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Effect of heat treatment on mechanical and thermal properties of SiC/SiC composites with three-dimensional carbon network

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Abstract

SiC/SiC composites with high thermal conductivity shows promising application in field of fusion reactors. In this work, CNTs papers were fabricated by a vacuum filtration strategy while using pitch-based carbon fibers to build a network structure into SiC/SiC composite (SiC-CNTs-C/SiC, SCCS). The thermal conductivity and related mechanical properties before and after heat treatment at different temperature were investigated. The bonding between CNTs paper layers and SiC matrix were mainly mechanical. Compared to the composite without transfer channels, the bending strength of SCCS (434.54MPa) increased by 19% due to the reinforcement of transfer channels from the network structure. However, the damage to SiC fibers resulting from high temperature treatment adversely affected the mechanical properties. The disorder degree of SiC matrix and SiC fibers decreased after heat treatment while mean free path of phonons increased, which are conducive to heat transfer. Contracted to room temperature, the measured thermal conductivity at 1600°C was 53.83 W/(m • K) in vertical direction and 29.85 W/(m • K) in plane. In summary, heat treatment apparently enhanced thermal conductivity of SCCS composites while partly sacrificed the mechanical properties.

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Key words: carbon network, thermal conductivity, nanoindentation, bending strength

Introduction

Continuous SiC fiber reinforced SiC ceramic matrix composites (SiC/SiC) are excellent in high temperature strength^[1], oxidation resistance^[2, 3] and irradiation performance^[4, 5]. In nuclear application, it is important that the heat dissipation performance of fuel cladding tube, which means high thermal conductivity is essential for materials during service. SiC/SiC composites have been considered as potential structure materials for cladding tube^[6, 7]. It is always expected to improve thermal conductivity of SiC/SiC composites.

There is a wide variation in the thermal conductivity data of SiC/SiC composites depending on various preforms, composition and preparation process. Katoh et al.^[8] found three-dimensional (3D) SiC/SiC composites had the best thermal conductivity after comparing the data of SiC/SiC composites with 2D SiC/SiC composites. Yamada et al.^[9] proved that the thermal conductivity of 3D SiC/SiC composites could reach 40-50 W/(m·K) at room temperature (RT). Yet it is hard to weave three-dimensional preforms for the high modulus of SiC fibers^[10]. In addition, the cost of fabricating 3D SiC/SiC is expensive. Densifying SiC/SiC composites is also a favorable strategy to improve its thermal conductivity. For instance, Tao et al.^[11] reduced the porosity of composites via depositing SiC nanowires on SiC fabrics and the thermal conductivity reached 26.7 W/(m·K) at room temperature. In addition, many research efforts were devoted to introduce second phase into composites for improving thermal conductivity. Carbon nanotubes (CNTs) have a large mean free path of phonons because of their high aspect ratio, and the theoretical thermal conductivity can reach 3000 W/(m·K).^[12] Feng et al.^[13] added CNTs films to the preform, which increased thermal conductivity to 23.9 W/(m·K). Feng et al.^[14] introduced CNTs into PyC interface and the thermal conductivity increased by 2.158 times due to the decline of interface thermal resistance. In the research of Yoshida et al.^[15], submicron-sized α -SiC with coarse α -SiC particles addition was used as raw materials for SiC matrix, which improved the thermal conductivity to 56 W/(m·K). However, the mechanical properties of SiC/SiC composites in literatures could not meet the requirements, which were equally important for nuclear application.

As for effect of preparation process, several techniques have been reported to fabricate SiC/SiC composites, such as Chemical Vapor Infiltration (CVI)^[16], Polymer

Impregnation and Pyrolysis (PIP)^[17], Nano-Infiltration and Transient Eutectic-phase (NITE)^[18], Reaction Sintering (RS)^[19] and Electrophoretic Deposition (EPD)^[20]. All these strategies have non-ignorable disadvantages for thermal applications. Comparing with other processes, the bottle-neck effect of CVI process generates high porosity. The existence of pores results in the low thermal conductivity of SiC/SiC at room temperature^[19]. However, the temperature of CVI process is low which has little damage to SiC fibers. Besides, CVI method yields stoichiometric and crystalline β -SiC matrix with fine-grained microstructure, which are preferred for heat conduction. In our previous work, laser-assisted CVI (LA-CVI) method combining CVI with laser processing was used to establish a CVI mass transfer channel^[21-25]. The mass transfer channel not only increased the density, but also strengthened the mechanical properties and thermal conductivity of C/SiC composites. Furthermore, heat treatment has been employed to release thermal residual stress, enhance thermal stability, improve interface crystallinity. Ma et al.^[26] noticed the enhancement in flexural strength and fracture toughness of SiC/BN/SiC composites after heat treatment at 1300°C. Feng et al.^[27] increased thermal conductivity of SiC/SiC to 138.4 W/(m·K) at room temperature through 1900°C heat treatment. Although excellent thermal conductivity were shown in this work. Nevertheless, the loading capacity of SiC fibers would be seriously damaged due to the growth of SiC grains and the decomposition of amorphous SiOC^[28].

In this study, laser technology with high machining accuracy and fast processing speed^[29] was applied to manufacture mass transfer channels. Then transfer channels were filled by pitched-based C fibers and constructed a network structure with CNTs papers in SiC/SiC composites, which made the integration of structure and function. Subsequently, heat treatment process was employed to improve the thermal conductivity of SiC-CNTs-C/SiC composite.

2.Experimental

2.1 Materials

Multi-walled carbon nanotubes (outer diameters 8-15nm, Length 10-50 μ m, Purity >95wt%) were supplied by Chengdu Organic Chemicals Co, Ltd., Chinese Academy of Sciences. SiC fabrics (0.5K, plain weave) were provided by Xiamen University. Pitch-based carbon fiber made in Shaanxi Tiance New Material Technology Co., Ltd., specific properties are shown in Table 1.

Table 1 Specific properties of pitch-based carbon fiber.

C fiber	Strength/MPa	Modulus/GPa	Linear density/g/m	Thermal Conductivity/W/(m·K)
	2082	843	0.4508	500

2.2 Preparation

The procedure of making CNTs papers were described elsewhere^[30]. Each paper contains 0.15g CNTs. Use 4 layers of as-obtained CNTs papers and 10 layers of SiC clothes to prepare preforms. The stacking pattern is shown in Fig. 1. Pyrolytic carbon (PyC) interface with a thickness around 200nm was deposited on the preforms at 870°C in a reduced pressure of 5kPa. Then the SiC matrix was produced by CVI method, the details can be referred to Ref. ^[13]. SiC-CNTs/SiC composites were marked as SCS. Subsequently, femtosecond laser system was employed to process holes with a diameter of 0.5mm on semi-dense SCS composite (density 2.2g/cm³). Parameters can be found in literature^[21]. After that, pitch-based carbon fibers were introduced into holes, followed by CVI SiC matrix until completely dense. SiC-CNTs-C/SiC composites were named SCCS. Finally, the SCCS composites are vacuum heat treated at 1400°C, 1500°C, 1600°C for 2h. The samples are labeled HT1400, HT1500, HT1600.

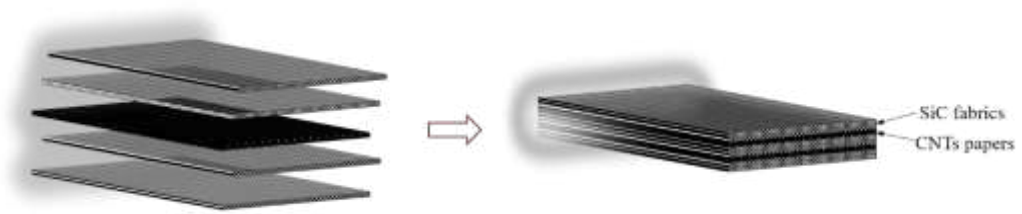


Fig. 1 Stacking pattern of SiC-CNTs/SiC composites(SCS).

2.3 Characterization

Archimedes method was used to measure the density of composites. The micromorphology was observed by scanning electron microscope (SEM, FEI, Helios G4 CX, USA). X-ray diffractometry (Rigaku D/max-2400, Japan) was employed to analyze the phase composition. The Elastic modulus and hardness of the CNTs papers and SiC fibers can be obtained by Nanoindentation technology. (Hysitron TI980, USA), which requires smooth surface of samples. The Young's modulus of the material can be calculated by Eq.(1).

$$\frac{1}{E_r} = \frac{1 - \nu_{sample}^2}{E_{sample}} + \frac{1 - \nu_{indenter}^2}{E_{indenter}} \quad (1)$$

Where E_r is the modulus obtained from indentation test, ν represents the

Poisson's ratio of the material, E_{sample} and $E_{indenter}$ is the Young's modulus of the sample and the diamond indenter.

The interlaminar shear strength and three-point bending strength were obtained on a universal testing machine (CMT4304, China) at a room temperature and the loading rate was 0.5mm/min. The size of three-point bending strength samples and interlaminar shear strength samples were 40mm × 5mm × 3mm and 30mm × 15mm × 3mm respectively. Thermal diffusivity is tested by laser flash method (LFA 427, NETZSCH, Germany) at room temperature with heating rate of 2 °C/min. The dimension of specimens were Φ12.7mm × 3mm. Thermal conductivity was calculated by the formula:

$$\lambda = \alpha \times C_p \times \rho \quad (2)$$

where ρ is the specimen density and C_p is the specific heat capacity.

3. Results and discussion

3.1 Microstructure.

The density of SiC/SiC, SCS, SCCS are 2.53, 2.47, and 2.49g/cm³ respectively. The detailed data of phases content has been shown in Table 2.

Due to the introduction of CNTs papers, the volume fraction of SiC fiber decreased which leads to a decline in density of SCS. The morphologies of CNTs paper are exhibited in Fig. 2. Macroscopically, the carbon nanotube paper could be bent arbitrarily (Fig. 2(b)), and it had good flexibility. The surface of paper was uniform (as shown in Fig. 2(c)). At high magnification, CNTs were randomly distributed to form a network structure with many holes in CNTs paper, which was beneficial to the infiltration of SiC matrix.

Table 2 The volume fractions of SiC fiber, pitched-based carbon fiber and CNTs in SS, SCS, SCCS.

	Volume fractions of SiC fiber	Volume fractions of CNTs	Volume fractions of Pitch-based C fiber	Open Porosity	Total Porosity
SiC/SiC	40%	-	-	9%	22.1%
SCS	30%	6%	-	7.2%	23.4%
SCCS	29.1%	5.82%	3%	6.6%	19%

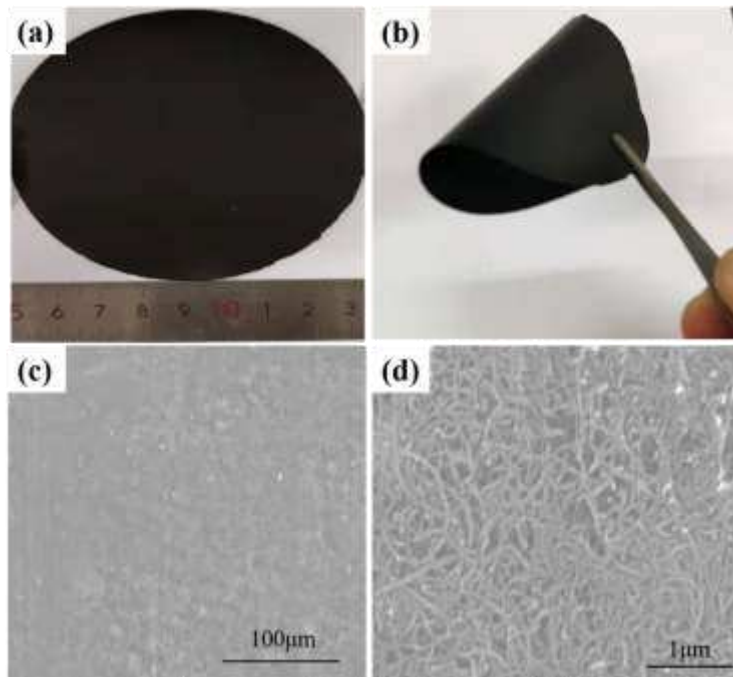


Fig. 2 Morphologies of CNTs paper. (a) macro view; (b) flexibility of CNT paper (c) CNT paper at low magnification; (d) CNT paper at high magnification.

As for the SCCS composites, its density was higher than that of the SCS composites. That means the existence of mass transfer channels was conducive to further densification of samples. The mass transfer channel opened the closed pores inside composites. During the subsequent CVI process, the reaction gas could infiltrate through the mass transfer channel, which effectively filled the internal pores of the composites and improved the density.

The cross-sectional morphologies of SCCS composites could be seen from Fig. 3. No gaps were observed between CNTs paper layers, SiC matrix and pitch-based carbon fibers. Heat treatment did not yields significant layer debonding in SCCS composite. A little matrix infiltrate into the CNTs papers during CVI process. CNTs paper layers were compact without pores. Atom diffusion was not found at interface from energy spectrum, which indicated that the bonded of interface between CNTs paper layer and SiC matrix was mechanically. This combination was achieved by the mutual restriction of the convex structure of the rough surface and friction. Yet the combination could not carried load effectively, when composite was subjected to a vertical force.

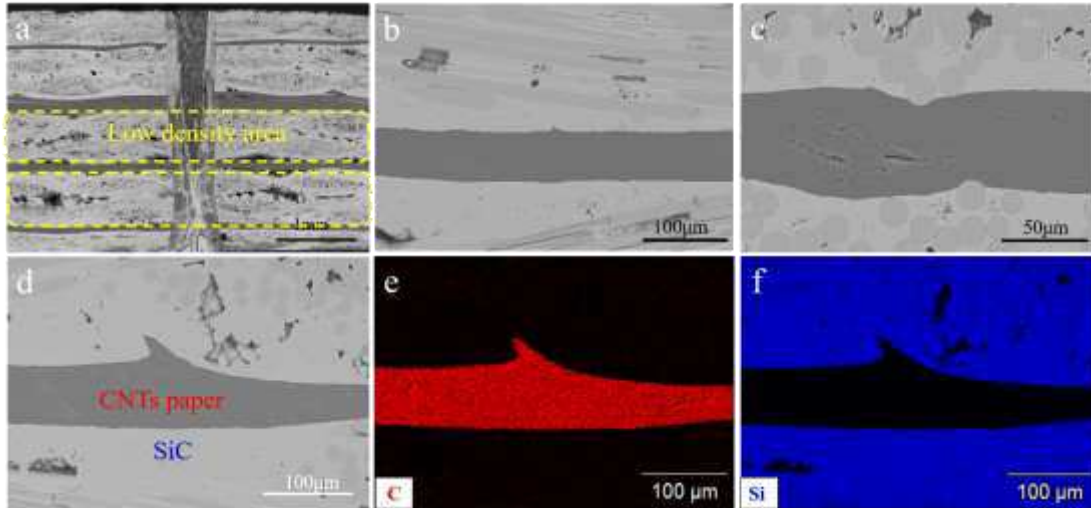


Fig. 3 Morphologies of CNTs paper layers in SCS composite. (a)-(c) BSE images of SCCS composite. (d)-(f) Energy dispersive near the CNTs papers.

After SCCS composites were heat-treated at 1400°C and 1500°C for 2 hours, the spherical morphology of SiC matrix between CNTs layers gradually became larger. The diameter of spherical SiC matrix further increased. As a result of matrix being treated at 1600°C for 2 hours, the surface morphology of SiC matrix showed two shapes: triangular pyramid-shaped sharp corners or hexagonal prism-shaped side protruding (circled part in the Fig.4), indicating that the SiC matrix grain growth had preferred orientation^[31].

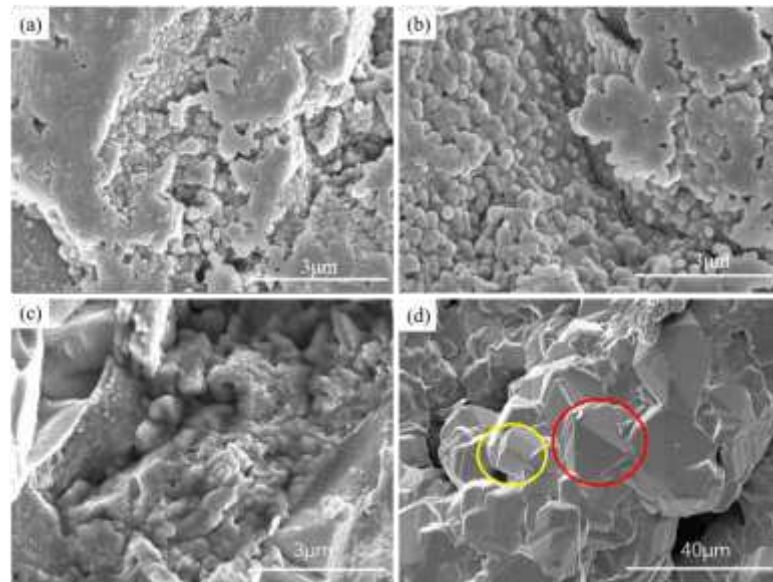


Fig. 4 Morphology of SiC matrix after heat treatment at different temperatures for 2 hours. (a) Room temperature; (b) 1400°C treatment; (c) 1500°C treatment; (d) 1600°C treatment.

XRD patterns of samples after being treated at different temperatures were shown in Fig. 5. The SiC prepared by CVI was mainly composed of β -SiC nanocrystals, a

small amount of α -SiC, amorphous SiC and a small amount of free carbon^[32]. Due to the transformation of amorphous SiC matrix to β -SiC matrix, the crystallinity of SCCS composites increases, which caused the diffraction peaks of (111), (220) and (311) crystal planes of SiC matrix to gradually sharpen with the increase of temperature. The relative intensity of the (111) crystal plane increased, indicating that more SiC matrix tends to grow at the (111) crystal plane.

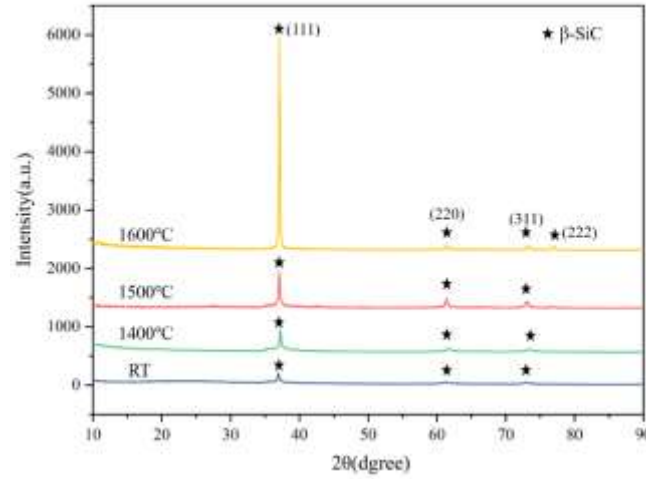


Fig. 5 X-ray diffraction patterns of samples at different heat treatment temperatures.

3.2 Micromechanics

Oliver and Pharr^[33] believed that the elastic modulus measured by nanoindentation method be an average value of the elastic modulus in different crystal axis directions. The nanoindentation Load-Displacement curves of CNTs paper layers after heat treatment at different temperatures were indicated for Fig. 6a. The ordinate represents the load, and the abscissa represents the depth of indenter. The slopes of the loading and unloading curves in Fig. 6a are not the same. The sample produces plastic deformation during the loading process. After unloading, the compressed area cannot be elastically deformed to return to its original state. In addition, the origin of loading curve was close to the end of unloading curve, which means the deformation was mainly elastic deformation and the plastic deformation was low. The maximum load for CNTs paper was 5mN. However, the depth of indenters were different, indicating that hardness of four samples changed after heat treatment.

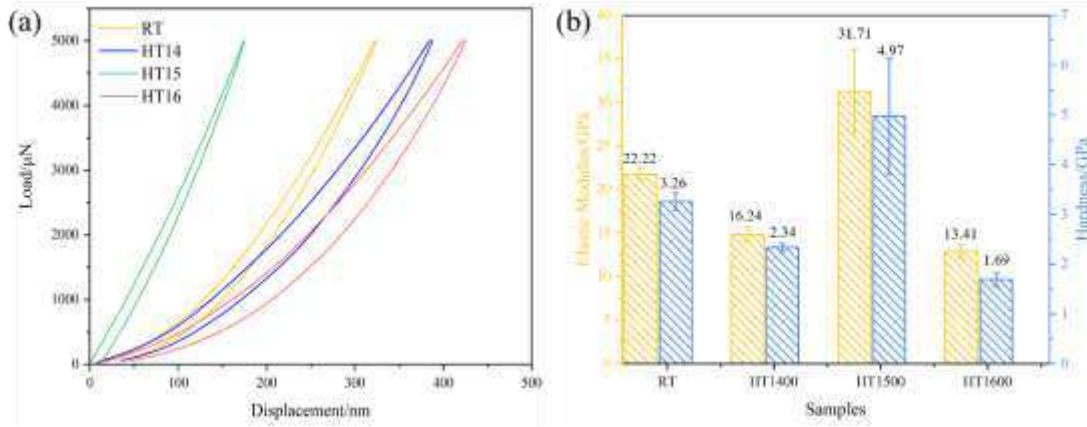


Fig. 6 Micromechanical properties of CNTs paper layers in SCCS composites (tested by nanoindentation).

(a) Load-Displacement curves of CNTs papers; (b) Elastic modulus and Hardness of CNTs papers after heat treatment.

Fig. 6b lists the measured elastic modulus and hardness of CNTs paper layers according to Eq.(1). Generally, the elastic modulus of material is positively related to their hardness. The main factors affecting the elastic modulus of CNTs paper layers were combination, grain size and atomic arrangement. In CNTs paper layers, the bonding force between CNTs was mainly van der Waals force. While the bonding between SiC matrix and CNTs was mainly mechanical bonding. Therefore, the modulus and hardness of CNTs paper layers were much lower than that of SiC fibers. When the temperature of treatment raised, the grain size of SiC and CNTs increased^[27], which was smaller than dimension of indenter (100nm). The relationship between hardness and grain size can be expressed as follows^[34]:

$$H=H_0+Kd^{-\frac{1}{2}} \quad (3)$$

In formula, H_0 and K are constants, H represents the hardness, d is the size of grain. With the size enlarged, the decrease of the number of grain boundaries that hinder slip reduced the hardness of CNTs paper layer. After 1600°C treatment, the hardness and modulus of CNTs paper layer decreased by 39.6% and 48.2% respectively.

3.3 Mechanical properties

In Fig. 3(a), the pitch-based-C fiber in transfer channel and CNTs papers form a macroscopic network structure, which has an important effect on the mechanical properties of SCCS composites. Bending strength of SCCS composites is listed in Fig. 8. The maximum flexural strength of SCCS composites reaches 434.54Mpa. From the cross morphology of the fracture (Fig. 10), the long fiber extraction is mostly

concentrated in the low-density area of the material (see the circle in Fig. 3(a)). At the position of small holes in CNTs papers, the reaction speed of the CVI gas source (including trichloromethyl-silane, hydrogen) is greater than the diffusion speed of the gas, forming a bottleneck effect^[11]. The rapid densification of CNTs paper makes the matrix density between layers lower than other areas. The relative pull-out length of fibers should also be longer.

Compared with SCS composites, transfer channels in SCCS composites play an important role in significant enhancement of the bending strength. First, the transfer channels increase the density of SCCS composites as mentioned in Section 3.1. Second, the introduction of pitch-based C fibers can fill the mass transfer channel so that avoiding the problem of the transfer channel shrinking and leaving large holes in the subsequent CVI process^[25]. In addition, when the crack propagates between the layers and encounters the transfer channel in the Z direction, the main crack passes through the fiber, then the C fiber bundle are sheared, and the remaining cracks by-pass the transfer channel and continue to expand (Fig. 10(a)). The above two expansion methods will consume a lot of energy. Thus, the mechanical properties of SCS composites are lower than SCCS composites.

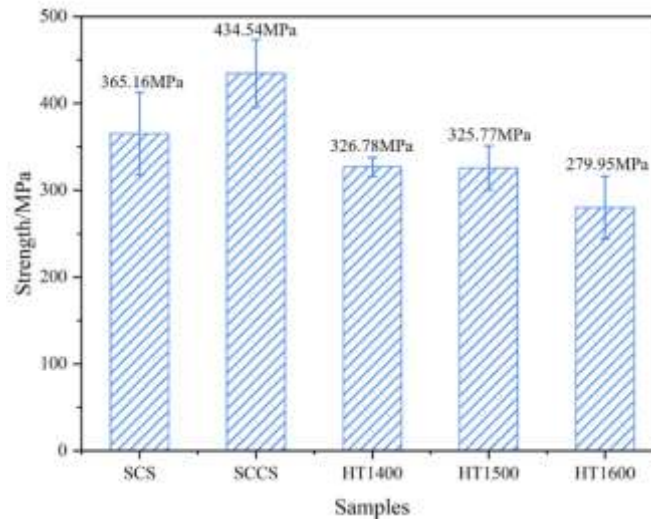


Fig. 8 The bending strength of SCCS composites after heat treatment.

When the heat treatment temperature rises, the bending strength of SCCS composites gradually decreases. On the one hand, the interlayer bonding strength of the samples decreases with the temperature increases. Owing to large difference of modulus between CNTs paper and SiC matrix, the deformation were different, which led to generation of micro-cracks. The cracks between CNTs paper layer and the SiC substrate could be clearly seen in Fig. 10(b), (d). Due to the decrease of interlayer bonding

strength after heat treatment, the crack tends to expand along the interface between CNTs paper and SiC matrix. In this work, the interlaminar shear strength has been shown in Fig. 9. After heat treatment, the interlaminar shear strength of composites drops to about half of that at room temperature. The pitch-based-C fibers in transfer channel is completely preserved when material destroyed, indicating that the fracture surface is not in the plane where the transfer channel located. The gap between the CNTs paper layers and the SiC matrix can be observed in the fracture images of the HT1400 and HT1600 samples. On the other hand, long-term high temperature treatment improves the crystallization degree of SiC fibers, potentially leading to fibers embrittlement^[35]. Although heat treatment can release the stress concentration at the crack tip and eliminate the residual stress, it cannot compensate for the damage to the mechanical properties of SiC fibers. The brittle fibers can't afford higher forces, which affects the mechanical properties of SCCS composites.

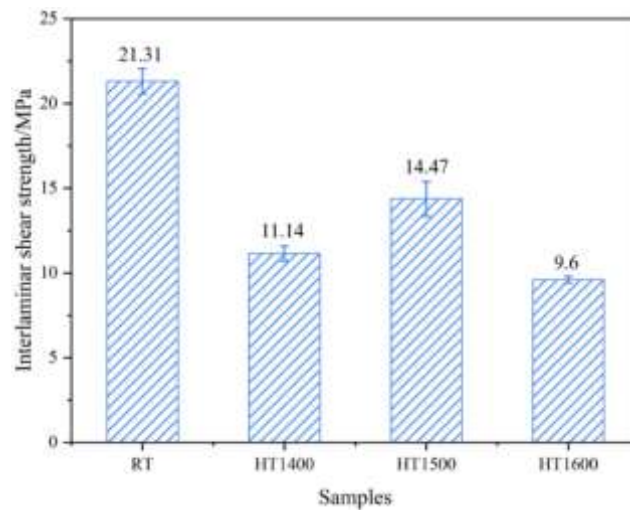


Fig. 9 The interlaminar shear strength of the composites after heat treatment.

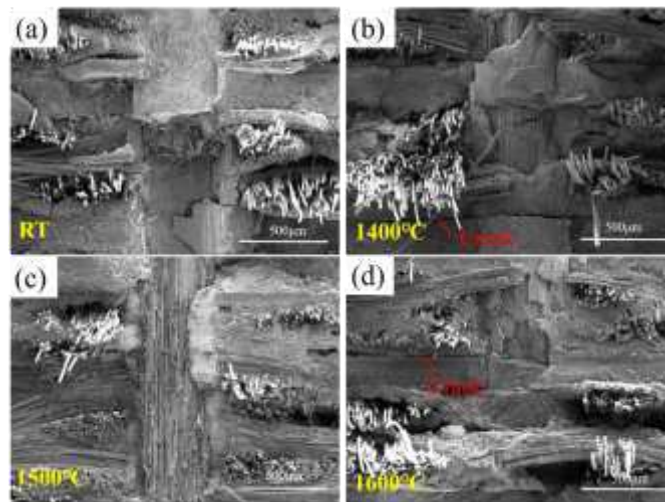


Fig. 10 Cross section of fracture at (a) room temperature; (b) 1400°C; (c) 1500°C; (d) 1600°C.

As exhibited on the fracture surface of interlaminar shear test (Fig. 11), SCCS composites exhibit three forms of failure. Cracks were generated in the plane between two notches at room temperature (Fig. 11(a)), passing through adjacent CNTs paper layer to SiC cloth layer until fiber cloth layer was destroyed. Multi-layer failure was observed in HT1400 composites, indicating that the main failure mode was stratified cross-over failure. The fracture of HT1500 sample was an ideal type of interlaminar failure, because the entire failure occurred at same layer, resulting in relatively pure interlaminar shear stress. Thus, the interlaminar fracture morphology was smooth. Furthermore, the modulus and hardness of CNTs paper are improved, which is conducive to the combination of CNTs paper layers and SiC matrix, resulting in abnormally increased interlayer shear strength of SCCS composites. The higher temperature reduced the hardness of the CNTs paper layer. Then cracks were easier to propagate in this layer. A large number of CNTs and scattered matrix were observed in the partial position of fracture (Fig.11(d)), which was left after the CNTs paper layer was destroyed.

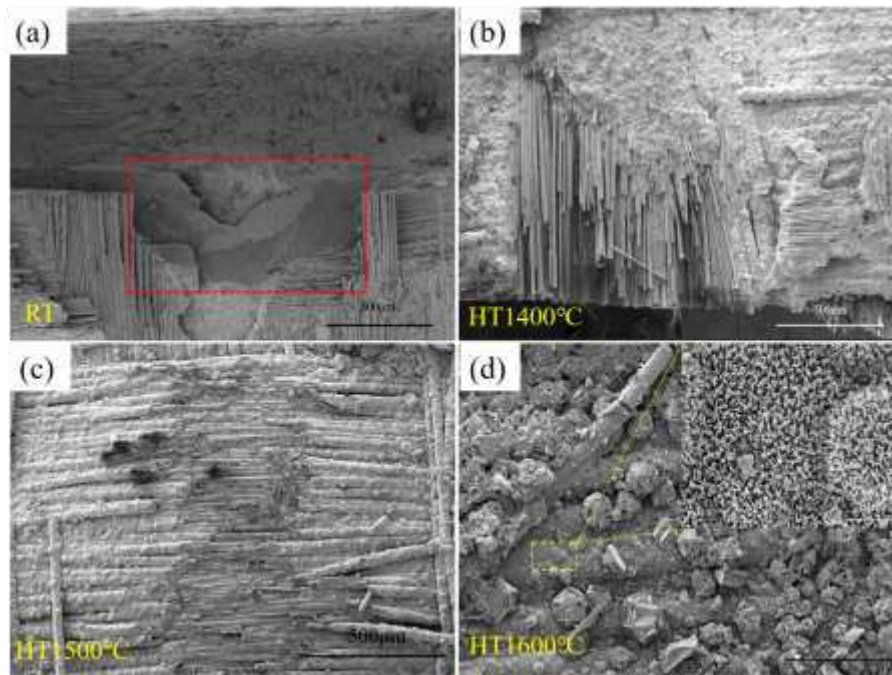


Fig. 11 Interlayer shear fracture morphology of composites at (a) room temperature; (b) 1400°C; (c) 1500°C; (d) 1600°C.

3.3 Thermal conductivity

In Katoh's research^[8], it was pointed out that the axial thermal conductivity of composites is determined by the volume fraction of axial fiber bundle and the matrix around the fiber. Cao et al^[36] built a vertical heat transfer channels in C/SiC composites,

which has a positive effect on improving the thermal conductivity of the material. In this paper, the three-dimensional network formed by C materials (CNTs, C fibers) significantly improves the thermal conductivity of SCCS composites.

The vertical thermal conductivity of SCCS composites has been analyzed based on the parallel serial model^[14], as shown in Fig. 12. In the direction of heat transfer, the volume fraction of the PyC interface is less than 3%, and its influence on thermal conductivity can be ignored^[37]. Similarly, the contribution of the SiC matrix in the pitch-based-C/SiC micropillars to the thermal conductivity can be ignored. As a result, the SCS composites has been considered as a multilayered composite consisting of the SiC/SiC composite layers and the CNTs paper layers. The thermal conductivity of SCCS composites could be represented as follows:

$$\frac{1}{K_{SCCS}} = \frac{V_{SiC/SiC}}{K_{SiC/SiC}} + \frac{V_{CNTs/SiC}}{K_{CNTs/SiC}} + \frac{V_{C_{fiber}}}{K_{C_{fiber}}} \quad (4)$$

Where $K_{SiC/SiC}$ is the thermal conductivity of traditional SiC/SiC composite, K_{CNTs} is the thermal conductivity of carbon nanotubes, $K_{C_{fiber}}$ is the thermal conductivity of pitch-based C fiber. V is the volume fraction of each part.

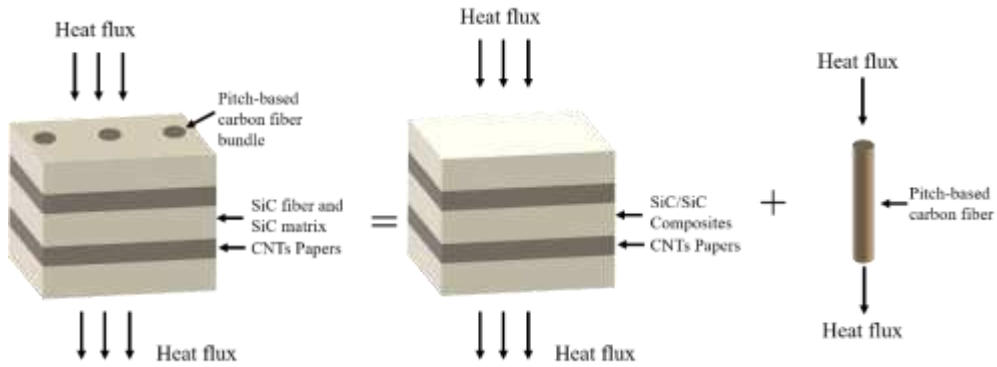


Fig. 12 Thermal conductivity calculation model of SCCS composites.

Fig. 13 exhibits vertical thermal conductivity of SCCS composites and SCS composites at room temperature. The thermal conductivity of SCS and SCCS composites is higher than that of traditional SiC/SiC composites. The main reason is that high thermal conductivity phase provides a thermal conduction path for the transmission of phonons in SCS and SCCS composites. The vibration of phonons makes a major contribution to the heat conduction in insulating solid, which limited by phonon-boundary scattering, phonon-defect scattering and umklapp processes^[38]. Considering the thermal resistance of the interface between CNTs layer and SiC matrix, the thermal conductivity of SCS composites is lower than the value calculated by Eq.

(2)^[39]. As for SCCS composite, the vertical transfer channel prevents phonons from being transmitted to the interface and scattered.

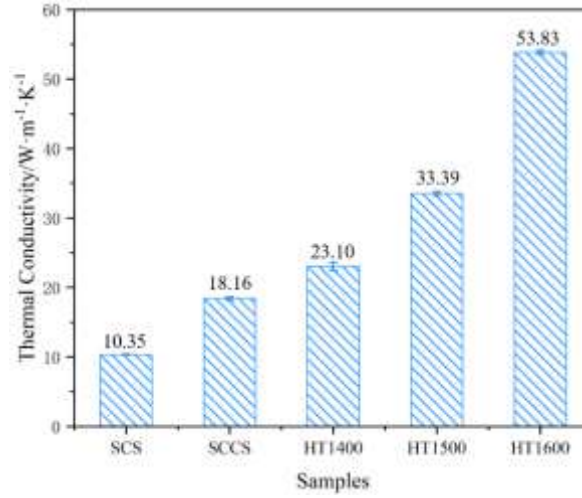


Fig. 13. Thermal conductivity of SCS and SCCS composites at room temperature (vertical direction).

In addition to high thermal conductivity phase content and transfer channels, the crystallization degree of the SiC matrix and SiC fiber can also improve the thermal conductivity of SCCS composite. The atoms in the untreated SiC fiber were arranged completely randomly. However, the disorder of the SiC fiber is reduced after heat treatment. Thermal conductivity can be described as follow formula in dynamics theory:

$$K = \frac{1}{3} C v \Lambda \quad (5)$$

Where v is the average speed of phonons, C is the specific heat capacity, and Λ is the mean free path of phonons. According to Feng's research^[27], the higher the heat treatment temperature, the larger the grain size of the SiC matrix, which means that the mean free path of phonons increases. So as we see in Fig. 13, the thermal conductivity of SCCS composites increase to 2.96 times with the temperature of treatment rises from room temperature to 1600°C.

In-plane thermal diffusivity and thermal conductivity of SCCS composites were exhibited in Table 3.

Table 3 In-plane thermal diffusivity and thermal conductivity of SCCS composites at room temperature and after 1600°C heat treatment.

SCCS composites	Test temperature/°C	Thermal diffusivity/mm/s ²	Thermal conductivity/W/(m • K)
RT	25.1	7.47	18.60
HT1600	25.1	11.99	29.85

Generally, the interfacial thermal resistance was considered when it was not parallel to the direction of heat flow. In CNTs layers, abundant interfaces between CNTs and SiC matrix were randomly distributed and hinder the heat transfer. The thermal conductivity of CNTs/SiC ceramic is much lower than theoretical thermal conductivity of CNT^[40]. The direction of transfer channels were perpendicular to the direction of plane heat flow, which could not improve the efficiency of phonon transfer. On the contrary, the interface thermal resistance between transfer channels and CNTs/SiC ceramic layers, SiC/SiC composite layers were generated. As the data in Table 3 shows, in-plane thermal conductivity were similar to vertical thermal conductivity (Fig. 13) of SCCS composites at room temperature. In-plane thermal conductivity shown the same trend as vertical thermal conductivity due to higher degree of crystallization after 1600°C heat treatment.

4. Conclusion

In this paper, the heat treatment of SiC-CNTs-C/SiC composites prepared by CVI has been studied. The microstructure, the bonding status between CNTs/SiC layer and SiC matrix, the mechanical properties and the thermal conductivity were discussed.

After heat treatment, grain size of SiC fibers raised and the crystallization degree of the SiC matrix increased. At 1600°C, SiC matrix showed two shapes: triangular pyramid-shaped sharp or hexagonal prism-shaped.

The elastic modulus and hardness of CNTs paper layers had decreased due to the growth of grains. Although transfer channel consumes energy and had a certain reinforcing effect, SiC fibers could not withstand long-term high temperature treatment. Thus, the bending strength of heat-treated SCCS composites was lower than that of composites untreated.

CNTs paper and pitch-based C fiber construct the three-dimensional network structure of carbon materials, which plays an important role in improving the thermal conductivity of SCCS composites. After heat treatment, the rise of mean free path of phonons increases the thermal conductivity (vertical direction) to 2.96 times. In plane, a large number of interfacial phases reduced advantage of CNT in thermal conductivity and the existence of transfer channels increased interfacial thermal resistance. As a result, in-plane thermal conductivity was close to vertical thermal conductivity.

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Figures

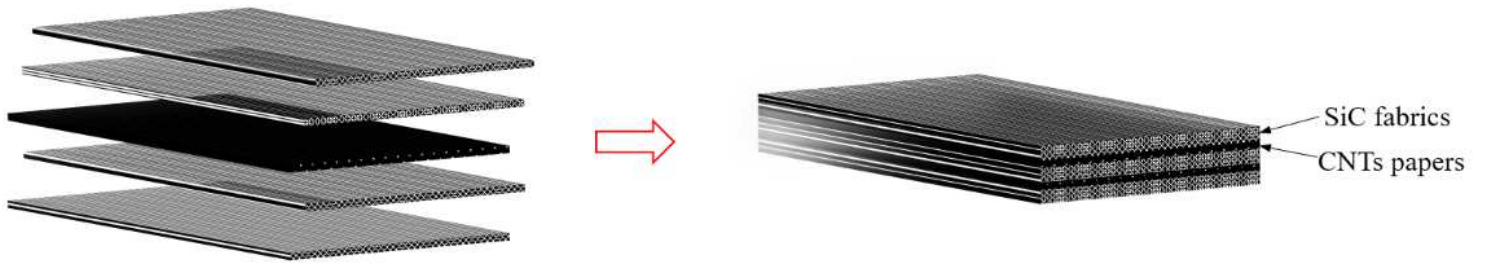


Figure 1

Stacking pattern of SiC-CNTs/SiC composites(SCS).

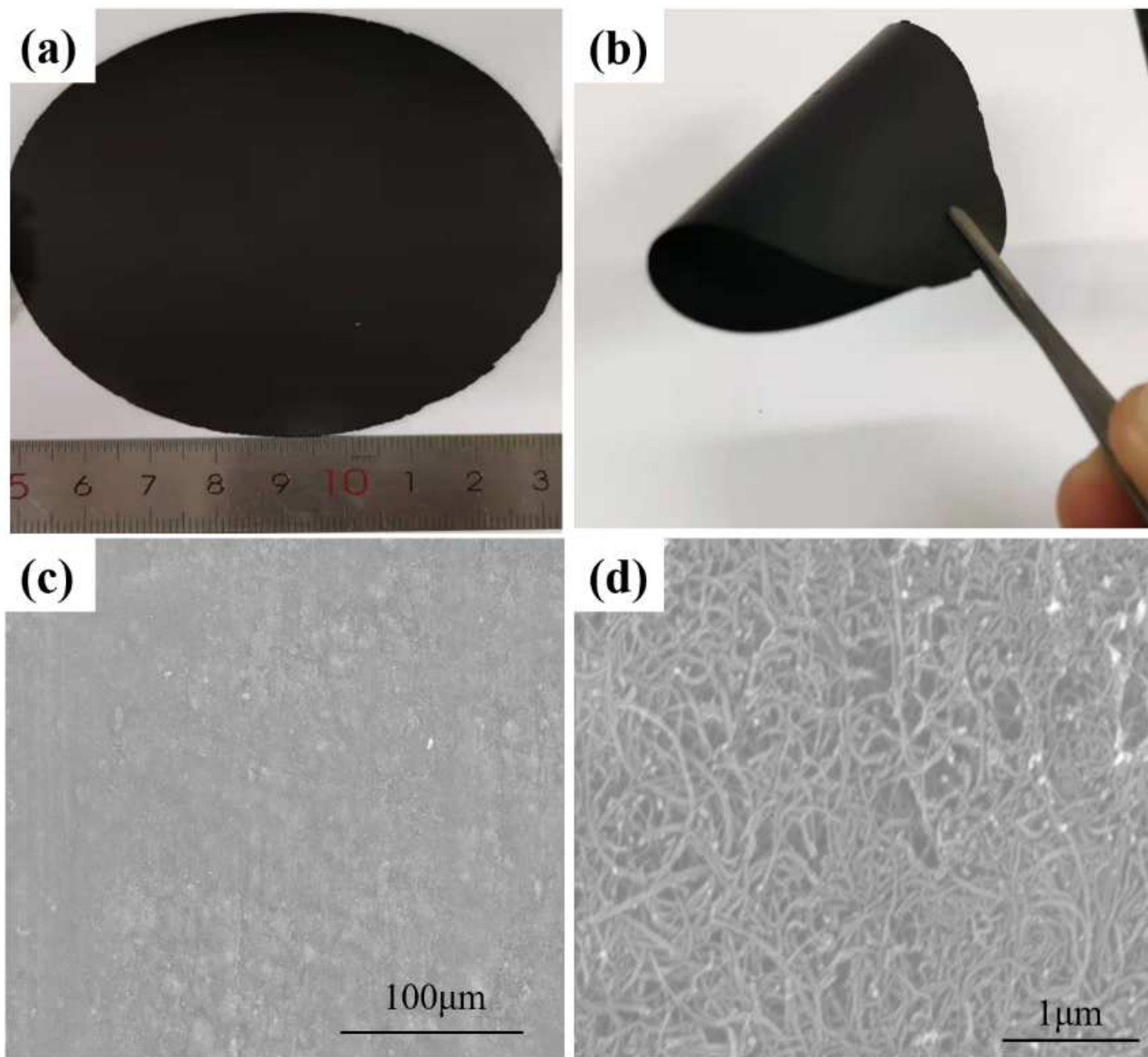


Figure 2

Morphologies of CNTs paper. (a) macro view; (b) flexibility of CNT paper (c) CNT paper at low magnification; (d) CNT paper at high magnification.

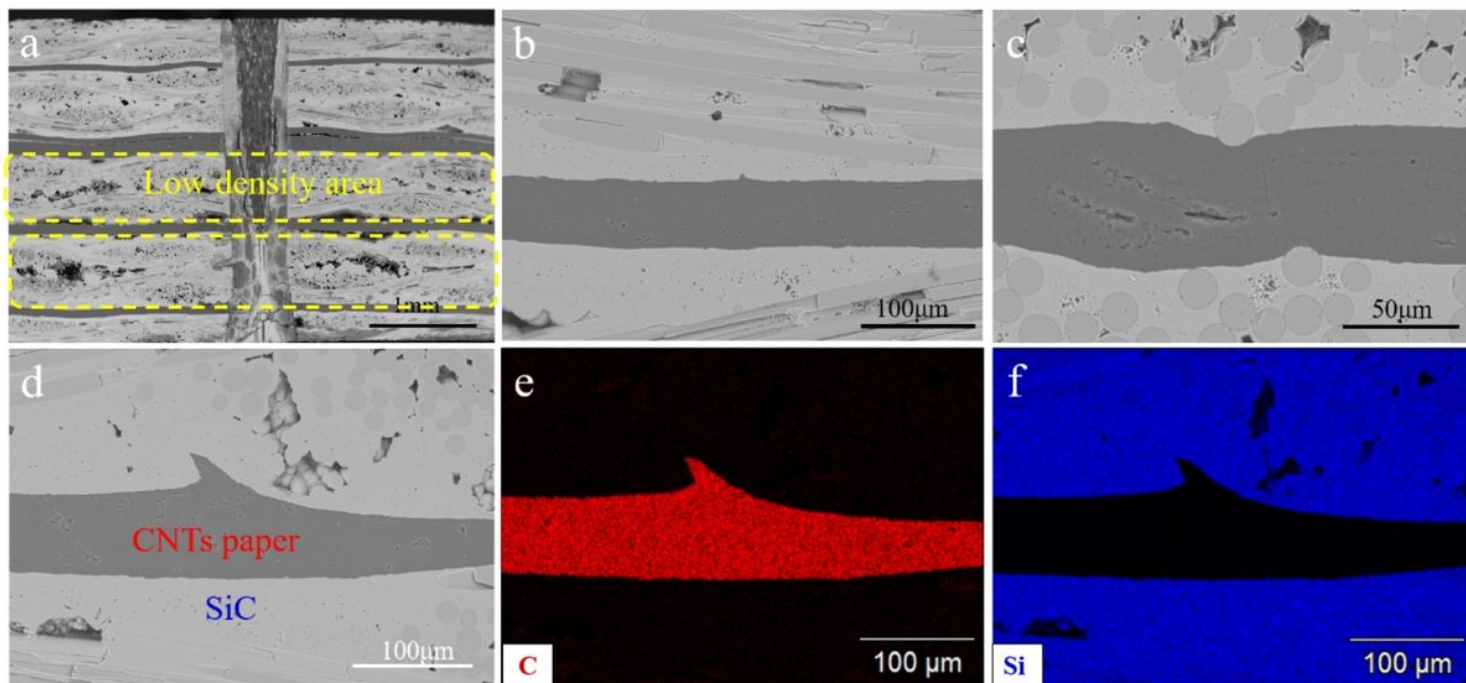


Figure 3

Morphologies of CNTs paper layers in SCS composite. (a)-(c) BSE images of SCCS composite. (d)-(f) Energy dispersive near the CNTs papers.

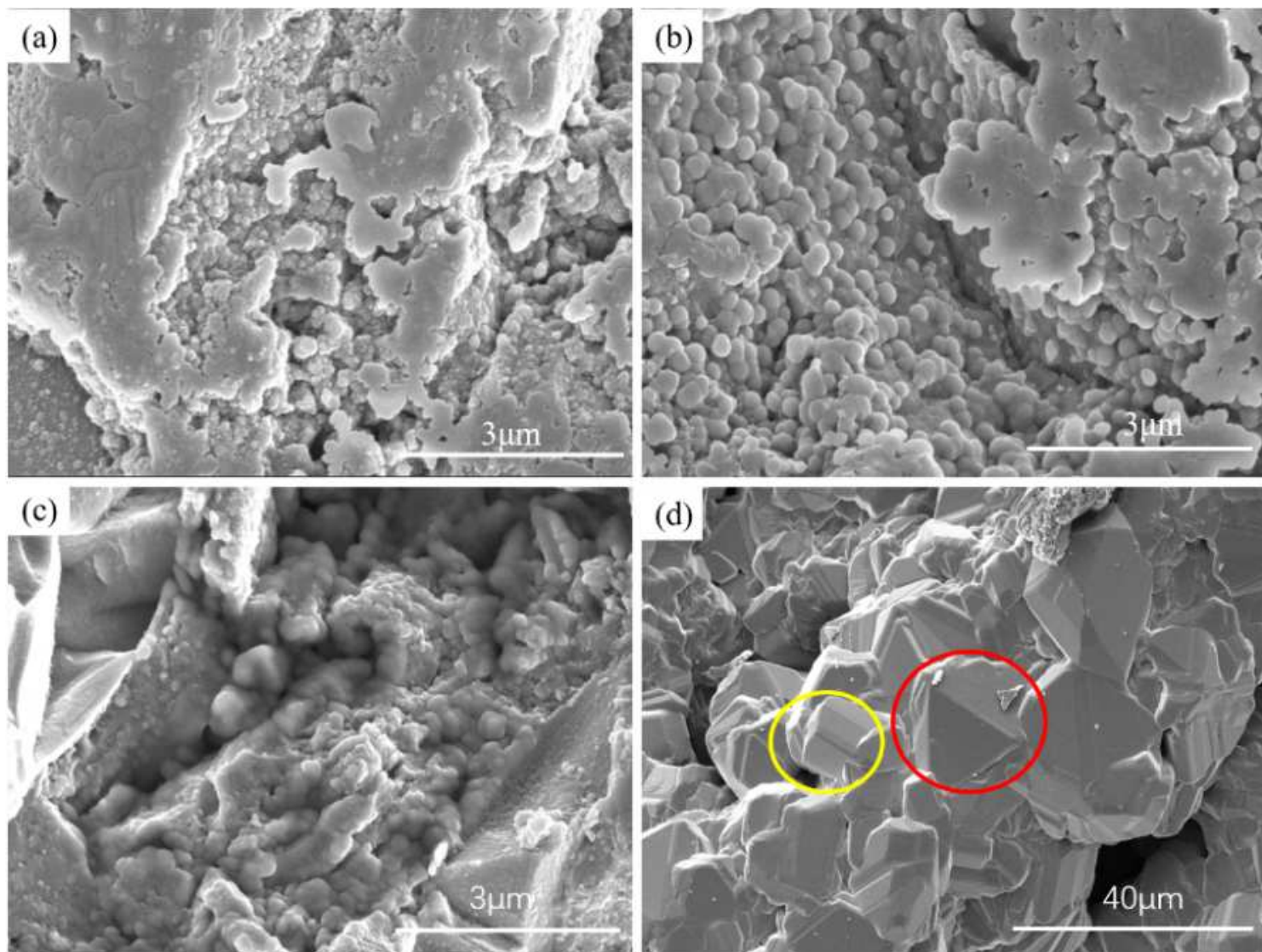


Figure 4

Morphology of SiC matrix after heat treatment at different temperatures for 2 hours. (a) Room temperature; (b) 1400°C treatment; (c) 1500°C treatment; (d) 1600°C treatment.

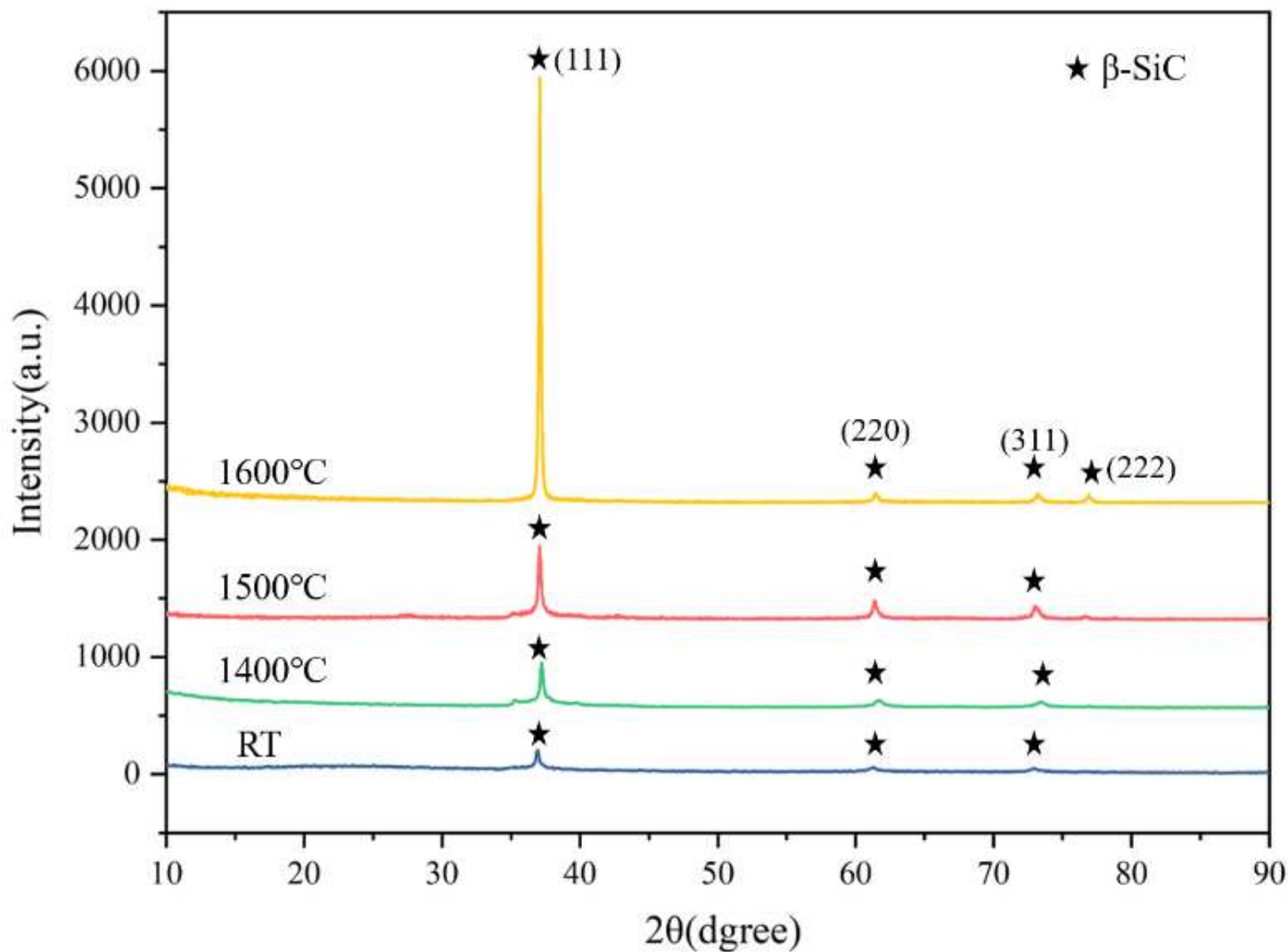


Figure 5

X-ray diffraction patterns of samples at different heat treatment temperatures.

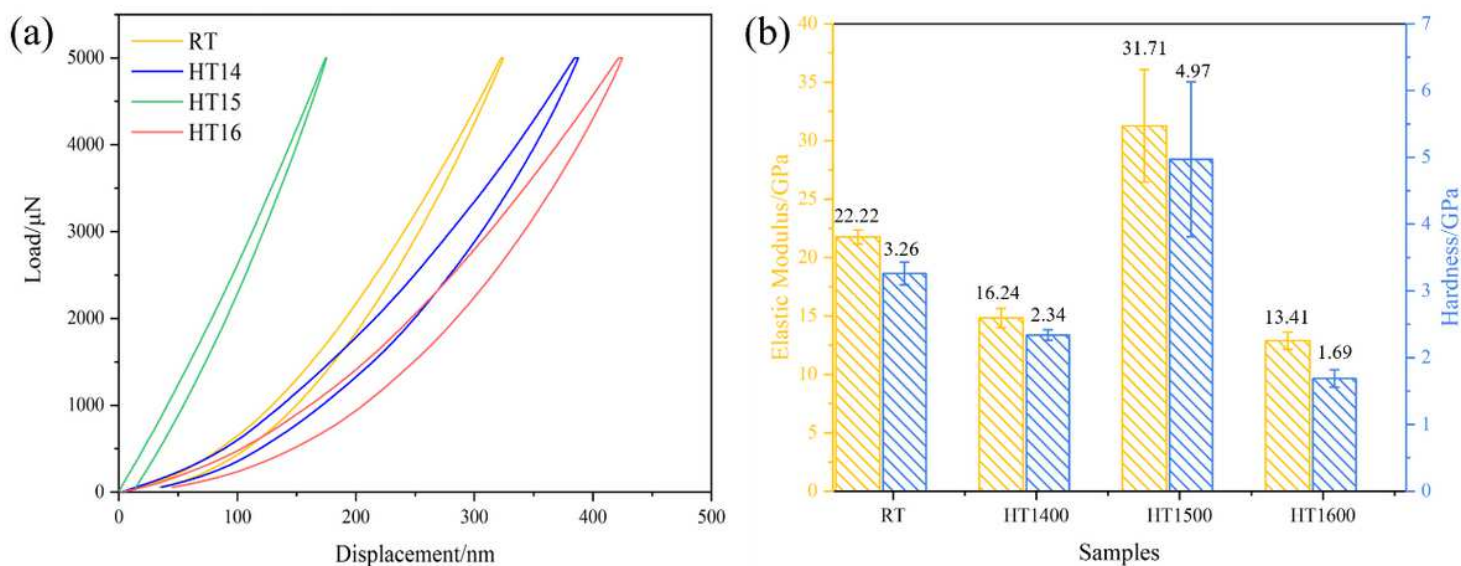


Figure 6

Micromechanical properties of CNTs paper layers in SCCS composites (tested by nanoindentation). (a) Load-Displacement curves of CNTs papers; (b) Elastic modulus and Hardness of CNTs papers after heat treatment.

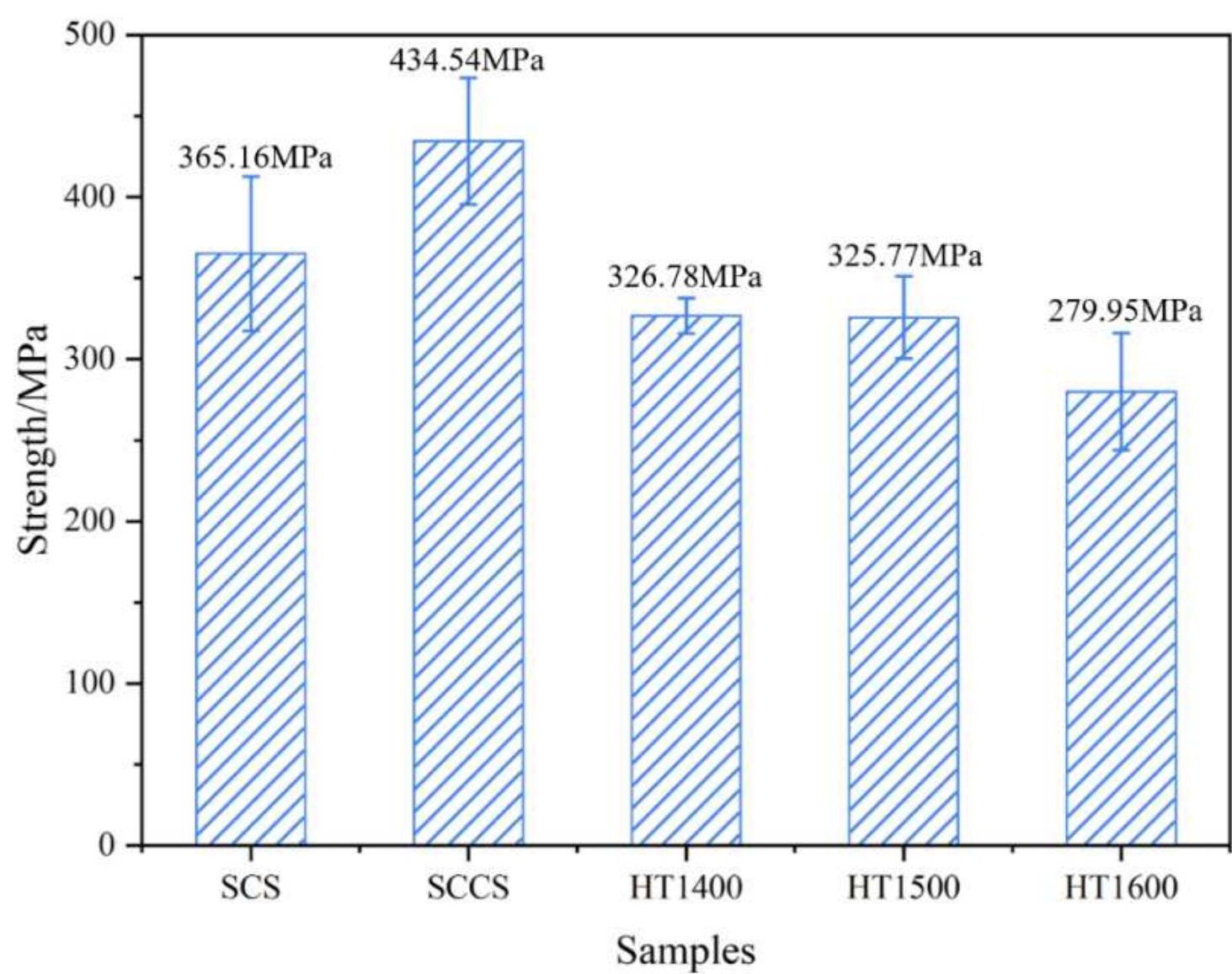


Figure 7

The bending strength of SCCS composites after heat treatment.

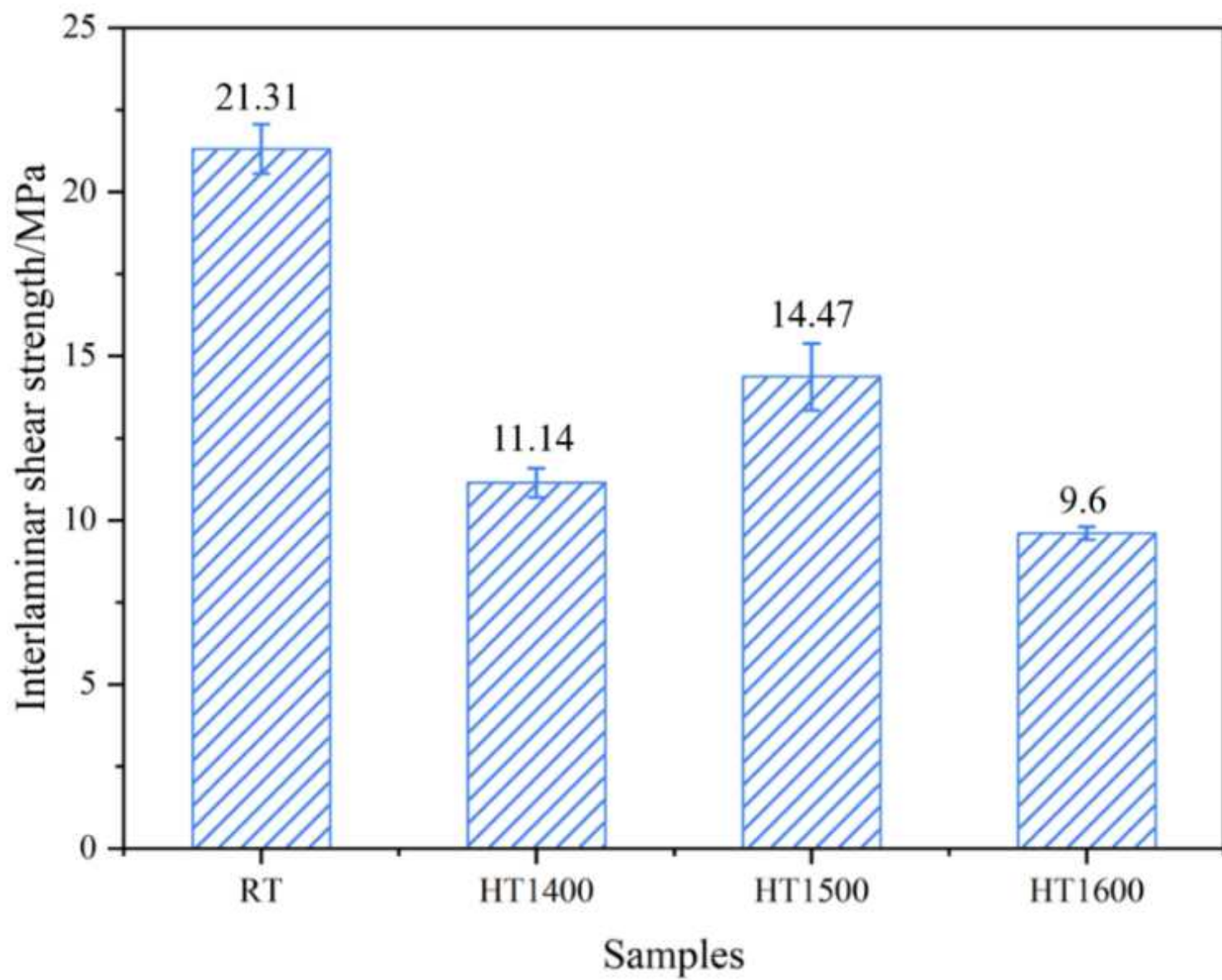


Figure 8

The interlaminar shear strength of the composites after heat treatment.

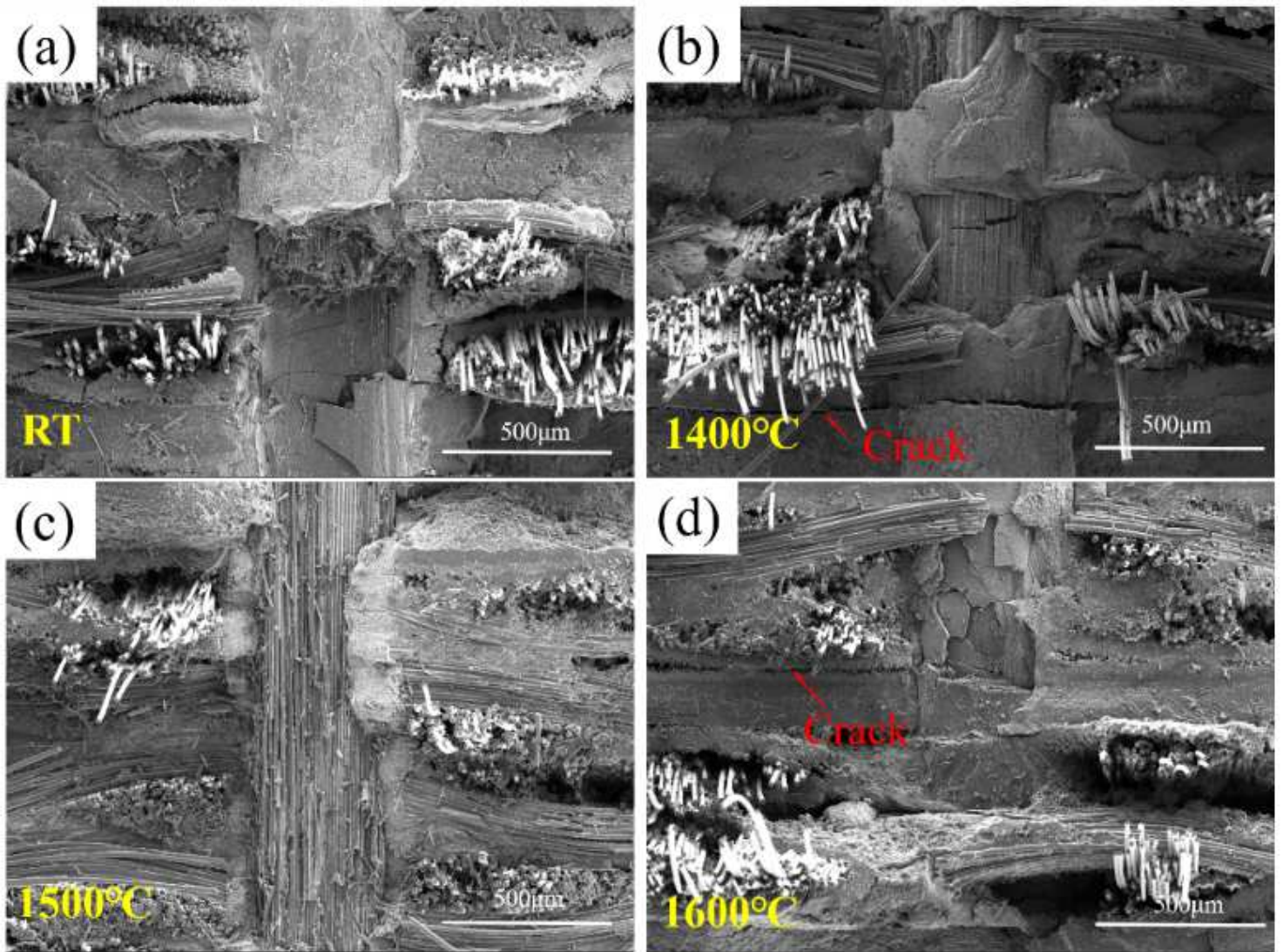


Figure 9

Cross section of fracture at (a) room temperature; (b) 1400°C; (c) 1500°C; (d) 1600°C.

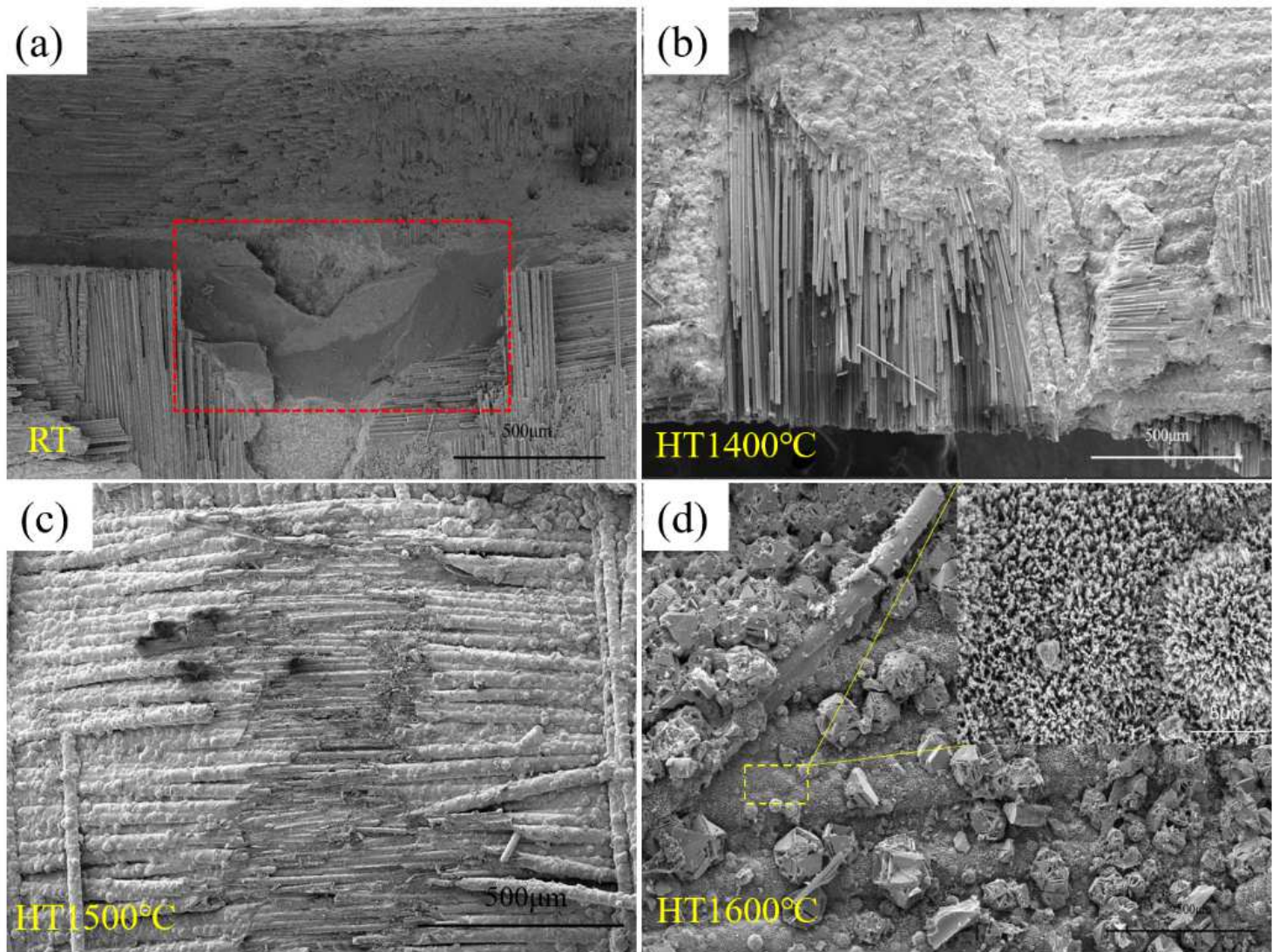


Figure 10

Interlayer shear fracture morphology of composites at (a) room temperature; (b) 1400℃; (c) 1500℃; (d) 1600℃.

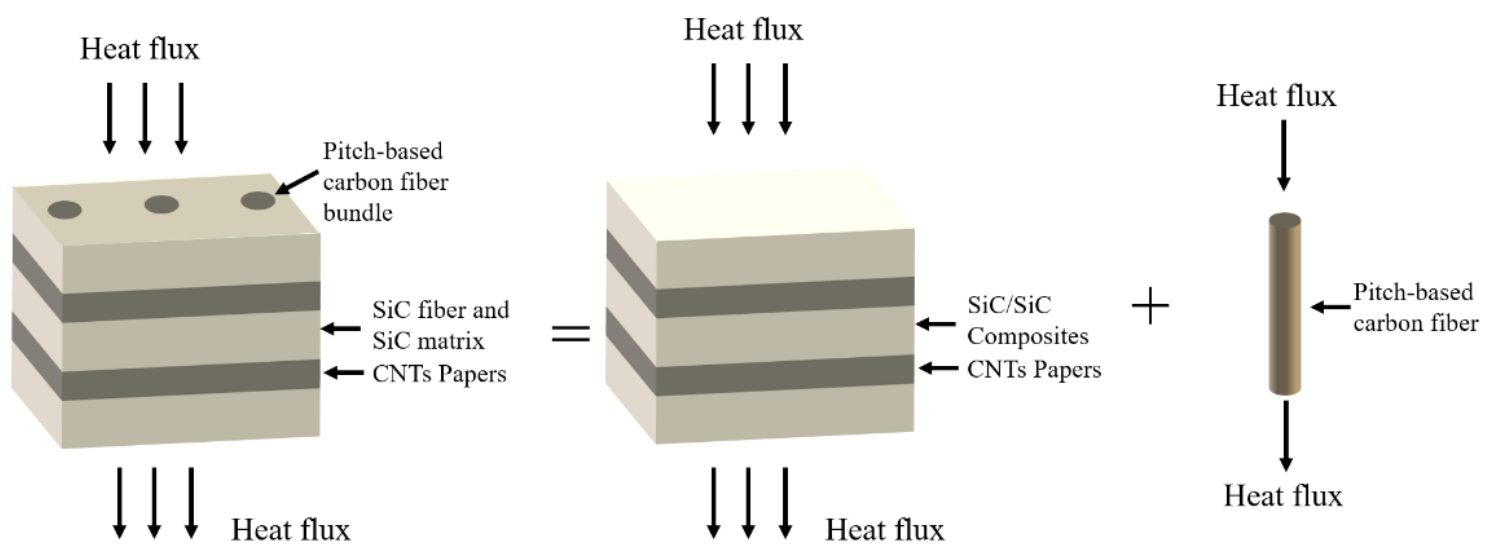


Figure 11

Thermal conductivity calculation model of SCCS composites.

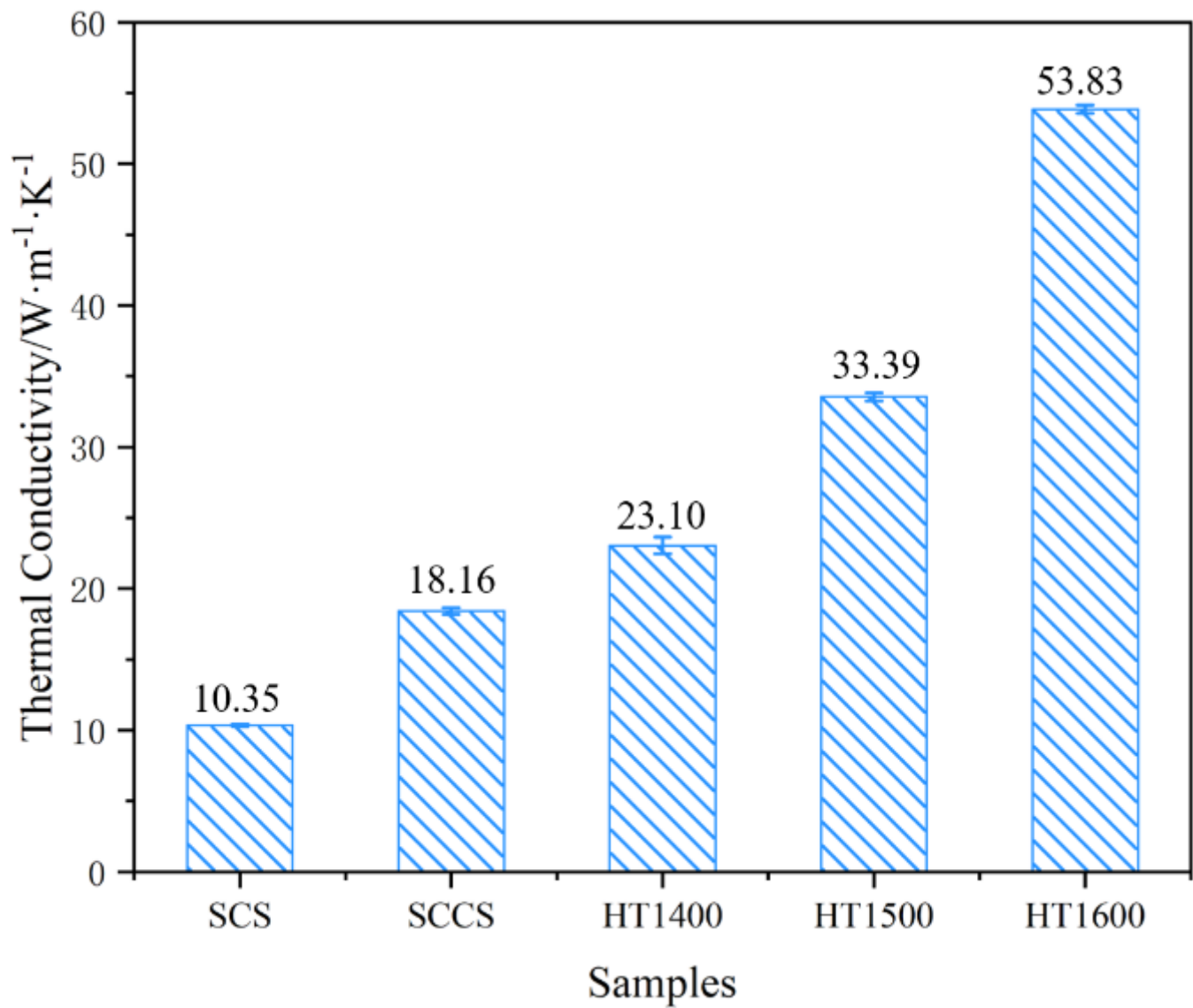


Figure 12

Thermal conductivity of SCS and SCCS composites at room temperature (vertical direction).