RME-101, ST 2, SOL, Odd, 1718 Section A Q1 Write the assumptions made in the analysis of tress. i) All members have negligible weight ii) All members have uniform cross-section iii) All members have only axial force. Explain E, G and K. 92 Modulus of elasticity (E).

Normal stress ( $\sigma$ ) is directly proportional to normal strain( $\epsilon$ ), and the ratio is known as modulus of clasticity. Sol. Modulus of Rigidity (G). The rate of shear stress to shear strain is known as modules of Rigidity Bulk modules (K). The Rate of volumetric stress to volumetric strain is a constant known as bulk moduly. Q3 Write the relationship between load, shear force and bending moment. Consider a Section ABCD fa which (D is used for analysis. Relation Yw load & Loar force  $\frac{dV}{dx} = -\omega(x)$ Relation b/w shear face & bending M.  $\sqrt{\sqrt{(M+\Delta M)}}$ dm = V

Q4 State the parallel-axis theorem and perfendicular axis theorem for moment of mertias of areas. i) Perfondicular axes theorem. Moment of inestia of an area about an axis perpendicular le ets plane at any point is equal to the sum of monunts of inertia about any two mutually perpendicular axis through the same point in the plane of the area 11) Parallel axes theorem Moment of inertia of any area about an axis in its plane is the sume of moment of inertie about a parallel and passing through the centroid of the area and the product of area and square of the distance between two parallel axes Draw stress strain diagram for mild steel. Qs Sol. lower yield point 5 Ultimalistics Rufture point c. Upper Yield point B. Elastic Limit A Proportional Yielding Plastic Region

Q6 Determine the centroid of the staded plane are shown.

Sol The shaded area can be obtained by subtracting the simicircle of triangle from the given square

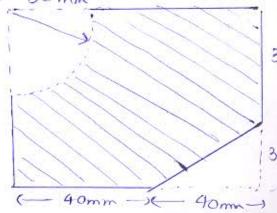
> The calculations are tabulated as follows.

	*	-100	-	<u>&gt;</u>	125
/				5 ]	1
					100
					725

Part-No	Alia.	×	y
1	Square 150×150 = 22500	75	75
2	Triangle -5 x 50x100 = -2500	50%	150-100
3	Semicicle - 3927	150 - 4×50	50+25

$$\overline{X} = \frac{\sum A_X}{\sum A} = \frac{8459003.94}{16073} = 70.93 \text{ units}$$
  
 $\overline{Y} = \frac{\sum A_Y}{\sum A} = \frac{1101308.33}{16073} = 68.52 \text{ units}$ 

Q7 Find the moment of inertia of given figure about loizontal centroidal axis. 30 mm &d. The shaded area can be obtained by subtracting the area of a quarter cycle and triangle from a rectangle given.



For sectangle. Y = A, y, -A2 /2 - A3/3 A,= (40+40)x(30+30) A, -A2-A3 For quarter incle 104588.5  $A_1 = - \underbrace{\pi \times 30^2}_{4}$ 3493.14 29.94 mm  $y_{L} = 60 - 4 \times 30$ For triangle A3 = - 1 × 40 × 30 y3 = 30  $I_{\times \times} = \mathbb{Z}\left(I_{\times} + A(y-\overline{y})^{*}\right)$  $= \left[ \frac{80 \times 60^{3}}{12} + 80 \times 60 \times (30 - 29.94)^{4} \right]$  $-\left[0.055\times30^{4}+\frac{1}{12}\times30^{4}\times(17.33)^{4}\right]$  $-\left[\frac{40\times30^{3}}{36}+\frac{1}{2}\times40\times30\times\left(\frac{30}{3}-29-94\right)^{2}\right]$ = 914,885.85 mm Q8 Derive the expression for elongation of rectangular lapaed bar subjected to longitudinal load.

Lapared bar subjected to longitudinal load.

Sol- Tapared bars with rectangular cross-section considure a tapaced bar of length L, constant thickness thank wieth varying per a linearly from a 6 6 to day of day of the say as shown.

Area of steip = 
$$6't$$
  
=  $\left[\alpha + \left(\frac{\alpha - \alpha}{l}\right)\pi\right]t$ .

Elongation of differential element =  $\frac{PL}{AE}$ =  $\frac{Pdn}{[\alpha + (b-a)\gamma]+E}$ 

Total elongation 
$$SL = \frac{P \ln \left[a + \left(b - a\right)x\right]L}{\left[a + \left(b - a\right)x\right]}$$

$$= \frac{PL \left(\ln b - \ln a\right)}{t \left(b - a\right)E} = \frac{PL \ln \left[a + \left(b - a\right)x\right]L}{\left[a + a\right]}$$

Q9 For the truss shown in figure, calculate the forces in members BD, CD and CE by the medhod of section.

Let extensions of FA - 1.5m

and GC meet at a point

O. Now from similar triangle + 2m + 2m - 1.5m

we can have,

$$\frac{OF}{FG} = \frac{OB}{BC}$$

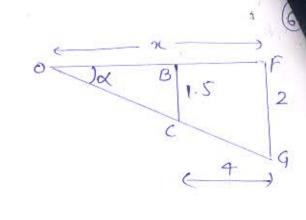
$$\frac{AC}{2} = \frac{x-4}{1.5}$$

$$x = 16$$

$$ACSO$$

$$tan x = \frac{FG}{OF}$$

$$= \frac{2}{16}$$



Taking a section through the members whose value is to be determed we have. 40KN FBD >

$$\left( \frac{\tan 0}{1.5} \right)$$

-40-30+FCD (0)0-FCE Sind =0

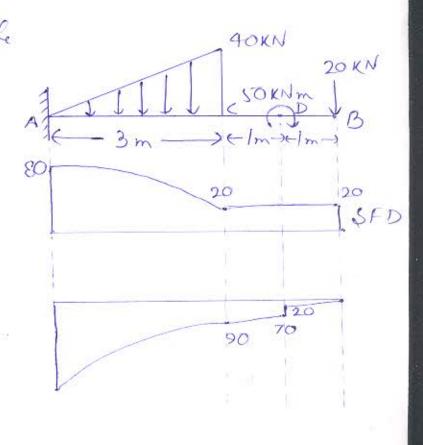
Also SFx =0

From equations O 20, we have,

Sob. Let RA and MA be the vertical component of deaction and reaction moment respectively at A.

E Fy = 0

RA = \frac{1}{2} \times \frac{3}{2} \times \frac{4}{3} \times \frac{3}{3} \times \frac{4}{3} \times \frac{3}{3} \ti



Shear foice values.  $V_A = 80$   $V_C = 180 - \frac{1}{2} \times 3 \times 40 = 20$  $V_D = 0$  Binding moment values  $M_{A}=-2.70$   $M_{B}=-2.70+80\times3-60\times1$   $M_{D}=-2.70+80\times4-60\times2+50$   $M_{B}=-2.70+80\times5-60\times3$  +50

## Section C

PII Find the axial forces in all the members of the truss shown in figure.

Sol. From FBD of the tours shown, 5 10 = 0 8 KN -8×2.4-8×4.8-10×7.2+RH×9.6=0 RH = 13.5 2 Fy=0 RA-8-8-10+ RH =0 1-2.4mx-24m-1-24m-1-24m-1 RA = 12.5 From FBD QA, 5 Fy 12.5 + FAB Sinx =0 FAB = -12.5 Sinx  $t_{\text{max}} = \frac{3.6}{4.8} = 36.87$ = -20.83 KN EFX FABCOSX + FAC =0 FAC = 16.67 KN From FBD of B, -8 + FABSin x - FBC + FBD Sin x = 0 FBD sin x - FBC = -4.498 2 FX + FBD (OX + FAB (OX = O FBD = -20.83 KN In triangle CDE, Tang = DE = 3.6 2.4 B = 56.31

2 Fy =0

-8 + FCD sin B = 0

FCD= 9.61 KN

5Fx=0

-16.67 +FCE +FCD (08 B = 0

FCG = 11.34 KN

From FBD of H

2 Fy=0

13.5+ FFHSind = 0

FFH = -22.5 KN

EFX

- FFH COSX - FGH=0

Fan= 18 KN

From FBD OF F

5 Fx = 0

FDF COSX = 22.5 COSX

FDF = 22.5

5 Fy=0

-FDF sinx-10+225 sinx+FFG=0

FFG =10

From FBD & G

2 Fy

FDG Smp - 10 = 0

FDG = 12. KN

2FX

- FDG(OB-FEG+FGH=0

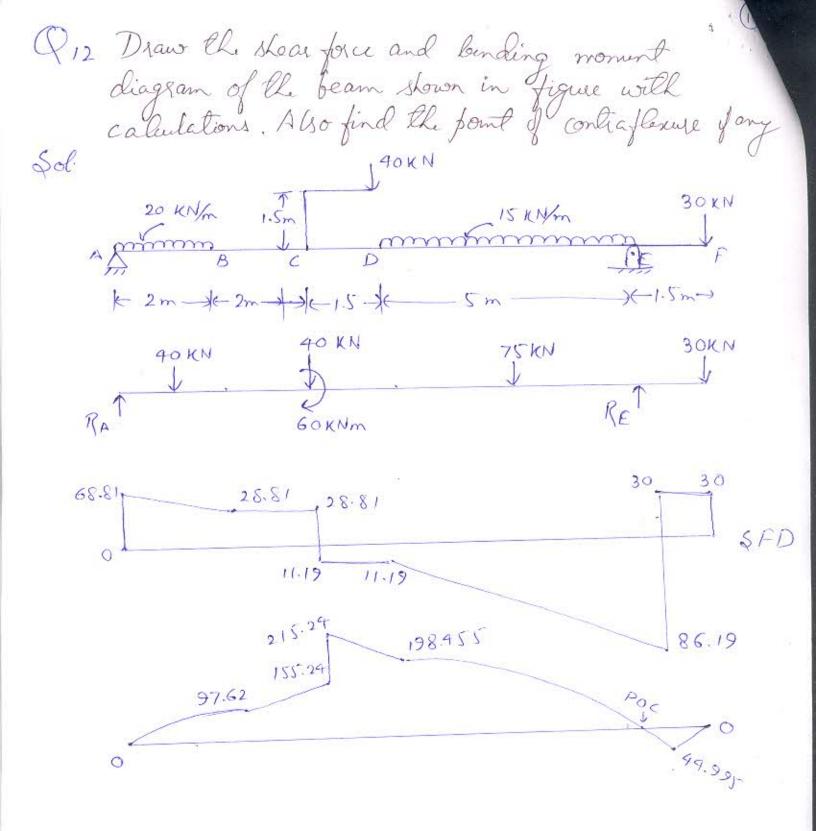
FEC = 11-34 KN

16-67 FCE

FEH 13.5

FDF 110
F 15 × 22.5
F F 9

FDG BC 10
FEG FGH



Let  $R_A$  and  $R_E$  be the vertical reactions at  $A \lambda E$ . We have  $2M_A = 0$   $-40 \times 1 - 40 \times 4 - 60 - 75 \times 8 + R_E \times 10.5 - 30 \times 12 = 0$ RE = 116.19 KN Shear Force Values

 $V_{A}^{L} = 0$  R = 68.81

VB =+68.81-40 = 28.81

 $V_{c}$  L = 28.81 R = -11.19

VD = -11.19

 $V_E = -11.19 - 75 = -86.19$  R = 30  $V_F = 0$ 

Bending Moment Values

MA = 0

MB = 68.81 × 2 = 40 × 1 = 97.62

 $M_{\dot{c}} = 68.81 \times 4 - 40 \times 3 = 155.24$ R = 155.24 + 60 = 215.24

MD = 68.81 x 5.5 - 40 x 4.5 - 40 x 1.5 +60 = 198.455

 $M_{C} = 68.81 \times 10.5 - 40 \times 9.5 - 40 \times 6.5 + 60 - 75 \times 2.5$  = -44.995

 $M_F = 68.81 \times 12 - 40 \times 11 - 40 \times 8 + 60 - 75 \times 4 + 116.19 \times 1.5 = 0$ 

Point of Contraflexure.

There is a point of contraflexure between D and E. Let it be at a distance  $\alpha$ , from A. The binding moment at this point is zero.

+68.81×  $\alpha$  - 40×  $(\alpha - 1)$  - 40×  $(\alpha - 4)$  + 60 = 75×  $(\alpha - 8)$ =0

68.81× - 40  $\alpha$  + 40 - 40× + 160 + 60 - 75  $\alpha$  + 600 = 0

× ----×

x = 9.98 m.

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