         88.65671641791045         89         89           2.0         82.35701906412478         82         82           3.0         76.89320388349515         77         77           4.0         72.1092564491654         72         72           5.0         67.88571428571429         68         68           6.0         64.12955465587045         64         64           7.0         60.767263427109974         61         61           8.0         57.739975698663415         58         58           9.0         54.99999999999999         55         55           10.0         50.10816658852111         50         50           11.0         45.622063036212374         46         46           12.0         41.475988862696376         41         41           13.0         37.61659930730753         38         38           14.0         34.00002062308155         34         34           15.0         30.589724513917773         31         31           16.0         27.35493651754378         27         27           17.0         24.269426053394415         24  | 1 ime                   |                         |         |          |
| 0.0       96.0       96       96         1.0       88.65671641791045       89       89         2.0       82.35701906412478       82       82         3.0       76.89320388349515       77       77         4.0       72.1092564491654       72       72         5.0       67.88571428571429       68       68         6.0       64.12955465587045       64       64         7.0       60.767263427109974       61       61         8.0       57.739975698663415       58       58         9.0       54.99999999999999       55       55         10.0       50.10816658852111       50       50         11.0       45.622063036212374       46       46         12.0       41.475988862696376       41       41         13.0       37.61659930730753       38       38         14.0       34.00002062308155       34       34         15.0       30.589724513917773       31       31         16.0       27.35493651754378       27       27         17.0       24.269426053394415       24       24         18.0       21.3105731783461       21       21   |                         | Speed                   |         | Speed    |
| 1.0     88.65671641791045     89     89       2.0     82.35701906412478     82     82       3.0     76.89320388349515     77     77       4.0     72.1092564491654     72     72       5.0     67.88571428571429     68     68       6.0     64.12955465587045     64     64       7.0     60.767263427109974     61     61       8.0     57.739975698663415     58     58       9.0     54.99999999999999     55     55       10.0     50.10816658852111     50     50       11.0     45.622063036212374     46     46       12.0     41.475988862696376     41     41       13.0     37.61659930730753     38     38       14.0     34.00002062308155     34     34       15.0     30.589724513917773     31     31       16.0     27.35493651754378     27     27       17.0     24.269426053394415     24     24       18.0     21.3105731783461     21     21       19.0     18.45863841578133     18     18       20.0     15.696183121094782     16     16       21.0     13.00760227741885     13     13       22.0 <td< td=""><td>0.0</td><td>00.0</td><td>•</td><td>0.0</td></td<>  | 0.0                     | 00.0                    | •       | 0.0      |
| 2.0       82.35701906412478       82       82         3.0       76.89320388349515       77       77         4.0       72.1092564491654       72       72         5.0       67.88571428571429       68       68         6.0       64.12955465587045       64       64         7.0       60.767263427109974       61       61         8.0       57.739975698663415       58       58         9.0       54.9999999999999       55       55         10.0       50.10816658852111       50       50         11.0       45.622063036212374       46       46         12.0       41.475988862696376       41       41         13.0       37.61659930730753       38       38         14.0       34.00002062308155       34       34         15.0       30.589724513917773       31       31         16.0       27.35493651754378       27       27         17.0       24.269426053394415       24       24         18.0       21.3105731783461       21       21         19.0       18.45863841578133       18       18         20.0       15.696183121094782       16       16 </td <td></td> <td></td> <td></td> <td></td>   |                         |                         |         |          |
| $\begin{array}{cccccccccccccccccccccccccccccccccccc$  |                         |                         |         |          |
| $\begin{array}{cccccccccccccccccccccccccccccccccccc$  |                         |                         |         |          |
| 5.0       67.88571428571429       68       68         6.0       64.12955465587045       64       64         7.0       60.767263427109974       61       61         8.0       57.739975698663415       58       58         9.0       54.9999999999999       55       55         10.0       50.10816658852111       50       50         11.0       45.622063036212374       46       46         12.0       41.475988862696376       41       41         13.0       37.61659930730753       38       38         14.0       34.00002062308155       34       34         15.0       30.589724513917773       31       31         16.0       27.35493651754378       27       27         17.0       24.269426053394415       24       24         18.0       21.3105731783461       21       21         19.0       18.45863841578133       18       18         20.0       15.696183121094782       16       16         21.0       13.00760227741885       13       13         22.0       10.378741615250261       10       10         23.0       7.796577949697343       8   |                         |                         |         |          |
| 6.0       64.12955465587045       64       64         7.0       60.767263427109974       61       61         8.0       57.739975698663415       58       58         9.0       54.99999999999999       55       55         10.0       50.10816658852111       50       50         11.0       45.622063036212374       46       46         12.0       41.475988862696376       41       41         13.0       37.61659930730753       38       38         14.0       34.00002062308155       34       34         15.0       30.589724513917773       31       31         16.0       27.35493651754378       27       27         17.0       24.269426053394415       24       24         18.0       21.3105731783461       21       21         19.0       18.45863841578133       18       18         20.0       15.696183121094782       16       16         21.0       13.00760227741885       13       13         22.0       10.378741615250261       10       10         23.0       7.796577949697343       8       8         24.0       5.248946558956161       5   |                         |                         |         |          |
| $\begin{array}{cccccccccccccccccccccccccccccccccccc$  |                         |                         |         |          |
| 8.0     57.739975698663415     58     58       9.0     54.99999999999999     55     55       10.0     50.10816658852111     50     50       11.0     45.622063036212374     46     46       12.0     41.475988862696376     41     41       13.0     37.61659930730753     38     38       14.0     34.00002062308155     34     34       15.0     30.589724513917773     31     31       16.0     27.35493651754378     27     27       17.0     24.269426053394415     24     24       18.0     21.3105731783461     21     21       19.0     18.45863841578133     18     18       20.0     15.696183121094782     16     16       21.0     13.00760227741885     13     13       22.0     10.378741615250261     10     10       23.0     7.796577949697343     8     8       24.0     5.248946558956161     5     5       25.0     2.7243028986249413     3     3  |                         |                         |         |          |
| 9.0     54.999999999999999999999999999999999999   | 7.0                     | 60.767263427109974      | 61      | 61       |
| $\begin{array}{c ccccccccccccccccccccccccccccccccccc$   | 8.0                     | 57.739975698663415      | 58      | 58       |
| 11.0       45.622063036212374       46       46         12.0       41.475988862696376       41       41         13.0       37.61659930730753       38       38         14.0       34.00002062308155       34       34         15.0       30.589724513917773       31       31         16.0       27.35493651754378       27       27         17.0       24.269426053394415       24       24         18.0       21.3105731783461       21       21         19.0       18.45863841578133       18       18         20.0       15.696183121094782       16       16         21.0       13.00760227741885       13       13         22.0       10.378741615250261       10       10         23.0       7.796577949697343       8       8         24.0       5.248946558956161       5       5         25.0       2.7243028986249413       3       3  | 9.0                     | 54.9999999999999        | 55      | 55       |
| $\begin{array}{cccccccccccccccccccccccccccccccccccc$  | 10.0                    | 50.10816658852111       | 50      | 50       |
| $\begin{array}{cccccccccccccccccccccccccccccccccccc$  | 11.0 45.622063036212374 |                         | 46      | 46       |
| $\begin{array}{cccccccccccccccccccccccccccccccccccc$  | 12.0                    | 12.0 41.475988862696376 |         | 41       |
| 15.0     30.589724513917773     31     31       16.0     27.35493651754378     27     27       17.0     24.269426053394415     24     24       18.0     21.3105731783461     21     21       19.0     18.45863841578133     18     18       20.0     15.696183121094782     16     16       21.0     13.00760227741885     13     13       22.0     10.378741615250261     10     10       23.0     7.796577949697343     8     8       24.0     5.248946558956161     5     5       25.0     2.7243028986249413     3     3  | 13.0                    |                         |         | 38       |
| 16.0     27.35493651754378     27     27       17.0     24.269426053394415     24     24       18.0     21.3105731783461     21     21       19.0     18.45863841578133     18     18       20.0     15.696183121094782     16     16       21.0     13.00760227741885     13     13       22.0     10.378741615250261     10     10       23.0     7.796577949697343     8     8       24.0     5.248946558956161     5     5       25.0     2.7243028986249413     3     3  | 14.0                    | 14.0 34.00002062308155  |         | 34       |
| 17.0     24.269426053394415     24     24       18.0     21.3105731783461     21     21       19.0     18.45863841578133     18     18       20.0     15.696183121094782     16     16       21.0     13.00760227741885     13     13       22.0     10.378741615250261     10     10       23.0     7.796577949697343     8     8       24.0     5.248946558956161     5     5       25.0     2.7243028986249413     3     3   | 15.0                    | 15.0 30.589724513917773 |         | 31       |
| 18.0     21.3105731783461     21     21       19.0     18.45863841578133     18     18       20.0     15.696183121094782     16     16       21.0     13.00760227741885     13     13       22.0     10.378741615250261     10     10       23.0     7.796577949697343     8     8       24.0     5.248946558956161     5     5       25.0     2.7243028986249413     3     3   | 16.0                    | 16.0 27.35493651754378  |         | 27       |
| 19.0     18.45863841578133     18     18       20.0     15.696183121094782     16     16       21.0     13.00760227741885     13     13       22.0     10.378741615250261     10     10       23.0     7.796577949697343     8     8       24.0     5.248946558956161     5     5       25.0     2.7243028986249413     3     3   | 17.0                    | 24.269426053394415      | 24      | 24       |
| 20.0     15.696183121094782     16     16       21.0     13.00760227741885     13     13       22.0     10.378741615250261     10     10       23.0     7.796577949697343     8     8       24.0     5.248946558956161     5     5       25.0     2.7243028986249413     3     3  | 18.0                    | 21.3105731783461        | 21      | 21       |
| 21.0       13.00760227741885       13       13         22.0       10.378741615250261       10       10         23.0       7.796577949697343       8       8         24.0       5.248946558956161       5       5         25.0       2.7243028986249413       3       3  | 19.0                    | 18.45863841578133       | 18      | 18       |
| 22.0     10.378741615250261     10     10       23.0     7.796577949697343     8     8       24.0     5.248946558956161     5     5       25.0     2.7243028986249413     3     3   | 20.0                    | 15.696183121094782      | 16      | 16       |
| 22.0     10.378741615250261     10     10       23.0     7.796577949697343     8     8       24.0     5.248946558956161     5     5       25.0     2.7243028986249413     3     3   | 21.0                    |                         |         | 13       |
| 23.0       7.796577949697343       8       8         24.0       5.248946558956161       5       5         25.0       2.7243028986249413       3       3   | 22.0                    |                         |         | 10       |
| 24.0       5.248946558956161       5       5         25.0       2.7243028986249413       3       3  | 23.0                    |                         |         | 8        |
| 25.0 2.7243028986249413 3 3   |                         |                         |         |          |
|   |                         |                         |         |          |
|   |                         |                         |         |          |

| Maximum Error       | Average Error       | Root mean square   |
|---------------------|---------------------|--------------------|
| 0.47598886269637575 | 0.23822424753496707 | 0.2776875104911393 |

I'll now look at the two configurations that I obtained and plot them. The red line shows the worst configuration, and the purple line shows the best configuration.



As you can see in 2.3 rounded predictions of the best configuration exactly match the given data.

#### 2.5 Conclusion of Model 1

$$\begin{cases} v(t) = \frac{m}{kt - c_1}, & 0 \le t \le 9 \\ v(t) = \sqrt{\frac{B}{k}} \tan(\frac{c_2 - \sqrt{kB}t}{m}), & 9 \le t \le 26 \end{cases}$$

$$c_1 = -1250.0$$

$$k = 103.\dot{5}\dot{3}$$

$$c_2 = 145677.3177225051$$

$$B = 301257.94278185006$$

$$x = \int_0^{26} v dt = \int_0^9 v dt + \int_9^{26} v dt$$

$$\int \frac{m}{kt - c_1} dt = \frac{m}{k} \int \frac{k}{kt - c_1} dt = \frac{m}{k} \ln(kt - c_1) + \text{constant}$$

$$\int \sqrt{\frac{B}{k}} \tan(\frac{c_2 - \sqrt{kB}t}{m}) dt = \sqrt{\frac{B}{k}} \times \frac{-m}{\sqrt{kB}} \int \tan(\frac{c_2 - \sqrt{kB}t}{m}) \times \frac{-\sqrt{kB}}{m} dt =$$

$$= \frac{m}{k} \int \frac{-\sin(u)}{\cos u} du = \frac{m}{k} \ln(\cos(\frac{c_2 - \sqrt{kB}t}{m})) + \text{constant}$$

$$\Rightarrow x = \left[\frac{m}{k} \ln(kt - c_1)\right]_0^9 + \left[\frac{m}{k} \ln(\cos(\frac{c_2 - \sqrt{kB}t}{m}))\right]_0^{26} = \frac{m}{k} \left(\ln(\frac{c_1 - 9k}{c_1}) + \ln(\frac{\cos(\frac{c_2 - 26\sqrt{kB}}{m})}{\cos(\frac{c_2 - 9\sqrt{kB}}{m})})\right)$$

$$\Rightarrow x = \frac{m}{k} \ln\left(\frac{(c_1 - 9k)\cos(\frac{c_2 - 26\sqrt{kB}}{m})}{c_1\cos(\frac{c_2 - 9\sqrt{kB}}{m})}\right)$$

```
A.glob::home-arch ⇒ optimizer → ghci

optimizer-0.1.0.0: initial-build-steps (lib + exe)

The following GHC options are incompatible with GHCi and have not been passed to it: -threaded -02

Configuring GHCi with the following packages: optimizer

Using main module: 1. Package 'optimizer' component exe:optimizer-exe with main-is file: /media/storage/drive/maths/de_coursework/optimizer/app/Main.hs

GHCi, version 8.2.2: http://www.haskell.org/ghc/ :? for help

Loaded GHCi configuration from /home/gleb/.ghci

[1 of 5] Compiling AutoDiff (/media/storage/drive/maths/de_coursework/optimizer/src/GivenData.hs, interpreted)

[3 of 5] Compiling FirstModel (/media/storage/drive/maths/de_coursework/optimizer/src/FirstModel.hs, interpreted)

[4 of 5] Compiling FirstModel (/media/storage/drive/maths/de_coursework/optimizer/src/FirstModel.hs, interpreted)

[5 of 5] Compiling SecondModel (/media/storage/drive/maths/de_coursework/optimizer/spc/FirstModel.hs, interpreted)

[6 of 5] Compiling SecondModel (/media/storage/drive/maths/de_coursework/optimizer/spc/FirstModel.hs, interpreted)

[6 of 5] Compiling SecondModel (/media/storage/drive/maths/de_coursework/optimizer/spc/SecondModel.hs, interpreted)

[7 of 5] Compiling SecondModel (/media/storage/drive/maths/de_coursework/optimizer/spc/SecondModel.hs, interpreted)

[8 of 5] Compiling SecondModel (/media/storage/drive/maths/de_coursework/optimizer/spc/SecondModel.hs, interpreted)

[9 of 5] Compiling Secon
```

$$\Rightarrow x \approx 1058.650842313513 \approx 1060$$

The aeroplane fully stops in approximately 1060 meters after touchdown, hence the runway has to be at least 1060 meters long. However, I would advise length of 2000 to be safe even if conditions change, for example in case touchdown occurs further, there is wind, friction between the wheels and the runway is lower.

#### 3 Model 2

#### 3.1 Redefining f(v)

Although the first model fits the given data very well, I think this model can be improved. This time I will add a linear term to the air resistance function.

$$f(v) = kv^{2} + \lambda v$$

$$\Rightarrow m\dot{v} = \begin{cases} -kv^{2} - \lambda v, & 0 \le t \le 9\\ -kv^{2} - \lambda v - B, & 9 \le t \le 26 \end{cases}$$

#### 3.2 General solution

#### 3.2.1 $0 \le t \le 9$

$$m\dot{v} = -kv^2 - \lambda v$$

$$\Rightarrow m \int \frac{1}{kv^2 + \lambda v} dv = -t + c_3$$

$$kv^2 + \lambda v \equiv v(kv + \lambda)$$

$$\frac{1}{v(kv + \lambda)} \equiv \frac{A}{v} + \frac{B}{kv + \lambda}$$

$$\Rightarrow 1 \equiv A(kv + \lambda) + Bv$$

$$\Rightarrow \begin{cases} A = \frac{1}{\lambda} \\ B = -\frac{k}{\lambda} \end{cases}$$

$$\Rightarrow \frac{1}{kv^2 + \lambda v} \equiv \frac{1}{\lambda v} - \frac{k}{k\lambda v + \lambda^2} (\equiv \frac{k\lambda v + \lambda^2 - k\lambda v}{\lambda v(k\lambda v + \lambda^2)} \equiv \frac{\lambda^2}{\lambda^2 (kv^2 + \lambda v)} \equiv \frac{1}{kv^2 + \lambda v})$$

$$\Rightarrow \int \frac{1}{kv^2 - \lambda v} dv = \frac{1}{\lambda} \int v^{-1} dv - \frac{1}{\lambda} \int \frac{k}{kv + \lambda} dv$$

$$\Rightarrow \frac{m}{\lambda} (\ln(v) - \ln(kv + \lambda)) = c_3 - t$$

$$\Rightarrow \ln(\frac{v}{kv+\lambda}) = \frac{\lambda}{m}(c_3 - t)$$

$$\Rightarrow \frac{v}{kv+\lambda} = e^{\frac{\lambda}{m}(c_3 - t)}$$

$$\Rightarrow v = ke^{\frac{\lambda}{m}(c_3 - t)}v + \lambda e^{\frac{\lambda}{m}(c_3 - t)}$$

$$v = \frac{\lambda e^{\frac{\lambda}{m}(c_3 - t)}}{1 - ke^{\frac{\lambda}{m}(c_3 - t)}}$$

$$v = \frac{\lambda e^{\frac{\lambda}{m}(c_3 - t)}}{e^{\frac{\lambda}{m}t} - ke^{\frac{\lambda}{m}c_3}}$$

#### $3.2.2 \quad 9 \le t \le 26$

$$m\dot{v} = -kv^2 - \lambda v - W$$

$$\Rightarrow m \int \frac{1}{kv^2 + \lambda v + W} dv = -\int dt$$

$$kv^2 + \lambda v + W = (\sqrt{k}v + \frac{\lambda}{2\sqrt{k}})^2 + W - \frac{\lambda^2}{4k} = (W - \frac{\lambda^2}{4k})((\frac{\sqrt{k}v + \frac{\lambda}{2\sqrt{k}}}{\sqrt{W - \frac{\lambda^2}{4k}}})^2 + 1) = (W - \frac{\lambda^2}{4k})((\frac{2kv + \lambda}{\sqrt{4kW - \lambda^2}})^2 + 1)$$

$$\text{Let } h(x) = \frac{2kx + \lambda}{\sqrt{4kW - \lambda^2}}$$

$$\Rightarrow h'(x) = \frac{2k}{\sqrt{4kW - \lambda^2}}$$

$$\text{arctan}'(x) = \frac{1}{1 + x^2}$$

$$\Rightarrow (\arctan(h(x)))' = \arctan'(h(x))h'(x) = \frac{1}{h^2(x) + 1}h'(x) = \frac{\frac{2k}{\sqrt{4kW - \lambda^2}}}{(\frac{2kx + \lambda}{\sqrt{4kW - \lambda^2}})^2 + 1}$$

$$\Rightarrow m \int \frac{1}{kv^2 + \lambda v + W} dv = m \int \frac{1}{(W - \frac{\lambda^2}{4k})((\frac{2kv + \lambda}{\sqrt{4kW - \lambda^2}})^2 + 1)} dv = \frac{2m\sqrt{4kW - \lambda^2}}{4k(W - \frac{\lambda^2}{4k})} \int \frac{\frac{2k}{\sqrt{4kW - \lambda^2}}}{(\frac{2kv + \lambda}{\sqrt{4kW - \lambda^2}})^2 + 1} dv$$

$$\Rightarrow \frac{2m}{\sqrt{4kW - \lambda^2}} \arctan(\frac{2kv + \lambda}{\sqrt{4kW - \lambda^2}}) = -t + c_4$$

$$\Rightarrow \frac{2kv + \lambda}{\sqrt{4kW - \lambda^2}} \arctan(\frac{\sqrt{4kW - \lambda^2}}{2m}(c_4 - t))$$

$$\Rightarrow v = \frac{\sqrt{4kW - \lambda^2}}{2m} \arctan(\frac{\sqrt{4kW - \lambda^2}}{2m}(c_4 - t)) - \lambda}{2k}$$

$$\Rightarrow v = \begin{cases} \frac{\lambda c \frac{m}{k} c_3}{2km}}{c \frac{m^2}{k} - kc \frac{m}{k} c_3}}, & t \in [0, 9] \\ \frac{\sqrt{4kW - \lambda^2}}{2km} (c_4 - t)) - \lambda}{2k}, & t \in [0, 9] \end{cases}$$

#### 3.3 Particular solution

$$\Rightarrow \begin{cases} \frac{\lambda e^{\frac{\lambda}{m} c_3}}{2^{\frac{\lambda}{m}} - k e^{\frac{\lambda}{m} c_3}} = 55 \\ \frac{\sqrt{4kW - \lambda^2} \tan(\frac{\sqrt{4kW - \lambda^2}}{2m}(c_4 - 9)) - \lambda}{2k} = 55 \end{cases}$$
Let  $(t_1, v_1), (t_2, v_2) \in S; t_1, t_2 \in [0, 9]; t_1 \neq t_2$ 

$$\frac{\lambda e^{\frac{\lambda}{m} c_3}}{e^{t_1 \frac{\lambda}{m}} - k e^{\frac{\lambda}{m} c_3}} = v_1$$

$$\Rightarrow v_1 k e^{\frac{\lambda}{m} c_3} = v_1 e^{t_1 \frac{\lambda}{m}} - \lambda e^{\frac{\lambda}{m} c_3}$$

$$\Rightarrow k = \frac{v_1 e^{t_1 \frac{\lambda}{m}} - \lambda e^{\frac{\lambda}{m} c_3}}{v_1 e^{\frac{\lambda}{m} c_3}}$$

$$\Rightarrow k = e^{\frac{\lambda}{m} (t_1 - c_3)} - \frac{\lambda}{v_1}$$

$$\frac{m}{\lambda} (\ln(v_2) - \ln(kv_2 + \lambda)) = c_3 - t_2$$

$$\Rightarrow c_3 = \frac{m}{\lambda} (\ln(v_2) - \ln(kv_2 + \lambda)) + t_2$$

$$\Rightarrow c_3 = \frac{m}{\lambda} (\ln(\frac{v_2}{v_2 (e^{\frac{\lambda}{m} (t_1 - c_3)} - \frac{\lambda}{v_1}) + \lambda})) + t_2$$

$$\Rightarrow e^{\frac{\lambda}{m} (c_3 - t_2)} = \frac{v_2}{v_2 (e^{\frac{\lambda}{m} (t_1 - c_3)} - \frac{\lambda}{v_1}) + \lambda}$$

$$\Rightarrow (v_2 e^{\frac{\lambda}{m} t_1} e^{-\frac{\lambda}{m} c_3} - v_2 \frac{\lambda}{v_1} + \lambda) e^{\frac{\lambda}{m} c_3} e^{-\frac{\lambda}{m} t_2} = v_2$$

$$\Rightarrow v_2 e^{\frac{\lambda}{m} (t_1 - t_2)} - (v_2 \frac{\lambda}{v_1} - \lambda) e^{\frac{\lambda}{m} (c_3 - t_2)} = v_2$$

$$\Rightarrow e^{\frac{\lambda}{m} (c_3 - t_2)} = \frac{v_1 v_2}{\lambda (v_2 - v_1)} (e^{\frac{\lambda}{m} t_1 - e^{\frac{\lambda}{m} t_2}})$$

$$\Rightarrow e^{\frac{\lambda}{m} c_3} = \frac{v_1 v_2}{\lambda (v_2 - v_1)} (e^{\frac{\lambda}{m} t_1} - e^{\frac{\lambda}{m} t_2})$$

$$\Rightarrow c_3 = \frac{m}{\lambda} \ln(\frac{v_1 v_2 (e^{\frac{\lambda}{m} t_1} - e^{\frac{\lambda}{m} t_2})}{\lambda (v_2 - v_1)})$$

$$\Rightarrow k = e^{\frac{\lambda}{m} (9 - c_3)} - \frac{\lambda}{55} \text{ (to make } v \text{ continuous)}$$

$$\hat{v} = \frac{\lambda e^{\frac{\lambda}{m} c_3}}{e^{\frac{\lambda}{m} t} - k e^{\frac{\lambda}{m} c_3}}$$

$$J = \sum_{(t,v) \in S, t \leq 9} (\hat{v} - v)^2$$

J is a sum of squares of all errors for  $t \leq 9$ . We want to minimize this sum, so I will set its partial derivative to zero to find the value of  $\lambda$  that minimizes J.

$$\operatorname{Let} \zeta(\lambda) = \frac{\partial J}{\partial \lambda} = 0$$

$$\Rightarrow \zeta(\lambda) = \partial_{\lambda} \sum_{(t,v) \in S, t \leq 9} (\hat{v} - v)^{2}$$

$$\lambda_{n+1} = \lambda_{n} - \frac{\zeta(\lambda)}{\zeta'(\lambda)} \text{ (Newton-Raphson method)}$$

$$\frac{\sqrt{4kW - \lambda^{2}} \tan(\frac{\sqrt{4kW - \lambda^{2}}}{2m}(c_{4} - 9)) - \lambda}{2k} = 55$$

$$\Rightarrow \sqrt{4kW - \lambda^{2}} \tan(\frac{\sqrt{4kW - \lambda^{2}}}{2m}(c_{4} - 9)) = 2k55 + \lambda$$

$$\Rightarrow \frac{\sqrt{4kW - \lambda^{2}}}{2m}(c_{4} - 9) = \arctan(\frac{2k55 + \lambda}{\sqrt{4kW - \lambda^{2}}})$$

$$\Rightarrow c_{4} = 9 + \frac{2m \arctan(\frac{2k55 + \lambda}{\sqrt{4kW - \lambda^{2}}})}{\sqrt{4kW - \lambda^{2}}}$$

$$\frac{\sqrt{4kW - \lambda^{2}}}{2m}(c_{4} - t) = \arctan(\frac{2kv + \lambda}{\sqrt{4kW - \lambda^{2}}})$$

$$\Rightarrow \frac{\sqrt{4kW - \lambda^{2}}}{2m}(c_{4} - t) - \arctan(\frac{2kv + \lambda}{\sqrt{4kW - \lambda^{2}}}) = 0$$

$$I = \sum_{(t,v) \in S, t \geq 9} \left(\frac{\sqrt{4kW - \lambda^{2}}}{2m}(c_{4} - t) - \arctan(\frac{2kv + \lambda}{\sqrt{4kW - \lambda^{2}}})\right)^{2}$$

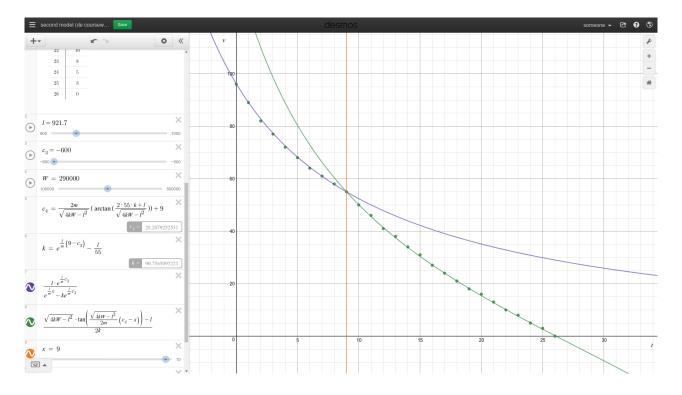
We want to minimize I.

Let 
$$\phi(W) = \frac{\partial I}{\partial W} = 0$$

$$\Rightarrow \phi(W) = \partial_W \sum_{(t,v) \in S, t \ge 9} \left( \frac{\sqrt{4kW - \lambda^2}}{2m} (c_4 - t) - \arctan(\frac{2kv + \lambda}{\sqrt{4kW - \lambda^2}}) \right)^2$$

$$\Rightarrow W_{n+1} = W_n - \frac{\phi(W)}{\phi'(W)}$$

I found  $\lambda_0$  and  $W_0$  the same way I found  $B_0$  for the first model - I made a graph and adjusted parameters  $c_3$ ,  $\lambda$ , and W until the curve roughly fit the data.



$$\begin{cases}
c_3 = \frac{m}{\lambda} \ln\left(\frac{v_1 v_2 \left(e^{\frac{\lambda}{m}t_1} - e^{\frac{\lambda}{m}t_2}\right)}{\lambda (v_2 - v_1)}\right) \\
k = e^{\frac{\lambda}{m}(9 - c_3)} - \frac{\lambda}{55} \\
\zeta(\lambda) = \partial_{\lambda} \sum_{(t,v) \in S, t \leq 9} \left(\frac{\lambda e^{\frac{\lambda}{m}c_3}}{e^{\frac{\lambda}{m}t} - ke^{\frac{\lambda}{m}c_3}} - v\right)^2 \\
\lambda_{n+1} = \lambda_n - \frac{\zeta(\lambda_n)}{\zeta'(\lambda_n)} \\
\lambda_0 = 921.7 \\
c_4 = 9 + \frac{2m \arctan\left(\frac{110k + \lambda}{\sqrt{4kW - \lambda^2}}\right)}{\sqrt{4kW - \lambda^2}} \\
\phi(W) = \partial_W \sum_{(t,v) \in S, t \geq 9} \left(\frac{\sqrt{4kW - \lambda^2}}{2m}(c_4 - t) - \arctan\left(\frac{2kv + \lambda}{\sqrt{4kW - \lambda^2}}\right)\right)^2 \\
W_{n+1} = W_n - \frac{\phi(W)}{\phi'(W)} \\
W_0 = 2900000
\end{cases}$$
(3)

I wrote another module for the second model:

```
{-# LANGUAGE RecordWildCards #-}
{-# LANGUAGE TypeFamilies #-}
```

module Solution. Second (Parameters, SolutionGen) where

import Data.Proxy

import AutoDiff
import GivenData
import qualified Solution.Model as M

```
data Parameters a =
    Parameters { pLambda :: a
               , pC3
                        :: a
               , pK
                        :: a
               , pW
                        :: a
               , pC4
                        :: a
                        :: SolutionGen a
               , pGen
data SolutionGen a =
    SolutionGen { sgPoint1 :: Point a
                , sgPoint2 :: Point a
instance Show a => Show (SolutionGen a) where
    show SolutionGen{..} =
         ", p1 = (" ++ show (pTime sgPoint1) ++ ", " ++ show (pSpeed sgPoint1) ++ ")"
      ++ ", p2 = (" ++ show (pTime sgPoint2) ++ ", " ++ show (pSpeed sgPoint2) ++ ")"
instance Show a => Show (Parameters a) where
    show Parameters{..} = "lambda = " ++ show pLambda
                        ++ ", c3 = " ++ show pC3
                         ++ ", K = " ++ show pK
                         ++ ", W = " ++ show pW
                         ++ ", c4 = " ++ show pC4
                         ++ show pGen ++ "\n"
c3F :: Floating a => Point a -> Point a -> a -> a
c3F (Point t1 v1) (Point t2 v2) lambda =
  m / lambda * log ((v1*v2*(exp (lambda / m * t1) - exp (lambda / m * t2))) / (lambda * (v2 - v1)))
kF :: (Floating a, Ord a, Enum a) => a -> a -> a
kF c3 lambda = exp (lambda / m * (9 - c3)) - lambda / 55
sumOfSquares :: (Num a, Enum a) => [Point a] -> (Point a -> a -> a) -> a -> a
sumOfSquares ps f u = sum $ (^2) . flip f u <$> ps
zeta :: (Floating a, Ord a, Enum a) => Point a -> Point a -> a -> a
zeta p1 p2 = d $ sumOfSquares (take 10 points) j
  where j (Point t v) lambda = lambda * exp (h*c3) / (exp (h*t) - k * exp (h*c3)) - v
          where c3 = c3F (toDualPoint p1) (toDualPoint p2) lambda
               k = kF c3 lambda
                h = lambda / m
c4F :: Floating a => a -> a -> a -> a
c4F c3 k lambda w =
  9 + 2 * m * atan ((2*v*k + lambda) / denom) / denom
  where denom = sqrt (4*k*w - lambda^2)
       h = lambda / m
        v = lambda * exp (h*c3) / (exp (h*9) - k * exp (h*c3))
```

```
phi :: (Floating a, Enum a, Eq a) => a -> a -> a -> a
phi c3 k lambda = d $ sumOfSquares (drop 9 points) j
  where j (Point t v) w =
          root * (c4 - t) / (2*m) - atan ((2 * constDual k * v + constDual lambda) / root)
          where c4 = c4F (constDual c3) (constDual k) (constDual lambda) w
                root = sqrt $ 4 * constDual k * w - constDual lambda ^2
findParams :: (Floating a, Ord a, Enum a) => SolutionGen a -> Parameters a
findParams gen@SolutionGen{..} = parameters
  where parameters = Parameters
          { pLambda = newton (zeta (toDualPoint sgPoint1) (toDualPoint sgPoint2)) (Left 1000) 921.7
          , pC3 = c3F sgPoint1 sgPoint2 (pLambda parameters)
          , pK = kF (pC3 parameters) (pLambda parameters)
          , pW = newton ( phi (constDual $ pC3 parameters)
                              (constDual $ pK parameters)
                              (constDual $ pLambda parameters) )
                        (Left 1000)
                        290000
          , pC4 = c4F (pC3 parameters) (pK parameters) (pLambda parameters) (pW parameters)
          , pGen = gen
          }
predict :: (Ord a, Floating a) => Parameters a -> a -> a
predict Parameters{..} t
  | 0 <= t && t <= 9 =
    let h = pLambda / m in pLambda * exp (h*pC3) / (exp (h*t) - pK * exp (h*pC3))
  | 9 < t && t <= 26 =
    let r = sqrt  $ 4*pK*pW - pLambda^2 in (r * tan (r * (pC4 - t) / (2 * m)) - pLambda) / (2 * pK)
  | otherwise = error "Invalid time!"
combinations :: (Num a, Enum a, Eq a) => [SolutionGen a]
combinations = fmap (uncurry SolutionGen)
             $ filter (uncurry (/=))
             $ (\l -> [ (p1, p2) | p1 <- 1, p2 <- 1])
             $ take 10 points
instance M.ModelParams Parameters where
    type SolutionGen Parameters = SolutionGen
    predict = predict
    findParams = findParams
    combinations Proxy = combinations
```

I also changed import Solution. First as Sol to import Solution. Second as Sol in the main module. This code gives us the following result:

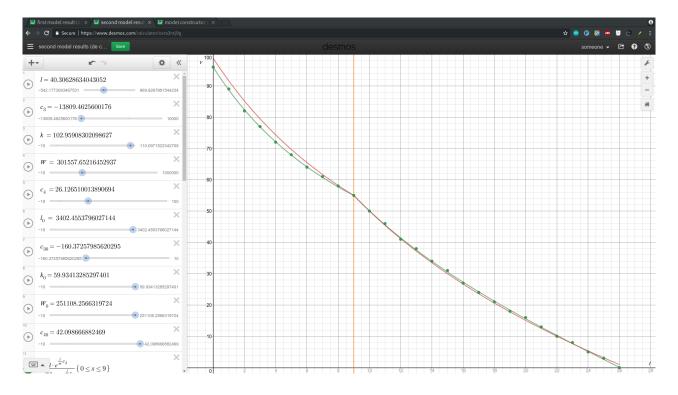
```
| Accessive | Acce
```

## 3.4 Graphs and Analysis

| Time  | Predicted               | Rounded   | Observed |
|-------|-------------------------|-----------|----------|
| 1 mie | Speed                   | Predicted |          |
|       | speed                   |           | speed    |
| 0.0   | 06.0000000000014        | Speed     | 0.6      |
| 0.0   | 96.000000000054         | 96        | 96       |
| 1.0   | 88.66582512227822       | 89        | 89       |
| 2.0   | 82.37077686914407       | 82        | 82       |
| 3.0   | 76.90862555559508       | 77        | 77       |
| 4.0   | 72.12432763292139       | 72        | 72       |
| 5.0   | 67.89907302369585       | 68        | 68       |
| 6.0   | 64.14028474770049       | 64        | 64       |
| 7.0   | 60.77475738769026       | 61        | 61       |
| 8.0   | 57.743842139329196      | 58        | 58       |
| 9.0   | 55.00000000000179       | 55        | 55       |
| 10.0  | 50.10157524003789       | 50        | 50       |
| 11.0  | 45.60871998373162       | 46        | 46       |
| 12.0  | 12.0 41.45588373779139  |           | 41       |
| 13.0  | 37.5898231332195        | 38        | 38       |
| 14.0  | 33.96673336319917       | 34        | 34       |
| 15.0  | 30.550133354391157      | 31        | 31       |
| 16.0  | 27.309281417030515      | 27        | 27       |
| 17.0  | 24.217970303658813      | 24        | 24       |
| 18.0  | 21.253597490201017      | 21        | 21       |
| 19.0  | 18.396437545757497      | 18        | 18       |
| 20.0  | 15.629064386691416      | 16        | 16       |
| 21.0  | 21.0 12.935885534732083 |           | 13       |
| 22.0  | 22.0 10.30276043083657  |           | 10       |
| 23.0  | 23.0 7.716681813438704  |           | 8        |
| 24.0  | 5.165504072768728       | 5         | 5        |
| 25.0  | 2.6377059483218517      | 3         | 3        |
| 26.0  | 0.12217734574065967     | 0         | 0        |

| Maximum Error      | Average Error       | Root mean square    |  |
|--------------------|---------------------|---------------------|--|
| 0.4558837377913889 | 0.23458170693637476 | 0.27311676642511934 |  |

I'll now look at the two configurations that I obtained and plot them. The red line shows the worst configuration, and the green line shows the best configuration.



As you can see in 3.3 rounded predictions of the best configuration exactly match the given data.

#### 3.5 Conclusion of Model 2

$$\begin{cases} v = \frac{\lambda e^{\frac{\lambda}{m} \cdot 3}}{e^{\frac{\lambda}{m}t} - ke^{\frac{\lambda}{m} \cdot 3}}, & t \in [0, 9] \\ v = \frac{\sqrt{4kW - \lambda^2} \tan(\frac{\sqrt{4kW - \lambda^2}}{2km}(c_4 - t)) - \lambda}}{2km}, & t \in [9, 26] \\ \lambda = 40.30628634043052 \\ c_3 = -13809.4625600176 \\ k = 102.95908302098627 \\ W = 301557.65216452937 \\ c_4 = 26.126510013890694 \end{cases}$$

$$x = \int_0^{26} v dt = \int_0^9 v dt + \int_9^{26} v dt \\ x = \int_0^{26} v dt = \int_0^9 v dt + \int_9^{26} v dt$$

$$v_1 = \frac{\lambda e^{\frac{\lambda}{m}c_3}}{e^{\frac{\lambda}{m}t} - ke^{\frac{\lambda}{m}(c_3 - t)}} = \frac{\lambda e^{\frac{\lambda}{m}(c_3 - t)}}{1 - ke^{\frac{\lambda}{m}(c_3 - t)}} = \frac{\lambda e^{\frac{\lambda}{m}(c_3 - t)}}{1 - ke^{\frac{\lambda}{m}(c_3 - t)}} = \frac{\lambda e^{\frac{\lambda}{m}(c_3 - t)}}{1 - ke^{\frac{\lambda}{m}(c_3 - t)}} = \frac{\lambda e^{\frac{\lambda}{m}(c_3 - t)}}{1 - ke^{\frac{\lambda}{m}(c_3 - t)}} = \frac{\lambda e^{\frac{\lambda}{m}(c_3 - t)}}{1 - ke^{\frac{\lambda}{m}(c_3 - t)}} = \frac{\lambda e^{\frac{\lambda}{m}(c_3 - t)}}{1 - ke^{\frac{\lambda}{m}(c_3 - t)}} = \frac{\lambda e^{\frac{\lambda}{m}(c_3 - t)}}{1 - ke^{\frac{\lambda}{m}(c_3 - t)}} = \frac{\lambda e^{\frac{\lambda}{m}(c_3 - t)}}{1 - ke^{\frac{\lambda}{m}(c_3 - t)}} = \frac{\lambda e^{\frac{\lambda}{m}(c_3 - t)}}{1 - ke^{\frac{\lambda}{m}(c_3 - t)}} = \frac{\lambda e^{\frac{\lambda}{m}(c_3 - t)}}{1 - ke^{\frac{\lambda}{m}(c_3 - t)}} = \frac{\lambda e^{\frac{\lambda}{m}(c_3 - t)}}{1 - ke^{\frac{\lambda}{m}(c_3 - t)}} = \frac{\lambda e^{\frac{\lambda}{m}(c_3 - t)}}{1 - ke^{\frac{\lambda}{m}(c_3 - t)}} = \frac{\lambda e^{\frac{\lambda}{m}(c_3 - t)}}{1 - ke^{\frac{\lambda}{m}(c_3 - t)}} = \frac{\lambda e^{\frac{\lambda}{m}(c_3 - t)}}{1 - ke^{\frac{\lambda}{m}(c_3 - t)}} = \frac{\lambda e^{\frac{\lambda}{m}(c_3 - t)}}{1 - ke^{\frac{\lambda}{m}(c_3 - t)}} = \frac{\lambda e^{\frac{\lambda}{m}(c_3 - t)}}{1 - ke^{\frac{\lambda}{m}(c_3 - t)}} = \frac{\lambda e^{\frac{\lambda}{m}(c_3 - t)}}{1 - ke^{\frac{\lambda}{m}(c_3 - t)}} = \frac{\lambda e^{\frac{\lambda}{m}(c_3 - t)}}{1 - ke^{\frac{\lambda}{m}(c_3 - t)}} = \frac{\lambda e^{\frac{\lambda}{m}(c_3 - t)}}{1 - ke^{\frac{\lambda}{m}(c_3 - t)}} = \frac{\lambda e^{\frac{\lambda}{m}(c_3 - t)}}{1 - ke^{\frac{\lambda}{m}(c_3 - t)}} = \frac{\lambda e^{\frac{\lambda}{m}(c_3 - t)}}{1 - ke^{\frac{\lambda}{m}(c_3 - t)}} = \frac{\lambda e^{\frac{\lambda}{m}(c_3 - t)}}{1 - ke^{\frac{\lambda}{m}(c_3 - t)}} = \frac{\lambda e^{\frac{\lambda}{m}(c_3 - t)}}{1 - ke^{\frac{\lambda}{m}(c_3 - t)}} = \frac{\lambda e^{\frac{\lambda}{m}(c_3 - t)}}{1 - ke^{\frac{\lambda}{m}(c_3 - t)}} = \frac{\lambda e^{\frac{\lambda}{m}(c_3 - t)}}{1 - ke^{\frac{\lambda}{m}(c_3 - t)}} = \frac{\lambda e^{\frac{\lambda}{m}(c_3 - t)}}{1 - ke^{\frac{\lambda}{m}(c_3 - t)}} = \frac{\lambda e^{\frac{\lambda}{m}(c_3 - t)}}{1 - ke^{\frac{\lambda}{m}(c_3 - t)}} = \frac{\lambda e^{\frac{\lambda}{m}(c_3 - t)}}{1 - ke^{\frac{\lambda}{m}(c_3 - t)}} = \frac{\lambda e^{\frac{\lambda}{m}(c_3 - t)}}{1 - ke^{\frac{\lambda}{m}(c_3 - t)}} =$$

$$\Rightarrow \int v_2 dt = \frac{1}{2k} \left( \sqrt{4kW - \lambda^2} \times \left( -\frac{2m}{\sqrt{4kW - \lambda^2}} \right) \int \tan(u) du - \int \lambda dt \right)$$

$$\Rightarrow \int v_2 dt = \frac{1}{2k} \left( 2m \int \frac{-\sin u}{\cos u} du - \lambda \int dt \right) = \frac{2m \ln(\cos(\frac{\sqrt{4kW - \lambda^2}}{2m}(c_4 - t))) - \lambda t}{2k} + \text{constant}$$

$$\Rightarrow x = \left[ \frac{m \ln(e^{\frac{\lambda}{m}(t - c_3)} - k) - \lambda t}{k} \right]_0^9 + \left[ \frac{2m \ln(\cos(\frac{\sqrt{4kW - \lambda^2}}{2m}(c_4 - t))) - \lambda t}{2k} \right]_9^{26}$$

$$\Rightarrow x = \frac{1}{k} \left( \left[ m \ln(e^{\frac{\lambda}{m}(t - c_3)} - k) \right]_0^9 + \left[ m \ln(\cos(\frac{\sqrt{4kW - \lambda^2}}{2m}(c_4 - t))) \right]_9^{26} - (13\lambda + 4.5\lambda) \right)$$

$$\Rightarrow x = \frac{m}{k} \left( \ln\left(\frac{e^{\frac{\lambda}{m}(9 - c_3)} - k}{e^{\frac{\lambda}{m}(-c_3)} - k}\right) + \ln\left(\frac{\cos(\frac{\sqrt{4kW - \lambda^2}}{2m}(c_4 - 26))}{\cos(\frac{\sqrt{4kW - \lambda^2}}{2m}(c_4 - 9))}\right) - 17.5\frac{\lambda}{k}$$

$$\Rightarrow x = \frac{m}{k} \ln\left(\frac{e^{\frac{\lambda}{m}(9 - c_3)} - k}{e^{\frac{\lambda}{m}(-c_3)} - k} \times \frac{\cos(\frac{\sqrt{4kW - \lambda^2}}{2m}(c_4 - 26))}{\cos(\frac{\sqrt{4kW - \lambda^2}}{2m}(c_4 - 9))}\right) - 17.5\frac{\lambda}{k}$$

$$\Rightarrow x \approx 1057.8652498929307 \approx 1060$$

As you can see the value of x is approximately equal to the one found from the first model, so recommendations are the same.

## 4 Assessment of the improvement obtained

#### 4.1 Prediction

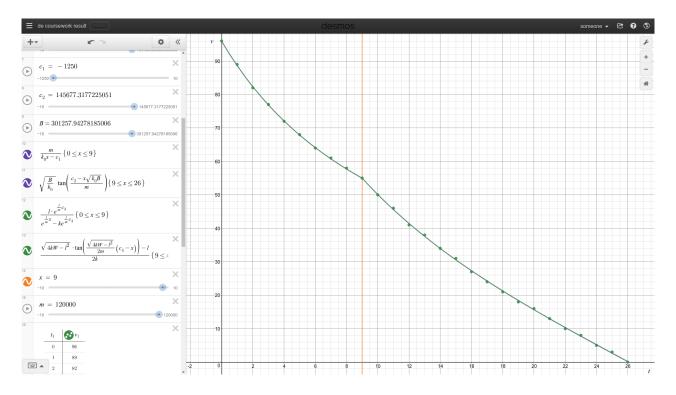
Based on the models I predict that the aeroplane stopped in 1060 meters. The length of runway that I recommend is 2000 meters for the reasons stated in the work.

## 4.2 Comparing the models

| Time | Predicted          | Predicted           | Observed | Better |
|------|--------------------|---------------------|----------|--------|
|      | Speed              | Speed               | Speed    | Model  |
|      | (1st Model)        | (2nd Model)         | _        |        |
| 0.0  | 96.0               | 96.0000000000054    | 96       | 1st    |
| 1.0  | 88.65671641791045  | 88.66582512227822   | 89       | 2nd    |
| 2.0  | 82.35701906412478  | 82.37077686914407   | 82       | 1st    |
| 3.0  | 76.89320388349515  | 76.90862555559508   | 77       | 2nd    |
| 4.0  | 72.1092564491654   | 72.12432763292139   | 72       | 1st    |
| 5.0  | 67.88571428571429  | 67.89907302369585   | 68       | 2nd    |
| 6.0  | 64.12955465587045  | 64.14028474770049   | 64       | 1st    |
| 7.0  | 60.767263427109974 | 60.77475738769026   | 61       | 2nd    |
| 8.0  | 57.739975698663415 | 57.743842139329196  | 58       | 2nd    |
| 9.0  | 54.9999999999999   | 55.00000000000179   | 55       | 1st    |
| 10.0 | 50.10816658852111  | 50.10157524003789   | 50       | 2nd    |
| 11.0 | 45.622063036212374 | 45.60871998373162   | 46       | 2nd    |
| 12.0 | 41.475988862696376 | 41.45588373779139   | 41       | 2nd    |
| 13.0 | 37.61659930730753  | 37.5898231332195    | 38       | 1st    |
| 14.0 | 34.00002062308155  | 33.96673336319917   | 34       | 1st    |
| 15.0 | 30.589724513917773 | 30.550133354391157  | 31       | 1st    |
| 16.0 | 27.35493651754378  | 27.309281417030515  | 27       | 2nd    |
| 17.0 | 24.269426053394415 | 24.217970303658813  | 24       | 2nd    |
| 18.0 | 21.3105731783461   | 21.253597490201017  | 21       | 2nd    |
| 19.0 | 18.45863841578133  | 18.396437545757497  | 18       | 2nd    |
| 20.0 | 15.696183121094782 | 15.629064386691416  | 16       | 1st    |
| 21.0 | 13.00760227741885  | 12.935885534732083  | 13       | 1st    |
| 22.0 | 10.378741615250261 | 10.30276043083657   | 10       | 2nd    |
| 23.0 | 7.796577949697343  | 7.716681813438704   | 8        | 1st    |
| 24.0 | 5.248946558956161  | 5.165504072768728   | 5        | 2nd    |
| 25.0 | 2.7243028986249413 | 2.6377059483218517  | 3        | 1st    |
| 26.0 | 0.2115083630415522 | 0.12217734574065967 | 0        | 2nd    |

| Model | Maximum Error       | Average Error       | Root mean square    | Num. of better |
|-------|---------------------|---------------------|---------------------|----------------|
|       |                     |                     |                     | predictions    |
| 1st   | 0.47598886269637575 | 0.23822424753496707 | 0.2776875104911393  | 12             |
| 2nd   | 0.4558837377913889  | 0.23458170693637476 | 0.27311676642511934 | 15             |

Here is a graph of both of the models.



As you can see the second model gave more accurate predictions, but the increase in accuracy is very small.