18-1 一对架空传输线的原参数是 $L_0 = 2.89 \times 10^{-3} \, \text{H/km}$, $C_0 = 3.85 \times 10^{-9} \, \text{F/km}$, $R_0 = 0.3 \, \Omega / \text{km}$, $G_0 = 0$. 试求当工作频率为 $50 \, \text{Hz}$ 时的特性阻抗 Z_c , 传播常数 γ , 相位速度 v_φ 和波长 λ . 如果频率为 $10^4 \, \text{Hz}$, 重求上述各参数.

解

則
$$Z_{c} = \sqrt{\frac{Z_{0}}{Y_{0}}} = \sqrt{\frac{0.9562 / 71.715^{\circ}}{1.2095 \times 10^{-6} / 90^{\circ}}} = 889.138 / -9.143^{\circ}\Omega$$

 $\gamma = \sqrt{Z_{0}Y_{0}} = \sqrt{0.9562 / 71.715^{\circ} \times 1.209 \times 10^{-6} / 90^{\circ}}$
 $= 1.075 \times 10^{-3} / 80.858^{\circ}$
 $= 0.171 \times 10^{-3} + j1.062 \times 10^{-3} 1/km$

$$\alpha = 0.171 \times 10^{-3} Np/\text{km}, \beta = 1.062 \times 10^{-3} \text{ rad/km}$$

$$v_{\varphi} = \frac{\omega}{\beta} = \frac{100\pi}{1.062 \times 10^{-3}} = 2.958 \times 10^{5} \text{ km/s}$$

$$\lambda = \frac{v_{\varphi}}{f} = \frac{2.958 \times 10^{5}}{50} = 5.916 \times 10^{3} \text{ km}$$

(2) $\stackrel{\text{def}}{=} f = 10^4 \text{ Hz ipl}$ $Z_0 = 0.3 + \text{j}181.584 = 181.58 \frac{89.91^{\circ} \Omega}{\text{km}}$ $Y_0 = \text{j}2\pi \times 10^4 \times 3.85 \times 10^{-9} = \text{j}2.419 \times 10^{-4} \text{ S/km}$

则
$$Z_c = \sqrt{Z_0/Y_0} = 8.664 \times 10^2 / -0.045^{\circ} \Omega$$

 $\gamma = \sqrt{Z_0 Y_0} = 20.958 \times 10^{-2} / 89.955^{\circ}$
 $= 1.646 \times 10^{-4} + j20.958 \times 10^{-2} l/km$

 $\alpha = 1.646 \times 10^{-4} Np/\text{km}, \beta = 20.958 \times 10^{-2} \text{ rad/km}$ $v_{\varphi} = \frac{\omega}{\beta} = \frac{2\pi \times 10^4}{20.958 \times 10^{-2}} = 2.998 \times 10^5 \text{ km/s}$ $\lambda = \frac{v_{\varphi}}{f} = \frac{2.998 \times 10^5}{10^4} = 29.98 \text{ km}$

18-2. 一同轴电缆的原参数为: $R_0 = 7\Omega/\text{km}$, $L_0 = 0.3\text{mH/km}$,

 $C_0 = 0.2 \mu F/km$, $G_0 = 0.5 \times 10^{-6} \text{ S/km}$. 试计算当工作频率为 800 Hz 时此电缆的特性阻抗 Z_c 、传播常数 γ 、相位速度 v_{φ} 和波长 λ .

解

$$Z_0 = R_0 + j\omega L_0 = 7 + j2\pi \times 800 \times 0.3 \times 10^{-3}$$
 $= 7.1606 / 12.157^{\circ} \Omega / km$
 $Y_0 = G_0 + j\omega C_0 = 0.5 \times 10^{-6} + j2\pi \times 800 \times 0.2 \times 10^{-6}$
 $= 1.0053 \times 10^{-3} / 89.97^{\circ} S / km$
 \mathbb{M}
 $Z_c = \sqrt{Z_0 / Y_0} = 84.397 / -38.91^{\circ} \Omega$
 $\gamma = \sqrt{Z_0 Y_0} = 8.484 \times 10^{-2} / 51.064^{\circ}$
 $= 5.332 \times 10^{-2} + j6.599 \times 10^{-2} 1 / km$
 $\Omega = 5.332 \times 10^{-2} Np / km, \beta = 6.599 \times 10^{-2} rad / km$

 $v_{\varphi} = \frac{\omega}{\beta} = \frac{2\pi \times 800}{6.5996 \times 10^{-2}} = 7.616 \times 10^4 \,\mathrm{km/s}$

$$\lambda = \frac{v_{\varphi}}{f} = \frac{7.616 \times 10^4}{800} = 95.206 \text{km}$$

解

$$Z_{c} = \sqrt{\frac{R_{0} + j\omega L_{0}}{G_{0} + j\omega C_{0}}} = \sqrt{\frac{R_{0}}{j\omega C_{0}}} = \sqrt{\frac{1}{j4 \times 10^{-4}}} = 50 \ \underline{/ - 45^{\circ}} \Omega / \text{km}$$

$$\gamma = \sqrt{(R_{0} + j\omega L_{0})(G_{0} + j\omega C_{0})} = \sqrt{R_{0} \times j\omega C_{0}}$$

$$= \sqrt{1 \times j4 \times 10^{-4}} = 0.02 \ \underline{/ 45^{\circ}}$$

$$= 1.41 \times 10^{-2} + j1.41 \times 10^{-2} \ 1/\text{km}$$

因 $Z_2 = Z_c$,故传输线中没有反射波,其工作在匹配状态.设传输线的终端为坐标起点,则沿线电压波的分布为

$$\dot{U}_{(x)} = \dot{U} + e^{-\gamma x}$$

把 $U(0) = U_2 = 3 / 0^{\circ}$ 代人,可得

$$\dot{U}^+ = \dot{U}_2 = 3 / 0^{\circ} V$$

始端电压为

$$U_1(-l) = 3 / 0^{\circ} e^{\gamma \times 70.8} = 3 / 0^{\circ} e^{0.02 / 45^{\circ} \times 70.8}$$

= 8. 164 e^{j1.001} V

始端电流为

$$I_1(-l) = \frac{U_1(-l)}{Z_c} = \frac{8.164 e^{j1.001}}{50/-45^\circ} = 0.1633 e^{j1.786} A$$

则始端电压、电流的有效值为

$$U_1 = 8.164 \text{V}, I_1 = 0.1633 \text{A}$$

18—4 一高压输电线长 300km,线路原参数 $R_0 = 0.06\Omega/\text{km}$, $L_0 = 1.40 \times 10^{-3} \,\text{H/km}$, $G_0 = 3.75 \times 10^{-8} \,\text{S/km}$, $C_0 = 9.0 \times 10^{-9} \,\text{F/km}$. 电源的频率为 50 Hz. 终端为一电阻负载,终端的电压为 220kV,电流为 455 A. 试求始端的电压 U_1 和电流 I_1 .

解

$$Z_0 = R_0 + j\omega L_0 = 0.06 + j0.4398 = 0.4439 /82.3^{\circ}\Omega/km$$

$$Y_0 = G_0 + j\omega C_0 = 3.75 \times 10^{-8} + j100\pi \times 9 \times 10^{-9}$$

$$= 2.8277 \times 10^{-6} \ \underline{/89.24^{\circ}} \text{ S/km}$$

$$\mathbb{D} \quad Z_0 = \sqrt{Z_0/Y_0} = \sqrt{0.4439} \ \underline{/82.3^{\circ}}/(2.8277 \times 10^{-6} \ \underline{/89.24^{\circ}})$$

$$= 396.21 \ \underline{/-3.47^{\circ}\Omega}$$

$$\gamma = \sqrt{Z_0Y_0} = 1.1204 \times 10^{-3} \ \underline{/85.77^{\circ}}$$

$$= 8.264 \times 10^{-5} + j1.1173 \times 10^{-3} 1/\text{km}$$

设传输线终端电压为 $U_2=220 / 0 \text{ kV}$, $I_2=455 / 0 \text{ A}$ 代入电压、电 流的通解式中,有

解得
$$\begin{cases} \dot{U}(0) = \dot{U}_2 = \dot{U}^+ + \dot{U}^- \\ \dot{I}(0) = \dot{I}_2 = \frac{\dot{U}^+ - \dot{U}^-}{Z_c} \\ \dot{U}^+ = \frac{\dot{U}_2 + Z_c \dot{I}_2}{2} \end{cases}, \quad \dot{U}^- = \frac{\dot{U}_2 - Z_c \dot{I}_2}{2}$$

故沿线电压、电流分布为一个企业企业设施的。企业企业企业企业

$$\dot{U}(x) = \frac{\dot{U}_2 + Z_c \dot{I}_2}{2} e^{+\gamma x} + \frac{\dot{U}_2 - Z_c \dot{I}_2}{2} e^{-\gamma x}
= \dot{U}_2 \cosh(\gamma x) + Z_c \dot{I}_2 \sinh(\gamma x)
\dot{I}(x) = \frac{1}{Z_c} \left[\frac{\dot{U}_2 + Z_c \dot{I}_2}{2} e^{+\gamma x} - \frac{\dot{U}_2 - Z_c \dot{I}_2}{2} e^{-\gamma x} \right]
= \dot{I}_2 \cosh(\gamma x) + \frac{\dot{U}_2}{Z_c} \sinh(\gamma x)$$

当
$$x = 300 \text{km}$$
 时,有
$$\cosh(\gamma x) = 0.9446 + j8.14 \times 10^{-3}$$

$$\sinh(\gamma x) = 2.337 \times 10^{-2} + j0.329$$

故传输线始端电压、电流为

$$\dot{U}_{1} = \dot{U}(300) = 220 / 0^{\circ} \times (0.9446 + j8.14 \times 10^{-3}) + 396.21 \times 10^{-3} / -3.47^{\circ} \times 445 \times (2.337 \times 10^{-2} + j0.329)$$

$$= 223.486 / 15.425^{\circ} kV$$

$$I_{1} = I(300) = 445 \times (0.9446 + j8.14 \times 10^{-8}) + 10^{3} \times \frac{220 \times (2.337 \times 10^{-2} + j0.329)}{396.21 / -3.47^{\circ}}$$

= 422.242 + j186.754 = 461.698/23.86°A

18-5 架空无损耗传输线的特性阻抗 $Z_c = 300 \Omega$,线长 l = 2 m. 当频率为 300 MHz 和 150 MHz 时,试分别画出终端开路、短路及接上匹配负载时,电压 u 和 | U | 沿线的分布.

解 无损耗传输线沿线电压的分布为

$$U(x) = U_2 \cos(\beta x) + jZ_c I_2 \sin(\beta x)$$

当 f = 300MHz 时,相位常数

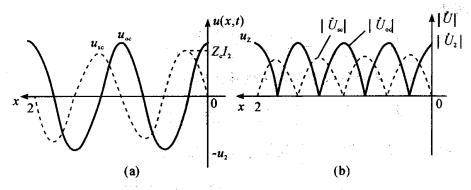
$$\beta = \frac{\omega}{v_{\varphi}} = \frac{2\pi f}{v_{\varphi}} = \frac{2\pi \times 300 \times 10^6}{3 \times 10^8} = 2\pi \text{ rad/m}$$

(1) 终端开路,即 $I_2 = 0$,则沿线电压为

$$\dot{U}_{\rm oc}(x) = \dot{U}_2 \cos(\beta x) = \dot{U}_2 \cos(2\pi x)$$

则 $u_{\rm oc}(x,t) = \sqrt{2}U_2\cos(2\pi x)\cos(\omega t)$

即 $u_{oc}(x,t)$ 是驻波分布,在x=0,1,2m处 $u_{oc}(x,t)$ 值最大,在x=0.5,1.5m 处 $u_{oc}(x,t)$ 值最小,在x=0.25,0.75,1.25,1.75m 处, $u_{oc}(x,t)$ 值为零. $u_{oc}(x,t)$ 的波形如题解 18-5 图(a) 所示, $|U_{oc}|$ 的分布如图(b) 所示.



題解 18-5 图

(2) 终端短路,即 $U_2 = 0$,沿线电压为

$$\dot{U}_{\rm sc}(x) = \mathrm{i} Z_{\rm c} \dot{I}_{2} \sin(\beta x) = \mathrm{i} Z_{\rm c} \dot{I}_{2} \sin 2(\pi x)$$

则 $u_{\rm sc}(x,t) = \sqrt{2}Z_{\rm c}I_{\rm 2}\sin 2(\pi x) \cdot \cos(\omega t - 90^{\circ})$

 $u_{sc}(x,t)$ 仍呈驻波分布,在 $|u_{oc}|$ 取最大值处, $u_{sc}(x,t)$ 为零值,而在 $u_{oc} = 0$ 处, $|u_{sc}|$ 取最大值, $u_{sc}(x,t)$ 的波形见图(a) 中的虚线所示.

(3) 传输线接匹配负载时,即 $Z_L = Z_c$,线上无反射波,故沿线电压

分布为

$$\dot{U}(x) = \dot{U}_2 e^{+j\beta x} = \dot{U}_2 e^{+j2\pi x}$$

$$u(x,t) = \sqrt{2} U_2 \cos(\omega t + 2\pi x)$$

则

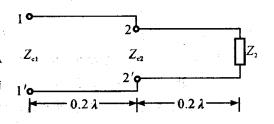
即传输线工作在行波状态,沿线各处的电压幅值相等. 当 f = 150 MHz 时,

$$\beta = \frac{\omega}{v_{\varphi}} = \frac{2\pi \times 150 \times 10^6}{3 \times 10^8} = \pi \text{ rad/m}$$

在各种终端情况下,电压表达式与上述相似,波形相反.

18-6 两段特性阻抗分别为 Zel 和 Ze2 的无损耗线连接的传输线如

图. 已知终端所接负载为 $Z_2 =$ (50 + j50)Ω. $\& Z_{cl} = 75$ Ω, $Z_{c2} =$ 50Ω. 两段线的长度都为 0.2λ(λ 为线的工作波长),试求1-1'端 的输入阻抗.



无损耗传输线的输入 解 阻抗为

 $Z_{\rm in} = \frac{\dot{U}(x)}{I(x)} = Z_{\rm c} \frac{Z_2 + \mathrm{j} Z_{\rm c} \tan(\beta x)}{Z_{\rm c} + \mathrm{j} Z_{\rm c} \tan(\beta x)}$

$$Z_{\rm in} = \frac{U(x)}{I(x)} = Z_{\rm c} \frac{Z_2 + jZ_{\rm c} \tan(\beta x)}{Z_{\rm c} + jZ_2 \tan(\beta x)}$$

由
$$2-2'$$
 端向负载端看进去的输入阻抗为
$$Z_{\rm in1} = Z_{\rm c2} = \frac{Z_2 + {\rm j} Z_{\rm c2} \tan(eta imes 0.2\lambda)}{Z_{\rm c2} + {\rm j} Z_2 \tan(eta imes 0.2\lambda)}$$

把
$$\beta = \frac{\omega}{v_{\varphi}} = \frac{2\pi f}{\lambda f} = \frac{2\pi}{\lambda}$$
 代人上式中,有
$$Z_{\rm inl} = 50 \times \frac{(50 + {\rm j}50) + {\rm j}50 \times {\rm tan}(0.4\pi)}{50 + {\rm j}(50 + {\rm j}50) {\rm tan}(0.4\pi)}$$

=
$$56.5327 / -47.8^{\circ} = 37.973 - j41.881\Omega$$

把 Z_{inl} 看作传输线 1 的负载,则 1-1' 端的输入阻抗为

$$Z_{\text{in}} = Z_{\text{cl}} \frac{Z_{\text{inl}} + jZ_{\text{cl}} \tan(\beta x)}{Z_{\text{cl}} + jZ_{\text{inl}} \tan(\beta x)}$$

$$= 75 \times \frac{(37.973 - j41.881) + j75 \tan(0.4\pi)}{75 + j(37.973 - j41.881) \tan(0.4\pi)}$$

$$= 61.503 /48.816^{\circ} = 40.498 + j46.287\Omega$$

18-7 特性阻抗为 50Ω 的同轴线,其中介质为空气,终端连接的负载 $Z_2 = (50 + j100)$ Ω. 试求终端处的反射系数,距负载 2.5cm 处的输入阻抗和反射系数.已知线的工作波长为 10cm.

解 当频率较高时,同轴线可看作是无损耗的. 传输线上任一点的反射系数为该点反射波电压和入射波电压之比,即

$$n = \frac{\dot{U}^{-} e^{-\beta x'}}{\dot{U}^{+} e^{\beta x'}} = \frac{\dot{U}^{-}}{\dot{U}^{+}} e^{-2\beta x'} = \frac{\dot{U}_{2} - Z_{c} \dot{I}_{2}}{\dot{U}_{2} + Z_{c} \dot{I}_{2}} e^{-2\beta x'} = \frac{Z_{2} - Z_{c}}{Z_{2} + Z_{c}} e^{-2\beta x'}$$

无损耗线有 $\gamma = i\beta$,因此在 x' = 0 的终端,反射系数为

$$n_z = \frac{Z_2 - Z_c}{Z_2 + Z_c} = \frac{50 + j100 - 50}{50 + j100 + 50} = \frac{j}{1 + j} = \frac{\sqrt{2}}{2} / 45^{\circ}$$

离负载 2.5cm 处的反射系数为(把 $\beta = 2\pi/\lambda$ 代人)

$$n = \frac{Z_2 - Z_c}{Z_2 + Z_c} e^{j2\beta \times 2.5} = n_z e^{j\pi} = \frac{\sqrt{2}}{2} / 45^\circ + 180^\circ = 0.707 / 135^\circ$$

离负载 2.5cm 处的输入阻抗为

$$Z_{\text{in}} = Z_{\text{c}} \frac{Z_2 + jZ_{\text{c}} \tan(\frac{2\pi}{\lambda} \times 2.5)}{Z_{\text{c}} + jZ_{\text{2}} \tan(\frac{2\pi}{\lambda} \times 2.5)} = \frac{Z_{\text{c}}^2}{Z_2} = \frac{2500}{50 + j100}$$
$$= 10 - 20j = 22.361 / -63.435^{\circ}\Omega$$

18-8 试证明无损耗线沿线电压和电流的分布及输入导纳可以表示 为下面的形式:

$$\dot{U} = \dot{U}_2 \left[\cos(\beta x) + \mathrm{j} \frac{Y_2}{Y_\mathrm{c}} \sin(\beta x) \right]$$
 $\dot{I} = \dot{I}_2 \left[\cos(\beta x) + \mathrm{j} \frac{Y_\mathrm{c}}{Y_2} \sin(\beta x) \right]$
 $Y_\mathrm{in} = Y_\mathrm{c} \frac{Y_2 + \mathrm{j} Y_\mathrm{c} \tan(\beta x)}{Y_\mathrm{c} + \mathrm{j} Y_2 \tan(\beta x)}$

其中 $Y_c = \frac{1}{Z_c}$, $Y_2 = \frac{1}{Z_2}$, Z_2 为负载阻抗.

证 当传输线为无损耗线时,传播常数 $\gamma = j\beta$,线上电压、电流的通解为

$$U(x') = U^+ e^{-j\beta x'} + U^- e^{j\beta x'}$$

$$I(x') = \frac{U^{+}}{Z_{c}} e^{-i\beta x'} - \frac{U^{-}}{Z_{c}} e^{i\beta x'}$$

"女人精发生"这种"一囊"。 第二章

把 x' = 0(终端)代入,有

$$U(0) = U_2 = U^+ + U^ I(0) = I_2 = Y_c(U^+ - U^-)$$

解得
$$\dot{U}^+ = (\dot{U}_2 + \frac{\dot{I}_2}{Y_c})/2$$
 $\dot{I}^+ = (\dot{U}_2 - \frac{\dot{I}_2}{Y_c})/2$

が
$$\dot{V} = (\dot{U}_2 + \frac{\dot{I}_2}{Y_c})/2$$

$$\dot{U}(x') = \frac{\dot{U}_2 + \frac{\dot{I}_2}{Y_c}}{2} e^{-j\beta x'} + \frac{\dot{U}_2 - \frac{\dot{I}_2}{Y_c}}{2} e^{j\beta x'}$$

$$= \dot{U}_2 \cos(\beta x') - j \frac{\dot{I}_2}{Y_c} \sin(\beta x')$$

$$= \dot{U}_2 \Big[\cos(\beta x') - j \frac{Y_2}{Y_c} \sin(\beta x')\Big]$$

$$V_1(\dot{I}_2 + \dot{I}_2)$$

$$\begin{split} \dot{I}(x') &= \frac{Y_{c}(\dot{U}_{2} + \frac{\dot{I}_{2}}{Y_{c}})}{2} e^{-j\beta x'} - Y_{c} \frac{\dot{U}_{2} - \frac{\dot{I}_{2}}{Y_{c}}}{2} e^{j\beta x'} \\ &= \dot{I}_{2} \cos(\beta x') - j Y_{c} \dot{U}_{2} \sin(\beta x') \\ &= \dot{I}_{2} \left[\cos(\beta x') - j \frac{Y_{c}}{Y_{2}} \sin(\beta x')\right] \end{split}$$

线上任一点的输入导纳为

$$Y_{in} = \frac{I(x')}{U(x')} = \frac{I_2 \left[\cos(\beta x') - j\frac{Y_c}{Y_2}\sin(\beta x')\right]}{U_2 \left[\cos(\beta x') - j\frac{Y_2}{Y_c}\sin(\beta x')\right]}$$
$$= Y_c \frac{Y_2 - jY_c \tan(\beta x')}{Y_c - jY_2 \tan(\beta x')}$$

以上式子中认为传输线上沿线的坐标为负值,若把x'=-x代人, 则有沿线的电压、电流和输入导纳分别为

$$\dot{U}(x) = \dot{U}_2 \left[\cos(\beta x) + \mathrm{j} \frac{Y_2}{Y_c} \sin(\beta x) \right]$$

$$\dot{I}(x) = I_2 \left[\cos(\beta x) + \mathrm{j} \frac{Y_c}{Y_2} \sin(\beta x) \right]$$

$$Y_{\rm in} = \frac{I(x)}{U(x)} = Y_{\rm c} \frac{Y_2 + jY_{\rm c} \tan(\beta x)}{Y_{\rm c} + jY_2 \tan(\beta x)}$$

18.4 典型题分析

例 1 两段无损耗均匀传输线,连接如图 18-1 所示. 其特性阻抗分别为: $Z_1 = 600\Omega$, $Z_2 = 800\Omega$, 终端负载电阻 $R_L = 800\Omega$, 为了在连接处 AB不产生反射, 若在 AB间接一个集中参数电阻 R 可达此目的, 试问 R 值应是多少?

解 因 $R_L = Z_2 = 800\Omega$,故第二段传输线工作于匹配状态,从 AB端向负载方向看的入端阻抗 Z'_{AB} 为

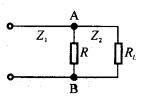


图 18-1

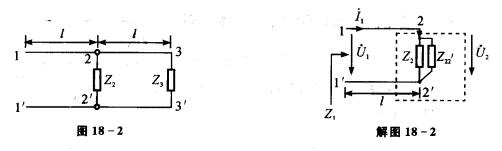
$$Z'_{AB}=Z_2=R_L=800\Omega$$

为使在连接处 AB 不产生反射,则要求 AB 处的总阻抗

$$Z_{AB} = Z_1 = 600 \Omega$$

又 $Z_{AB} = R /\!\!/ Z'_{AB}$
则 $600 = \frac{800 R}{800 + R}$
得 $R = \frac{600 \times 800}{800 - 600} = 2400 \Omega$

例2 图 18-2 为均匀传输线,在正弦稳态下,设特性阻抗为 Z_c ,传播系数为 γ ,又 $Z_2=Z_3=Z_c$,求 11' 端输入阻抗 Z_1 .



解 因 $Z_3 = Z_c$,第二段传输线工作于匹配状态,从 2-2' 端口向终端看进去的输入阻抗 $Z_{22'} = Z_c$. 又因为在 2-2' 端口接有阻抗 Z_2 ,则 2-2' 端口的总阻抗为

$$Z_{\rm L} = Z_2 \ /\!/ \ Z_{22'} = Z_{\rm c} \ /\!/ \ Z_{\rm c} = 0.5 Z_{\rm c}$$

 Z_L 即是第一段传输线的终端阻抗. 由于 $Z_L \neq Z_c$,则第一段传输线工作在非匹配状态,输入阻抗 Z_1 将由 Z_L 、线长 l 及特性阻抗 Z_c 共同决定. 作等效电路解图 18-2 所示.

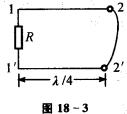
$$Z_{1} = \frac{\dot{U}}{I} = \frac{\dot{U}_{2} \cosh(\mathcal{H}) + Z_{c} \dot{I}_{2} \sinh(\mathcal{H})}{\dot{I}_{2} \cosh(\mathcal{H}) + \frac{\dot{U}_{2}}{Z_{c}} \sinh(\mathcal{H})}$$

$$= \frac{0.5 Z_{c} \dot{I}_{2} \cosh(\mathcal{H}) + Z_{c} \dot{I}_{2} \sinh(\mathcal{H})}{\dot{I}_{2} \cosh(\mathcal{H}) + \frac{0.5 Z_{c} \dot{I}_{2}}{Z_{c}} \sinh(\mathcal{H})}$$

$$= Z_{c} \frac{\cosh(\mathcal{H}) + 2 \sinh(\mathcal{H})}{2 \cosh(\mathcal{H}) + \sinh(\mathcal{H})} = Z_{c} \frac{1 + \tanh(\mathcal{H})}{2 + \tanh(\mathcal{H})}$$

解 终端短路 $\lambda/4$ 无损耗均匀传输线的输入阻抗 $Z_1 = \infty$,则 1-1' 端的入端阻抗为

$$Z_{\rm i}=R \ /\!/ \ Z_{\rm 1}=R=600\Omega$$



$$(Z_1 = jZ_c \tan(\beta \lambda) = jZ_c \tan(\frac{2\pi}{\lambda}l) = jZ_c \tan\frac{\pi}{2} = \infty)$$

例 4 如图 18-4 所示的无损耗架空线的波阻抗为 400Ω ,电源频率为 100MHz,若要使输入端相当于 100pF 的电容,问线长 l 最短应为多少?

解 这是段终端开路传输线,其输入阻抗

$$Z_i = -jZ_c \cot(\beta l) = -jZ_c \cot(\frac{2\pi}{\lambda}l)\Omega$$

当电源频率 f = 100 MHz 时,波长 λ 和 100 pF 的容抗 Z_1 分别为

$$\lambda = \frac{C}{f} = \frac{3 \times 10^8}{100 \times 10^6} = 3 \text{m}$$

$$Z_1 = -\mathrm{j}\,\frac{1}{2\pi f\mathrm{C}} = -\mathrm{j}\,\frac{100}{2\pi}\Omega$$

为使终端开路线的输入端相当于 100pF 的电容就要求 $Z_i = Z_1$,即

$$-jZ_{c}\cot(\frac{2\pi}{\lambda}l) = -j\frac{100}{2\pi}$$

代入相关数据,代入上式解出 l=0.731m

例 5 已知一空气中的无损耗均匀传输线的长度为 1.5m,特性阻抗 $Z_{c1} = 100\Omega$,相速 $v_{\varphi} = 3 \times 10^8 \, \text{m/s}$,终端负载阻抗 $Z_{L} = 10\Omega$,在距终端 0.75m 处接有另一特性阻抗 $Z_{c2} = 100\Omega$,长为 0.75m 的无损耗均匀传输线(终端短路),如图 18-5 所示.始端所接正弦电压源电压 $u_{s}(t) = 10\cos2 \times 10^8 \, \text{mV}$.求稳态运行下的始端电流的幅值.

解 由題意得电源频率 $f=10^8\,\mathrm{Hz}$,则波长

$$\lambda = \frac{1}{f} \times v_{\varphi} = 10^{-8} \times 3 \times 10^8 \,\mathrm{m} = 3 \,\mathrm{m}$$

故 0.75m 长度的传输线正好是 λ/4. 因为 λ/4 长度的无损耗均匀传输线起一个阻抗变换器的作用,从 ab 两端向终端看去的输入阻抗为

$$Z_{i1} = \frac{Z_{c1}^2}{2_L} = \frac{100^2}{10}\Omega = 1000\Omega$$

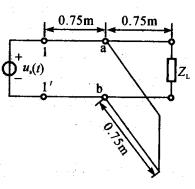


图 18-5

由于在 ab 端接的另一传输线是一终端的 $\lambda/4$ 线,因此从 ab 端向这一短路线条输入阻抗为 ∞ ,或

$$Z_{i2} = \frac{Z_{c2}^2}{0} = \infty$$

则可以求出 ab 端的等效阻抗

$$Z_{\rm ab} = Z_{\rm il} \ /\!/ \ Z_{\rm i2} = 1000 \Omega$$

从 ab 端到电源又是经过 $\lambda/4$,因此从 1-1' 端口向终端看的输入阻抗为

$$Z_{11'} = \frac{1}{Z_{ab}} \times Z_{c1}^2 = \frac{1}{1000} \times 100^2 \Omega = 10\Omega$$

计算始端电流

$$\dot{I}_1 = \frac{1}{Z_{11}} \times \dot{U}_s = \frac{1}{10} \times \frac{10}{\sqrt{2}} / 0^{\circ} A = \frac{\sqrt{2}}{2} / 0^{\circ} A$$

则始端电流幅值为 $I_{1m}=1A$.