

## Design of Beams

### 2 MODULE NO. 2: ULTIMATE FLEXURE STRENGTH (T&L-SECTION)

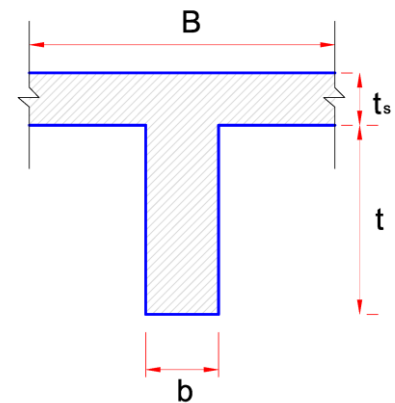
#### 2.1 Inputs

##### 2.1.1 Material Properties

- ✓ Concrete compressive strength ( $f_{cu}$ )
- ✓ Reduction factor of concrete compressive strength ( $\gamma_c=1.50$ )
- ✓ Yield strength of longitudinal reinforcing steel bars ( $f_y$ )
- ✓ Reduction factor of reinforcing steel yield strength ( $\gamma_s=1.15$ )
- ✓ Modulus of elasticity of reinforcing steel bars ( $E_s = 200,000 \text{ N/mm}^2$ )

##### 2.1.2 Section Definition

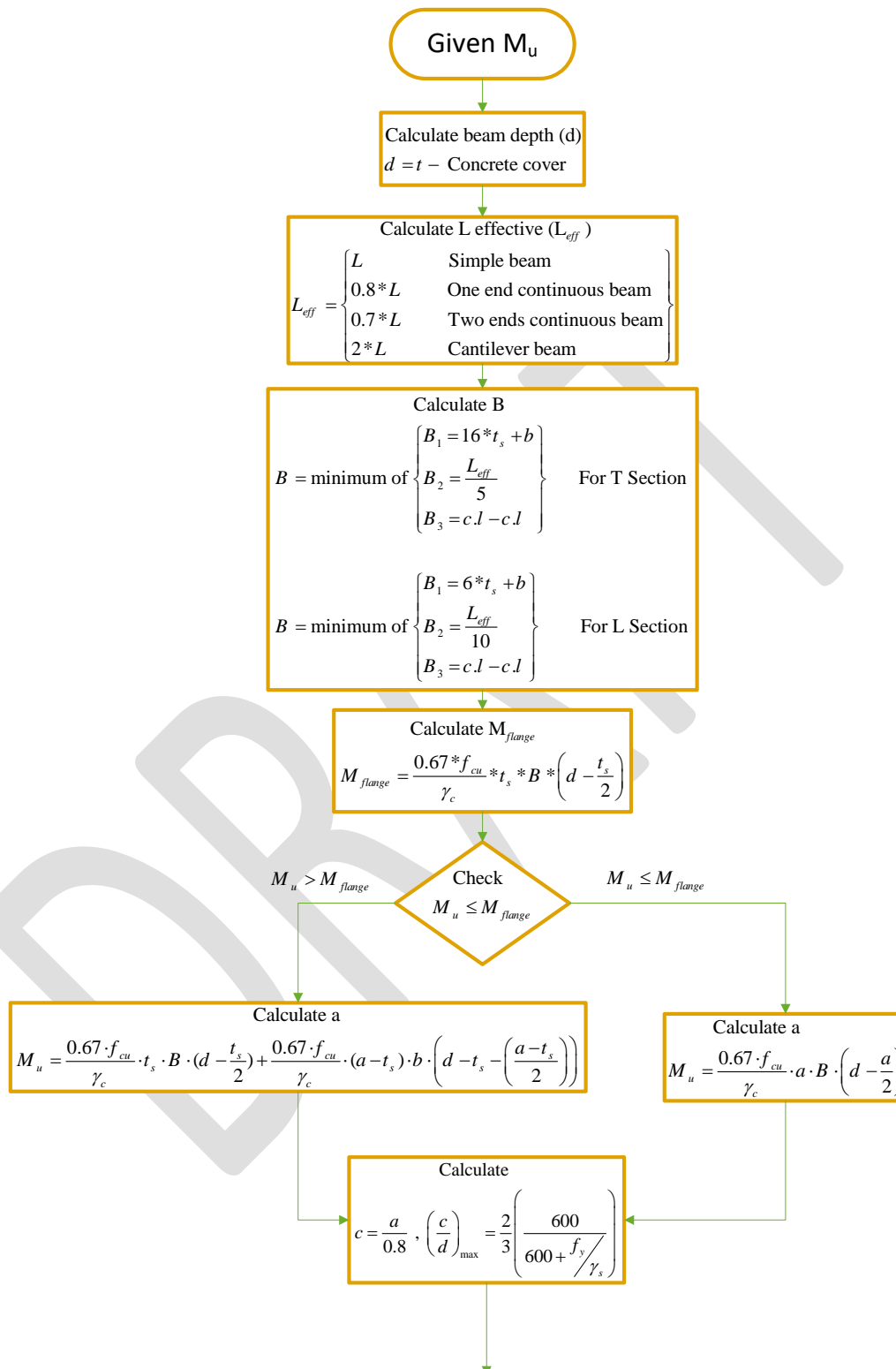
- ✓ Beam width ( $b$ )
- ✓ Total beam depth ( $t$ )
- ✓ Concrete cover
- ✓ Slab thickness ( $t_s$ )
- ✓ Beam span ( $L$ )
- ✓ Centerline to centerline span
- ✓ Beam condition
  - (Simple, one end continuous, two ends continuous)
- ✓ Section type (L, T)

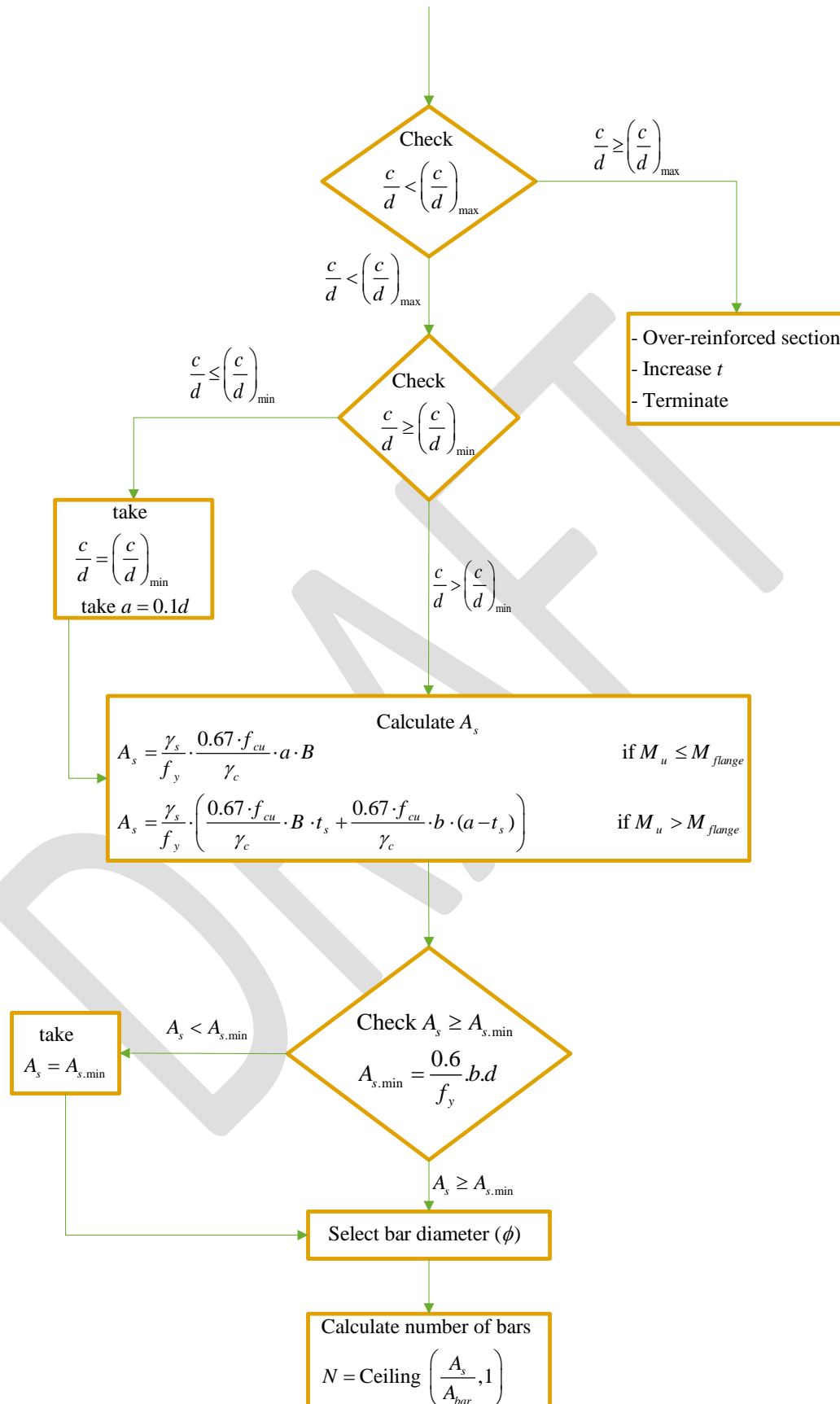


##### 2.1.3 Internal Forces

- ✓ Ultimate Factored Moment from analysis ( $M_u$ )

## 2.2 Calculation Procedure





## 2.3 Design Outputs

- ✓ Beam total depth (t).
- ✓ Diameter of bars.
- ✓ Number of bars.

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## 2.4 Example of Calculations using Mathcad

### 2.1 Input

#### 2.1.1 Material Properties

$$f_{cu} := 30 \frac{N}{mm^2}$$

Concrete compressive strength

$$f_y := 400 \frac{N}{mm^2}$$

Yield strength of reinforcing steel bar

$$E_s := 200000 \frac{N}{mm^2}$$

Modulus of elasticity of steel

$$\gamma_c := 1.5$$

Concrete strength reduction factor

$$\gamma_s := 1.15$$

Steel strength reduction factor

#### 2.1.2 Section Definition

$$b := 250 \text{ mm}$$

Beam width

$$t_s := 180 \text{ mm}$$

Slab thickness

$$t := 700 \text{ mm}$$

Total beam depth

$$\text{conc.cover} := 50 \text{ mm}$$

Concrete Cover

$$L := 5 \text{ m}$$

Beam span

$$cl.cl := 5.15 \text{ m}$$

Center line to center line span

$$\text{sec.type} := \text{"L"}$$

sec.type values:

"T" for T section

"L" for L section

$$\text{beam.cond} := \text{"one end connected"}$$

beam.cond values

"simple"

"one end connected"

"two ends connected"

#### 2.1.3 Internal Forces

$$M_u := 400 \text{ kN}\cdot\text{m}$$

Ultimate factored moment from analysis

**2.2 Calculation Procedure**

$$d := t - \text{conc.cover} = 650 \text{ mm}$$

Calculate beam depth

$$L_{eff} := \begin{cases} \text{if beam.cond} = \text{"simple"} & = 4000 \text{ mm} \\ \parallel L \\ \text{also if beam.cond} = \text{"one end connected"} & \\ \parallel 0.8 \cdot L \\ \text{also if beam.cond} = \text{"two ends connected"} & \\ \parallel 0.7 \cdot L \\ \text{else} & \\ \parallel 2 \cdot L \end{cases}$$

$$B_1 := \text{if}(\text{sec.type} = \text{"T"}, (16 \cdot t_s) + b, \text{if}(\text{sec.type} = \text{"L"}, (6 \cdot t_s) + b, b)) = 1330 \text{ mm}$$

$$B_2 := \text{if}\left(\text{sec.type} = \text{"T"}, \frac{L_{eff}}{5} + b, \text{if}\left(\text{sec.type} = \text{"L"}, \frac{L_{eff}}{10} + b, b\right)\right) = 650 \text{ mm}$$

$$B_3 := \text{cl.cl} = 5150 \text{ mm}$$

$$B := \min(B_1, B_2, B_3) = 650 \text{ mm}$$

$$M_{flange} := \frac{0.67 \cdot f_{cu}}{\gamma_c} \cdot t_s \cdot B \cdot \left(d - \frac{t_s}{2}\right) = 878 \text{ kN}\cdot\text{m}$$

$$a := 1 \text{ mm}$$

$$a := \begin{cases} \text{if } M_u \leq M_{flange} & \\ \parallel \text{root}\left(M_u - 0.67 \frac{f_{cu}}{\gamma_c} \cdot a \cdot B \cdot \left(d - \frac{a}{2}\right), a\right) & \\ \text{else} & \\ \parallel \text{root}\left(M_u - 0.67 \frac{f_{cu}}{\gamma_c} \cdot a \cdot B \cdot \left(d - \frac{a}{2}\right) - 0.67 \cdot \frac{f_{cu}}{\gamma_c} \cdot (a - t_s) \cdot b \cdot \left(d - t_s - \left(\frac{a - t_s}{2}\right)\right), a\right) & \end{cases}$$

$$a = 74.98 \text{ mm}$$

$$c := \frac{a}{0.8} = 93.7 \text{ mm}$$

$$c/d = f_{c1} := \text{if}\left(\frac{c}{d} \geq \frac{2}{3} \cdot \frac{0.003}{0.003 + \frac{f_y}{\gamma_s \cdot E_s}}, \text{"Over reinforced section, increase ts"}, \frac{c}{d}\right)$$

$$f_{c1} = 0.1$$

$$c := f_{c1} \cdot d = 93.7 \text{ mm}$$

$$c := \text{if}(c < 0.125 \cdot d, 0.125 \cdot d, c)$$

$$c = 93.7 \text{ mm}$$

$$a := 0.8 \cdot c = 75 \text{ mm}$$



$$A_s := \text{if } M_u \leq M_{flange}$$

$$\left\| 0.67 \cdot \frac{f_{cu}}{\gamma_c} \cdot \frac{\gamma_s}{f_y} \cdot a \cdot B \right\|$$

else

$$\left\| \frac{\gamma_s}{f_y} \cdot \left( \frac{2}{3} \cdot \frac{f_{cu}}{\gamma_c} \cdot t_s \cdot B + \frac{2}{3} \cdot \frac{f_{cu}}{\gamma_c} \cdot (a - t_s) \cdot b \right) \right\|$$

Calculate required area steel

$$A_s = 1877.5 \text{ mm}^2$$

$$A_{smin} := \frac{0.6 \cdot \frac{N}{\text{mm}^2} \cdot B \cdot d}{f_y} = 634 \text{ mm}^2$$

Calculate minimum required area steel

$$A_s := \text{if } (A_s < A_{smin}, A_{smin}, A_s)$$

$$A_s = (2 \cdot 10^3) \text{ mm}^2$$

$$\phi 6 := 28.3 \text{ mm}^2$$

$$\phi 8 := 50.3 \text{ mm}^2$$

$$\phi 10 := 78.5 \text{ mm}^2$$

$$\phi 12 := 113 \text{ mm}^2$$

$$\phi 16 := 201 \text{ mm}^2$$

$$\phi 18 := 254 \text{ mm}^2$$

$$\phi 20 := 314 \text{ mm}^2$$

$$\phi 22 := 380 \text{ mm}^2$$

$$\phi 25 := 491 \text{ mm}^2$$

$$\phi 28 := 616 \text{ mm}^2$$

$$\phi 32 := 804 \text{ mm}^2$$

$$N := \frac{A_s}{\phi 18} = 7.4$$

$$N := \text{Ceil}(N, 1) = 8$$

### 2.3 Output

$$t = 700 \text{ mm}$$

$$b = 250 \text{ mm}$$

$$\text{Use } N = 8 \quad \phi 18$$