16-1 求图示二端口的 Y, Z和 T 参数矩阵.

解 提示 注意求 T 参数时方程中的负号.

图(a)
$$I_1 = \frac{1}{j\omega L}(\dot{U}_1 - \dot{U}_2) = -j\frac{1}{\omega L}\dot{U}_1 + j\frac{1}{\omega L}\dot{U}_2$$
$$I_2 = -\frac{1}{j\omega L}(\dot{U}_1 - \dot{U}_2) + j\omega LC\dot{U}_2$$

同理
$$U_1 = j\omega L I_1 + \frac{1}{j\omega L} (I_1 + I_2) = j(\omega L - \frac{1}{\omega C}) I_1 + \frac{1}{j\omega C} I_2$$

$$U_2 = \frac{1}{j\omega C} (I_1 + I_2) = \frac{1}{j\omega C} I_1 + \frac{1}{j\omega C} I_2$$

$$Z$$
参数矩阵为 $Z = \begin{bmatrix} j(\omega L - \frac{1}{\omega C}) & \frac{1}{j\omega C} \\ \frac{1}{j\omega C} & \frac{1}{j\omega C} \end{bmatrix}$

$$I_1 = j\omega C U_2 - I_2 \tag{2}$$

将(2) 式代人(1) 式得

$$\dot{U}_1 = j\omega L(j\omega C\dot{U}_2 - \dot{I}_2) + \dot{U}_2 = (1 - \omega^2 LC)\dot{U}_2 - j\omega L\dot{I}_2$$
 (3)
将(3) 与(2) 联立得 T 参数矩阵为

$$T = \begin{bmatrix} 1 - \omega^2 LC & j\omega L \\ j\omega C & 1 \end{bmatrix}$$
怪(b)
$$\dot{I}_1 = j\omega C\dot{U}_1 + \frac{1}{j\omega L}(\dot{U}_1 - \dot{U}_2)$$

$$= j(\omega C - \frac{1}{\omega L})\dot{U}_1 + j\frac{1}{\omega L}\dot{U}_2$$

$$\dot{I}_2 = -\frac{1}{j\omega L}(\dot{U}_1 - \dot{U}_2) = j\frac{1}{\omega L}\dot{U}_1 - j\frac{1}{\omega L}\dot{U}_2$$

$$Y$$
數矩阵为
$$Y = \begin{bmatrix} j(\omega C - \frac{1}{\omega L}) & j\frac{1}{\omega L} \\ j\frac{1}{\omega L} & -j\frac{1}{\omega L} \end{bmatrix}$$

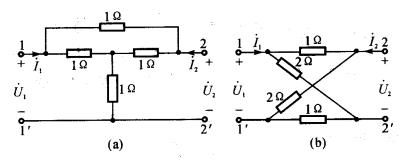
同理
$$\dot{U}_1 = \frac{1}{j\omega C}(\dot{I}_1 + \dot{I}_2) = \frac{1}{j\omega C}\dot{I}_1 + \frac{1}{j\omega C}\dot{I}_2$$

 $\dot{U}_2 = j\omega L\dot{I}_2 + \frac{1}{j\omega C}(\dot{I}_1 + \dot{I}_2)$

将(4)代入(5)中,再与(4)联立,可得T参数方程

$$\dot{U}_1 = \dot{U}_2 - \mathrm{j}\omega L\dot{I}_2$$
 $\dot{I}_1 = \mathrm{j}\omega C\dot{U}_2 - (1 - \omega^2 LC)\dot{I}_2$ T 参数矩阵为 $T = \begin{bmatrix} 1 & \mathrm{j}\omega L \\ \mathrm{j}\omega C & 1 - \omega^2 LC \end{bmatrix}$

16-2 求图示二端口的 Y和 Z参数矩阵.



題 16-2 图

解 提示 图(a)为对称互易二端口,只有两个参数独立,求Z参数时可先利用 $\Delta-Y$ 变换.利用定义来求.

图(a) 求 Y_{11} 和 Y_{21} 时,把端口 2-2' 短路,在端口 1-1' 处外施电压 U_1 .

则可得
$$\dot{I}_1 = \dot{U}_1 + (\frac{1}{1+\frac{1}{2}})\dot{U}_1 = \frac{5}{3}\dot{U}_1$$

$$-\dot{I}_2 = \dot{U}_1 + \frac{1}{2} \times (\frac{1}{1+\frac{1}{2}}\dot{U}_1) = \frac{4}{3}\dot{U}_1$$

根据定义可求得
$$Y_{11} = \frac{I_1}{U_1}\Big|_{U_2=0} = \frac{5}{3}S$$
 $Y_{21} = \frac{I_2}{U_1}\Big|_{U_1=0} = -\frac{4}{3}S$

由对称性和互易性可得

$$Y_{22} = Y_{11} = \frac{5}{3}S, Y_{12} = Y_{21} = -\frac{4}{3}S$$

$$Y = \begin{bmatrix} \frac{5}{3} & -\frac{4}{3} \\ -\frac{4}{3} & \frac{5}{3} \end{bmatrix} S$$

Y参数矩阵为

对图(a) 进行 $\Delta - Y$ 变换,如题解 16-2 图所示,则

$$\dot{U}_{1} = \frac{1}{3}\dot{I}_{1} + (\frac{1}{3} + 1)(\dot{I}_{1} + \dot{I}_{2})
= \frac{5}{3}\dot{I}_{1} + \frac{4}{3}\dot{I}_{2}$$

$$\dot{U}_{2} = \frac{1}{3}\dot{I}_{2} + (\frac{1}{3} + 1)(\dot{I}_{1} + \dot{I}_{2})$$

$$= \frac{4}{3}\dot{I}_{1} + \frac{5}{3}\dot{I}_{2}$$

$$\ddot{I}_{1} = \frac{1}{3}\Omega$$

$$\dot{U}_{1} = \frac{1}{3}\Omega$$

$$\dot{U}_{2} = \frac{1}{3}\Omega$$

$$\dot{U}_{1} = \frac{1}{3}\Omega$$

$$\dot{U}_{2} = \frac{1}{3}\Omega$$

$$\ddot{U}_{1} = \frac{1}{3}\Omega$$

$$\ddot{U}_{2} = \frac{1}{3}\Omega$$

$$\ddot{U}_{2} = \frac{1}{3}\Omega$$

$$\ddot{U}_{2} = \frac{1}{3}\Omega$$

$$\ddot{U}_{3} = \frac{1}{3}\Omega$$

$$\ddot{U}_$$

Z参数矩阵为

$$oldsymbol{Z} = egin{bmatrix} rac{5}{3} & rac{4}{3} \ rac{4}{3} & rac{5}{3} \end{bmatrix} \Omega$$

图(b) 求 Y_{11} 和 Y_{21} 时,把端口 2-2' 短路,即 $U_2=0$,在端口 1-1' 处施加 U_1 .

可得
$$I_1 = \frac{2}{\frac{2}{1+2} + \frac{2}{1+2}} \dot{U}_1 = \frac{3}{4} \dot{U}_1$$
$$-\dot{I}_2 = \frac{2}{1+2} \dot{I}_1 - \frac{1}{2+1} \dot{I}_1 = \frac{1}{3} \dot{I}_1 = \frac{1}{4} \dot{U}_1$$
则
$$Y_{11} = \frac{\dot{I}_1}{\dot{U}_1} \Big|_{\dot{U}_2 = 0} = \frac{3}{4} S, \qquad Y_{21} = \frac{\dot{I}_2}{\dot{U}_1} \Big|_{\dot{U}_2 = 0} = -\frac{1}{4} S$$
由对称性和互易性可得

$$Y_{22} = Y_{11} = \frac{3}{4}S, \quad Y_{12} = Y_{21} = -\frac{1}{4}S$$

$$Y = \begin{bmatrix} \frac{3}{4} & -\frac{1}{4} \\ -\frac{1}{4} & \frac{3}{4} \end{bmatrix} S$$

Y参数矩阵为

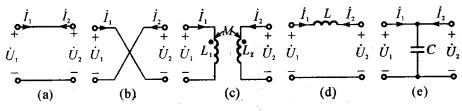
同理,在求Z参数的 Z_{11} 和 Z_{21} 时,把端口2-2'开路,即 $I_2=0$,在端口1-1'处施加电流 I_1 ,可得

$$\dot{U}_1=(3\ /\!/\ 3)\dot{I}_1=rac{3}{2}\dot{I}_1$$
 $\dot{U}_2=rac{2}{1+2}\dot{U}_1-rac{1}{2+1}\dot{U}_1=rac{1}{3}\dot{U}_1=rac{1}{2}\dot{I}_1$ 根据定义可得 $Z_{11}=rac{\dot{U}_1}{I_1}\Big|_{I_2=0}=rac{3}{2}\Omega$, $Z_{21}=rac{\dot{U}_2}{I_1}\Big|_{I_2=0}=rac{1}{2}\Omega$,由对称性和互易性,得 $Z_{22}=Z_{11}=rac{3}{2}\Omega$, $Z_{12}=Z_{21}=rac{1}{2}\Omega$,

故 Z 参数矩阵为

$$\mathbf{Z} = \begin{bmatrix} \frac{3}{2} & \frac{1}{2} \\ \frac{1}{2} & \frac{3}{2} \end{bmatrix} \mathbf{\Omega}$$

16-3 求图示二端口的 T 参数矩阵.



膜 16-3 图

解 设端口电压 U_1 , U_2 和电流 I_1 , I_2 的参考方向如图所示.

(1)
$$\mathbb{B}(a) + U_1 = U_2, I_1 = -I_2, \mathbb{M}$$

$$T = \begin{bmatrix} 1 & 0 \\ 0 & 1 \end{bmatrix}$$

(2) 图(b) 中 $\dot{U}_1 = -\dot{U}_2$, $\dot{I}_1 = \dot{I}_2$,则

$$T = \begin{bmatrix} -1 \begin{bmatrix} 0 \\ 0 \\ -1 \end{bmatrix}$$

(3)
$$\mathbb{Z}(c) + \dot{U}_1 = j\omega L_1 \dot{I}_1 + j\omega M \dot{I}_2$$
 (1)

$$\dot{U}_2 = j\omega M \dot{I}_1 + j\omega L_2 \dot{I}_2 \tag{2}$$

由(2) 得
$$\dot{I}_1 = \frac{1}{j\omega M}\dot{U}_2 - \frac{L_2}{M}\dot{I}_2$$
 (3)

(3) 式代人(1) 中,得

$$\dot{U}_{1} = j\omega L_{1} \left(\frac{1}{j\omega M} \dot{U}_{2} - \frac{L_{2}}{M} \dot{I}_{2} \right) + j\omega M \dot{I}_{2}
= \frac{L_{1}}{M} \dot{U}_{2} - j\omega \frac{L_{1}L_{2} - M^{2}}{M} \dot{I}_{2}$$
(4)

联立(3),(4) 得 T 参数方程,则

$$T = egin{bmatrix} rac{L_1}{M} & \mathrm{j}\omega rac{L_1 L_2 - M^2}{M} \ -\mathrm{j}rac{1}{\omega M} & rac{L_2}{M} \end{bmatrix}$$

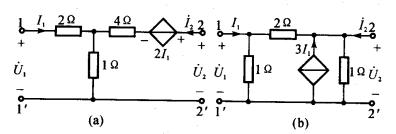
(4) 图(d) 中,其参数方程为 $\dot{U}_1 = \dot{U}_2 - j\omega L\dot{I}_2$, $\dot{I}_1 = -\dot{I}_2$,则

$$T = \begin{bmatrix} 1 & j\omega L \\ 0 & 1 \end{bmatrix}$$

(5) $\mathbb{E}(e) + U_1 = U_2, I_1 = j\omega C U_2 - I_2, M$

$$\mathbf{T} = \begin{bmatrix} 1 & 0 \\ i\boldsymbol{\omega}C & 1 \end{bmatrix}$$

16-4 求图示二端口的 Y 参数矩阵.



題 16-4 图

解 图(a) 端口电压 U_1 , U_2 和电流 I_1 , I_2 及参考方向如图所示,

则有

$$U_1 = (2+1)I_1 + I_2 = 3I_1 + I_2$$

 $U_2 = 2I_1 + (4+1)I_2 + I_1 = 3I_1 + 5I_2$

故

$$Z = \begin{bmatrix} 3 & 1 \\ 3 & 5 \end{bmatrix} \Omega$$

利用Y参数和Z参数之间的关系可得

$$\mathbf{Y} = Z^{-1} = \begin{bmatrix} \frac{5}{12} & -\frac{1}{12} \\ -\frac{1}{4} & \frac{1}{4} \end{bmatrix} \mathbf{S}$$

图(b)应用结点法,有

$$I_1 = (1 + \frac{1}{2})U_1 - \frac{1}{2}U_2 = \frac{3}{2}U_1 - \frac{1}{2}U_2 \tag{1}$$

$$I_2 = -\frac{1}{2}U_1 + (\frac{1}{2} + 1)U_2 - 3I_1 = -\frac{1}{2}U_1 + \frac{3}{2}U_2 - 3I_1$$
 (2)

将(1) 式代人(2) 中,消去 I1,得

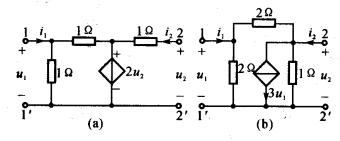
$$I_2 = -5U_1 + 3U_2 \tag{3}$$

联立(1),(3),则得Y参数方程,故

$$\mathbf{Y} = \begin{bmatrix} \frac{3}{2} & -\frac{1}{2} \\ -5 & 3 \end{bmatrix} \mathbf{S}$$

16-5

求图示二端口的混合参数(H)矩阵.



題 16-5 图

解 图(a)端口电压 u_1,u_2 和电流 i_1,i_2 的参考方向如图所示。

$$u_1 = (i_1 - u_1/1) \cdot 1 + 2u_2$$

则

即
$$u_1 = \frac{1}{2}i_1 + u_2$$
 而 $i_2 = u_2 - 2u_2 = -u_2$ 所以有 $\mathbf{H} = \begin{bmatrix} \frac{1}{2} & 1 \\ 0 & -1 \end{bmatrix}$

图(b)应用结点法,有

$$i_1 = (\frac{1}{2} + \frac{1}{2})u_1 - \frac{1}{2}u_2$$

$$= \frac{1}{2}u_2 + i_1 \tag{1}$$

 $u_1 = \frac{1}{2}u_2 + i_1$ 则

 $i_2 = -\frac{1}{2}u_1 + (\frac{1}{2} + 1)u_2 + 3u_1 = \frac{5}{2}u_1 + \frac{3}{2}u_2$ (2) 而

将(1)代入(2)中,得

$$i_2 = \frac{5}{2}i_1 + \frac{11}{4}u_2 \tag{3}$$

联立(1)与(3)即得 H参数方程,所以有

$$\mathbf{H} = \begin{bmatrix} 1 & \frac{1}{2} \\ \frac{5}{2} & \frac{11}{4} \end{bmatrix}$$

已知图示二端口的 Z 参数矩阵为

$$\mathbf{Z} = \begin{bmatrix} 10 []8 \\ 5 []10 \end{bmatrix} \mathbf{\Omega}$$

求 R_1 , R_2 , R_3 和 r 的值. 正确列写出Z参数 方程,由网孔电流法,有

$$U_1 = (R_1 + R_2)I_1 + R_3I_2 + rI_2 = (R_1 + R_3)I_1 + (R_3 + r)I_2$$

$$U_2 = R_3I_1 + (R_2 + R_3)I_2$$

 $\mathbf{Z} = \begin{bmatrix} R_1 + R_3 & R_3 + r \\ R_3 & R_2 + R_3 \end{bmatrix}$ 所以

与给定的 Z参数比较,可得

$$R_3 = 5\Omega$$
, $r = 3\Omega$, $R_2 = 5\Omega$, $R_1 = 5\Omega$

16-7 已知二端口的 Y 参数矩阵为

$$\mathbf{Y} = \begin{bmatrix} 1.5 & -1.2 \\ -1.2 & 1.8 \end{bmatrix} \mathbf{S}$$

求 H参数矩阵,并说明该二端口中是否有受控源.

解 由 Y 参数方程,

$$I_1 = Y_{11}U_1 + Y_{12}U_2 \tag{1}$$

$$I_2 = Y_{21}U_1 + Y_{22}U_2 \tag{2}$$

因 $Y_{11} \neq 0$,所以

$$U_1 = \frac{1}{Y_{11}} I_1 - \frac{Y_{12}}{Y_{11}} U_2 \tag{3}$$

将(3)代人(2)中,得

$$I_2 = \frac{Y_{21}}{Y_{11}}I_1 + \frac{Y_{11}Y_{22} - Y_{12}Y_{21}}{Y_{11}}U_2 \tag{4}$$

(3),(4) 即为 *H* 参数方程,可得

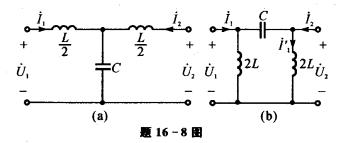
$$H_{11} = \frac{1}{Y_{11}}, H_{12} = -\frac{Y_{12}}{Y_{11}}, H_{21} = \frac{Y_{21}}{Y_{11}}, H_{22} = \frac{Y_{11}Y_{22} - Y_{12}Y_{21}}{Y_{11}}$$

代入数值,

$$\mathbf{H} = \begin{bmatrix} 0.667 & 0.8 \\ -0.8 & 0.84 \end{bmatrix}$$

由于 $Y_{12} = Y_{21} = -1.2S$, 二端口不含有受控源、

16-8 求图示二端口的 Z参数、T参数.



解 图(a) 电路,先求 Z_{11} 和 Z_{21} ,令 $I_2 = 0$,在端口 1-1' 处施加电流 I_1 ,可根据实验测定法得

$$Z_{11} = \frac{\dot{U}_1}{\dot{I}_1} \Big|_{\dot{I}_2 = 0} = j\omega \frac{L}{2} + \frac{1}{j\omega C} = j\left(\frac{\omega L}{2} - \frac{1}{\omega C}\right)$$

$$Z_{21} = \frac{\dot{U}_2}{\dot{I}_1} \Big|_{\dot{I}_2 = 0} = \frac{1}{j\omega C} = -j\frac{1}{\omega C}$$

由电路的对称性和互易性,得

$$Z_{22} = Z_{11} = j\left(\frac{\omega L}{2} - \frac{1}{\omega C}\right), Z_{12} = Z_{21} = -j\frac{1}{\omega C}$$

$$Z = \begin{bmatrix} j\left(\frac{\omega L}{2} - \frac{1}{\omega C}\right) & -j\frac{1}{\omega C} \\ -j\frac{1}{\omega C} & j\left(\frac{\omega L}{2} - \frac{1}{\omega C}\right) \end{bmatrix}$$

所以

根据 T参数与 Z参数之间的关系,得

$$A = D = \frac{Z_{11}}{Z_{21}} = \frac{j\omega \frac{L}{2} + \frac{1}{j\omega C}}{\frac{1}{j\omega C}} = 1 - \frac{\omega^2 LC}{2}$$

$$B = \frac{Z_{11}Z_{22} - Z_{12}Z_{21}}{Z_{21}} = j\omega L (1 - \frac{\omega^2 LC}{4})$$

$$C = \frac{1}{Z_{21}} = j\omega C$$

$$\left[1 - \frac{\omega^2 LC}{2} + \frac{\omega^2 LC}{2}\right]$$

所以

$$T = \begin{bmatrix} 1 - \frac{\omega^2 LC}{2} & j\omega L (1 - \frac{\omega^2 LC}{4}) \\ j\omega C & 1 - \frac{\omega^2 LC}{2} \end{bmatrix}$$

图(b) 电路,经分析该电路也只有对称性和互易性,即有

$$Z_{22}=Z_{11}, Z_{12}=Z_{21}.$$

求 Z_{11} 和 Z_{21} 时,令 $I_2=0$,在端口 1-1' 施加电流 I_1 ,则

$$Z_{22} = Z_{11} = \frac{\dot{U}_1}{I_1} \Big|_{I_2 = 0} = \frac{(j2\omega L)(j2\omega L + \frac{1}{j\omega C})}{i2\omega L + j2\omega L + \frac{1}{j\omega C}}$$

$$= \frac{j2\omega L(1 - 2\omega^2 LC)}{1 - 4\omega^2 LC}$$

$$Z_{12} = Z_{21} = \frac{\dot{U}_2}{I_1} \Big|_{I_2 = 0} = \frac{j2\omega L\dot{I}_1}{I_1}$$

$$=\frac{\mathrm{j}2\omega L}{I_1}\times\frac{\mathrm{j}2\omega L}{\mathrm{j}2\omega L+\frac{1}{\mathrm{j}\omega C}+\mathrm{j}2\omega L}I_1=-\mathrm{j}\frac{4\omega^3L^2C}{1-4\omega^2LC}$$

同理,根据T参数与Z参数之间的关系,可得

$$A = D = \frac{Z_{11}}{Z_{21}} = 1 - \frac{1}{2\omega^2 LC}$$

$$B = \frac{Z_{11}^2 - Z_{21}^2}{Z_{21}} = -j \frac{1}{\omega C}$$

$$C = \frac{1}{Z_{21}} = j \frac{1 - 4\omega^2 LC}{4\omega^3 L^2 C}$$

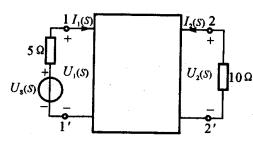


电路如图所示,已知二端口的 H 参数矩阵为

$$\mathbf{H} = \begin{bmatrix} 40 & 0.4 \\ 10 & 0.1 \end{bmatrix}$$

求电压转移函数 $\frac{U_2(s)}{U_1(s)}$.

设端口电压为 U1(s) 则由 H 参数矩阵,写出对应的方 程



$$U_1(s) = 40I_1(s) + 0.4U_2(s)$$
 (1)

$$I_2(s) = 10I_1(s) + 0.1U_2(s)$$
 (2)

而端口外接电路的伏安特性为

$$U_1(s) = U_s(s) - 5I_1(s)$$
 (3)

$$I_2(s) = -\frac{1}{10}U_2(s) \tag{4}$$

将(3),(4)代人(1),(2)中,整理后得

$$45I_1(s) + 0.4U_2(s) = U_s(s)$$

$$10I_1(s) + 0.2U_2(s) = 0$$

消去
$$I_1(s)$$
,可得 $\frac{U_2(s)}{U_s(s)} = \frac{1}{-0.5} = -2$



● ■ 已知二端口参数矩阵为

(a)
$$Z = \begin{bmatrix} 60/9 & 40/9 \\ 40/9 \end{bmatrix} \Omega;$$

(b)
$$\mathbf{Y} = \begin{bmatrix} 5 \begin{bmatrix} 1-2 \\ 0 \end{bmatrix} \end{bmatrix}$$
 S.

试问该二端口是否有受控源,并求它的等效 Ⅱ形电路.

解 提示 若求 Ⅱ型电路,设法求其 Y 参数最为直接和简单

(a) 由 $Z_{12} = Z_{21} = \frac{40}{9} \Omega$,所以该二端口不含有受控源. 利用 Z 和 Y

参数的关系

$$\mathbf{Y} = \mathbf{Z}^{-1} = \begin{bmatrix} 0.2045 & -0.0818 \\ -0.0818 \end{bmatrix} \mathbf{S}$$

其Ⅱ型等效电路如题解16-10图(a)所示,其中

$$Y_a = Y_{11} + Y_{12} = 0.1227S$$

 $Y_b = -Y_{12} = 0.0818S$
 $Y_c = Y_{22} + Y_{12} = 0.0409S$

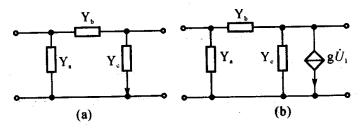
(b) 因为 $Y_{12} \neq Y_{21}$,所以该二端口中含有受控源,其等效 Π 型电路不惟一,受控源可以在靠近端口 1-1' 处,也可在靠近端口 2-2' 处.由 Y 参数,写出 Y 参数方程,有

$$\dot{I}_1 = Y_{11}\dot{U}_1 + Y_{12}\dot{U}_2 = Y_{11}\dot{U}_1 + Y_{12}\dot{U}_2 \tag{1}$$

$$\dot{I}_2 = Y_{21}\dot{U}_1 + Y_{22}\dot{U}_2 = Y_{12}\dot{U}_1 + Y_{22}\dot{U}_2 + (Y_{21} - Y_{12})\dot{U}_1 \qquad (2)$$

可以看出除了 $(Y_{21}-Y_{12})U_1$ 项之外,上述方程即为互易二端口的 Y 参数方程,因此,可以把 $(Y_{21}-Y_{12})U_1$ 项看成一个电压控制电流源,且并接在端口 2-2' 处,代入 Y 参数的数值,可得 Π 型等效电路,如图题解 16-10 图(b) 所示.

$$Y_a = Y_{11} + Y_{12} = 3S$$
, $Y_b = -Y_{12} = 2S$, $Y_c = Y_{22} + Y_{12} = 1S$, $g = Y_{21} - Y_{12} = 2S$.



題解 16-10 图

如果将Y参数方程写成

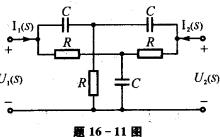
$$\dot{I}_1 = Y_{11}\dot{U}_1 + Y_{21}\dot{U}_2 + (Y_{12} - Y_{21})\dot{U}_2$$

 $\dot{I}_2 = Y_{21}\dot{U}_1 + Y_{22}\dot{U}_2$

则 Π 型等效电路的端口 1-1' 处并接一个大小为 $(Y_{12}-Y_{21})U_2$ 的受控 电流源,方法同上.

11 求图示双 T 电路的 Y 参数.

提示 此为双T电路,此外 + R 还有双 Π 电路,可以分别看成两个 $T_{U,(s)}$ 型(或 IT型) 电路并联. 也可利用实验 测定法分析,由于电路具有对称性和 互易性,本题选择实验测定法.



$$Y_{22} = Y_{11} = \frac{I_1(s)}{U_1(s)} \Big|_{U_2(s)=0} = \frac{sC(s + \frac{1}{RC})}{2(s + \frac{1}{2RC})} + \frac{s + \frac{1}{RC}}{R(2 + \frac{2}{RC})}$$

$$Y_{12} = Y_{21} = \frac{I_2(s)}{U_1(s)} \Big|_{U_2(s)=0} = \frac{s^2C}{2(s + \frac{1}{2RC})} + \frac{\frac{1}{R^2C}}{2 + \frac{2}{RC}}$$

16-12 求图示二端口的 T参数矩阵,设内部二端口 P_1 的 T参数矩阵 为

$$T_1 = \begin{bmatrix} A & B \\ C \cap D \end{bmatrix}$$

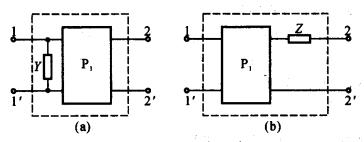
将导纳 Y或阻抗 Z 看作二端口与 P_1 的级联. 图(a) 由导纳 Y 组成的二端口的 T 参数方程为

$$\dot{U}_1 = \dot{U}_2 \qquad \qquad \dot{I}_1 = Y\dot{U}_2 - \dot{I}_2$$

所以 T 参数矩阵为 $T_r = \begin{bmatrix} 1 & 0 \\ \mathbf{v} & 1 \end{bmatrix}$

可得,图(a) 电路的 T参数矩阵为

$$T = T_r \cdot T_1 = \begin{bmatrix} 1 \begin{bmatrix} 0 \\ Y \end{bmatrix} \begin{bmatrix} A & B \\ C & D \end{bmatrix} = \begin{bmatrix} A & B \\ AY + C \end{bmatrix} B$$



題 16-12 图

图(b),由阻抗 Z组成的二端口的 T 参数方程为

$$U_1 = U_2 - ZI_2 \qquad I_1 = -I_2$$

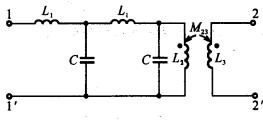
所以其 T 参数矩阵为 $T_Z = \begin{bmatrix} 1 & Z \\ 0 & 1 \end{bmatrix}$

可得图(b) 二端口的 T 参数矩阵

$$T = T_1 T_Z = \begin{bmatrix} A[]AZ + B \\ C[]CZ + D \end{bmatrix}$$

利用题 16-1,16-3 的结果,求出图示二端口的 T 参数矩阵.

设已知 $\omega L_1 = 10\Omega$, $\frac{1}{\omega C} = 20\Omega$, $\omega L_2 = \omega L_3 = 8\Omega$, $\omega M_{23} = 4\Omega$.



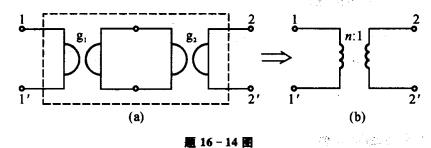
題 16-13 图

解 提示 将该二端口看成三个二端口的级联,利用题 16-1 图 (a)、16-3 图(c) 的 T 参数结果,可得

$$T = \begin{bmatrix} 1 - \omega^2 L_1 C & j\omega L_1 \\ j\omega C & 1 \end{bmatrix}^2 \begin{bmatrix} \frac{L_2}{M} & j\omega \frac{L_2 L_3 M^2}{M} \\ -j\frac{1}{\omega M} & \frac{L_3}{M} \end{bmatrix}$$

$$= \begin{bmatrix} 1 - \frac{10}{20} & j10 \\ j \frac{1}{20} & 1 \end{bmatrix}^{2} \begin{bmatrix} \frac{8}{4} & j \frac{8^{2} - 4^{2}}{4} \\ -j \frac{1}{4} & \frac{8}{4} \end{bmatrix} = \begin{bmatrix} 3.25 & j27 \\ j0.025 & 0.1 \end{bmatrix}$$

或证明两个回转器级联后[如图(a) 所示],可等效为一个理想变压器[如同图(b) 所示],并求出变化n与两个回转器的回转电导 g_1 和 g_2 的关系.



解 由回转器的特性方程,可得其 T 参数矩阵

$$T = \begin{bmatrix} 0 & \frac{1}{g} \\ g & 0 \end{bmatrix}$$

则图(a)的 T参数矩阵为

$$\mathbf{T} = \mathbf{T}_1 \mathbf{T}_2 = \begin{bmatrix} 0 & \frac{1}{g_1} \\ g_1 & 0 \end{bmatrix} \begin{bmatrix} 0 & \frac{1}{g_2} \\ g_2 & 0 \end{bmatrix} = \begin{bmatrix} \frac{g_2}{g_1} & 0 \\ 0 & \frac{g_1}{g_2} \end{bmatrix}$$

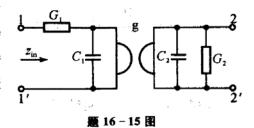
而理想变压器的 T参数矩阵为

$$T = \begin{bmatrix} n[\]0 \\ 0[\]\frac{1}{n} \end{bmatrix}$$

由以上T多数矩阵可以看出,两个回转器级联后,可等效的一个理想变压器,其等效变比为 $n = g_2/g_1$

15 15 试求图示电路的输入阻抗 Z_{in} . 已知 $C_1 = C_2 = 1$ F, $G_1 = G_2 = 1$ S, g = 2S.

解 图示电路中,当回转器输出端接一导纳 $Y_2(s) = G_2 + sC_2$ (端口 2-2' 开路) 时,根据回转器的特性方程,可得从回转器输入端看进去的输入导纳为



$$Y_1(s) = \frac{g^2}{Y_2(s)} = \frac{g^2}{G_2 + sC_2}$$

所以 该电路的输入阻抗为

$$Z_{\text{in}}(s) = \frac{1}{G_1} + \frac{1}{sC_1 + Y_1(s)} = \frac{1}{G_1} + \frac{1}{sC_1 + \frac{g^2}{G_2 + sC_2}}$$
$$= \frac{s^2 + 2s + 5}{s^2 + s + 4}$$