扩散方程

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第十四讲. 扩散方程

- 1. 质量传递微分方程
- 2. 通过静止气膜的扩散
- 3. 等分子反方向稳态扩散
- 4. 非定常分子扩散
- 5. 颗粒溶解

1. 质量传递微分方程

守恒原理的一般表达式

控制体内 A 质量 对时间的变化量

$$\frac{\partial M_A}{\partial t} = W_{A1} - W_{A2} + R_A$$

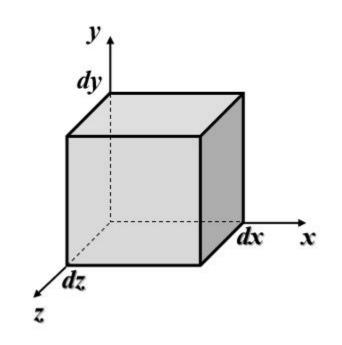
单位时间控制体内 因化学或物理过程 产生或消失的 A 质量

单位时间从控制面 输入和输出控制体的 A 质量

对流传质微分方程

控制体内 A 物质的质量变化速率:

$$\frac{\partial M_A}{\partial t} = \frac{\partial \rho_A}{\partial t} dx dy dz$$



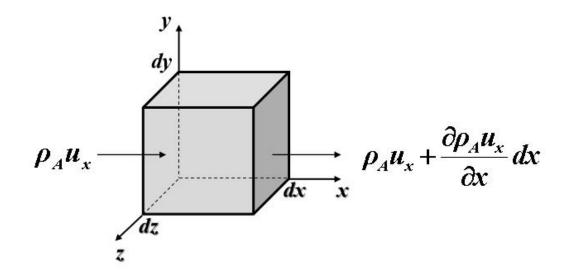
控制体内因化学反应产生或消失的A物质的质量, 则其生成速率:

$$R_A = r_A dx dy dz$$

其中 r_A 为单位体积控制体内 A 物质的质量生成速率。

质量输入和输出速率

流体流动带入和带出的质量净速率:



x 方向流动带入和带出的质量净速率:

$$\rho_A u_x dy dz - \left(\rho_A u_x + \frac{\partial \rho_A u_x}{\partial x} dx\right) dy dz = -\frac{\partial \rho_A u_x}{\partial x} dx dy dz$$

同理

y 方向流动带入和带出的质量净速率:

$$\rho_{A}u_{y}dxdz - \left(\rho_{A}u_{y} + \frac{\partial\rho_{A}u_{y}}{\partial x}dy\right)dxdz = -\frac{\partial\rho_{A}u_{y}}{\partial y}dxdydz$$

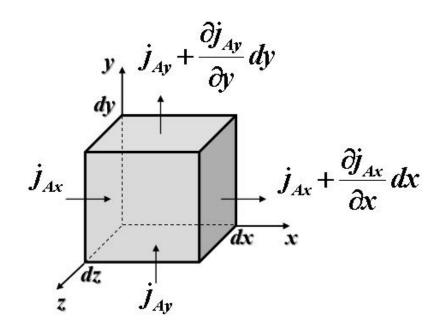
z 方向流动带入和带出的质量净速率:

$$\rho_{A}u_{z}dxdy - \left(\rho_{A}u_{z} + \frac{\partial\rho_{A}u_{z}}{\partial z}dz\right)dxdz = -\frac{\partial\rho_{A}u_{z}}{\partial z}dxdydz$$

流体流动带入和带出的总质量净速率:

$$-\left(\frac{\partial \rho_A u_x}{\partial x} + \frac{\partial \rho_A u_y}{\partial y} + \frac{\partial \rho_A u_z}{\partial z}\right) dx dy dz$$

扩散产生的质量净速率:



x 方向扩散产生的质量净速率:

$$j_{Ax}dydz - \left(j_{Ax} + \frac{\partial j_{Ax}}{\partial x}dx\right)dydz = -\frac{\partial j_{Ax}}{\partial x}dxdydz$$

同理 y方向扩散产生的质量净速率:

$$j_{Ay}dxdz - \left(j_{Ay} + \frac{\partial j_{Ay}}{\partial y}dy\right)dxdz = -\frac{\partial j_{Ay}}{\partial y}dxdydz$$

z 方向扩散产生的质量净速率:

$$j_{Az}dxdy - \left(j_{Az} + \frac{\partial j_{Az}}{\partial z}dz\right)dxdy = -\frac{\partial j_{Az}}{\partial z}dxdydz$$

扩散产生的总质量净速率:

$$-\left(\frac{\partial j_{Ax}}{\partial x} + \frac{\partial j_{Ay}}{\partial y} + \frac{\partial j_{Az}}{\partial z}\right) dx dy dz$$

质量输入和输出净速率:

$$W_{A1} - W_{A2} = -\left(\frac{\partial \rho_A u_x}{\partial x} + \frac{\partial \rho_A u_y}{\partial y} + \frac{\partial \rho_A u_z}{\partial z}\right) dx dy dz - \left(\frac{\partial j_{Ax}}{\partial x} + \frac{\partial j_{Ay}}{\partial y} + \frac{\partial j_{Az}}{\partial z}\right) dx dy dz$$

根据质量守恒
$$\frac{\partial M_A}{\partial t} = W_{A1} - W_{A2} + R_A$$

$$\frac{\partial \rho_A}{\partial t} = -\left(\frac{\partial \rho_A u_x}{\partial x} + \frac{\partial \rho_A u_y}{\partial y} + \frac{\partial \rho_A u_z}{\partial z}\right) - \left(\frac{\partial j_{Ax}}{\partial x} + \frac{\partial j_{Ay}}{\partial y} + \frac{\partial j_{Az}}{\partial z}\right) + r_A$$

$$\frac{\partial \rho_{A}}{\partial t} = -\left(\frac{\partial \rho_{A} u_{x}}{\partial x} + \frac{\partial \rho_{A} u_{y}}{\partial y} + \frac{\partial \rho_{A} u_{z}}{\partial z}\right) - \left(\frac{\partial j_{Ax}}{\partial x} + \frac{\partial j_{Ay}}{\partial y} + \frac{\partial j_{Az}}{\partial z}\right) + r_{A}$$

引入连续性方程:
$$\frac{\partial u_x}{\partial x} + \frac{\partial u_y}{\partial y} + \frac{\partial u_z}{\partial z} = 0$$

费克分子扩散定律:
$$j_{Ax} = -D_{AB} \frac{d\rho_A}{dx}$$

可得对流传质微分方程:

$$\frac{\partial \rho_A}{\partial t} + u_x \frac{\partial \rho_A}{\partial x} + u_y \frac{\partial \rho_A}{\partial y} + u_z \frac{\partial \rho_A}{\partial z} = D_{AB} \left(\frac{\partial^2 \rho_A}{\partial x^2} + \frac{\partial^2 \rho_A}{\partial y^2} + \frac{\partial^2 \rho_A}{\partial z^2} \right) + r_A$$

摩尔浓度 C_A 形式的对流传质微分方程:

$$\rho_{A} = M_{A}C_{A}$$

$$\frac{\partial C_A}{\partial t} + u_{Mx} \frac{\partial C_A}{\partial x} + u_{My} \frac{\partial C_A}{\partial y} + u_{Mz} \frac{\partial C_A}{\partial z} = D_{AB} \left(\frac{\partial^2 C_A}{\partial x^2} + \frac{\partial^2 C_A}{\partial y^2} + \frac{\partial^2 C_A}{\partial z^2} \right) + R_A$$

$$R_A = \frac{r_A}{M_A}$$

其中 R_A 为单位体积控制体内 A 物质的摩尔生成速率。

分子扩散微分方程

若A在静止介质B中扩散,可得分子扩散微分方程:

$$\frac{\partial \rho_A}{\partial t} = D_{AB} \left(\frac{\partial^2 \rho_A}{\partial x^2} + \frac{\partial^2 \rho_A}{\partial y^2} + \frac{\partial^2 \rho_A}{\partial z^2} \right) + r_A$$

$$\frac{\partial \rho_A}{\partial t} = D_{AB} \left(\frac{\partial^2 \rho_A}{\partial x^2} + \frac{\partial^2 \rho_A}{\partial y^2} + \frac{\partial^2 \rho_A}{\partial z^2} \right)$$

费克第二定律

$$\frac{\partial^2 \rho_A}{\partial x^2} + \frac{\partial^2 \rho_A}{\partial y^2} + \frac{\partial^2 \rho_A}{\partial z^2} = -\frac{r_A}{D_{AB}}$$

定常且无化学反应
$$\frac{\partial^2 \rho_A}{\partial x^2} + \frac{\partial^2 \rho_A}{\partial y^2} + \frac{\partial^2 \rho_A}{\partial z^2} = 0$$

摩尔浓度 C_{Λ} 形式的分子扩散微分方程:

$$\frac{\partial C_A}{\partial t} = D_{AB} \left(\frac{\partial^2 C_A}{\partial x^2} + \frac{\partial^2 C_A}{\partial y^2} + \frac{\partial^2 C_A}{\partial z^2} \right) + R_A$$

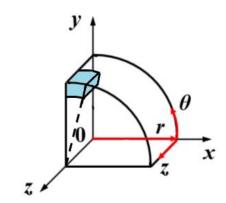
无化学反应
$$\frac{\partial C_A}{\partial t} = D_{AB} \left(\frac{\partial^2 C_A}{\partial x^2} + \frac{\partial^2 C_A}{\partial y^2} + \frac{\partial^2 C_A}{\partial z^2} \right)$$

$$\frac{\partial^2 C_A}{\partial x^2} + \frac{\partial^2 C_A}{\partial y^2} + \frac{\partial^2 C_A}{\partial z^2} = -\frac{R_A}{D_{AB}}$$

$$\frac{\partial^2 C_A}{\partial x^2} + \frac{\partial^2 C_A}{\partial y^2} + \frac{\partial^2 C_A}{\partial z^2} = 0$$
 拉普拉斯方程

参考资料

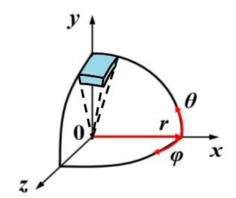
1.柱坐标系中的传质方程



$$\frac{\partial \rho_{A}}{\partial t} + u_{r} \frac{\partial \rho_{A}}{\partial r} + \frac{u_{\theta}}{r} \frac{\partial \rho_{A}}{\partial \theta} + u_{z} \frac{\partial \rho_{A}}{\partial z} = D_{AB} \left[\frac{1}{r} \frac{\partial}{\partial r} \left(r \frac{\partial \rho_{A}}{\partial r} \right) + \frac{1}{r^{2}} \frac{\partial^{2} \rho_{A}}{\partial \theta^{2}} + \frac{\partial^{2} \rho_{A}}{\partial z^{2}} \right] + r_{A}$$

$$\frac{\partial C_A}{\partial t} + u_{Mr} \frac{\partial C_A}{\partial r} + \frac{u_{M\theta}}{r} \frac{\partial C_A}{\partial \theta} + u_{Mz} \frac{\partial C_A}{\partial z} = D_{AB} \left[\frac{1}{r} \frac{\partial}{\partial r} \left(r \frac{\partial C_A}{\partial r} \right) + \frac{1}{r^2} \frac{\partial^2 C_A}{\partial \theta^2} + \frac{\partial^2 C_A}{\partial z^2} \right] + R_A$$

2.球坐标系中的传质方程



$$\frac{\partial \rho_A}{\partial t} + u_r \frac{\partial \rho_A}{\partial r} + \frac{u_\theta}{r} \frac{\partial \rho_A}{\partial \theta} + \frac{u_\phi}{r \sin \theta} \frac{\partial \rho_A}{\partial \phi}$$

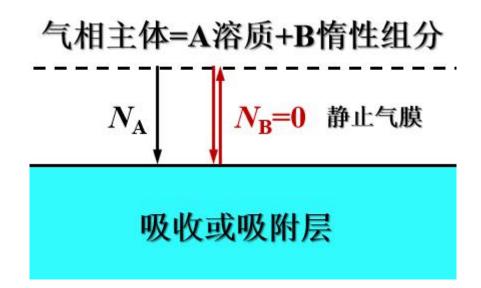
$$= D_{AB} \left[\frac{1}{r^2} \frac{\partial}{\partial r} \left(r^2 \frac{\partial \rho_A}{\partial r} \right) + \frac{1}{r^2 \sin\theta} \frac{\partial}{\partial \theta} \left(\sin\theta \frac{\partial \rho_A}{\partial \theta} \right) + \frac{1}{r^2 \sin^2 \theta} \frac{\partial^2 \rho_A}{\partial \varphi^2} \right] + r_A$$

$$\frac{\partial C_A}{\partial t} + u_{Mr} \frac{\partial C_A}{\partial r} + \frac{u_{M\theta}}{r} \frac{\partial C_A}{\partial \theta} + \frac{u_{M\phi}}{r \sin \theta} \frac{\partial C_A}{\partial \varphi}$$

$$= D_{AB} \left[\frac{1}{r^2} \frac{\partial}{\partial r} \left(r^2 \frac{\partial C_A}{\partial r} \right) + \frac{1}{r^2 \sin\theta} \frac{\partial}{\partial \theta} \left(\sin\theta \frac{\partial C_A}{\partial \theta} \right) + \frac{1}{r^2 \sin^2 \theta} \frac{\partial^2 C_A}{\partial \varphi^2} \right] + R_A$$

2. 通过静止气膜的扩散

在气体吸收或吸附单元操作中,气体由溶质A和惰性组分B组成的二元混合物中,组分A通过静止组分B扩散至吸收表面被吸收。



$$\frac{\partial C_A}{\partial t} + u_{Mx} \frac{\partial C_A}{\partial x} + u_{My} \frac{\partial C_A}{\partial y} + u_{Mz} \frac{\partial C_A}{\partial z} = D_{AB} \left(\frac{\partial^2 C_A}{\partial x^2} + \frac{\partial^2 C_A}{\partial y^2} + \frac{\partial^2 C_A}{\partial z^2} \right) + R_A$$

定常:
$$\frac{\partial C_A}{\partial t} = 0$$

静止气膜中:
$$\begin{cases} u_{Mx} = 0 \\ u_{My} \neq 0 \\ u_{Mz} = 0 \end{cases}$$

$$\begin{cases} \frac{\partial C_A}{\partial x} = \mathbf{0} \\ \frac{\partial C_A}{\partial y} \neq \mathbf{0} \\ \frac{\partial C_A}{\partial z} = \mathbf{0} \end{cases}$$

$$\begin{cases} \frac{\partial^2 C_A}{\partial x^2} = 0 \\ \frac{\partial^2 C_A}{\partial y^2} \neq 0 \\ \frac{\partial^2 C_A}{\partial z^2} = 0 \end{cases}$$

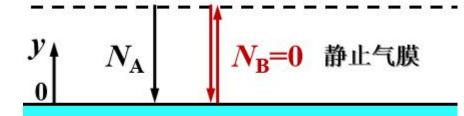
无化学反应: $R_{\lambda}=0$

简化对流传质微分方程得:

$$u_{My} \frac{\partial C_A}{\partial y} = D_{AB} \frac{\partial^2 C_A}{\partial y^2}$$

$$u_{My} \frac{\partial x_A}{\partial y} = D_{AB} \frac{\partial^2 x_A}{\partial y^2}$$

气相主体=A溶质+B惰性组分



吸收或吸附层

$$:: Cu_{My} = C_A u_{Ay} + C_B u_{By} = N_A + N_B = N_A$$

$$\therefore u_{My} = \frac{N_A}{C}$$

$$N_A \frac{dx_A}{dv} = CD_{AB} \frac{d^2x_A}{dv^2}$$

积分:
$$\frac{N_A}{CD_{AB}}y = ln\frac{dx_A}{dy} + C_1$$

边界条件: $y=0, x_A=0, N_A=-CD_{AB}\frac{dx_A}{dy}\Big|_{y=0}$

$$\therefore C_1 = -\ln\left(-\frac{N_A}{CD_{AB}}\right)$$

气相主体=A溶质+B惰性组分

V_A N_A N_B=0 静止气膜

W收或吸附层

$$\frac{dx_A}{dy} = -\frac{N_A}{CD_{AB}} e^{\frac{N_A}{CD_{AB}}y}$$

$$\int_{0}^{x_{A}} dx_{A} = \int_{0}^{y} -\frac{N_{A}}{CD_{AB}} e^{\frac{N_{A}}{CD_{AB}} y} dy$$

$$x_{A} = 1 - e^{\frac{N_{A}}{CD_{AB}}y}$$
 $N_{A}y = CD_{AB}\ln(1 - x_{A})$

$$y = y_1$$
 $x_A = x_{A1}$; $N_A y_1 = CD_{AB} \ln(1 - x_{A1})$
 $y = y_2$ $x_A = x_{A2}$; $N_A y_2 = CD_{AB} \ln(1 - x_{A2})$

$$N_{A} = \frac{CD_{AB}}{y - y_{1}} \ln \frac{1 - x_{A}}{1 - x_{A1}} \qquad N_{A} = \frac{CD_{AB}}{y_{2} - y_{1}} \ln \frac{1 - x_{A2}}{1 - x_{A1}}$$

静止气膜中浓度分布: $ln\frac{x_A-1}{x_{A_1}-1} = \frac{y-y_1}{y_2-y_1}ln\frac{x_{A_2}-1}{x_{A_1}-1}$

气相主体=A溶质+B惰性组分 V N_A N_B=0 静止气膜 吸收或吸附层

问题探讨

气膜中组分 B 静止吗?

$$\therefore x_A + x_B = 1 \qquad \therefore N_A = \frac{CD_{AB}}{y_2 - y_1} \ln \frac{x_{B2}}{x_{B1}}$$

定义:
$$x_{B,ln} = \frac{x_{B2} - x_{B1}}{ln \frac{x_{B2}}{x_{B1}}}$$

$$N_{A} = \frac{CD_{AB}}{x_{B,ln}} \frac{x_{B2} - x_{B1}}{y_{2} - y_{1}} = \frac{CD_{AB}}{x_{B,ln}} \frac{x_{A1} - x_{A2}}{y_{2} - y_{1}}$$

用对流传质模型表示:

$$N_{A} = \frac{CD_{AB}}{(y_{2} - y_{1})x_{B,ln}} (x_{A1} - x_{A2}) = k_{x}(x_{A1} - x_{A2})$$

传质系数:
$$k_x = \frac{CD_{AB}}{(y_2 - y_1)x_{B,ln}}$$

气体扩散系数测定

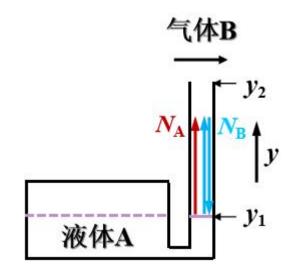
蒸发管测定气体扩散系数。组分A蒸发,通过静止组分B扩散 至流体主流。B不溶于液体,过程定常,气体为理想气体。

解: 理想气体

$$\frac{pV}{T} = nR \qquad C = \frac{n}{V} = \frac{p}{RT}$$

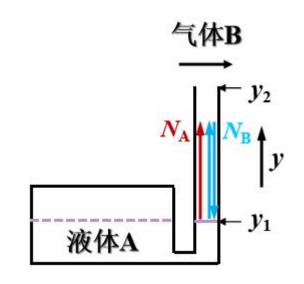
$$x_A = \frac{p_A}{p}$$

$$x_{B,ln} = \frac{p_{B2} - p_{B1}}{p \ln \frac{p_{B2}}{p_{B1}}} = \frac{p_{B,ln}}{p}$$



$$N_{A} = \frac{CD_{AB}}{x_{B,ln}} \frac{x_{A1} - x_{A2}}{y_{2} - y_{1}} = \frac{pD_{AB}}{RTp_{B,ln}} \frac{p_{A1} - p_{A2}}{y_{2} - y_{1}}$$

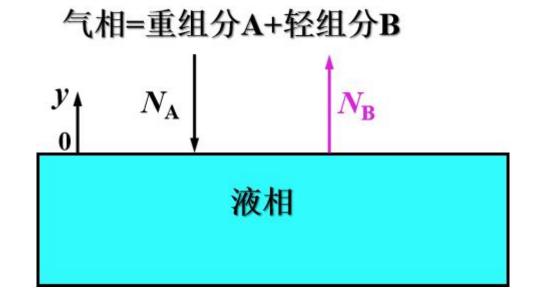
$$D_{AB} = \frac{N_A R T p_{B,ln}}{p} \frac{y_2 - y_1}{p_{A1} - p_{A2}}$$



组分 A 蒸发过程定常, N_A 由实验测得; 蒸发管中 $y = y_1$, $p = p_{A1}$, p_{A1} 为 p、T 下组分A的饱和蒸气压; $y = y_2$, $p = p_{A2} \approx 0$,组分A扩散到管口处,立即被大量气体B 带走,故 $p_{A2} \approx 0$ 。

3. 等分子反方向稳态扩散

在蒸馏和精馏单元操作中,组分 A、B 进行反方向扩散,若二者扩散的通量相等,则称为等分子反方向扩散。



$$\therefore Cu_{My} = C_A u_{Ay} + C_B u_{By} = N_A + N_B = N_A - N_A = 0$$

$$\therefore u_{My} = 0$$

定常:
$$\frac{\partial C_A}{\partial t} = 0$$

静止气膜中:

无化学反应:
$$R_A=0$$

\mathbf{A}_{A}

简化对流传质微分方程得:

$$\begin{cases} \frac{\partial C_A}{\partial x} = 0 \\ \frac{\partial C_A}{\partial y} \neq 0 \\ \frac{\partial C_A}{\partial z} = 0 \end{cases} \begin{cases} \frac{\partial^2 C_A}{\partial x^2} = 0 \\ \frac{\partial^2 C_A}{\partial y^2} \neq 0 \\ \frac{\partial^2 C_A}{\partial z^2} = 0 \end{cases}$$

$$\frac{\partial^2 C_A}{\partial y^2} = 0$$

$$\frac{d^2C_A}{dy^2} = 0$$

$$C_A = C_1 y + C_2$$

边界条件: $\begin{cases} y = y_1, & C_A = C_{A1} \\ y = y_2, & C_A = C_{A2} \end{cases}$

$$\begin{cases}
C_1 = \frac{C_{A1} - C_{A2}}{y_1 - y_2} \\
C_2 = C_{A1} - \frac{C_{A1} - C_{A2}}{y_1 - y_2} y_1
\end{cases}$$

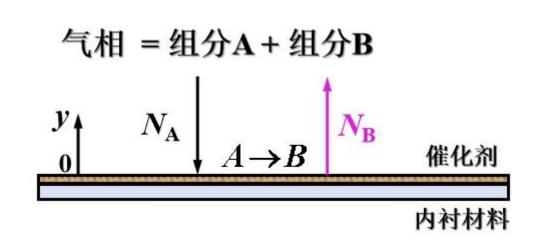
液相表面上气膜中浓度分布:

$$\frac{C_A - C_{A1}}{C_{A1} - C_{A2}} = \frac{y - y_1}{y_1 - y_2}$$

传质通量:
$$N_{Ax} = J_{Ax} + x_A (N_{Ax} + N_{Bx}) = J_{Ax} = -D_{AB} \frac{dC_A}{dy}$$

课后思考

- 1.伴有化学反应的扩散过程
- (1) 若反应速率大大高于扩散速率,扩散决定传质速率,称为扩散控制过程;
- (2)若反应速率远远低于扩散速率,化学反应决定传质速率,称为 反应控制过程。

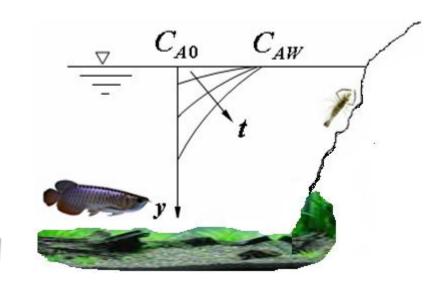




4. 非定常分子扩散

冰冻的湖面融化,水中的氧含量 随时间,沿深度变化。

将湖水简化为半无限大平壁,氧扩散为 非定常分子扩散。



分子扩散微分方程:

$$\frac{\partial C_A}{\partial t} = D_{AB} \left(\frac{\partial^2 C_A}{\partial x^2} + \frac{\partial^2 C_A}{\partial y^2} + \frac{\partial^2 C_A}{\partial z^2} \right) + R_A$$

相似的问题,相似的解:
$$\frac{\partial C_A}{\partial t} = D_{AB} \frac{\partial^2 C_A}{\partial v^2}$$

解方程得浓度分布:

$$\frac{C_{A} - C_{AW}}{C_{A0} - C_{AW}} = \frac{2}{\sqrt{\pi}} \int_{0}^{\eta} e^{-\eta^{2}} d\eta = erf(\eta)$$

式中: $\eta = \frac{y}{\sqrt{4D_{AB}t}}$

t 时刻水面处的氧扩散通量:

$$N_{At,y=0} = -D_{AB} \frac{\partial C_A}{\partial y} \bigg|_{y=0} = -D_{AB} \left(\frac{\partial C_A}{\partial \eta} \frac{\partial \eta}{\partial y} \right) \bigg|_{y=0} = \sqrt{\frac{D_{AB}}{\pi t}} \left(C_{AW} - C_{A0} \right)$$

0~t 时间内通过单位面积水面的氧扩散量:

$$N_{A} = \int_{0}^{t} N_{At,y=0} dt = \int_{0}^{t} \sqrt{\frac{D_{AB}}{\pi t}} (C_{AW} - C_{A0}) dt = 2\sqrt{\frac{D_{AB}t}{\pi}} (C_{AW} - C_{A0})$$

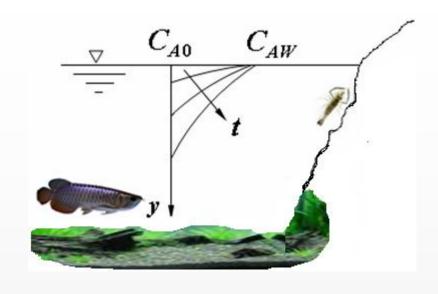
湖水中含氧量变化

已知: $C_{A0} = 3.0 \times 10^{-5} \text{ kmol/m}^3$,

 $C_{AW} = 3.06 \times 10^{-4} \text{ kmol/m}^3$,

 $D_{AB} = 1.58 \times 10^{-9} \text{ m}^{-2}/\text{s}_{\circ}$

求:三天后,离湖面0.06m深处的氧浓度。



解:
$$\eta = \frac{y}{\sqrt{4D_{AB}t}} = \frac{0.06}{\sqrt{4 \times 1.58 \times 10^{-9} \times 3 \times 24 \times 3600}} = 1.48$$

查误差函数表,线性内插得:
$$\frac{C_A - C_{AW}}{C_{A0} - C_{AW}} = erf(\eta) = 0.9633$$

氧浓度为:
$$C_A = 4.01 \times 10^{-5} \text{ kmol/m}^3$$

课后思考

1.对比静止流体中的平板启动、半无限大平壁非定常导热和湖水中 含氧量变化。体会传递现象的类似性。

$$\frac{u_x - U_W}{U_0 - U_W} = erf(\eta) \qquad \eta = \frac{y}{\sqrt{4vt}}$$

$$\frac{T - T_W}{T_0 - T_W} = erf(\eta) \qquad \eta = \frac{y}{\sqrt{4at}}$$

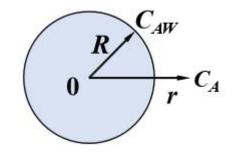
$$\frac{C_A - C_{AW}}{C_{A0} - C_{AW}} = erf(\eta) \qquad \eta = \frac{y}{\sqrt{4D_{AB}t}}$$

5. 颗粒溶解

球形颗粒中含有微量的可溶物质A,向周围静止的液相中扩散。假定颗粒表面为饱和浓度 C_{AW} ,且维持不变,液相主体浓度为 0,传质过程定常。

球坐标系

$$\frac{\partial C_A}{\partial t} + u_{Mr} \frac{\partial C_A}{\partial r} + \frac{u_{M\theta}}{r} \frac{\partial C_A}{\partial \theta} + \frac{u_{M\varphi}}{r \sin \theta} \frac{\partial C_A}{\partial \varphi}$$

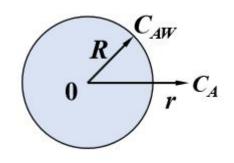


$$=D_{AB}\left[\frac{1}{r^{2}}\frac{\partial}{\partial r}\left(r^{2}\frac{\partial C_{A}}{\partial r}\right)+\frac{1}{r^{2}sin\theta}\frac{\partial}{\partial \theta}\left(sin\theta\frac{\partial C_{A}}{\partial \theta}\right)+\frac{1}{r^{2}sin^{2}\theta}\frac{\partial^{2}C_{A}}{\partial \varphi^{2}}\right]+R_{A}$$

简化得:
$$0 = D_{AB} \frac{1}{r^2} \frac{\partial}{\partial r} \left(r^2 \frac{\partial C_A}{\partial r} \right)$$

$$\frac{d}{dr}\left(r^2\frac{dC_A}{dr}\right) = 0$$

边界条件:
$$\begin{cases} r = R, C_A = C_{AW} \\ r \to \infty, C_A = 0 \end{cases}$$



颗粒表面液相中浓度分布: $\frac{C_A}{C} = \frac{R}{R}$

$$\frac{C_A}{C_{AW}} = \frac{R}{r}$$

物质A的溶解速率:

$$W = J_{Ar}|_{r=R} 4\pi R^{2} = -D_{AB} \frac{dC_{A}}{dr}|_{r=R} 4\pi R^{2} = \frac{D_{AB}C_{AW}}{R}$$

课后思考

1.缓释药片、缓释化肥和农药有何优点。如何控制其缓释速率。

