第2章 热力学定律和热力学基本方程

习题解答

1. 27℃时, 5 mol NH₃(g) 由 5 dm³恒温可逆膨胀至 50 dm³, 试计算体积功。假设 NH₃(g) 服从范德华方程。

解:由表 1-6 查得,NH₃(g)的 $a = 0.423 \text{ Pa} \cdot \text{mol}^{-2}$, $b = 0.0371 \times 10^{-3} \text{ m}^3 \cdot \text{mol}^{-1}$ 。对于 $1 \text{ mol NH}_3(g)$

$$\begin{split} W_{\rm R} &= -\int_{V_{\rm m,1}}^{V_{\rm m,2}} p \mathrm{d}V_{\rm m} = -\int_{V_{\rm m,1}}^{V_{\rm m,2}} \left(\frac{RT}{V_{\rm m} - b} - \frac{a}{V_{\rm m}^2} \right) \mathrm{d}V_{\rm m} \\ &= -RT \ln \frac{V_{\rm m,2} - b}{V_{\rm m,1} - b} - a \left(\frac{1}{V_{\rm m,2}} - \frac{1}{V_{\rm m,1}} \right) \\ &= \left\{ -8.3145 \times \left(27 + 273.15 \right) \times \ln \frac{\left(50/5 \right) - 0.0371}{\left(5/5 \right) - 0.0371} \right. \\ &\left. - 0.423 \times \left[\frac{1}{\left(50/5 \right)} - \frac{1}{\left(5/5 \right)} \right] \times 10^3 \right\} \mathrm{J} \\ &= -5446 \, \mathrm{J} \cdot \mathrm{mol}^{-1} \end{split}$$

对于5 mol NH₃(g)

$$W_{\rm R} = 5 \times (-5446) \,\text{J} = -27.23 \times 10^3 \,\text{J} = -27.23 \,\text{kJ}$$

2. 某一热机的低温热源温度为 40°C, 若高温热源温度为: (1) 100 °C(101325 Pa 下水的沸点); (2) 265°C(5 MPa 下水的沸点); 试分别计算卡诺循环的热机效率。

解: (1)
$$\eta_{R} = \frac{T_{1} - T_{2}}{T_{1}} = \frac{100 - 40}{100 + 273.15} = 0.161 = 16.1\%$$
(2) $\eta_{R} = \frac{265 - 40}{265 + 273.15} = 0.418 = 41.8\%$

3. 某电冰箱内的温度为 0℃,室温为 25℃,今欲使 1000g 温度为 0℃的水变成冰,问最少需做功多少?已知 0℃时冰的熔化焓为 $333.4~\rm J\cdot g^{-1}$ 。

解:
$$W_{R}' = \frac{T_{1} - T_{2}}{T_{2}} Q_{R_{2}}'$$

= $\left[\frac{25 - 0}{0 + 273.15} \times (333.4 \times 1000) \right] J = 30.51 \times 10^{3} J = 30.51 kJ$

4. 某系统与环境的温度均为 300 K,设系统经历了一个恒温不可逆过程,从状态 A 变化到状态 B,对环境做功,W = -4 kJ。已知该过程的不可逆程度为 $\int_A^B (\mathrm{d}Q_\mathrm{R}/T) - \int_A^B (\mathrm{d}Q/T_\mathrm{FF}) = 20\,\mathrm{J}\cdot\mathrm{K}^{-1}$ 。试计算欲使系统复原,环境至少需做多少功。

解:
$$\int_{A}^{B} \frac{dQ_{R}}{T} - \int_{A}^{B} \frac{dQ_{R}}{T_{yx}} = \frac{Q_{R}}{T} - \frac{Q}{T_{yx}} = \frac{Q_{R} - Q}{T} = \frac{(\Delta U - W_{R}) - (\Delta U - W)}{T}$$
$$= \frac{-W_{R} + W}{T} = 20 \text{ J} \cdot \text{K}^{-1}$$
$$-W_{R} + W = (20 \times 300) \text{ J} = 6 \text{ kJ}$$
$$-W_{R} = -W + 6 \text{ kJ} = (4 + 6) \text{ kJ} = 10 \text{ kJ}$$

即环境至少需作功10kJ。

5. 10 A 的电流通过一个 10Ω 的电阻,时间为10 s ,此电阻放在流动的水中而保持在 10 °C 。假设水的数量很大,水温也保持在 10 °C 。求这个电阻的熵变及水的熵变。

解: 电阻
$$\Delta S = 0$$
 水 $\Delta S = \frac{Q_R}{T} = \frac{I^2 R \tau}{T} = \left(\frac{10^2 \times 10 \times 10}{10 + 273.15}\right) J \cdot K^{-1} = 35.32 J \cdot K^{-1}$

6. 10 A 的电流通过一个 10Ω 的电阻,时间为1 s ,此电阻被绝热的物质包住。电阻的初始温度为 $10 \, \text{℃}$,质量为 $10 \, \text{g}$,比热容为 $1 \, \text{J} \cdot \text{K}^{-1} \cdot \text{g}^{-1}$,求电阻的熵变及绝热物质的熵变。

解: 电阻
$$\Delta T = \frac{I^2 R \tau}{cm} = \left(\frac{10^2 \times 10 \times 1}{1 \times 10}\right) \text{K} = 100 \text{ K}$$

$$\Delta S = cm \ln \frac{T_2}{T_1}$$

$$= \left(1 \times 10 \times \ln \frac{110 + 273.15}{10 + 273.15}\right) \text{J} \cdot \text{K}^{-1} = 3.02 \text{ J} \cdot \text{K}^{-1}$$

绝热物质 $\Delta S = 0$

7. 有一反应器,其温度恒定在373 K,环境温度为300 K。反应器向环境散热5000 J。试通过计算判断过程的可逆性。

解:
$$\Delta S = \frac{Q_R}{T} = \left(\frac{-5000}{373}\right) \mathbf{J} \cdot \mathbf{K}^{-1} = -13.4 \, \mathbf{J} \cdot \mathbf{K}^{-1}$$

$$\Delta S_{\mathfrak{F}} = \frac{Q}{T_{\mathfrak{F}}} = \left(\frac{5000}{300}\right) \mathbf{J} \cdot \mathbf{K}^{-1} = 16.7 \, \mathbf{J} \cdot \mathbf{K}^{-1}$$

$$\Delta S_{\mathfrak{G}} = \Delta S + \Delta S_{\mathfrak{F}} = \left(-13.4 + 16.7\right) \mathbf{J} \cdot \mathbf{K}^{-1} = 3.3 \, \mathbf{J} \cdot \mathbf{K}^{-1}$$

$$\therefore \Delta S_{\mathfrak{G}} > 0, \quad \therefore \quad \text{散热过程是一个不可逆过程}.$$

8. 在 0.1 MPa 下,1 mol 气态 NH₃ 由−25 ℃ 变为 0 ℃,试计算此过程中 NH₃ 的 熵 变 。 已 知 NH₃ 的 $C_{p,m}^{\bullet}/(J \cdot K^{-1} \cdot mol^{-1}) = 24.77 + 37.49 \times 10^{-3} (T/K)$ 。若热源的温度为 0 ℃,试判断此过程的可逆性。

解:
$$\Delta S = \int_{T_1}^{T_2} nC_{p,m}^{\Theta} \frac{dT}{T} = \int_{T_1}^{T_2} \left[1 \times \left(24.77 + 37.49 \times 10^{-3} \frac{T}{K} \right) J \cdot K^{-1} \right] \frac{dT}{T}$$

$$= \left\{ 1 \times 24.77 \times \ln \frac{0 + 273.15}{-25 + 273.15} + 1 \times 37.49 \times 10^{-3} \left[0 - \left(-25 \right) \right] \right\} J \cdot K^{-1}$$

$$= 3.315 \,\mathrm{J} \cdot \mathrm{K}^{-1}$$

$$Q = \int_{T_{1}}^{T_{2}} n C_{p,\mathrm{m}}^{\Theta} dT = \int_{T_{1}}^{T_{2}} \left[1 \times \left(24.77 + 37.49 \times 10^{-3} \, \frac{T}{\mathrm{K}} \right) \mathrm{J} \cdot \mathrm{K}^{-1} \right] dT$$

$$= \left[1 \times 24.77 \times \left(273.15 - 248.15 \right) + \frac{1}{2} \times 1 \times 37.49 \times 10^{-3} \right]$$

$$\times \left(273.15^{2} - 248.15^{2} \right) \,\mathrm{J} = 863.6 \,\mathrm{J}$$

$$\frac{Q}{T_{\mathrm{JK}}} = \frac{863.6}{273.15} \,\mathrm{J} \cdot \mathrm{K}^{-1} = 3.162 \,\mathrm{J} \cdot \mathrm{K}^{-1}$$

$$\Delta S - \frac{Q}{T_{\mathrm{JK}}} = \left(3.315 - 3.162 \right) \,\mathrm{J} \cdot \mathrm{K}^{-1} = 0.153 \,\mathrm{J} \cdot \mathrm{K}^{-1} > 0$$

- : 这是一个不可逆过程。
- 9. 证明下列各式:

(1)
$$\left(\frac{\partial U}{\partial T}\right)_p = C_p - p\left(\frac{\partial V}{\partial T}\right)_p;$$
 (2) $\left(\frac{\partial U}{\partial V}\right)_p = C_p\left(\frac{\partial T}{\partial V}\right)_p - p;$

(3)
$$\left(\frac{\partial U}{\partial p}\right)_{V} = C_{V} \left(\frac{\partial T}{\partial p}\right)_{V}$$
; (4) $\left(\frac{\partial H}{\partial V}\right)_{p} = C_{p} \left(\frac{\partial T}{\partial V}\right)_{p}$;

(5)
$$\left(\frac{\partial U}{\partial p}\right)_T = -T\left(\frac{\partial V}{\partial T}\right)_p - p\left(\frac{\partial V}{\partial p}\right)_T$$
;

(6)
$$\left(\frac{\partial H}{\partial V}\right)_T = T \left(\frac{\partial p}{\partial T}\right)_V + V \left(\frac{\partial p}{\partial V}\right)_T$$

$$\widetilde{\mathbf{u}}\mathbf{E} \colon (1) \left(\frac{\partial U}{\partial T} \right)_{p} = \left[\frac{\partial (H - pV)}{\partial T} \right]_{p} = \left(\frac{\partial H}{\partial T} \right)_{p} - p \left(\frac{\partial V}{\partial T} \right)_{p}$$

$$= C_{p} - p \left(\frac{\partial V}{\partial T} \right)$$

(2)
$$\left(\frac{\partial U}{\partial V}\right)_{p} = \left[\frac{\partial (H - pV)}{\partial V}\right]_{p} = \left(\frac{\partial H}{\partial V}\right)_{p} - p$$

$$= \left(\frac{\partial H}{\partial T}\right)_{p} \left(\frac{\partial T}{\partial V}\right)_{p} - p = C_{p} \left(\frac{\partial T}{\partial V}\right)_{p} - p$$

(3)
$$\left(\frac{\partial U}{\partial p}\right)_{V} = \left(\frac{\partial U}{\partial T}\right)_{V} \left(\frac{\partial T}{\partial p}\right)_{V} = C_{V} \left(\frac{\partial T}{\partial p}\right)_{V}$$

(4)
$$\left(\frac{\partial H}{\partial V}\right)_{p} = \left(\frac{\partial H}{\partial T}\right)_{p} \left(\frac{\partial T}{\partial V}\right)_{p} = C_{p} \left(\frac{\partial T}{\partial V}\right)_{p}$$

(5)
$$dU = TdS - pdV$$

$$\left(\frac{\partial U}{\partial p}\right)_{T} = T \left(\frac{\partial S}{\partial p}\right)_{T} - p \left(\frac{\partial V}{\partial p}\right)_{T} = -T \left(\frac{\partial V}{\partial T}\right)_{p} - p \left(\frac{\partial V}{\partial p}\right)_{T};$$

(6)
$$dH = TdS + Vdp$$

$$\left(\frac{\partial H}{\partial V}\right)_{T} = T\left(\frac{\partial S}{\partial V}\right)_{T} + V\left(\frac{\partial p}{\partial V}\right)_{T} = T\left(\frac{\partial p}{\partial T}\right)_{V} + V\left(\frac{\partial p}{\partial V}\right)_{T}$$

10. 证明下列各式:

$$(1) \quad C_p - C_V = \left[\left(\frac{\partial U}{\partial V} \right)_T + p \right] \left(\frac{\partial V}{\partial T} \right)_p; \quad (2) \quad C_p - C_V = T \left(\frac{\partial p}{\partial T} \right)_V \left(\frac{\partial V}{\partial T} \right)_p;$$

(3)
$$C_p - C_V = -\left[\left(\frac{\partial H}{\partial p}\right)_T - V\right]\left(\frac{\partial p}{\partial T}\right)_V;$$

(4)
$$C_p - C_V = \frac{\alpha^2 VT}{\kappa}$$
: 式中 $\alpha = \frac{1}{V} \left(\frac{\partial V}{\partial T} \right)_p$, $\kappa = -\frac{1}{V} \left(\frac{\partial V}{\partial p} \right)_T$.

i.E. (1) $C_p - C_V = \left(\frac{\partial H}{\partial T} \right)_p - \left(\frac{\partial U}{\partial T} \right)_V$

$$= \left(\frac{\partial U}{\partial T} \right)_p + p \left(\frac{\partial V}{\partial T} \right)_p - \left(\frac{\partial U}{\partial T} \right)_V$$

$$dU = \left(\frac{\partial U}{\partial T} \right)_v + V \left(\frac{\partial U}{\partial V} \right)_T \left(\frac{\partial V}{\partial T} \right)_p$$

$$\vdots$$

$$C_p - C_V = \left(\frac{\partial U}{\partial V} \right)_T \left(\frac{\partial V}{\partial T} \right)_p + p \left(\frac{\partial V}{\partial T} \right)_p$$

$$= \left[\left(\frac{\partial U}{\partial V} \right)_T + p \right] \left(\frac{\partial V}{\partial T} \right)_p$$

$$= \left[\left(\frac{\partial U}{\partial V} \right)_T + p \right] \left(\frac{\partial V}{\partial T} \right)_p$$
(2) 以\left(\frac{\partial U}{\partial V} \right)_p - p \partial \text{\tau}(1) \right) \frac{\partial V}{\partial T} \right)_p
$$C_p - C_V = T \left(\frac{\partial P}{\partial T} \right)_V \left(\frac{\partial V}{\partial T} \right)_p$$
(3) $C_p - C_V = \left(\frac{\partial H}{\partial T} \right)_p - \left(\frac{\partial U}{\partial T} \right)_V$

$$= \left(\frac{\partial H}{\partial T} \right)_p - \left(\frac{\partial H}{\partial T} \right)_V + V \left(\frac{\partial P}{\partial T} \right)_V$$

$$dH = \left(\frac{\partial H}{\partial T} \right)_p dT + \left(\frac{\partial H}{\partial P} \right)_T dP$$

$$\left(\frac{\partial H}{\partial T} \right)_V = \left(\frac{\partial H}{\partial T} \right)_v + \left(\frac{\partial H}{\partial P} \right)_T \left(\frac{\partial P}{\partial T} \right)_V$$

$$C_{p} - C_{V} = -\left(\frac{\partial H}{\partial p}\right)_{T} \left(\frac{\partial p}{\partial T}\right)_{V} + V\left(\frac{\partial p}{\partial T}\right)_{V}$$

$$= -\left[\left(\frac{\partial H}{\partial p}\right)_{T} - V\right] \left(\frac{\partial p}{\partial T}\right)_{V}$$

$$(4) \quad \boxplus \left(\frac{\partial p}{\partial T}\right)_{V} \left(\frac{\partial T}{\partial V}\right)_{p} \left(\frac{\partial V}{\partial p}\right)_{T} = -1, \quad \rightleftarrows$$

$$\left(\frac{\partial p}{\partial T}\right)_{V} = -\frac{\left(\frac{\partial V}{\partial T}\right)_{p}}{\left(\frac{\partial V}{\partial p}\right)_{T}}$$

以此代入(2)的结果,得

$$C_{p} - C_{V} = T \left[-\frac{\left(\frac{\partial V}{\partial T}\right)_{p}}{\left(\frac{\partial V}{\partial p}\right)_{T}} \right] \left(\frac{\partial V}{\partial T}\right)_{p} = T \frac{\left[\left(\frac{\partial V}{\partial T}\right)_{p}\right]^{2}}{\left[-\left(\frac{\partial V}{\partial p}\right)_{T}\right]}$$

$$= T \frac{\left[\frac{1}{V}\left(\frac{\partial V}{\partial T}\right)_{p}\right]^{2} V}{\left[-\frac{1}{V}\left(\frac{\partial V}{\partial p}\right)_{T}\right]} = T \frac{\alpha^{2}V}{\kappa} = \frac{\alpha^{2}VT}{\kappa}$$

11. 某实际气体的状态方程为 $pV_m = RT + \alpha p$, 其中 α 是常数。 1 mol 该气体在恒定的温度 T 下,经可逆过程由 p_1 变到 p_2 。试用 T 、 p_1 、 p_2 表示过程的 W 、 Q 、 ΔU 、 ΔH 、 ΔS 、 ΔA ΔG 。

解:
$$p = \frac{RT}{V_{\text{m}} - \alpha}$$

$$W = W_{\text{R}} = -\int_{V_{\text{ml}}}^{V_{\text{m2}}} p dV_{\text{m}} = \int_{V_{\text{m2}}}^{V_{\text{ml}}} \frac{RT}{V_{\text{m}} - \alpha} dV_{\text{m}}$$

$$= RT \ln \frac{V_{\text{m_1}} - \alpha}{V_{\text{m_2}} - \alpha} = RT \ln \frac{p_2}{p_1}$$

$$dU_{\text{m}} = T dS_{\text{m}} - p dV_{\text{m}}$$

$$\left(\frac{\partial U_{\mathrm{m}}}{\partial V_{\mathrm{m}}}\right)_{T} = T\left(\frac{\partial S_{\mathrm{m}}}{\partial V_{\mathrm{m}}}\right)_{T} - p = T\left(\frac{\partial p}{\partial T}\right)_{V_{\mathrm{m}}} - \frac{RT}{V_{\mathrm{m}} - \alpha}$$

$$= T \cdot \frac{R}{V_{\mathrm{m}} - \alpha} - \frac{RT}{V_{\mathrm{m}} - \alpha} = 0$$

$$\therefore dU_{\mathrm{m}} = 0, \quad \mathbb{R} \square \Delta U = 0$$

$$Q = \Delta U - W = 0 - RT \ln \frac{p_{2}}{p_{1}} = RT \ln \frac{p_{1}}{p_{2}}$$

$$\Delta S = \frac{Q_{\mathrm{R}}}{T} = R \ln \frac{p_{1}}{p_{2}}$$

$$\Delta H = \Delta U + \Delta (pV) = 0 + (p_{2}V_{\mathrm{m},2} - p_{1}V_{\mathrm{m},1})$$

$$= (RT + \alpha p_{2}) - (RT + \alpha p_{1}) = \alpha (p_{2} - p_{1})$$

$$\Delta A = W_{\mathrm{R}} = RT \ln \frac{p_{2}}{p_{1}}$$

$$\Delta G = \Delta A + \Delta (pV) = RT \ln \frac{p_{2}}{p_{1}} + \alpha (p_{2} - p_{1})$$

12. 200 K 时,固态 Hg 的 α = 1.43×10⁻⁴ K⁻¹, κ = 3.44×10⁻¹¹ Pa⁻¹,摩 尔 体 积 为 14.14 cm³·mol⁻¹, $C_{p,m}$ = 27.11 J·K⁻¹·mol⁻¹。 试 利 用 式 $C_{p,m}$ – $C_{V,m}$ = $\alpha^2 V_m T / \kappa$ 求 200K 时 固态 Hg 的 $C_{V,m}$ 。

解:
$$C_{p,m} - C_{V,m} = \frac{\alpha^2 V_m T}{\kappa}$$

$$= \left[\frac{\left(1.43 \times 10^{-4} \right)^2 \times \left(14.14 \times 10^{-6} \right) \times 200}{3.44 \times 10^{-11}} \right] J \cdot K^{-1} \cdot \text{mol}^{-1}$$

$$= 1.68 J \cdot K^{-1} \cdot \text{mol}^{-1}$$

$$\therefore C_{V,m} = \left(27.11 - 1.68 \right) J \cdot K^{-1} \cdot \text{mol}^{-1} = 25.43 J \cdot K^{-1} \cdot \text{mol}^{-1}$$

13. 试证明对1 mol 理想气体,无论进行可逆过程或不可逆过程,都有:

$$\begin{split} \Delta S &= C_{V,\mathrm{m}}^{\,\mathrm{e}} \ln\!\left(\frac{T_2}{T_1}\right) + R \ln\!\left(\frac{V_2}{V_1}\right) = C_{p,\mathrm{m}}^{\,\mathrm{e}} \ln\!\left(\frac{T_2}{T_1}\right) + R \ln\!\left(\frac{p_1}{p_2}\right) \\ &= C_{p,\mathrm{m}}^{\,\mathrm{e}} \ln\!\left(\frac{V_2}{V_1}\right) + C_{V,\mathrm{m}}^{\,\mathrm{e}} \ln\!\left(\frac{p_2}{p_1}\right) \end{split}$$

证:因为熵是状态函数,故熵变只决定于初、终状态而与过程的可 逆与否无关。设想由初态开始先进行恒压可逆的加热或冷却过程使温度 变为终态的,然后进行恒温可逆的膨胀或压缩过程使压力变为终态的, 于是

$$\begin{split} \Delta S &= \Delta S_1 + \Delta S_2 = C_{p,\text{m}}^{\text{e}} \ln \frac{T_2}{T_1} + R \ln \frac{p_1}{p_2} \\ & \text{pr} \quad \Delta S = C_{p,\text{m}}^{\text{e}} \ln \frac{T_2}{T_1} + R \ln \frac{T_1/V_1}{T_2/V_2} = C_{V,\text{m}}^{\text{e}} \ln \frac{T_2}{T_1} + R \ln \frac{V_2}{V_1} \\ & \text{pr} \quad \Delta S = C_{p,\text{m}}^{\text{e}} \ln \frac{p_2 V_2}{p_1 V_1} + R \ln \frac{p_1}{p_2} = C_{p,\text{m}}^{\text{e}} \ln \frac{V_2}{V_1} + C_{V,\text{m}}^{\text{e}} \ln \frac{p_2}{p_1} \end{split}$$

14. 12 g O_2 从 $20 \degree$ 被冷却到– $40 \degree$,同时压力从 0.1 MPa 变为 6 MPa ,求其熵变。设 O_2 可作为理想气体, $C_{p,m}^{\bullet} = 29.16 \text{ J · K}^{-1} \cdot \text{mol}^{-1}$ 。

解:
$$\Delta S = n \left(C_{p,m}^{\Theta} \ln \frac{T_2}{T_1} + R \ln \frac{p_1}{p_2} \right)$$

$$= \left[\frac{12}{32.00} \times \left(29.16 \times \ln \frac{-40 + 273.15}{20 + 273.15} + 8.3145 \times \ln \frac{0.1}{6} \right) \right] \mathbf{J} \cdot \mathbf{K}^{-1}$$

$$= -15.27 \,\mathbf{J} \cdot \mathbf{K}^{-1}$$

15. 把 1 mol He 在 127 \mathbb{C} 和 0.5 MPa 下恒温压缩至1 MPa,试求其 Q、W、 ΔU 、 ΔH 、 ΔS 、 ΔA 、 ΔG 。He 可作为理想气体。(1) 设为可逆过程;(2) 设压缩时外压自始至终为1 MPa。

解: (1)
$$\Delta U = 0$$
, $\Delta H = 0$
 $W = -nRT \ln \frac{p_1}{p_2} = \left[-1 \times 8.3145 \times (127 + 273.15) \times \ln \frac{0.5}{1} \right] J$
 $= 2306 J$
 $Q = \Delta U - W = -2306 J$
 $\Delta S = nR \ln \frac{p_1}{p_2} = \left(1 \times 8.3145 \times \ln \frac{0.5}{1} \right) J \cdot K^{-1} = -5.763 J \cdot K^{-1}$
 $\Delta A = W_R = 2306 J$
(2) $\Delta U \times \Delta H \times \Delta S \times \Delta A \times \Delta G$ 同 (1)
 $W = -p_{\frac{1}{2}} \Delta V = -p_2 \left(\frac{nRT}{p_2} - \frac{nRT}{p_1} \right) = -nRT \left(1 - \frac{p_2}{p_1} \right)$
 $= \left[-1 \times 8.3145 \times (127 + 273.15) \times \left(1 - \frac{1}{0.5} \right) \right] J = 3327 J$
 $Q = \Delta U - W = -3327 J$

16. 0° 、0.5 MPa 的 $N_2(g)$ 2 dm³,在外压为0.1 MPa 下恒温膨胀,直至氮气的压力等于0.1 MPa,求过程的Q、W、 ΔU 、 ΔH 、 ΔS 、 ΔG 和 ΔA 。假设氮气服从理想气体状态方程。

解:
$$\Delta U = 0$$
, $\Delta H = 0$
 $V_2 = \frac{p_1}{p_2} V_1 = \frac{0.5}{0.1} \times 2 \text{ dm}^3 = 10 \text{ dm}^3$
 $W = -p_{\%} \Delta V = \left[-\left(0.1 \times 10^6\right) \times \left(10 - 2\right) \times 10^{-3} \right] \text{J} = -800 \text{ J}$
 $Q = \Delta U - W = -W = 800 \text{ J}$
 $\Delta S = nR \ln \left(\frac{p_1}{p_2}\right) = \frac{p_1 V_1}{T_1} \ln \left(\frac{p_1}{p_2}\right)$
 $= \left[\frac{0.5 \times 10^6 \times 2 \times 10^{-3}}{273.15} \times \ln \left(\frac{0.5}{0.1}\right)\right] \text{J} \cdot \text{K}^{-1}$
 $= 5.892 \text{ J} \cdot \text{K}^{-1}$
 $\Delta G = \Delta H - T\Delta S = 0 - 273.15 \times 5.892 \text{ J} = -1609 \text{ J} = -1.609 \text{ kJ}$
 $\Delta A = \Delta G = -1.609 \text{ kJ}$

17. $1 \mod H_2(g)$ 在 25 \mathbb{C} 和 $0.1 \mod Pa$ 下可逆绝热压缩至体积为 $5 \mod^3$,试求终态温度、压力及过程的 Q 、W 、 ΔU 、 ΔH 、 ΔS 。假设氢气为理想气体, $C_{V,m}^{\rm e}=(5/2)R$ 。

解:
$$\gamma = \frac{C_{p,m}^{e}}{C_{v,m}^{e}} = \frac{(7/2)R}{(5/2)R} = 1.4$$

$$V_{1} = \frac{nRT_{1}}{p_{1}} = \left[\frac{1 \times 8.3145 \times (25 + 273.15)}{0.1 \times 10^{6}}\right] \text{m}^{3}$$

$$= 24.79 \times 10^{-3} \text{ m}^{3} = 24.79 \text{ dm}^{3}$$

$$p_{2} = \left(\frac{V_{1}}{V_{2}}\right)^{\gamma} p_{1} = \left(\frac{24.79}{5}\right)^{1.4} \times 0.1 \text{ MPa}$$

$$= 0.941 \text{ MPa}$$

$$T_{2} = \frac{p_{2}V_{2}}{nR} = \left[\frac{\left(0.941 \times 10^{6}\right) \times \left(5 \times 10^{-3}\right)}{1 \times 8.3145}\right] \text{K} = 565.9 \text{ K}$$

$$\Delta U = nC_{v,m}^{e} \Delta T = \left[1 \times \frac{5}{2} \times 8.3145 \times \left(565.9 - 298.15\right)\right] \text{J} = 5566 \text{ J}$$

$$\Delta H = nC_{p,m}^{e} \Delta T = \left[1 \times \frac{7}{2} \times 8.3145 \times \left(565.9 - 298.15\right)\right] \text{J} = 7792 \text{ J}$$

$$Q = 0$$

$$W = \Delta U = 5566 \text{ J}$$

$$\Delta S = \int \frac{dQ_R}{T} = 0$$

18. $1 \, \text{mol} \, 0^\circ \mathbb{C}$ 、0.2 MPa 的理想气体沿着 p/V=常数的可逆途径到达压力为 0.4 MPa 的终态。已知 $C^\circ_{V,m}=(5/2)R$,求过程的 Q 、W 、 ΔU 、 ΔH 、 ΔS 。

解:
$$V_1 = \frac{nRT_1}{p_1} = \left(\frac{1 \times 8.3145 \times 273.15}{0.2 \times 10^6}\right) \text{m}^3$$

 $= 11.35 \times 10^{-3} \text{ m}^3 = 11.35 \text{ dm}^3$
 $\frac{p_2}{V_2} = \frac{p_1}{V_1}$
 $\therefore V_2 = \frac{p_2}{p_1} V_1 = \frac{0.4}{0.2} \times 11.35 \text{ dm}^3 = 22.70 \text{ dm}^3$
 $T_2 = \frac{p_2 V_2}{nR} = \left[\frac{\left(0.4 \times 10^6\right) \times \left(22.70 \times 10^{-3}\right)}{1 \times 8.3145}\right] \text{K} = 1092 \text{ K}$
 $W = -\int_{V_1}^{V_2} p dV = -\int_{V_1}^{V_2} \left(\frac{p_1}{V_1}V\right) dV = -\frac{p_1}{V_1} \cdot \frac{1}{2} \left(V_2^2 - V_1^2\right)$
 $= -\frac{1}{2} \left(p_2 V_2 - p_1 V_1\right)$
 $= \left[-\frac{1}{2} \times \left(0.4 \times 22.70 - 0.2 \times 11.35\right) \times 10^3\right] \text{J}$
 $= -3.405 \text{ kJ}$
 $\Delta U = nC_{V,m}^{\circ} \Delta T = \left[1 \times \frac{5}{2} \times 8.3145 \times \left(1092 - 273\right)\right] \text{J}$
 $= 17.02 \times 10^3 \text{ J} = 17.02 \text{ kJ}$
 $\Delta H = nC_{p,m}^{\circ} \Delta T = \left[1 \times \frac{7}{2} \times 8.3145 \times \left(1092 - 273\right)\right] \text{J}$
 $= 23.83 \times 10^3 \text{ J} = 23.83 \text{ kJ}$
 $Q = \Delta U - W = \left[17.02 - \left(-3.405\right)\right] \text{kJ} = 20.43 \text{ kJ}$

$$\Delta S = n \left(C_{p,m}^{\bullet} \ln \frac{T_2}{T_1} + R \ln \frac{p_1}{p_2} \right)$$

$$= 1 \times \left[\left(\frac{5}{2} + 1 \right) \times 8.3145 \times \ln \frac{1092}{273.15} + 8.3145 \times \ln \frac{0.2}{0.4} \right] \mathbf{J} \cdot \mathbf{K}^{-1}$$

$$= 34.56 \, \mathbf{J} \cdot \mathbf{K}^{-1}$$

- 19. 计算下列各恒温过程的熵变(气体为理想气体):
- (1) 1 mol体积为 $V \text{ 的 } N_2 = 1 \text{ mol }$ 体积为V 的 Ar混合,成为体积为2V 的混合气体:
- (2) 1 mol体积为 $V \text{ 的 } N_2 = 1 \text{ mol }$ 体积为V 的 Ar混合,成为体积为V 的混合气体:
- (3) 1 mol体积为 $V \text{ 的 } N_2 = 1 \text{ mol }$ 体积为 $V \text{ 的 } N_2 = 1 \text{ mol }$ 体积为 $V \text{ op } N_2 = 1 \text{ mol }$ 体积为 $V \text{ op } N_2 = 1 \text{ mol }$
- (4) 1 mol体积为 $V \text{ 的 } N_2 = 1 \text{ mol }$ 体积为 $V \text{ 的 } N_2 = 1 \text{ mol }$ 体积为 $V \text{ 的 } N_2 = 1 \text{ mol }$

解: (1)
$$\Delta S = n_1 R \ln 2 + n_2 R \ln 2 = (2 \times 8.3145 \times \ln 2) \text{J} \cdot \text{K}^{-1}$$

= 11.53 J·K⁻¹

- (2) $\Delta S = 0$
- (3) $\Delta S = 0$

(4)
$$\Delta S = nR \ln \frac{p_1}{p_2} = \left(2 \times 8.3145 \times \ln \frac{1}{2}\right) \mathbf{J} \cdot \mathbf{K}^{-1} = -11.53 \,\mathbf{J} \cdot \mathbf{K}^{-1}$$

20. 一绝热容器被隔板分成体积相等的两部分,左边有 $1 \mod 10$ \mathbb{C} 的 \mathbb{O}_2 ,右边有 $1 \mod 20$ \mathbb{C} 的 \mathbb{H}_2 。设两种气体均可当作理想气体, $C_{p,m}^{\text{e}} = (7/2)R$ 。求两边温度相等时总的熵变。若将隔板抽去,求总的熵变。

解:两边温度相等后,
$$Q=0$$
, $W=0$

$$\begin{split} & \therefore \quad \Delta U = 0 \\ & \Delta U = \Delta U_1 + \Delta U_2 = n_1 C_{V,m}^{\circ} \left(T - T_1 \right) + n_2 C_{V,m}^{\circ} \left(T - T_2 \right) = 0 \\ & T = \frac{1}{2} \left(T_1 + T_2 \right) = \frac{1}{2} \times \left[\left(10 + 273.15 \right) + \left(20 + 273.15 \right) \right] \text{K} = 288.15 \text{ K} \\ & \Delta S = \Delta S_1 + \Delta S_2 = n_1 C_{V,m}^{\circ} \ln \frac{T}{T_1} + n_2 C_{V,m}^{\circ} \ln \frac{T}{T_2} \\ & = \left[1 \times \left(\frac{5}{2} \times 8.3145 \right) \times \ln \frac{288.15}{283.15} + 1 \times \left(\frac{5}{2} \times 8.3145 \right) \times \ln \frac{288.15}{293.15} \right] \text{J} \cdot \text{K}^{-1} \end{split}$$

 $= 0.0063 \, J \cdot K^{-1}$

抽去隔板后,两气体在恒温下混合,每一种气体的分压均变为原来压力的一半

$$\Delta S = n_1 R \ln 2 + n_2 R \ln 2 = (n_1 + n_2) R \ln 2 = (2 \times 8.3145 \times \ln 2) \text{ J} \cdot \text{K}^{-1}$$
$$= 11.53 \text{ J} \cdot \text{K}^{-1}$$

故总的熵变为 (0.0063+11.53) J·K⁻¹ = 11.54 J·K⁻¹

21. 以旋塞隔开而体积相等的两个玻璃球,分别贮有 $1 \mod O_2$ 和 $1 \mod N_2$,温度均为 $25 \mathbb{C}$,压力均为 $0.1 \operatorname{MPa}$ 。在绝热条件下,打开旋塞使两种气体混合。取两种气体为系统,试求混合过程的 $Q \setminus W \setminus \Delta U \setminus \Delta H \setminus \Delta S \setminus \Delta A \setminus \Delta G$ 。(设 O,和 N,均为理想气体)

解:因为绝热,故
$$Q=0$$

因为系统的体积不变,故W=0

则
$$\Delta U = Q + W = 0$$

而
$$\Delta U = nC_{V_m}^{\Theta} \Delta T$$
, 故 $\Delta T = 0$

于是
$$\Delta H = nC_{p,m}^{\Theta} \Delta T = 0$$

两种气体的压力都从0.1 MPa 变为0.05 MPa

$$\Delta S = \Delta S_1 + \Delta S_2 = n_1 R \ln 2 + n_2 R \ln 2 = (n_1 + n_2) R \ln 2$$

$$= (2 \times 8.3145 \times \ln 2) J \cdot K^{-1} = 11.53 J \cdot K^{-1}$$

$$\Delta A = \Delta U - T \Delta S = [0 - (25 + 273.15) \times 11.53] J = -3438 J$$

$$\Delta G = \Delta A = -3438 J$$

22. 1 mol CO₂ 自 20℃、0.3040 MPa、7878 cm³ 反抗恒定的 0.101325 MPa 外压恒温膨胀至 0.101325 Pa 、23920 cm³。试求此过程的 Q 、W 、 ΔU 、 ΔH 。已知 CO₂ 在 20℃、0.3040 MPa 下节流膨胀至 0.101325 MPa 时 的 温 度 为 17.72 ℃; 在 0.101325 MPa 下 及 20 ℃ 附 近 其 $C_{p,m}$ = 37.07 J·K⁻¹·mol⁻¹。

解:
$$W = -p_{\text{sh}}\Delta V$$

 $= \left[-\left(0.101325 \times 10^{6}\right) \times \left(23920 - 7878\right) \times 10^{-6}\right] J = -1625 J$
 $\Delta H = \Delta H_{1} + \Delta H_{2} = 0 + nC_{p,m}\Delta T$
 $= \left[1 \times 37.07 \times \left(20 - 17.72\right)\right] J = 84.5 J$
 $\Delta U = \Delta H - \Delta (pV)$
 $= \left[84.5 - \left(0.101325 \times 23920 - 0.3040 \times 7878\right)\right] J = 55.7 J$
 $Q = \Delta U - W = \left[55.7 - \left(-1625\right)\right] J = 1681 J$

23. 2 mol 液态 O_2 在正常沸点(−182.97 $^{\circ}$ C)时蒸发成为101325 Pa 的气体,求其熵变。已知此时液态 O_2 的摩尔蒸发焓为 $6.820~{\rm kJ\cdot mol^{-1}}$ 。

解:
$$\Delta S = \frac{\Delta H}{T} = \left(\frac{2 \times 6.820 \times 10^3}{-182.97 + 273.15}\right) \text{ J} \cdot \text{K}^{-1} = 151.3 \text{ J} \cdot \text{K}^{-1}$$

24. $100 \,\mathrm{g}\ 10\,^{\circ}$ 的水与 $200 \,\mathrm{g}\ 40\,^{\circ}$ 的水在绝热条件下混合,求此过程的熵变。已知水的比热容为 $4.184\,\mathrm{J\cdot K^{-1}\cdot g^{-1}}$ 。

解: 绝热条件下混合,
$$\Delta H = Q_p = 0$$

$$\Delta H = \Delta H_1 + \Delta H_2 = cm_1(t - t_1) + cm_2(t - t_2) = 0$$

$$t = \frac{m_1 t_1 + m_2 t_2}{m_1 + m_2} = \left(\frac{100 \times 10 + 200 \times 40}{100 + 200}\right) \text{ $^{\circ}$C} = 30 \text{ $^{\circ}$C}$$

$$\Delta S = \Delta S_1 + \Delta S_2 = cm_1 \ln \frac{T}{T_1} + cm_2 \ln \frac{T}{T_2}$$

$$= \left(4.184 \times 100 \times \ln \frac{30 + 273.15}{10 + 273.15} + 4.184 \times 200 \times \ln \frac{30 + 273.15}{40 + 273.15}\right) \text{J} \cdot \text{K}^{-1}$$

$$= 1.40 \text{J} \cdot \text{K}^{-1}$$

25. 在一个绝热的容器中有1000 g 25℃的水,投入150 g 0℃的冰,计算总的熵变。已知冰的熔化焓为333.4 $J \cdot g^{-1}$,水的比热容为4.184 $J \cdot K^{-1} \cdot g^{-1}$ 。

解: 绝热过程,
$$\Delta H = Q_p = 0$$

$$\Delta H = \Delta H_1 + \Delta H_2 = cm_1(t-t_1) + m_2 \Delta_{\text{fus}} H + cm_2(t-t_2)$$

$$= \left[4.184 \times 1000 \left(\frac{t}{^{\circ}\text{C}} - 25 \right) + 150 \times 333.4 + 4.184 \times 150 \times \left(\frac{t}{^{\circ}\text{C}} - 0 \right) \right] J$$

$$= 0$$

$$t = 11.34 \, ^{\circ}\text{C}$$

$$\Delta S_1 = cm_1 \ln \frac{T}{T_1} = \left(4.184 \times 1000 \times \ln \frac{11.34 + 273.15}{25 + 273.15} \right) J \cdot K^{-1}$$

$$= -196.2J \cdot K^{-1}$$

$$\Delta S_2 = m_2 \frac{\Delta_{\text{fus}} H}{T_2} + cm_2 \ln \frac{T}{T_2}$$

$$= \left(150 \times \frac{333.4}{0 + 273.15} + 4.184 \times 150 \times \ln \frac{11.34 + 273.15}{0 + 273.15} \right) J \cdot K^{-1}$$

$$= 208.6 \, J \cdot K^{-1}$$

$$\Delta S = \Delta S_1 + \Delta S_2 = (-196.2 + 208.6) \text{ J} \cdot \text{K}^{-1} = 12.4 \text{ J} \cdot \text{K}^{-1}$$

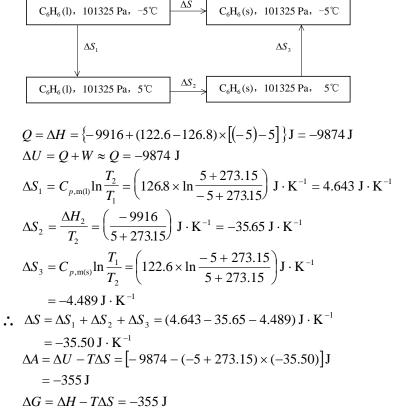
26. $1 \text{ mol } \mathbf{C}_6\mathbf{H}_5\mathbf{CH}_3$ 在其正常沸点 110.6 \mathbb{C} 时蒸发为101325 Pa 的气体,求该过程的 Q 、 W 、 ΔU 、 ΔH 、 ΔS 、 ΔA 、 ΔG 。已知在该温度下 $\mathbf{C}_6\mathbf{H}_5\mathbf{CH}_3$ 的摩尔蒸发焓为33.38 kJ·mol⁻¹。与蒸气相比较,液体的体积可略去,蒸气可作为理想气体。(1) 设外压为101325 Pa;(2) 设外压为10132.5 Pa。

解: (1)
$$W = -p_{\frac{1}{2}}\Delta V = -p[V(g) - V(1)] \approx -pV(g) \approx -nRT$$

 $= [-1 \times 8.3145 \times (110.6 + 273.15)] J$
 $= -3190 J = -3.190 kJ$
 $Q = \Delta H = 33.38 kJ$
 $\Delta U = Q + W = (33.38 - 3.190) kJ = 30.19 kJ$
 $\Delta S = \frac{\Delta H}{T} = \left(\frac{33.38 \times 10^3}{110.6 + 273.15}\right) J \cdot K^{-1} = 87.0 J \cdot K^{-1}$
 $\Delta A = W_R = -3.190 kJ$
 $\Delta G = 0$
(2) $\Delta U \times \Delta H \times \Delta S \times \Delta A \times \Delta G = 10$
 $W = -p_{\frac{1}{2}}\Delta V \approx -p_{\frac{1}{2}}V(g) \approx -p_{\frac{1}{2}} \cdot \frac{nRT}{p} = -\frac{p_{\frac{1}{2}}}{p} \cdot nRT$
 $= \left[-\frac{10132.5}{101325} \times 1 \times 8.3145 \times (110.6 + 273.15)\right] J$
 $= -319 J = -0.319 kJ$
 $Q = \Delta U - W = [30.19 - (-.0319)] kJ = 30.51 kJ$

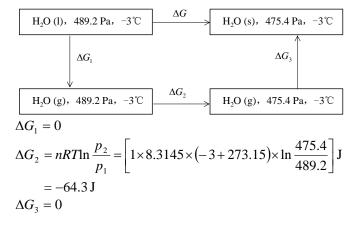
27. C_6H_6 的正常熔点为 5℃,摩尔熔化焓为 9916 J·mol⁻¹, $C_{p,m(l)}=126.8$ J·K⁻¹·mol⁻¹, $C_{p,m(s)}=122.6$ J·K⁻¹·mol⁻¹。求 101325 Pa 下 1 mol −5℃的过冷 C_6H_6 凝固成−5℃的固态 C_6H_6 的Q、 ΔU 、 ΔH 、 ΔS 、 ΔA 、 ΔG 。设凝固过程的体积功可略去不计。

解:



28. 在-3℃时,冰的蒸气压为 475.4 Pa,过冷水的蒸气压为 489.2 Pa。试求在-3℃时1 mol 过冷H,O 转变为冰的ΔG。

解:

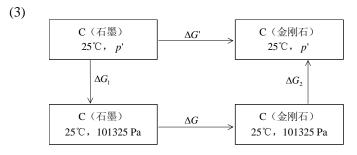


$$\Delta G = \Delta G_1 + \Delta G_2 + \Delta G_3 = 0 - 64.3 \text{J} + 0 = -64.3 \text{ J}$$

29. 25° 、101325 Pa 时,石墨转变为金刚石的 $\Delta H = 1895$ J·mol⁻¹, $\Delta S = -3.363$ J·K⁻¹·mol⁻¹。石墨的密度为 2.260 g·cm⁻³,金刚石的密度为 3.513 g·cm⁻³。(1) 求 25° 、101325 Pa 下石墨转变为金刚石的 ΔG ; (2) 在这种情况下,哪一种晶型比较稳定?(3) 增加压力能否使原来不稳定的晶型成为稳定的晶型?如果可能,所需的压力是多少?假设密度不随压力而变。

解: (1) $\Delta G = \Delta H - T\Delta S = [1895 - (25 + 273.15) \times (-3.363)]$ J = 2898 J

(2) $\Delta G > 0$,表示石墨不可能转变成金刚石,即石墨是稳定的。



设 25℃, 压力为 p' 时石墨与金刚石正好能平衡共存, 则 $\Delta G' = 0$

$$\Delta G_1 = \int_{p'}^{p} V_1 d \ p \approx V_1(p - p')$$

$$\Delta G_2 = \int_{p}^{p'} V_2 d \ p \approx V_2(p' - p)$$

$$\Delta G' = \Delta G_1 + \Delta G + \Delta G_2$$

$$\mathbb{E} I \quad 0 = V_1(p - p') + \Delta G + V_2(p' - p) = (V_2 - V_1)(p' - p) + \Delta G$$

$$p' - p = -\frac{\Delta G}{V_2 - V_1} = -\frac{\Delta G}{M[(1/\rho_2) - (1/\rho_1)]}$$

$$= \left\{ -\frac{2898}{12.011 \times 10^{-3} \times [(1/3.515) - (1/2.260)] \times 10^{-3}} \right\} \text{Pa}$$

$$= 1527 \times 10^6 \text{ Pa} = 1527 \text{ MPa}$$

\therefore $p \approx 1527 \text{ MPa}$

30. 将 1 mol Hg(l) 在 25 ℃ 的恒定温度下,从 0.1 MPa 压缩至 10 MPa,试求其状态变化的 ΔS 和 ΔG 。已知 25 ℃时 Hg(l) 的密度为 13.534 g·cm⁻³,密度随压力的变化可以略去, Hg(l) 的体积膨胀系数 $\alpha = 1.82 \times 10^{-4} \, \mathrm{K}^{-1}$, Hg 的摩尔质量为 200.61 g·mol⁻¹。

解:
$$\Delta G = \int_{p_1}^{p_2} V dp = V(p_2 - p_1) = \frac{nM}{\rho} (p_2 - p_1)$$

$$= \left[\left(\frac{1 \times 200.61}{13.534} \times 10^{-6} \right) \times (10 - 0.1) \times 10^6 \right] J = 146.7 J$$

$$\Delta S = \int_{p_1}^{p_2} \left(\frac{\partial S}{\partial p} \right)_T dp = -\int_{p_1}^{p_2} \left(\frac{\partial V}{\partial T} \right)_p dp = -\int_{p_1}^{p_2} \alpha V dp$$

$$= -\alpha V(p_2 - p_1)$$

$$= \left[-1.82 \times 10^{-4} \times \left(\frac{1 \times 200.61}{13.534} \times 10^{-6} \right) \times (10 - 0.1) \times 10^6 \right] J \cdot K^{-1}$$

$$= -0.0267 J \cdot K^{-1}$$

31. 70℃时四氯化碳的蒸气压为82.81 kPa,80℃时为112.43 kPa。 试计算四氯化碳的摩尔蒸发焓及正常沸点。设四氯化碳的摩尔蒸发焓不 随温度而变化。

解:
$$\Delta_{\text{vap}} H_{\text{m}} = \frac{RT_2T_1}{T_2 - T_1} \ln \frac{p^*(T_2)}{p^*(T_1)}$$

$$= \left[\frac{8.3145 \times (80 + 273.15) \times (70 + 273.15)}{80 - 70} \times \ln \frac{112.43}{82.81} \right] \text{J} \cdot \text{mol}^{-1}$$

$$= 30.81 \times 10^3 \text{J} \cdot \text{mol}^{-1} = 30.81 \text{ kJ} \cdot \text{mol}^{-1}$$

$$\frac{1}{T_2} = \frac{1}{T_1} - \frac{R}{\Delta H} \ln \frac{p^*(T_2)}{p^*(T_1)}$$

$$= \left[\frac{1}{70 + 273.15} - \frac{8.3145}{30.81 \times 10^3} \times \ln \frac{101.325}{82.81} \right] \text{K}^{-1}$$

$$= 2.8597 \times 10^{-3} \text{K}^{-1}$$

$$\therefore T_2 = 349.69 \text{ K}, t_2 = 76.54 \, ^{\circ}\text{C}$$

32. 卫生部门规定汞蒸气在1 m³ 空气中的最高允许含量为0.01 mg。已知汞在 20℃的饱和蒸气压为0.160 Pa,摩尔蒸发焓为60.7 kJ·mol⁻¹。若在30℃时汞蒸气在空气中达到饱和,问此时空气中汞的含量是最高允许含量的多少倍。已知汞蒸气是单原子分子。

解:
$$\ln \frac{p^*(T_2)}{p^*(T_1)} = \frac{\Delta_{\text{vap}} H_{\text{m}}}{R} \cdot \frac{T_2 - T_1}{T_2 T_1}$$

$$= \frac{60.7 \times 10^3}{8.3145} \times \frac{30 - 20}{(30 + 273.15) \times (20 + 273.15)} = 0.821$$

$$\frac{p^*(T_2)}{p^*(T_1)} = 2.27 , \quad p^*(T_2) = 2.27 \times 0.160 \,\text{Pa} = 0.363 \,\text{Pa}$$

$$m = nM = \frac{pV}{RT} M = \left[\frac{0.363 \times 1}{8.3145 \times (30 + 273.15)} \times 200.6 \right] \text{g}$$

$$= 28.9 \times 10^{-3} \,\text{g} = 28.9 \,\text{mg}$$

- ∴ 空气中汞的含量是最高允许含量的28.9/0.01 = 2.89×10³ 倍。
- 33. 萘在其正常熔点 80° ℃时的熔化焓为 $150.6\,\mathrm{J\cdot g^{-1}}$ 。已知固态萘及液态萘的密度分别为1.145与 $0.981\,\mathrm{g\cdot cm^{-3}}$,试计算压力增加 $0.1\,\mathrm{MPa}$ 后熔点的变化。

解:对1g萘,由固态变为液态

$$\begin{split} & \Delta_{\text{fus}} V = V(1) - V(s) = \frac{1}{\rho(1)} - \frac{1}{\rho(s)} = \frac{\rho(s) - \rho(1)}{\rho(1)\rho(s)} \\ & \frac{\text{d}T}{\text{d}p} = \frac{T\Delta_{\text{fus}}V}{\Delta_{\text{fus}}H} = \frac{T}{\Delta_{\text{fus}}H} \cdot \frac{\rho(s) - \rho(1)}{\rho(1)\rho(s)} \\ & = \left[\frac{80.0 + 273.15}{150.6} \times \left(\frac{1.145 - 0.981}{0.981 \times 1.145} \times 10^{-6} \right) \right] \text{K} \cdot \text{Pa}^{-1} \\ & = 0.342 \times 10^{-6} \text{ K} \cdot \text{Pa}^{-1} \\ & \qquad \qquad \frac{\Delta T}{\Delta p} \approx \frac{\text{d}T}{\text{d}p} \end{split}$$

- $\Delta T = [0.342 \times 10^{-6} \times (0.1 \times 10^{6})] \text{ K} = 0.0342 \text{ K}$
- 34. $101325 \, \text{Pa} \, \text{下}$, $\, \text{HgI}_2 \, \text{的红}$ 、黄两种晶体的晶型转变温度为 $\, 127 \, ^{\circ} \, \text{C}$ 。已知由红色 $\, \text{HgI}_2 \, \text{转变为黄色} \, \text{HgI}_2 \, \text{时,转变焓为} \, 1250 \, \text{J} \cdot \text{mol}^{-1}$,体积变化为 $\, -5.4 \, \text{cm}^3 \cdot \text{mol}^{-1}$,试求压力为 $\, 10 \, \text{MPa} \, \text{时的晶型转变温度}$ 。

解:
$$\frac{dT}{dp} = \frac{T\Delta_{trs}V}{\Delta_{trs}H}, \quad \frac{dT}{T} = \frac{\Delta_{trs}V}{\Delta_{trs}H}dp$$

$$\ln \frac{T_2}{T_1} \approx \frac{\Delta_{trs}V}{\Delta_{trs}H}(p_2 - p_1)$$

$$= \frac{-5.4 \times 10^{-6}}{1250} \times \left[(10 - 101325 \times 10^{-6}) \times 10^{6} \right] = -0.0428$$

$$\frac{T_2}{T_1} = 0.958$$

$$\therefore \quad T_2 = [0.958 \times (127 + 273.15)] \text{ K} = 383 \text{ K}, \quad t_2 = 110 \text{ °C}$$

35. 在熔点附近的温度范围内, $TaBr_5$ 固体的蒸气压与温度的关系为: $lg(p^*/Pa) = 14.696 - 5650/(T/K)$,液体的蒸气压与温度的关系为: $lg(p^*/Pa) = 10.296 - 3265/(T/K)$ 。试求三相点的温度和压力,并求三相点时的摩尔升华焓、摩尔蒸发焓及摩尔熔化焓。

解:
$$14.696 - \frac{5650}{T/K} = 10.296 - \frac{3265}{T/K}$$
, $4.400 = \frac{2385}{T/K}$
∴ $T = \left(\frac{2385}{4.400}\right)$ K = 542.0 K
 $lg\left(\frac{p^*}{Pa}\right) = 10.296 - \frac{3265}{542.0} = 4.272$
 $p^* = 18.7 \times 10^3$ Pa = 18.7 kPa

对固气平衡

$$\frac{d\ln(p^*/Pa)}{dT} = \frac{\Delta_{\text{sub}}H_{\text{m}}}{RT^2} = \frac{\ln 10 \times 5650 \text{ K}}{T^2}$$

$$\therefore \quad \Delta_{\text{sub}}H_{\text{m}} = (8.3145 \times \ln 10 \times 5650) \text{ J} \cdot \text{mol}^{-1}$$

$$= 108.17 \times 10^3 \text{ J} \cdot \text{mol}^{-1} = 108.17 \text{ kJ} \cdot \text{mol}^{-1}$$

对液气平衡

$$\frac{d\ln(p^*/Pa)}{dT} = \frac{\Delta_{\text{vap}}H_{\text{m}}}{RT^2} = \frac{(\ln 10) \times 3265 \text{ K}}{T^2},$$

$$\therefore \quad \Delta_{\text{vap}}H_{\text{m}} = (8.3145 \times \ln 10 \times 3265) \text{ J} \cdot \text{mol}^{-1}$$

$$= 62.51 \times 10^3 \text{ J} \cdot \text{mol}^{-1} = 62.51 \text{ kJ} \cdot \text{mol}^{-1}$$

$$\Delta_{\text{fus}}H_{\text{m}} = \Delta_{\text{sub}}H_{\text{m}} - \Delta_{\text{vap}}H_{\text{m}} = (108.17 - 62.51) \text{ kJ} \cdot \text{mol}^{-1}$$

$$= 45.66 \text{ kJ} \cdot \text{mol}^{-1}$$

36. 方程 $\ln\{p^*\} = -(\Delta_{\text{vap}}H_{\text{m}}/RT) + C$ 是在假设摩尔蒸发焓不随温度而变的条件下导出的。如假设蒸发过程的 $\Delta C_{p,\text{m}}$ 是常数,试导出相应的方程式。此时 $\ln\{p^*\}$ 对(1/T)作图是否仍为直线?如何由所作之图求某一温度下的摩尔蒸发焓?

解:

$$\frac{\mathrm{d}\Delta_{\mathrm{vap}}H_{\mathrm{m}}}{\mathrm{d}T} = \Delta C_{p,\mathrm{m}}$$

上式不定积分后得

$$\Delta_{\rm vap} H_{\rm m} = \Delta C_{p,\rm m} T + A$$

式中A为积分常数。

$$\frac{\mathrm{dln}\left\{p^{*}\right\}}{\mathrm{d}T} = \frac{\Delta_{\mathrm{vap}}H_{\mathrm{m}}}{RT^{2}} = \frac{\Delta C_{p,\mathrm{m}}T + A}{RT^{2}} = \frac{\Delta C_{p,\mathrm{m}}}{R} \cdot \frac{1}{T} + \frac{A}{R} \cdot \frac{1}{T^{2}}$$

$$\therefore \quad \ln\left\{p^{*}\right\} = \frac{\Delta C_{p,\mathrm{m}}}{R}\ln\left\{T\right\} - \frac{A}{R} \cdot \frac{1}{T} + C$$

式中C为积分常数,故 $\ln\{p^*\}$ 对1/T作图不是直线。

武
$$\frac{\mathrm{d} \ln \left\{ p^* \right\}}{\mathrm{d} T} = \frac{\Delta_{\mathrm{vap}} H_{\mathrm{m}}}{R T^2}$$
 可写成
$$\frac{\mathrm{d} \ln \left\{ p^* \right\}}{\mathrm{d} \left(1/T \right)} = -\frac{\Delta_{\mathrm{vap}} H_{\mathrm{m}}}{R}$$

故 $\ln\{p^*\}$ — 1/T 图中曲线上任一点切线的斜率即为 — $\Delta_{\text{vap}}H_{\text{m}}/R$ 。于是在图中相应于某一温度处作切线,即可由切线的斜率求得该温度下的摩尔蒸发焓。

37. (1) 乙醇气相脱水制乙烯, 反应为:

$$C_2H_5OH(g) \longrightarrow C_2H_4(g) + H_2O(g)$$

试计算 25℃的 $\Delta_r S_m^e$ 。(2) 若将反应写成:

$$2C_2H_5OH(g) \longrightarrow 2C_2H_4(g) + 2H_2O(g)$$

则 25℃时的 $\Delta_r S_m^e$ 又是多少?

解: (1) 由附录查得

物 质	$C_2H_5OH(g)$	$C_2H_4(g)$	$H_2O(g)$
$S_{\mathrm{m}}^{\Theta}(298.15\mathrm{K})/(\mathrm{J}\cdot\mathrm{K}^{-1}\cdot\mathrm{mol}^{-1})$	282.70	219.56	188.825

$$\Delta_{r} S_{m}^{e}(298.15 \text{K}) = [(219.56 + 188.825) - 282.70] \text{J} \cdot \text{K}^{-1} \cdot \text{mol}^{-1}$$
$$= 125.69 \text{ J} \cdot \text{K}^{-1} \cdot \text{mol}^{-1}$$

(2)
$$\Delta_r S_m^{\theta}(298.15\text{K}) = 2 \times 125.69 \text{ J} \cdot \text{K}^{-1} \cdot \text{mol}^{-1} = 251.38 \text{ J} \cdot \text{K}^{-1} \cdot \text{mol}^{-1}$$

38. 已知 25 ℃ 时硝基甲烷 $CH_3NO_2(I)$ 的标准摩尔熵为 171.75 $J \cdot K^{-1} \cdot mol^{-1}$,摩尔蒸发焓为 38.36 $kJ \cdot mol^{-1}$,饱和蒸气压为 4.887 kPa。求 $CH_3NO_2(g)$ 在 25℃时的标准摩尔熵。设蒸气服从理想气体状态方程。

解:
$$\Delta S_1 = \frac{\Delta_{\text{vap}} H_{\text{m}}}{T} = \left(\frac{38.36 \times 10^3}{298.15}\right) J \cdot K^{-1} \cdot \text{mol}^{-1}$$

= 128.66 J·K⁻¹·mol⁻¹

$$\Delta S_2 = R \ln \frac{p_1}{p_2} = \left(8.3145 \times \ln \frac{4.887}{100} \right) \mathbf{J} \cdot \mathbf{K}^{-1} \cdot \text{mol}^{-1}$$
$$= -25.10 \,\mathbf{J} \cdot \mathbf{K}^{-1} \cdot \text{mol}^{-1}$$

$$S_{m}^{e}(g,298.15K) = S_{m}^{e}(1,298.15K) + \Delta S_{1} + \Delta S_{2}$$
$$= (171.75 + 128.66 - 25.10) J \cdot K^{-1} \cdot \text{mol}^{-1}$$
$$= 275.31 J \cdot K^{-1} \cdot \text{mol}^{-1}$$

39. 已 知 25 ℃ 时 $C_2H_5OH(g)$ 的 标 准 摩 尔 生 成 焓 为 $-235.10 \, kJ \cdot mol^{-1}$,试利用附录所载的 $C \times H_2 \times O_2 \times C_2H_5OH(g)$ 的标准 摩尔熵,计算 25℃时 $C_2H_5OH(g)$ 的标准摩尔生成吉氏函数。

解:

$$\begin{split} 2\text{C(s)} + 3\text{H}_{2}(\text{g}) + \frac{1}{2}\text{O}_{2}(\text{g}) &\longrightarrow \text{C}_{2}\text{H}_{5}\text{OH(g)} \\ \Delta_{r}S_{m}^{\bullet} &= \sum_{\text{B}} \nu_{\text{B}}S_{m}^{\bullet}(\text{B}) \\ &= \left[282.70 - \left(2 \times 5.740 + 3 \times 130.684 + \frac{1}{2} \times 205.138\right)\right] \text{J} \cdot \text{K}^{-1} \cdot \text{mol}^{-1} \\ &= -223.40 \, \text{J} \cdot \text{K}^{-1} \cdot \text{mol}^{-1} \\ \Delta_{f}G_{m}^{\bullet} &= \Delta_{f}H_{m}^{\bullet} - T\Delta_{r}S_{m}^{\bullet} \\ &= \left[-235.10 - 298.15 \times (-223.40) \times 10^{-3}\right] \text{kJ} \cdot \text{mol}^{-1} \\ &= -168.49 \, \text{kJ} \cdot \text{mol}^{-1} \end{split}$$

40. 已知 25 ℃ 时 $H_2O(1)$ 的 标准摩尔生成吉氏函数为 $-237.129 \, kJ \cdot mol^{-1}$,水的饱和蒸气压为 3.167 kPa,求 25 ℃ 时 $H_2O(g)$ 的标准摩尔生成吉氏函数。

解:
$$\Delta_f G_m^{\circ}(g,298.15K) = \Delta_f G_m^{\circ}(1,298.15K) + RT \ln \frac{p_2}{p_1}$$

$$= \left[-237.129 + 8.3145 \times 298.15 \times \left(\ln \frac{100}{3.167} \right) \times 10^{-3} \right] \text{kJ} \cdot \text{mol}^{-1}$$

$$= -228.57 \text{ kJ} \cdot \text{mol}^{-1}$$

41. 乙烯水化为乙醇的反应为:

$$C_2H_4(g) + H_2O(g) \longrightarrow C_2H_5OH(g)$$

各物质 $C_{p,m}^{e}$ 的数据如下表所列。试计算 225 \mathbb{C} 时该反应的 $\Delta_{r}H_{m}^{e}$ 、 $\Delta_{r}S_{m}^{e}$ 和 $\Delta_{r}G_{m}^{e}$ 。 所需其他数据可查附录。

物 质	$C_{p,\mathrm{m}}^{\Theta}/\operatorname{J}\cdot\operatorname{K}^{-1}\cdot\operatorname{mol}^{-1}$
$C_2H_5OH(g)$	$9.04 + 207.9 \times 10^{-3} (T / K)$
$C_2H_4(g)$	$8.70 + 130.1 \times 10^{-3} (T / K)$
$H_2O(g)$	$31.59 + 5.9 \times 10^{-3} (T/K)$

解:
$$\Delta_r H_{\mathrm{m}}^{\bullet}(298\mathrm{K}) = [-235.10 - 52.26 - (-241.818)] \,\mathrm{kJ \cdot mol^{-1}}$$

 $= -45.54 \,\mathrm{kJ \cdot mol^{-1}}$
 $\Delta_r a = (9.04 - 8.70 - 31.59) \mathrm{J \cdot K^{-1} \cdot mol^{-1}}$
 $= -31.25 \,\mathrm{J \cdot K^{-1} \cdot mol^{-1}}$
 $\Delta_r b = (207.9 - 130.1 - 5.9) \times 10^{-3} \,\mathrm{J \cdot K^{-2} \cdot mol^{-1}}$
 $= 71.9 \times 10^{-3} \,\mathrm{J \cdot K^{-2} \cdot mol^{-1}}$
 $\Delta_r H_{\mathrm{m}}^{\bullet}(498\mathrm{K}) = \Delta_r H_{\mathrm{m}}^{\bullet}(298\mathrm{K}) + \Delta_r a (T_2 - T_1) + \frac{\Delta_r b}{2} \left(T_2^2 - T_1^2\right)$
 $= \left\{ -45.54 + \left[(-31.25) \times (498 - 298) + \frac{71.9 \times 10^{-3}}{2} \times (498^2 - 298^2) \right] \times 10^{-3} \right\} \,\mathrm{kJ \cdot mol^{-1}}$
 $= -46.07 \,\mathrm{kJ \cdot mol^{-1}}$
 $\Delta_r S_{\mathrm{m}}^{\bullet}(298\mathrm{K}) = (282.70 - 219.56 - 188.825) \,\mathrm{J \cdot K^{-1} \cdot mol^{-1}}$
 $= -125.68 \,\mathrm{J \cdot K^{-1} \cdot mol^{-1}}$
 $\Delta_r S_{\mathrm{m}}^{\bullet}(498\mathrm{K}) = \Delta_r S_{\mathrm{m}}^{\bullet}(298\mathrm{K}) + \Delta_r a \ln \frac{T_2}{T_1} + \Delta_r b (T_2 - T_1)$
 $= \left[-125.68 + \left(-31.25 \right) \ln \frac{498}{298} + 71.9 \times 10^{-3} \left(498 - 298 \right) \right] \,\mathrm{J \cdot K^{-1} \cdot mol^{-1}}$
 $= -127.35 \,\mathrm{J \cdot K^{-1} \cdot mol^{-1}}$
 $\Delta_r G_{\mathrm{m}}^{\bullet}(498\mathrm{K}) = \Delta_r H_{\mathrm{m}}^{\bullet}(498\mathrm{K}) - 498\mathrm{K \cdot \Delta_r} S_{\mathrm{m}}^{\bullet}(498\mathrm{K})$
 $= \left[-46.07 - 498 \times \left(-127.35 \right) \times 10^{-3} \,\mathrm{kJ \cdot mol^{-1}} \right]$
 $= 17.35 \,\mathrm{kJ \cdot mol^{-1}}$

42. 求 400℃时反应

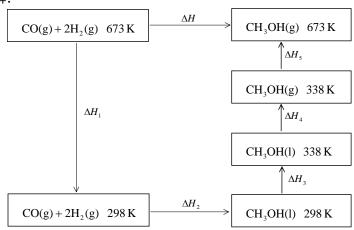
$$CO(g) + 2H_2(g) \longrightarrow CH_3OH(g)$$

的 $\Delta_r H_m^e$ 、 $\Delta_r S_m^e$ 和 $\Delta_r G_m^e$ 。已知甲醇的正常沸点为 64.7 \mathbb{C} , 摩尔蒸发焓

为35.27 kJ·mol⁻¹,其他所需数据可查附录,并见下表:

物 质	$\Delta_{\rm f} H_{\rm m}^{\rm e}(298.15{\rm K})/{\rm kJ\cdot mol^{-1}}$	$\overline{C}_{p,\mathrm{m}} / \operatorname{J} \cdot \operatorname{K}^{-1} \cdot \operatorname{mol}^{-1}$
CO(g)	-110.525	30.2 (25~400℃范围内)
$H_2(g)$	0	29.3 (25~400℃范围内)
CH ₃ OH(l)	- 238.66	77.2 (25~64.7℃范围内)
$CH_3OH(g)$		59.2 (64.7~400℃范围内)

解:



$$\Delta H_1 = [(30.2 + 2 \times 29.3) \times (298 - 673)] \text{ J} \cdot \text{mol}^{-1} = -33.3 \text{ kJ} \cdot \text{mol}^{-1}$$

$$\Delta H_2 = [-238.66 - (-110.525)] \text{ kJ} \cdot \text{mol}^{-1} = -128.14 \text{ kJ} \cdot \text{mol}^{-1}$$

$$\Delta H_3 = [77.2 \times (338 - 298)] \text{ J} \cdot \text{mol}^{-1} = 3.09 \text{ kJ} \cdot \text{mol}^{-1}$$

$$\Delta H_4 = 35.27 \text{ kJ} \cdot \text{mol}^{-1}$$

$$\Delta H_5 = [59.2 \times (673 - 338)] \text{ J} \cdot \text{mol}^{-1} = 19.8 \text{ kJ} \cdot \text{mol}^{-1}$$

$$\therefore \Delta_r H_m^{\bullet} \approx \Delta H = \Delta H_1 + \Delta H_2 + \Delta H_3 + \Delta H_4 + \Delta H_5$$

$$= (-33.3 - 128.14 + 3.09 + 35.27 + 19.8) \text{ kJ} \cdot \text{mol}^{-1}$$

$$= -103.3 \text{ kJ} \cdot \text{mol}^{-1}$$

$$\Delta S_1 = \left[(1 \times 30.2 + 2 \times 29.3) \ln \frac{298}{673} \right] \text{ J} \cdot \text{K}^{-1} \cdot \text{mol}^{-1}$$

$$= -72.3 \text{ J} \cdot \text{K}^{-1} \cdot \text{mol}^{-1}$$

$$\Delta S_2 = (126.8 - 197.674 - 2 \times 130.684) \text{ J} \cdot \text{K}^{-1} \cdot \text{mol}^{-1}$$

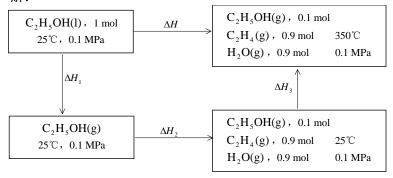
$$= -332.2 \text{ J} \cdot \text{K}^{-1} \cdot \text{mol}^{-1}$$

$$\begin{split} \Delta S_3 &= \left(77.2 \ln \frac{338}{298}\right) \mathbf{J} \cdot \mathbf{K}^{-1} \cdot \mathbf{mol}^{-1} = 9.72 \mathbf{J} \cdot \mathbf{K}^{-1} \cdot \mathbf{mol}^{-1} \\ \Delta S_4 &= \left(\frac{35.27 \times 10^3}{64.7 + 273.15}\right) \mathbf{J} \cdot \mathbf{K}^{-1} \cdot \mathbf{mol}^{-1} = 104.40 \mathbf{J} \cdot \mathbf{K}^{-1} \cdot \mathbf{mol}^{-1} \\ \Delta S_5 &= \left(59.2 \ln \frac{673}{338}\right) \mathbf{J} \cdot \mathbf{K}^{-1} \cdot \mathbf{mol}^{-1} = 40.8 \mathbf{J} \cdot \mathbf{K}^{-1} \cdot \mathbf{mol}^{-1} \\ \Delta_r S_m^{\, e} (673 \mathbf{K}) &= \Delta S_1 + \Delta S_2 + \Delta S_3 + \Delta S_4 + \Delta S_5 \\ &= \left(-72.3 - 332.2 + 9.72 + 104.40 + 40.8\right) \mathbf{J} \cdot \mathbf{K}^{-1} \cdot \mathbf{mol}^{-1} \\ &= -249.6 \mathbf{J} \cdot \mathbf{K}^{-1} \cdot \mathbf{mol}^{-1} \\ \Delta_r G_m^{\, e} (673 \mathbf{K}) &= \Delta_r H_m^{\, e} (673 \mathbf{K}) - 673 \mathbf{K} \cdot \Delta_r S_m^{\, e} (673 \mathbf{K}) \\ &= \left[-103.3 - 673 \times \left(-249.6\right) \times 10^{-3}\right] \mathbf{kJ} \cdot \mathbf{mol}^{-1} \\ &= 64.7 \mathbf{kJ} \cdot \mathbf{mol}^{-1} \end{split}$$

43. 在 0.1 MPa 下,1 mol 温度为 25℃的 C_2H_5OH (I) 变为温度为 350℃的 0.1mol C_2H_5OH (g)、0.9mol C_2H_4 (g)及 0.9mol H_2O (g)的混合物,试求这个过程的热量。设气体服从理想气体状态方程,已知数据为:

物质	$\Delta_{\rm f} H_{\rm m}^{\rm e}(298.15{\rm K})/{\rm kJ\cdot mol^{-1}}$	$C_{p,\mathrm{m}}^{\mathrm{e}} / \operatorname{J} \cdot \operatorname{K}^{-1} \cdot \operatorname{mol}^{-1}$
C ₂ H ₅ OH(l)	- 277.69	
$C_2H_5OH(g)$	- 235.10	$9.04 + 207.9 \times 10^{-3} (T/K)$
$C_2H_4(g)$	52.26	$8.70 + 130.1 \times 10^{-3} (T/K)$
$H_2O(g)$	- 241.818	$31.59 + 5.9 \times 10^{-3} (T/K)$

解:



$$\Delta H_1 = 1 \times [-235.10 - (-277.69)] \text{ kJ} = 42.59 \text{ kJ}$$

$$\Delta H_2 = 0.9 \times [52.26 + (-241.818) - (-235.10)] \text{ kJ} = 40.99 \text{ kJ}$$

$$\Delta H_3 = \int_{298\text{K}}^{623\text{K}} \left\{ 0.9 \times \left[8.70 + 31.59 + (130.1 + 5.9) \times 10^{-3} \left(T / \text{K} \right) \right] \right. \\ \left. + 0.1 \times \left[9.04 + 207.9 \times 10^{-3} \left(T / \text{K} \right) \right] \right\} J \cdot \text{K}^{-1} dT$$

$$= \int_{298\text{K}}^{623\text{K}} \left[37.17 + 143.2 \times 10^{-3} \left(T / \text{K} \right) \right] J \cdot \text{K}^{-1} dT$$

$$= \left[37.17 \times (623 - 298) + \frac{143.2 \times 10^{-3}}{2} \times (623^2 - 298^2) \right] J$$

$$= 33.51 \text{ kJ}$$

$$\Delta H = \Delta H_1 + \Delta H_2 + \Delta H_3 = (42.59 + 40.99 + 33.51) \text{ kJ} = 117.09 \text{ kJ}$$