

THE GEORGE WASHINGTON UNIVERSITY

WASHINGTON, DC

SCHOOL OF ENGINEERING AND APPLIED SCIENCE DEPARTMENT OF ELECTRICAL AND COMPUTER ENGINEERING ECE 2115: ENGINEERING ELECTRONICS LABORATORY

Tutorial #6: *Designing a Common-Collector Amplifier*

BACKGROUND

In the previous lab, you designed a common-emitter (CE) amplifier. Voltage gain (A_V) is easy to achieve with this type of amplifier. As you discovered, the input impedance (R_{in}) of the CE amplifier is moderate-to-high (on the order of a few k Ω). The output impedance (R_{out}) is high (roughly the value of R_C). This makes the common-emitter amplifier a poor choice for “driving” small loads.

A common-collector (CC) amplifier typically has a **high input impedance** (typically in the hundred k Ω range) and a very **low output impedance** (on the order of 1 Ω or 10 Ω). This makes the common-collector amplifier excellent for “driving” small loads. As you discovered in Lab 6, the common-collector amplifier has a voltage gain of about 1, or **unity gain**. The common-collector amplifier is considered a **voltage-buffer** since the voltage gain is unity. The voltage signal applied at the input will be duplicated at the output; for this reason, the common-collector amplifier is typically called an **emitter-follower amplifier**. The common-collector amplifier can be thought of as a **current amplifier**.

When the common-emitter amplifier is cascaded to a common-collector amplifier, the CC amplifier can be thought of as an **“impedance transformer.”** It can take the high output impedance of the CE amplifier and “transform” it to a low output impedance capable of driving small loads.

Figure 1 shows a typical configuration for a common-collector amplifier. The input voltage is applied to the base while the output voltage is measured at the emitter.

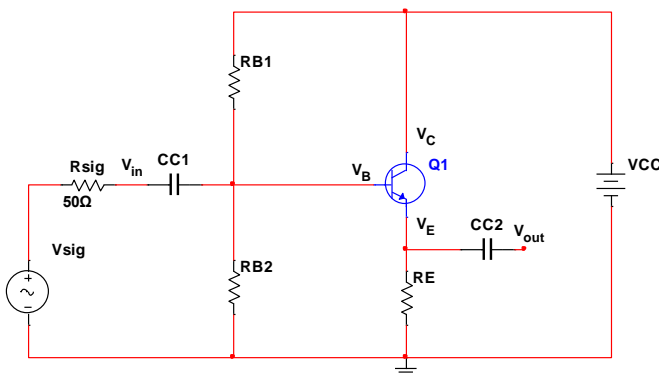


Figure 1 – Common-Collector Amplifier

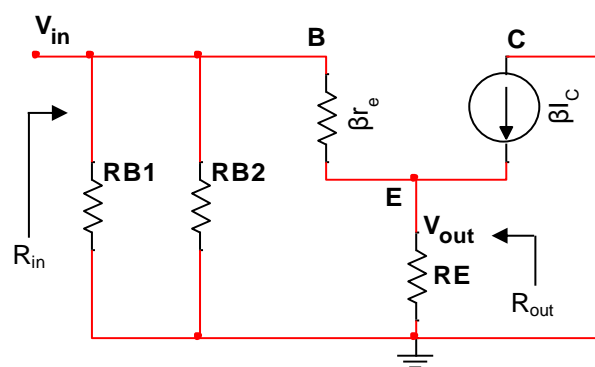


Figure 2 – Small Signal (AC) Equivalent (Neglecting R_{sig})

From the AC equivalent of the common-collector amplifier in **Figure 2**, we can derive expressions for the **input impedance**, **output impedance**, and **voltage gain**:

$$R_{in} = R_{B1} || R_{B2} || [\beta r_e + (\beta + 1)R_E] \quad (\text{no load}) \quad (\text{Remember: } r_e = V_T / I_E, \text{ where } V_T = 26\text{mV})$$

$$R_{out} = R_E || r_e \quad \text{but } r_e \ll R_E \rightarrow Z_o \approx r_e \quad (\text{notice this is VERY small})$$

$$A_V = \frac{V_{out}}{V_{in}} = \frac{(\beta+1)i_b R_E}{\beta i_b r_e + (\beta+1)i_b R_E} \cong \frac{\beta i_b R_E}{\beta i_b (r_e + R_E)} = \frac{R_E}{r_e + R_E}, \quad \text{but since } r_e \ll R_E, \text{ then}$$
$$A_V \approx 1$$

INSTRUCTIONS

Designing a Common-Collector Amplifier

Problem: Design a common-collector amplifier using the 2N3904 transistor that meets the following specs:

- $I_C = 1\text{mA}$
- $V_{CC} = 20\text{V}$
- $R_{in} = 70\text{k}\Omega$
- $R_L = 510\Omega$
- $V_{in} = 10\text{mV} @ 10\text{kHz}$

1. **Determine** the value of R_E .
 - a. We typically make $V_E = \frac{1}{2} V_{CC}$ to ensure the largest possible symmetric output voltage swing around V_E .
 - b. It is safe to assume that $I_E \approx I_C$.
 - c. **Calculate** the value of R_E .
2. **Determine** the “Q” point of the transistor.
 - a. Because you now know V_{CE} and I_C , you can use the same procedure from the “**Designing a Common-Emitter Amplifier**” tutorial to create an IV-curve for the transistor and determine the Q-point of the transistor. This will help you determine the necessary “base current” needed to achieve the specified I_C .
 - b. **Use** the Q-point data to find DC values for: I_B , V_B , I_E , and β .
3. **Use** V_{CC} , V_B , I_B , I_E , and R_{in} to find R_{B1} and R_{B2} .
 - a. **Follow** the procedure from the previous tutorial to generate the same **three** equations for V_{BB} (**Equation 1**), R_B (**Equation 2**), and I_B (**Equation 3**).
 - b. **Use** the equation derived in the first part of *this* tutorial for R_{in} as **Equation 4**.
 - c. **Calculate** R_{B1} and R_{B2} using the four equations.
4. **Check** your calculations.
 - a. **Use** the R_{in} equation to calculate R_{in} . Is it $70\text{k}\Omega$?
 - b. **Use** the R_{out} equation to calculate R_{out} . Is it very small?
5. **Set** values for C_{C1} and C_{C2} .
 - a. The impedance of a capacitor is $Z_C = \frac{1}{j2\pi fC}$. We can use this knowing that we want C_{C1} and C_{C2} to all look like “shorts” at 10kHz (the input frequency), and select a value that we have in the ECE 2115 kit.
6. **Determine** the **current gain** (A_i) of the amplifier.
 - a. **Current gain** is defined as $A_i = I_{out} / I_{in}$.
 - b. **Use** the equations for A_v , R_{in} , and R_{out} , Ohm’s law, and a little algebra to determine the equation for A_i .
 - c. **Calculate** A_i for your amplifier. **Verify** current gain using a Multisim transient simulation.
7. **Verify** your calculations using Multisim.
 - a. **Simulate** your amplifier. **Check** the bias-point (DC) analysis to determine if your transistor is at the Q-point you desire.
 - b. **Perform** a transient simulation to verify the **voltage gain**, **current gain**, R_{in} , and R_{out} .