Computational Aeroacoustics Methods with OpenFOAM v. 4.1

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Structure

Theoretical part

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- 2. Problem statement
- 3. Available CAA methods
- 4. Curle's analogy
- 5. FFWH analogy
- 6. Boundary Element Method
- 7. Implementation: libAcoustics library

Hands-on part: pulsating sphere

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- 2. One-dimensional case
 - Case description
 - How to set up FFWH analogy in OpenFOAM
 - Settings for hybrid CFD/BEM computations
 - Results
- 3. Basic BEM++ case
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 - Case description
 - Settings in OpenFOAM
 - Results
- 5. Discussion

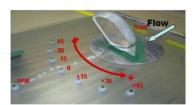
Part I Theoretical part

Computational Aeroacoustics: issues and methods

Computational Aeroacoustic applications



Rocket lift-off



Flow around wing mirror



Aircfart engines



Submarine propellers

Sound pressure levels around us

Sound source	SPL, dB
Good recording studio	20
Whisper	30
Average home	40-50
Conversational speech, 1 m	60
Vacuum cleaner	70
Diesel truck (10 m distance)	90
Disco (1 m distance)	100
Chainsaw (1 m distance), rock concert	110
Discomfort threshold, near an air	120
Pain threshold, near an air	130-140
Gun shot	140
Jet engine (1 m distance)	130-160
Rocket lift-off	140-180

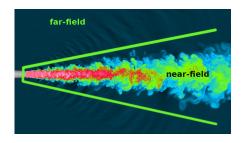
Danger zone: >140 dB!

Computational complexities

- Complicated structure of flows
- High-frequency acoustic waves
- Requirements for numerical solution:
 - stability;
 - low diffusivity;
 - correct simulation of turbulent structures;
 - correct simulation in the far-field,

consequently,

large volume of processed data.



How to solve?

- direct numerical simulation;
- aeroacoustic analogies;
- boundary element methods.

Lighthill's analogy

Hydrodynamic equations

Mass conservation:

$$\frac{\partial \rho}{\partial t} + \frac{\partial (\rho U_j)}{\partial x_j} = 0.$$

Momentum conservation:

$$\frac{\partial \rho U_i}{\partial t} + \frac{\partial (\rho U_i U_j)}{\partial x_j} = -\frac{\partial p}{\partial x_i} + \frac{\partial \tau_{ij}}{\partial x_j}, \quad \tau_{ij} = \mu \left(\frac{\partial U_i}{\partial x_j} + \frac{\partial U_j}{\partial x_i} - \frac{2}{3} \frac{\partial U_j}{\partial x_j} \delta_{ij} \right).$$

Lighthill's equation

$$\frac{\partial^2 \rho'}{\partial t^2} - c^2 \nabla^2 \rho' = \frac{\partial T_{ij}}{\partial x_i \partial x_j}$$
— quadrupole sources,

$$T_{ij} = \rho U_i U_j + \delta_{ij} \left(p' + c^2 \rho' - \tau_{ij} \right)$$
 — Lighthill's stress tensor

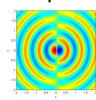
Acoustic sources

Monopole



$$\begin{split} &\frac{\partial^2 p'}{\partial t^2} + \nabla^2 p' = \\ &= -f(t) \ \delta(\mathbf{x} - \mathbf{x_0}) \end{split}$$

Dipole



$$\frac{\partial^2 p'}{\partial t^2} + \nabla^2 p' =$$

$$= -\frac{\partial}{\partial x_j} (f_j(t) \, \delta(\mathbf{x} - \mathbf{x_0}))$$

Quadrupole



$$\frac{\partial^2 \rho'}{\partial t^2} - c^2 \nabla^2 \rho' =$$

$$= \frac{\partial T_{ij}}{\partial x_i \partial x_j}$$

Curle's analogy¹

Fundamental result:

$$\rho' = \frac{1}{4\pi c^2} \frac{\partial^2}{\partial x_i \, \partial x_j} \int_V \frac{T_{ij}(\mathbf{y}, t - r/c)}{r} \, d\mathbf{y} + \frac{1}{4\pi c^2} \frac{\partial}{\partial x_i} \int_S \frac{P_i(\mathbf{y}, t - r/c)}{r} \, d\mathbf{y}$$

Simplifications:

- no volumetric sources;
- isentropic flow in the region of interest;
- retarded time is neglected.

Sound pressure computations

$$p' = \frac{1}{4\pi c} \frac{x_i}{r^2} \frac{\partial F_i}{\partial t}, \quad F_i = \int_S P_i(\mathbf{y}, t) \, dS(\mathbf{y})$$

¹Curle N. The influence of solid boundaries upon aerodynamic sound. Proc. Royal Soc., 1955. 231A. P. 505–514.

Curle's analogy

Computational algorithm

- 1. Define static solid surface around the source region
- 2. Compute resultant force F exerted upon the fluid by the surface
- 3. Compute sound pressure in the observer position

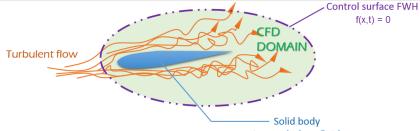
Limitations

- Low-speed flows
- Static non-deformable surface

Ffowcs-Williams — Hawkings analogy²

FFWH equation

$$\frac{\partial^{2} \rho' H(f)}{\partial t^{2}} - c^{2} \nabla^{2} \rho' H(f) =
= \frac{\partial T_{ij} H(f)}{\partial x_{i} \partial x_{j}} - \frac{\partial}{\partial x_{i}} \left(\tau_{ij} \delta(f) \frac{\partial f}{\partial x_{j}} \right) + \frac{\partial}{\partial t} \left(\rho_{0} u_{i} \delta(f) \frac{\partial f}{\partial x_{j}} \right)$$



in a turbulent fluid

²J.E. Ffowcs Williams and D.L. Hawkings: Sound generated by turbulence and surfaces in arbitrary motion, Philosophical Transactions of the Royal Society, A264, 1969, 321-342

Ffowcs-Williams — Hawkings analogy

Formulations³

Formulations

Farassat 1, 1A, Q1, Q1A...

Computational algorithm

- 1. Update surface position around the source region
- 2. Update distances from observers to surface
- 3. Compute sound pressure in the observer position using some formulation

³Farassat F. Derivation of Formulations 1 and 1A of Farassat. Langley Research Center, Hampton, Virginia. 2007

Transformation to frequency domain

Wave equation for exterior Dirichlet problem:

$$\frac{\partial^2 p(x,t)}{\partial t^2} - c^2 \nabla^2 p(x,t) = 0, \quad x \in \Omega_e = \mathbb{R}^3 \backslash \overline{\Omega}.$$

Sound pressure is the harmonic function:

$$p(x,t) = \text{Re } (u(x)e^{-i\omega t}).$$

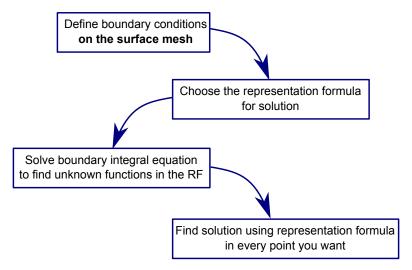
Helmholtz equation for complex sound pressure

$$\Delta u(x) + k^2 u(x) = 0$$
 for $x \in \Omega_e$.

Boundary conditions

$$\begin{split} u &= g(x) \text{ for } x \in \Gamma = \partial \Omega; \\ \lim_{r \to \infty} r \left(\frac{\partial u(x)}{\partial r} - iku(x) \right) &= 0, \quad r = |x|, \quad x \to \infty. \end{split}$$

Overview



Direct and indirect approach: representation formula

Direct approach

$$u(x) = \int_{\partial \Gamma} \frac{\partial G(x, y)}{\partial n_y} g(y) dS_y - \int_{\partial \Gamma} \frac{\partial u(y)}{\partial n_y} G(x, y) dS_y, \quad x \in \Omega_c.$$

Indirect approach

- via a single layer potential:

$$u(x) = (\tilde{V}_k w)(x) = \int_{\partial \Gamma} G(x, y) w(y) dS_y, \quad x \in \Omega_c.$$

- via a double layer potential:

$$u(x) = (W_k v)(x) = \int_{\partial \Gamma} \frac{\partial G(x, y)}{\partial n_y} v(y) dS_y, \quad x \in \Omega_c.$$

Direct and indirect approach: boundary integral equations

Direct approach

$$\int_{\partial \Gamma} G(x,y)t(y) dS_y = -\frac{1}{2}g(x) + \int_{\partial \Gamma} \frac{\partial G(x,y)}{\partial n_y} g(y) dS_y, \quad x \in \Gamma.$$

Indirect approach

- via a single layer potential:

$$(V_k w)(x) = \int_{\partial \Gamma} G(x, y) w(y) dS_y = g(x), \quad x \in \Gamma.$$

– via a double layer potential:

$$\frac{1}{2}v(x) + (K_k v)(x) = \frac{1}{2}v(x) + \int_{\partial \Gamma} \frac{\partial G(x, y)}{\partial n_y} v(y) \, dS_y = g(x), \quad x \in \Gamma.$$

Combined formulation of BIE4

Representation of solution

$$u(x) = (\tilde{V}_k w)(x) - i\eta(W_k w)(x), \quad x \in \Omega_c.$$

Boundary integral equation

$$\left(\frac{1}{2}I + K\right)w(x) - i\eta(V_k w)(x) = g(x), \quad x \in \Gamma.$$

Boundary integral operator is injective for all $k \in \mathbb{R}_+$.

 $^{^4}$ Engleder S., Steinbach O. Modified boundary integral formulations for the Helmholtz equation // Journal of Mathematical Analysis and Applications, 2007. Vol. 331. P. 396–407.

Computational algorithm

- 1. Define static solid surface around the source region
- 2. Run CFD simulation with pressure sampling on the surface
- 3. Transform sample data in the frequency domain
- 4. Export data to another open-source package
- 5. Solve boundary integral equations
- 6. Compute resultant sound pressure in the observer position

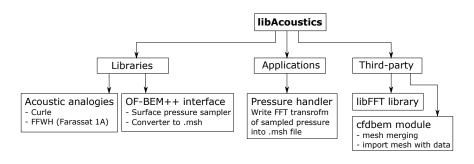
BEM++

Solver of elliptic equations with boundary element method.

Use Python interface and C++ kernel.

Actual version: v. 3.1.

libAcoustics



Download:

git clone https://github.com/unicfdlab/libAcoustics.git

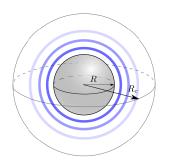
Install:

cd libAcoustics/OpenFOAM-4.1
./wmakeAll

Part II Practical part

libAcoustics training

Problem statement



Input data

Radius of sphere: R=0.1 m

Velocity oscillations:

 $U(R,t) = U_0 \sin(2\pi f t)$

Velocity amplitude: $U_0 = 0.01 \text{ m/s}$

Frequency: f = 100 Hz

Speed of sound: c = 100 m/s

Density of gas: $\rho_0 = 14.1855 \text{ kg/m}^3$

Check

Sound pressure and SPL in points:

(0,0,1), (0,0,2), (0,0,3), (0,0,4), (0,0,5), (0,0,10).

Analytical solution

$$p(r,t) = \mathrm{Re}\left[\frac{A}{r}e^{-i(\omega t - kr)}\right];$$

here $\omega = 2\pi f$, $A = \rho_0 c U_0 e^{-ikR}$, $k = \omega/c$.

Numerical simulation

Compare techniques

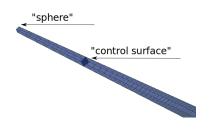
- direct Finite Volume Method (FVM) simulation with OpenFOAM;
- FFWH using OpenFOAM;
- pure BEM using BEM++;
- CFD/BEM using both OpenFOAM and BEM++.

Tests

- 1D-case in OpenFOAM
- 3D-case in bempp
- 3D-case in OpenFOAM

1D case

Flow domain



Mesh information

Length: 14.9 m.

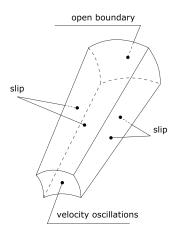
Mesh size: 2100 cells.

Numerical parameters

Solver: rhoCentralFoam

Turbulence model: laminar flow

Scheme of boundaries



1D case

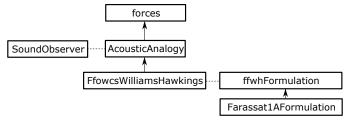
Boundary conditions

Name	T	U	p
sphere	fixedValue 24.8084307131	uniformFixedValue sine	zeroGradient
free	zeroGradient	waveTransmissive	waveTransmissive
сус	slip	slip	slip

Note

Temperature and density are calculated according to sound speed 100 m/s.

How to use FFWH in OpenFOAM



Use functionObjectAPI for running

```
In system/controlDict:
functions {
    ffwh1 {
       functionObjectLibs ("libAcoustics.so");
       ...
    }
}
```

Settings in dictionary I

- 1. General settings for acoustic analogies:
 - functionObjectLibs ("libAcoustics.so") usage of the libAcoustics library;
 - ▶ log logging info;
 - probeFrequency step for acoustic probe;
 - timeStart, timeEnd time interval;
 - ▶ c0 sound speed;
 - dRef domain depth (for 2D computations);
 - pName name of pressure field;
 - pInf reference pressure;
 - rhoName name of density field;
 - rhoInf reference density;
 - ▶ CofR origin;
 - list of observers.
- 2. Special settings for FFWH:
 - type type of acoustic analogy;

Settings in dictionary II

- ▶ interpolationScheme interpolation scheme for control surface:
- formulationType FFWH formulation;
- surfaces list of control surfaces:
- ▶ nonUniformSurfaceMotion true if surface can move with mesh;
- Ufwh fixed velocity of control surace moving;
- cleanFreq step for FFT computations;
- fixedResponceDelay true if responce delay is fixed;
- responceDelay value of responce delay.

Control surface in case: "sphere" patch or small quadrangle placed in the wedge.

Results for 1D case

FFWH

Results are increased: the control surface is just a small part of sphere, computations of surface integral are not correct.

CFD/BEM

Almost zero due to strong 3D statement of BIE.

Trick: just set the calculated value of complex pressure to all nodes of 3D sphere (separate geometry) and use this data for BIE computations.

Results for two first microphones

Microphone	Analytical	FFWH	CFD/BEM, 1D	CFD/BEM, 3D
$(0\ 0\ 1)$	≈ 0.7549	≈ 1.08	$\approx 10^{-5}$	≈ 0.73
$(0\ 0\ 2)$	≈ 0.3775	≈ 0.54	$\approx 10^{-5}$	≈ 0.35

How to use $BEM++^5$

How to run simple case

- Create a python script which uses BEM++ python library to solve Helmholtz equation.
- Run: python scriptname.py

Structure of bempp basic case folder

- Python script for case.
- Folder subscripts/: post-processing, computations of analytical solution.
- Folder output/: contains solution, result of post-processing.
 Appears after successful solution.
- Folder graph/: set of gnuplot scripts for data visualization.

Structure of folder is arbitrary.

⁵http://www.bempp.org/

bempp script for simple case I

1. Import Python libraries, bempp Python API, OF-bempp interface:

```
import bempp.api
import numpy as np
from cfdbem.grid import merge
from cfdbem.file_interfaces import FileReader
from bempp.api.linalg import gmres
```

2. Define basic variables:

```
freq = 100  # frequency
c = 100  # speed of sound
epsilon = 1E-5  # solution
    accuracy
k = freq * 2 * np.pi / c # wave number
muD = 1.0/k  # numerical
    constant for CBIE formulation
```

bempp script for simple case II

3. Import mesh from file using OF-bempp interface:

```
reader = FileReader(file_name = "cs.msh")
grid = reader.grid
```

4. Define spaces:

```
piecewise_lin_space =
   bempp.api.function_space(grid, "P", 1)
piecewise_const_space =
   bempp.api.function_space(grid, "DP", 0)
```

5. Choose spaces for boundary integral operators:

```
domain_space = piecewise_lin_space
range_space = piecewise_lin_space
dual_to_range_space = piecewise_lin_space
```

6. Define boundary integral operators:

bempp script for simple case III

```
identity = bempp.api.operators.
   boundary.sparse.identity(
        domain_space, range_space,
           dual to range space)
dlp = bempp.api.operators.
   boundary.helmholtz.double_layer(
        domain_space, range_space,
           dual_to_range_space,k)
slp = bempp.api.operators.
   boundary.helmholtz.single_layer(
    domain space, range space,
       dual to range space, k)
```

7. Define Dirichlet boundary condition using OpenFOAM data:

```
dirichlet fun =
   bempp.api.GridFunction(piecewise_lin_space,
   coefficients =
                            reader.node_data)
```

bempp script for simple case IV

8. Write left-hand side of boundary integral equation:

```
lhs = (.5*identity + dlp) - 1j * muD * slp
```

9. Solve boundary integral equation with GMRES method:

```
w_fun,info = gmres(lhs, dirichlet_fun,
     tol=epsilon)
```

10. Define function for computations of sound pressure in appropriate points:

```
def result (points):
    from bempp.api.operators.potential import
        helmholtz as helmholtz_potential

slp_pot = helmholtz_potential.single_layer(
        piecewise_lin_space, points, k)
```

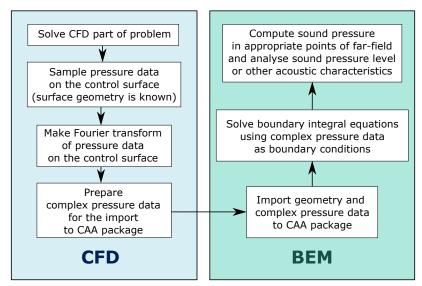
bempp script for simple case V

```
dlp_pot = helmholtz_potential.double_layer(
    piecewise_lin_space, points, k)

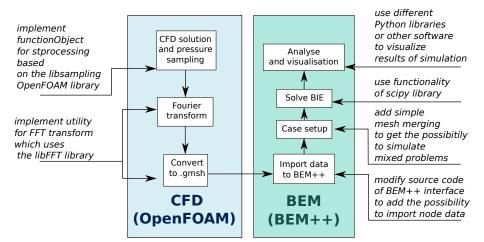
res = 1j * muD * slp_pot.evaluate(w_fun) -
    dlp_pot.evaluate(w_fun)
return res
```

11. Use standard or user-defined Python functions for data postprocessing.

General scheme of hybrid CFD/BEM technology



CFD/BEM implementation using OpenFOAM and BEM++



Setting in OpenFOAM for CFD/BEM interface I

soundPressureSampler functionObject

- functionObjectLibs ("libAcoustics.so") usage of the libAcoustics library;
- type typre of functionObject;
- writeControl what time poinst should be output;
- outputGeometryFormat format for control surface geometry;
- fields what fields should be sampled;
- pName name of pressure field;
- log if true view log info;
- interpolationScheme interpolation scheme for control surface;
- list of control surfaces.

Setting in OpenFOAM for CFD/BEM interface II

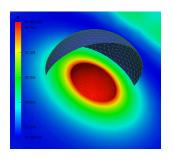
surfaceNoise utility

- outputFormat format for data output;
- inputFileName name of file of sampled pressure data;
- maxFrequency maximal frequency to be computed.

Notes for OF/bempp technology usage

- Only 3D problems.
- Control surface must be triangulated.
- Input format for bempp: only gmsh.
- No separate solver for BIE: all steps for solution are written in one script.

3D case I



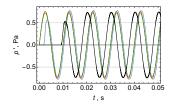
Spherical control surfaces

Radius: 0.2 m.

Mesh resolution:

- 1. $h_1 = 0.04$ m;
- 2. $h_2 = 0.02$ m;
- 3. $h_3 = 0.01$ m;

Due to long computational time all results are saved in the res/ folder.



Microphone (0 0 1) Control surface 1

Blue color — FFWH
Red color — analytical solution
Green color — CFD/BEM
Black line — FVM

Summary

- We made an overview of CAA methods.
- We have discussed the libAcoustics library for CAA computations in OpenFOAM.
- We have known about new open-source code BEM++ for BIE calculations.
- We have known how to make a hierarchical numerical model using OpenFOAM and BEM++.
- We have tested different methods on the test case (pulsating sphere): pure FVM modelling, FFWH acoustic analogy, CFD/CAA hybrid technique.

Thank you for your attention! Questions?