传递过程

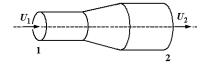
鲍 博 副教授华东理工大学 化工学院

2022年秋季

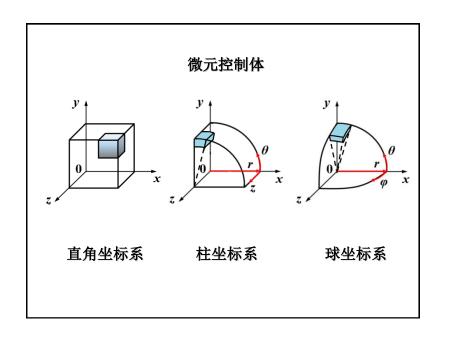
1.7 守恒原理

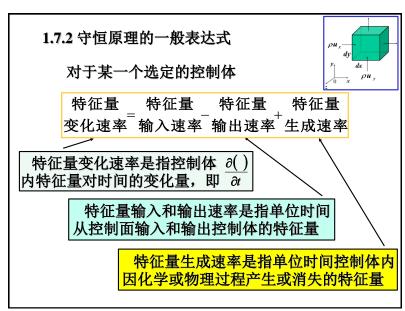
1.7.1控制面与控制体

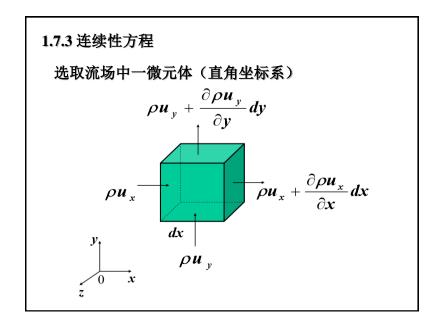
确定对象及范围:控制面 控制体

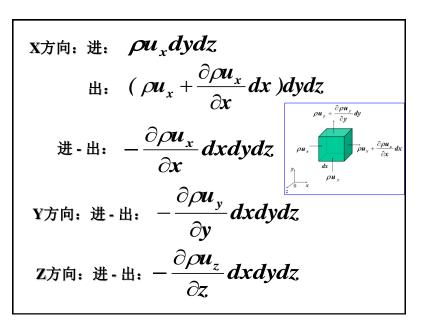


设备控制体









 $\frac{\partial \rho}{\partial t} dx dy dz$ 累积速率:

生成速率: R = 0

质量守恒: $\frac{\partial M}{\partial t} = W_1 - W_2 + R$

$$\frac{\partial \rho}{\partial t} dx dy dz = \left(-\frac{\partial \rho u_x}{\partial x} - \frac{\partial \rho u_y}{\partial y} - \frac{\partial \rho u_z}{\partial z}\right) dx dy dz$$

连续性方程
$$\frac{\partial \rho}{\partial t} + \frac{\partial \rho u_x}{\partial x} + \frac{\partial \rho u_y}{\partial y} + \frac{\partial \rho u_z}{\partial z} = 0$$

定常流动连续性方程

$$\frac{\partial \rho}{\partial t} = 0$$

$$\frac{\partial \rho u_x}{\partial x} + \frac{\partial \rho u_y}{\partial y} + \frac{\partial \rho u_z}{\partial z} = 0$$

不可压缩流体连续性方程

ρ为常数

$$\frac{\partial u_x}{\partial x} + \frac{\partial u_y}{\partial y} + \frac{\partial u_z}{\partial z} = 0$$

不可压缩流体定常流动,速度散度为零(流速在各方向的 变化率之和为零),意味着无源场,即满足连续性方程

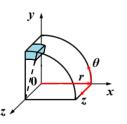
1.7.4 柱坐标系和球坐标系中连续性方程的形式

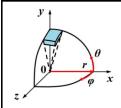
柱坐标系

$$\frac{\partial \rho}{\partial t} + \frac{1}{r} \frac{\partial \rho r u_r}{\partial r} + \frac{1}{r} \frac{\partial \rho u_{\theta}}{\partial \theta} + \frac{\partial \rho u_z}{\partial z} = 0$$

若定常且ρ为常数

$$\frac{1}{r}\frac{\partial ru_r}{\partial r} + \frac{1}{r}\frac{\partial u_\theta}{\partial \theta} + \frac{\partial u_z}{\partial z} = 0$$





球坐标系

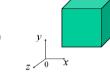
$$\frac{\partial \rho}{\partial t} + \frac{1}{r^2} \frac{\partial \rho r^2 u_r}{\partial r} + \frac{1}{r \sin \theta} \frac{\partial \rho u_{\theta} \sin \theta}{\partial \theta} + \frac{1}{r \sin \theta} \frac{\partial \rho u_{\varphi}}{\partial \varphi} = 0$$

若定常且ρ为常数

$$\frac{1}{r^2}\frac{\partial r^2 u_r}{\partial r} + \frac{1}{r\sin\theta}\frac{\partial u_\theta \sin\theta}{\partial \theta} + \frac{1}{r\sin\theta}\frac{\partial u_\varphi}{\partial \varphi} = 0$$



2.1粘性流体运动方程



选取流场中一微元体(直角坐标系)对非定常流体的动量守恒:

$$\frac{\partial (m\vec{u})}{\partial t} = (w\vec{u})_1 - (w\vec{u})_2 + \Sigma \vec{F}$$

x, y, z方向的分量守恒式:

$$\frac{\partial (m\bar{u}_x)}{\partial t} = (w\bar{u})_{1x} - (w\bar{u})_{2x} + \Sigma \vec{F}_x$$

$$\frac{\partial (m\bar{u}_y)}{\partial t} = (w\bar{u})_{1y} - (w\bar{u})_{2y} + \Sigma \vec{F}_y$$

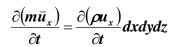
$$\frac{\partial (m\bar{u}_z)}{\partial t} = (w\bar{u})_{1z} - (w\bar{u})_{2z} + \Sigma \vec{F}_z$$

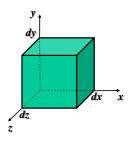
 ΣF 包括压力p、剪切应力 τ 、体积力X、其它外力。

粘性流体运动方程(动量守恒原理)

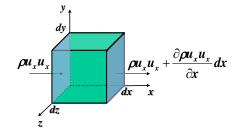
$$x$$
方向: $\frac{\partial (m\bar{u}_x)}{\partial t} = (w\bar{u})_{1x} - (w\bar{u})_{2x} + \Sigma \vec{F}_x$

微元体内动量累积速率:





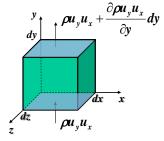
对流传递产生的动量净速率:



x方向流动产生的x方向动量净速率:

$$\rho u_x u_x dy dz - \left(\rho u_x u_x + \frac{\partial \rho u_x u_x}{\partial x} dx\right) dy dz = -\frac{\partial \rho u_x u_x}{\partial x} dx dy dz$$

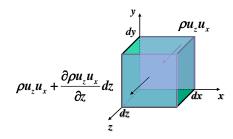
对流传递产生的动量净速率:



y方向流动产生的x方向动量净速率:

$$\rho u_y u_x dx dz - \left(\rho u_y u_x + \frac{\partial \rho u_y u_x}{\partial y} dy\right) dx dz = -\frac{\partial \rho u_y u_x}{\partial y} dx dy dz$$

对流传递产生的动量净速率:



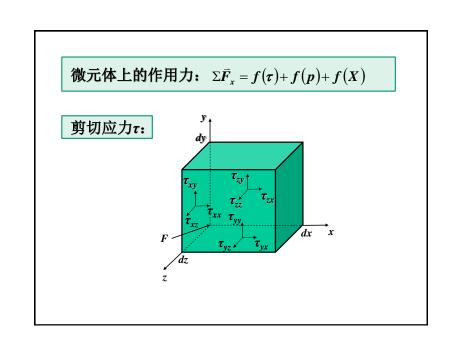
z方向流动产生的x方向动量净速率:

$$\rho u_z u_x dx dy - \left(\rho u_z u_x + \frac{\partial \rho u_z u_x}{\partial z} dz\right) dx dy = -\frac{\partial \rho u_z u_x}{\partial z} dx dy dz$$

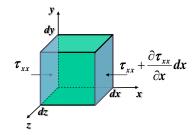
三者相加(前三页)

对流传递产生的x方向上动量净速率:

$$(w\bar{u})_{1x} - (w\bar{u})_{2x} = -\left(\frac{\partial \rho u_x u_x}{\partial x} + \frac{\partial \rho u_y u_x}{\partial y} + \frac{\partial \rho u_z u_x}{\partial z}\right) dx dy dz$$



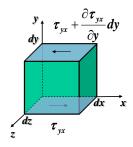
剪切应力τ产生的动量净速率:



x面上 τ 产生的x方向动量净速率:

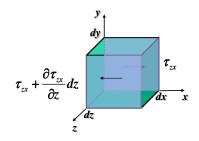
$$\tau_{xx}dydz - \left(\tau_{xx} + \frac{\partial \tau_{xx}}{\partial x}dx\right)dydz = -\frac{\partial \tau_{xx}}{\partial x}dxdydz$$

剪切应力τ产生的动量净速率:



y面上 τ 产生的x方向动量净速率:

$$\tau_{yx}dxdz - \left(\tau_{yx} + \frac{\partial \tau_{yx}}{\partial y}dy\right)dxdz = -\frac{\partial \tau_{yx}}{\partial y}dxdydz$$



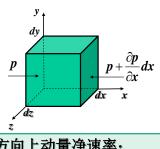
z面上τ产生的x方向动量净速率:

$$\tau_{zx}dxdy - \left(\tau_{zx} + \frac{\partial \tau_{zx}}{\partial z}dz\right)dxdy = -\frac{\partial \tau_{zx}}{\partial z}dxdydz$$

三者相加(前三页)

剪切应力τ产生的x方向上动量净速率:

$$f(\tau) = -\left(\frac{\partial \tau_{xx}}{\partial x} + \frac{\partial \tau_{yx}}{\partial y} + \frac{\partial \tau_{zx}}{\partial z}\right) dx dy dz$$



压力p产生的x方向上动量净速率:

$$f(p) = pdydz - \left(p + \frac{\partial p}{\partial x}dx\right)dydz = -\frac{\partial p}{\partial x}dxdydz$$

体积力X产生的x方向上动量净速率:

$$f(X) = \rho X dx dy dz$$

根据动量守恒原理

$$\frac{\partial (m\vec{u}_x)}{\partial t} = (w\vec{u})_{1x} - (w\vec{u})_{2x} + \Sigma \vec{F}_y$$

$$\frac{\partial(\rho u_x)}{\partial t} = -\left(\frac{\partial \rho u_x u_x}{\partial x} + \frac{\partial \rho u_y u_x}{\partial y} + \frac{\partial \rho u_z u_x}{\partial z}\right) - \left(\frac{\partial \tau_{xx}}{\partial x} + \frac{\partial \tau_{yx}}{\partial y} + \frac{\partial \tau_{zx}}{\partial z}\right) - \frac{\partial p}{\partial x} + \rho X$$

引入连续性方程
$$\frac{\partial u_x}{\partial x} + \frac{\partial u_y}{\partial y} + \frac{\partial u_z}{\partial z} = \mathbf{0}$$
 ρ 为常数

$$\left| \frac{\partial \rho u_x}{\partial t} + u_x \frac{\partial \rho u_x}{\partial x} + u_y \frac{\partial \rho u_x}{\partial y} + u_z \frac{\partial \rho u_x}{\partial z} \right| = -\left(\frac{\partial \tau_{xx}}{\partial x} + \frac{\partial \tau_{yx}}{\partial y} + \frac{\partial \tau_{zx}}{\partial z} \right) - \frac{\partial p}{\partial x} + \rho X$$

应力形式的 运动方程
$$\rho \frac{Du_x}{Dt} = -\frac{\partial p}{\partial x} + \rho X - \left(\frac{\partial \tau_{xx}}{\partial x} + \frac{\partial \tau_{yx}}{\partial y} + \frac{\partial \tau_{zx}}{\partial z} \right) \rho$$
 为常数

2.1.1奈维-斯托克斯方程

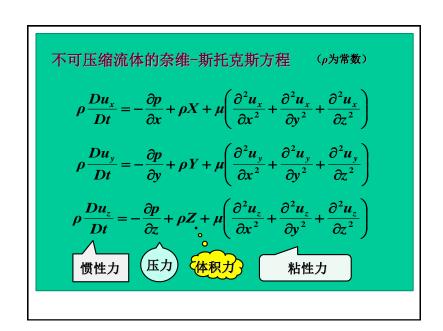
对于不可压缩流体,若应力各向同性以及应力与 应变率符合线性关系,可引入牛顿粘性定律的一 般表达式:

般表达式:

$$\tau_{xy} = \tau_{yx} = -\mu \left(\frac{\partial u_x}{\partial y} + \frac{\partial u_y}{\partial x} \right) \qquad \tau_{xx} = -2\mu \frac{\partial u_x}{\partial x}$$

$$\tau_{yz} = \tau_{zy} = -\mu \left(\frac{\partial u_y}{\partial z} + \frac{\partial u_z}{\partial y} \right) \qquad \tau_{yy} = -2\mu \frac{\partial u_y}{\partial y}$$

$$\tau_{zx} = \tau_{xz} = -\mu \left(\frac{\partial u_z}{\partial x} + \frac{\partial u_x}{\partial z} \right) \qquad \tau_{zz} = -2\mu \frac{\partial u_z}{\partial z}$$



2.1.2柱坐标系和球坐标系中的形式

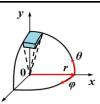


柱坐标系中剪切应力与形变的关系:

$$\begin{vmatrix} \tau_{r\theta} = \tau_{\theta r} = -\mu \left[r \frac{\partial}{\partial r} \left(\frac{u_{\theta}}{r} \right) + \frac{1}{r} \frac{\partial u_{r}}{\partial \theta} \right] & \tau_{rr} = -2\mu \frac{\partial u_{r}}{\partial r} \\ \tau_{\theta z} = \tau_{z\theta} = -\mu \left(\frac{\partial u_{\theta}}{\partial z} + \frac{1}{r} \frac{\partial u_{z}}{\partial \theta} \right) & \tau_{\theta\theta} = -2\mu \left(\frac{1}{r} \frac{\partial u_{\theta}}{\partial \theta} + \frac{u_{r}}{r} \right) \\ \tau_{zr} = \tau_{rz} = -\mu \left(\frac{\partial u_{z}}{\partial r} + \frac{\partial u_{r}}{\partial z} \right) & \tau_{zz} = -2\mu \frac{\partial u_{z}}{\partial z}$$

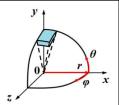
柱坐标系—条维-斯托克斯方程 $r方向: \rho \left(\frac{\partial u_r}{\partial t} + u_r \frac{\partial u_r}{\partial r} + \frac{u_\theta}{r} \frac{\partial u_r}{\partial \theta} - \frac{u_\theta^2}{r} + u_z \frac{\partial u_r}{\partial z} \right) \qquad z$ $= -\frac{\partial p}{\partial r} + \rho X_r + \mu \left[\frac{\partial}{\partial r} \left(\frac{1}{r} \frac{\partial r u_r}{\partial r} \right) + \frac{1}{r^2} \frac{\partial^2 u_r}{\partial \theta^2} - \frac{2}{r^2} \frac{\partial u_\theta}{\partial \theta} + \frac{\partial^2 u_r}{\partial z^2} \right]$ $\theta \dot{D} \dot{D}: \rho \left(\frac{\partial u_\theta}{\partial t} + u_r \frac{\partial u_\theta}{\partial r} + \frac{u_\theta}{r} \frac{\partial u_\theta}{\partial \theta} + \frac{u_r u_\theta}{r} + u_z \frac{\partial u_\theta}{\partial z} \right)$ $= -\frac{1}{r} \frac{\partial p}{\partial \theta} + \rho X_\theta + \mu \left[\frac{\partial}{\partial r} \left(\frac{1}{r} \frac{\partial r u_\theta}{\partial r} \right) + \frac{1}{r^2} \frac{\partial^2 u_\theta}{\partial \theta^2} + \frac{2}{r^2} \frac{\partial u_r}{\partial \theta} + \frac{\partial^2 u_\theta}{\partial z^2} \right]$ $z \dot{D} \dot{D}: \rho \left(\frac{\partial u_z}{\partial t} + u_r \frac{\partial u_z}{\partial r} + \frac{u_\theta}{r} \frac{\partial u_z}{\partial \theta} + u_z \frac{\partial u_z}{\partial z} \right)$ $= -\frac{\partial p}{\partial z} + \rho X_z + \mu \left[\frac{1}{r} \frac{\partial}{\partial r} \left(r \frac{\partial u_z}{\partial r} \right) + \frac{1}{r^2} \frac{\partial^2 u_z}{\partial \theta^2} + \frac{\partial^2 u_z}{\partial z^2} \right]$

球坐标系中剪切应力与形变的关系:



$$\begin{split} & \tau_{r\theta} = \tau_{\theta r} = -\mu \Bigg[r \frac{\partial}{\partial r} \bigg(\frac{u_{\theta}}{r} \bigg) + \frac{1}{r} \frac{\partial u_{r}}{\partial \theta} \Bigg] \qquad \tau_{rr} = -2\mu \frac{\partial u_{r}}{\partial r} \\ & \tau_{\theta \varphi} = \tau_{\varphi \theta} = -\mu \Bigg[\frac{\sin \theta}{r} \frac{\partial}{\partial \theta} \bigg(\frac{u_{\varphi}}{\sin \theta} \bigg) + \frac{1}{r \sin \theta} \frac{\partial u_{\theta}}{\partial \varphi} \Bigg] \qquad \tau_{\theta \theta} = -2\mu \bigg(\frac{1}{r} \frac{\partial u_{\theta}}{\partial \theta} + \frac{u_{r}}{r} \bigg) \\ & \tau_{\varphi r} = \tau_{r\varphi} = -\mu \Bigg[\frac{1}{r \sin \theta} \frac{\partial u_{r}}{\partial \varphi} + r \frac{\partial}{\partial r} \bigg(\frac{u_{\varphi}}{r} \bigg) \Bigg] \qquad \tau_{\varphi \varphi} = -2\mu \bigg(\frac{1}{r \sin \theta} \frac{\partial u_{\theta}}{\partial \varphi} + \frac{u_{r}}{r} + \frac{u_{\theta} \cot \theta}{r} \bigg) \end{split}$$

球坐标系--奈维-斯托克斯方程



r方向:

$$\begin{split} &\rho\Bigg(\frac{\partial u_r}{\partial t} + u_r \frac{\partial u_r}{\partial r} + \frac{u_\theta}{r} \frac{\partial u_r}{\partial \theta} + \frac{u_\varphi}{r \sin \theta} \frac{\partial u_r}{\partial \varphi} - \frac{u_\theta^2 + u_\varphi^2}{r}\Bigg) \\ &= -\frac{\partial p}{\partial r} + \rho X_r + \mu \Bigg[\frac{1}{r^2} \frac{\partial}{\partial r} \bigg(r^2 \frac{\partial u_r}{\partial r}\bigg) + \frac{1}{r^2 \sin \theta} \frac{\partial}{\partial \theta} \bigg(\sin \theta \frac{\partial u_r}{\partial \theta}\bigg) \\ &+ \frac{1}{r^2 \sin^2 \theta} \frac{\partial^2 u_r}{\partial \varphi^2} - \frac{2}{r^2} u_r - \frac{2}{r^2} \frac{\partial u_\theta}{\partial \theta} - \frac{2}{r^2} u_\theta \cot \theta - \frac{2}{r^2 \sin \theta} \frac{\partial u_\varphi}{\partial \varphi}\Bigg] \end{split}$$

