Demodulation of DSB-SC

Recovery of the original signal (demodulation) could be accomplished by another frequency shift, i.e. modulating with $\cos \omega_c t$ again.

$$\phi(t)\cos\omega_c t = f(t)\cos^2\omega_c t = \frac{1}{2}f(t)[1 + \cos 2\omega_c t]$$

■ Taking the Fourier transform,

$$\mathcal{F}\{\phi(t)\cos\omega_c t\} = \frac{1}{2}F(\omega) + \frac{1}{4}F(\omega + 2\omega_c) + \frac{1}{4}F(\omega - 2\omega_c)$$

- We can reject the signals around $\pm 2\nu_c$ with a low-pass filter and obtain output $e_0(t) = \frac{1}{2}f(t)$.
- However, we'll see with demodulation of DSB-SC that phase and frequency must exactly match.

Introduce an error in the phase $(\Delta\theta)$ into the locally generated carrier frequency.

$$\phi(t)\cos(\omega_c t + \Delta\theta) = f(t)\cos\omega_c t\cos(\omega_c t + \Delta\theta)$$
$$= \frac{1}{2}f(t)\cos\Delta\theta + \frac{1}{2}f(t)\cos(2\omega_c t + \Delta\theta)$$

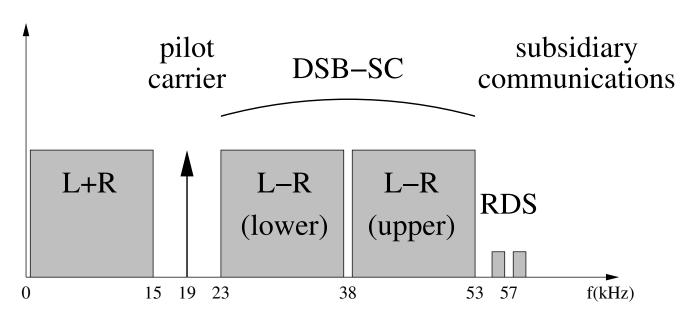
After a low-pass filter get output

$$e_0(t) = \frac{1}{2}f(t)\cos\Delta\theta$$

- A phase error causes a variable output (drops to zero if $\Delta\theta=\pm90^\circ$).
- \blacksquare A frequency mis-match $\Delta\theta=\Delta\omega t$ results in a low-frequency oscillation.
- Therefore with DSB-SC it is necessary to use a synchronised oscillator termed synchronous detection or ceherent detection.

Include Carrier in Transmission

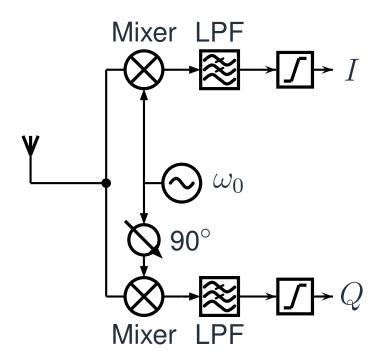
DSB-LC Double sideband large carrier allows asynchronous demodulation, e.g. envelope detector, but sidebands are limited to <33% power, therefore inefficient **pilot carrier** Include a pilot carrier. For example, in stereo FM there is a $19\,\mathrm{kHz}$ signal included (limited to 10% of peak frequency deviation) which allows generation of $38\,\mathrm{kHz}$ carrier for DSB-SC demodulation of (L-R) component, and $57\,\mathrm{kHz}$ for Radio Data System (RDS) demodulation.





Carrier Recovery

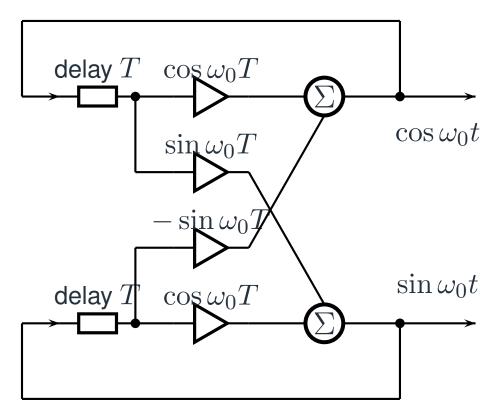
- How do we regenerate a phase-locked carrier at the receiver where there is no explicit carrier in the data stream?
- Need a controllable oscillator at the receiver, such as a voltage controlled oscillator (VCO), e.g. $\omega_0 = \omega_i + \alpha v$.
- Need a means to phase lock the oscillator to the input waveform.



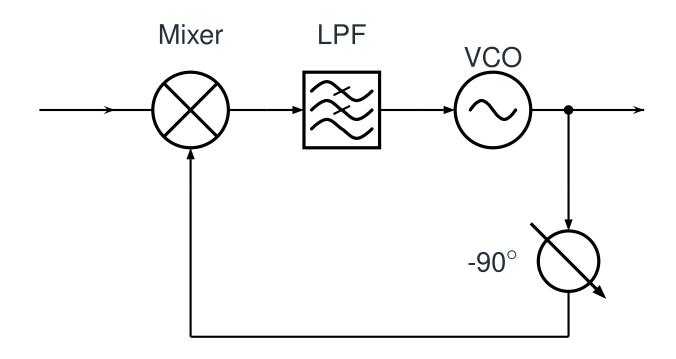
Digital Oscillator: Cordic Algorithm

$$\cos \omega_0(t+T) = \cos \omega_0 T \cos \omega_0 t - \sin \omega_0 T \sin \omega_0 t$$

$$\sin \omega_0(t+T) = \cos \omega_0 T \sin \omega_0 t + \sin \omega_0 T \cos \omega_0 t$$



Phase-Locked Loop



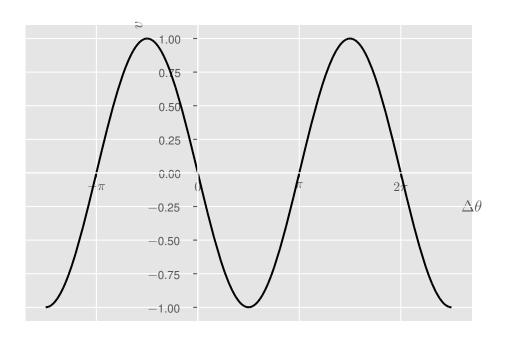
input: $\cos(\omega_{\text{ref}}t + \theta_{\text{ref}})$

mixed with: $-\sin(\omega_0 t + \theta_0)$

after LPF: $-\frac{1}{2}\sin\left(\Delta\omega t + \Delta\theta\right)$

stationary solution: $\Delta \omega = 0$ and hence $\sin \Delta \theta = \frac{2(\omega_i - \omega_{\text{ref}})}{\alpha}$.

Phase-Locked Loop

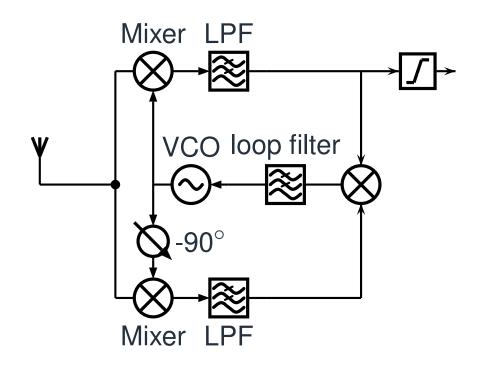


- \blacksquare phase is integral of frequency $\theta_0(t)=\int_0^t\omega_0(\tau)\,\mathrm{d}\tau+\theta_0(t=0)$
- $\Delta \theta = \sin^{-1} \frac{2(\omega_i \omega_{\text{ref}})}{\alpha}$ is a **stable** stationary point (negative feedback)
- $\Delta \theta = \pi \sin^{-1} \frac{2(\omega_i \omega_{\text{ref}})}{\alpha} \text{ is an } \textbf{unstable} \text{ stationary point (positive feedback)}$
- PLL locks in frequency and phase to a sinusoidal reference

Costas Loop

- but phase-modulated input would continually be trying to lock to instantaneous phase (suppressed carrier)
- we could initialise with an unmodulated carrier first, and then switch off lock (analogue PAL for colour info)
- Costas Loops allow the symbol phase info to be eliminated.
- In classical Costas loop use both in-phase and quadrature VCO outputs and combine LPF outputs to drive VCO.

Costas Loop



input: $s(t)\cos(\omega_{\text{ref}}t + \theta_{\text{ref}})$

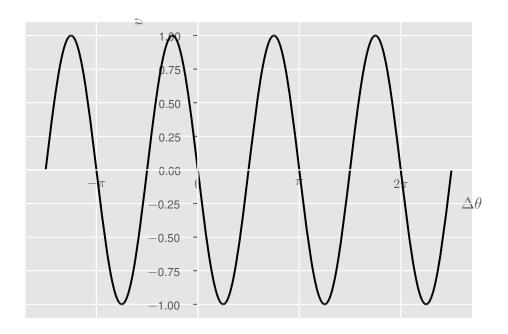
after LPF1: $\frac{1}{2}s(t)\cos(\Delta\omega t + \Delta\theta)$

after LPF2: $-\frac{1}{2}s(t)\sin(\Delta\omega t + \Delta\theta)$

VCO input: $-\frac{1}{8}s^2(t)\sin 2\left(\Delta\omega t + \Delta\theta\right)$ with $s(t) = \pm 1$

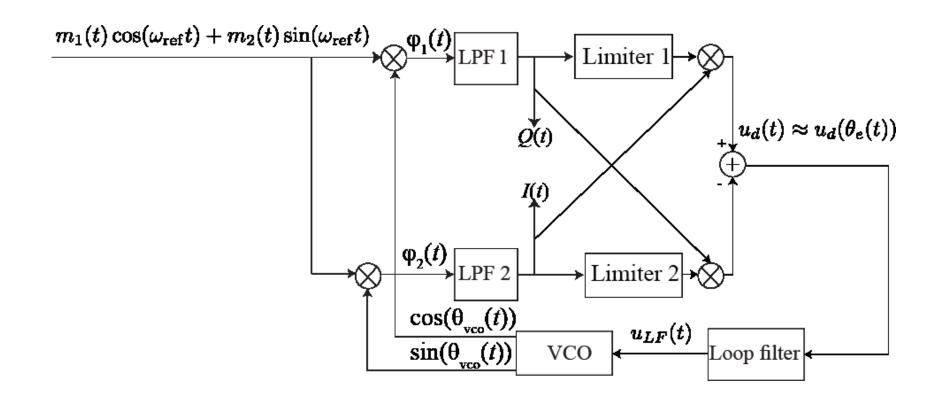
stationary solution: $\Delta \omega = 0$ and hence $\sin 2\Delta \theta = \frac{8(\omega_i - \omega_{\text{ref}})}{\alpha}$.

Costas Loop



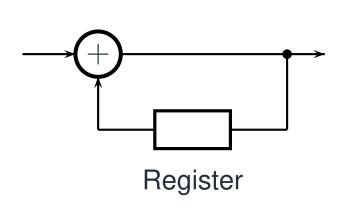
- **n** phase is integral of frequency $\theta_0(t) = \int_0^t \omega_0(\tau) d\tau + \theta_0(t=0)$
- $\Delta \theta = \frac{1}{2} \sin^{-1} \frac{8(\omega_i \omega_{\text{ref}})}{\alpha}$ is a **stable** stationary point (negative feedback)
- $\Delta \theta = \pi + \frac{1}{2} \sin^{-1} \frac{8(\omega_i \omega_{\text{ref}})}{\alpha}$ is also a **stable** stationary point
- Requires a check to see if BPSK binary data is inverted or not.

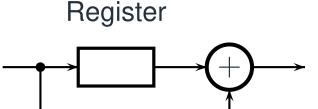
QPSK Costas Loop



Differential Encoding

Differential encoding prevents inversion of the signal (and symbols) from affecting the data. Note: adds an additional symbol requiring initialisation.





Differential Encoder

$$y_i = y_{i-1} \oplus x_i$$

Differential Decoder

$$x_i = y_i \oplus y_{i-1}$$

⊕ represents component-wise modulo 2 addition (XOR) for binary symbols.
There are also line codes designed to be polarity insensitive, such as Differential Manchester encoding.