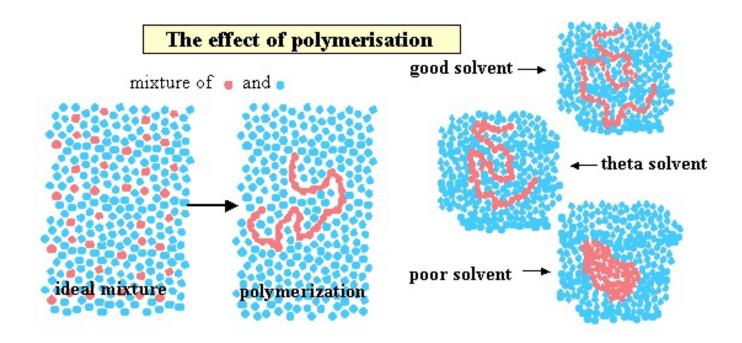
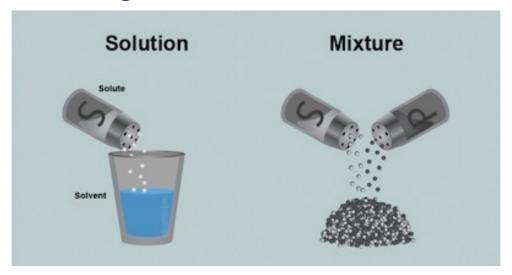
Chemical Engineering Thermodynamics

Lecture 8 Solution Thermodynamics Xiaofei Xu



Solutions and Mixtures

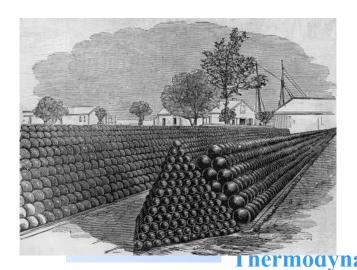
Solutions are homogeneous mixtures



Solution Type	Example	
gas-gas	air	
gas-liquid	carbon dioxide in soda	
gas-solid	hydrogen gas in palladium metal	
liquid-liquid	gasoline	
solid-liquid	sugar in water	
liquid-solid	mercury dental amalgam	
solid-solid	sterling silver	

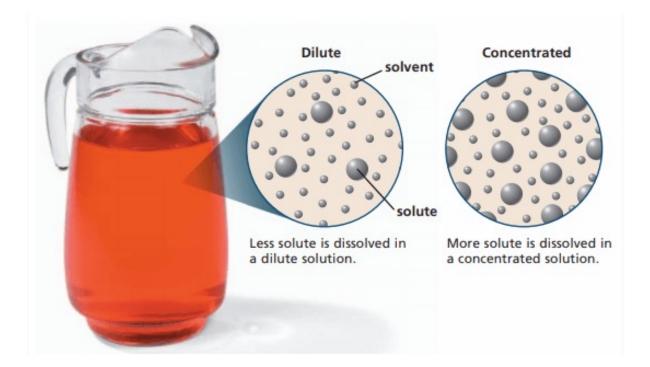
Measures of Composition

- Mass fraction: $x_i = \frac{m_i}{m}$
- Molar fraction: $x_i = \frac{n_i}{n}$
- Molar concentration: $C_i = \frac{x_i}{V}$
- Volume fraction: $\phi_i = \frac{V_i}{V}$
- Packing fraction: $\eta_i = \frac{\pi}{6} \rho_i \sigma_i^3$



Dilute and Concentrated Solution

Concentrated solution	Dilute solution	
A liquid with a high solute concentration is called a concentrated solution.	A liquid with a less solute concentration is called a dilute solution.	
The solution becomes more concentrated as more solute is applied to a solution	The dissolved salt from a well in the drinking water is a dilute solution.	
There is a significant amount of water in a concentrated solution.	By adding more water, the concentration of a solution can be further decreased and diluted	



Fundamental Property Relation

- $dG = VdP SdT + \sum_{i} \mu_{i} dn_{i}$
- Chemical potential: $\mu_i = \left[\frac{\partial G}{\partial n_i}\right]_{P,T,n_i}$
- $dG_n = V_n dP S_n dT + \sum_i \mu_i dx_i$

Partial Properties

- Partial molar properties: $\overline{M}_i \equiv \left[\frac{\partial M}{\partial n_i}\right]_{P,T,n_i}$
- A measure of the response of total property to the addition of an infinitesimal amount of species i.

Total properties	Molar properties	Partial properties	Pure-species properties
V	V_n	$\overline{V_i}$	V_i
U	U_n	$\overline{U_i}$	U_i
Н	H_n	$\overline{H_i}$	H_i
S	S_n	$\overline{\mathcal{S}_i}$	${\mathcal S}_i$
G	G_n	\overline{G}_i	G_i

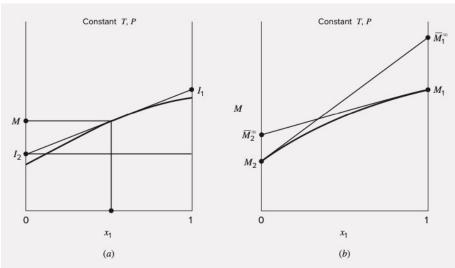
Some Important Formular

- Summability: $M = \sum_{i} n_i \overline{M_i}$
- $\overline{M}_i = M_n \sum_{k \neq i} x_k \frac{\partial M_n}{\partial x_k}$
- Gibbs-Duhem equation:

$$\left(\frac{\partial M_n}{\partial P}\right)_{T,x} dP + \left(\frac{\partial M_n}{\partial T}\right)_{P,x} dT - \sum_i x_i d\overline{M_i} = 0$$

• In binary system:

$$x_1 \frac{d\overline{M_1}}{dx_1} + x_2 \frac{d\overline{M_2}}{dx_1} = 0$$



1 nermodynamics

Example

Molar enthalpy

The enthalpy of a binary liquid system of species 1 and 2 at fixed T and P is represented by the equation:

$$H = 400x_1 + 600x_2 + x_1x_2(40x_1 + 20x_2)$$

where H is in J·mol⁻¹. Determine expressions for \bar{H}_1 and \bar{H}_2 as functions of x_1 , numerical values for the pure-species enthalpies H_1 and H_2 , and numerical values for the partial enthalpies at infinite dilution \bar{H}_1^{∞} and \bar{H}_2^{∞} .

Partial Properties

Original Properties	Partial Properties	
H = U + pV	$\overline{H_i} = \overline{U}_i + p\overline{V}_i$	
F = U - TS	$\bar{F}_i = \bar{U}_i - T\bar{S}_i$	
G = H - TS	$\bar{G}_i = \bar{H}_i - T\bar{S}_i$	
$\left(\frac{\partial H}{\partial p}\right)_T = V - T \left(\frac{\partial V}{\partial T}\right)_p$	$\left(\frac{\partial \overline{H}_i}{\partial p}\right)_T = \overline{V}_i - T\left(\frac{\partial \overline{V}_i}{\partial T}\right)_p$	
$c_p = \left(\frac{\partial H}{\partial T}\right)_p$	$\bar{c}_{p_i} = \left(\frac{\partial \overline{H_i}}{\partial T}\right)_p$	

The Ideal-Gas-State Mixture Model

- $\overline{V_i}^{id} = V_{n,i}^{id} = V_n^{id}$
- Partial pressure: $p_i = y_i P$
- Gibbs's theorem: $\overline{M_i}^{id}(T, P) = M_{n,i}^{id}(T, p_i)$
- Entropy: $\overline{S}_i^{id} = S_{n,i}^{id} R \ln y_i$
- Gibbs free energy: $\overline{G}_i^{id} = G_{n,i}^{id} + RT \ln y_i$

Mixing in ideal-gas state

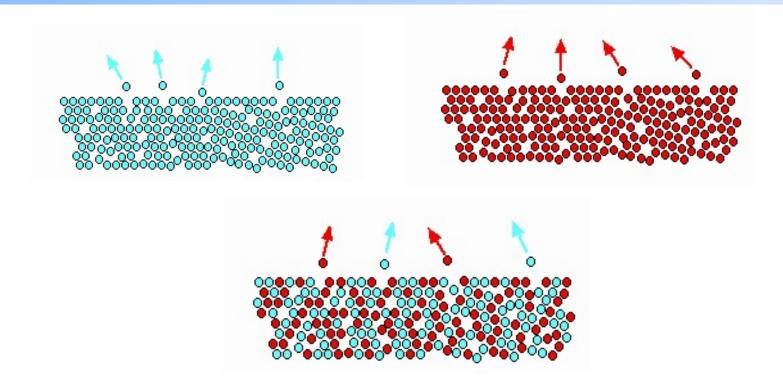
$$H_n^{id} = \sum_i y_i H_{n,i}^{id}$$

$$S_n^{id} = \sum_i y_i S_{n,i}^{id} - R \sum_i y_i \ln y_i$$

$$G_n^{id} = \sum_i y_i G_{n,i}^{id} + RT \sum_i y_i \ln y_i$$

- $\Delta H_{mix} = 0$
- $\Delta S_{mix} = -nR \sum y_i \ln y_i$
- $\Delta G_{mix} = nRT \sum y_i \ln y_i$

Fugacity



In an ideal mixture, the tendency of the two types of molecules to escape is the same as that in pure species.

In a real mixture, the tendency depends on the interaction between molecules.

Fugacity

- A measure of the tendency of a fluid to escape or expand
- Measure the behaviors deviating from ideal-gas
- Depends on molecular interactions
- The pressure value needed at a given T to make the properties of a non-ideal gas satisfy the equation for an ideal gas

Fugacity of Pure Species

- Ideal gas: $d\mu = RTd \ln P$
- Real fluid: $d\mu = RTd \ln f$
- Residual Gibbs free energy: $G_n^R = RT \ln \frac{f}{P}$
- Fugacity coefficient: $\phi \equiv \frac{f}{P}$
- $\ln \phi = \int_0^P (Z 1) \frac{dP}{P}$

Fugacity

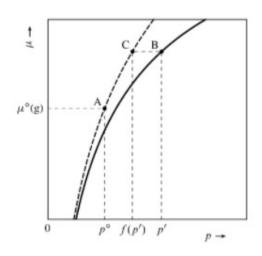


Figure 7.6 Chemical potential as a function of pressure at constant temperature, for a real gas (solid curve) and the same gas behaving ideally (dashed curve). Point A is the gas standard state. Point B is a state of the real gas at pressure p'. The fugacity f(p') of the real gas at pressure p' is equal to the pressure of the ideal gas having the same chemical potential as the real gas (point C).

Fugacity of a Pure Liquid

$$f_i^l(P) = \underbrace{\frac{f_i^{\nu}(P_i^{\text{sat}})}{P_i^{\text{sat}}}}_{(A)} \underbrace{\frac{f_i^l(P_i^{\text{sat}})}{f_i^{\nu}(P_i^{\text{sat}})}}_{(B)} \underbrace{\frac{f_i^l(P)}{f_i^l(P_i^{\text{sat}})}P_i^{\text{sat}}}_{(C)}$$

- A: vapor-phase fugacity coefficient
- B: Ratio of liquid-phase fugacity to vapor-phase fugacity
- C: The effect of pressure on the fugacity
- Evaluate the fugacity of compressed liquid by using the data at saturation

Example

For H₂O at a temperature of 300°C and for pressures up to 10,000 kPa (100 bar) calculate values of f_i and ϕ_i from data in the steam tables and plot them vs. P.

Fugacity of Species in Solution

- Fugacity in solution: $d\mu_i = RTd \ln \hat{f}_i$
- Fugacity residual: $\mu_i \mu_i^{ig} = RT \ln \frac{\hat{f}_i}{y_i P}$
- Fugacity coefficient: $\hat{\phi}_i = \frac{\hat{f}_i}{y_i P}$

Some Important Formulas

$$\bullet \quad \frac{H_n^R}{RT} = -T \left[\frac{\partial \left(\frac{G_n^R}{RT} \right)}{\partial T} \right]$$

•
$$\ln \hat{\phi}_i = \left[\frac{\partial \left(\frac{G^R}{RT} \right)}{\partial n_i} \right]$$

•
$$\ln \hat{\phi}_i = \int_0^P (\overline{Z}_i - 1) \frac{dP}{P}$$

Fugacity Coefficients from the Virial EOS

•
$$Z=1+\frac{BP}{RT}$$

•
$$B = y_1^2 B_{11} + 2y_1 y_2 B_{12} + y_2^2 B_{22}$$

•
$$\delta_{12} = 2B_{12} - B_{11} - B_{22}$$

•
$$\ln \hat{\phi}_1 = \frac{P}{RT} (B_{11} + y_2^2 \delta_{12})$$

•
$$\ln \hat{\phi}_2 = \frac{P}{RT} (B_{22} + y_1^2 \delta_{12})$$

Generalized Correlations for the Fugacity Coefficient

•
$$\ln \phi_i = \int_0^{P_r} (Z_i - 1) \frac{dP_r}{P_r}$$

•
$$\ln \phi = \int_0^{P_r} (Z^0 - 1) \frac{dP_r}{P_r} + \omega \int_0^{P_r} Z^1 \frac{dP_r}{P_r}$$

Ideal Gases versus Ideal Solutions

- Ideal gas: molecules occupy no volume; no intermolecular interactions; real gas at low pressure
- Ideal solution: molecules exhibit the same intermolecular interactions between all constituents; dilute solution or mixtures of molecularly-similar materials

$$\begin{aligned} & \text{ideal solution} \\ & \Delta v_{mix}^{ig} = 0 & \Delta v_{mix}^{is} = 0 \\ & \Delta h_{mix}^{ig} = 0 & \Delta h_{mix}^{is} = 0 \\ & \Delta s_{mix}^{ig} = -R \sum_i y_i \ln[y_i] & \Delta s_{mix}^{is} = -R \sum_i x_i \ln[x_i] \\ & \Delta g_{mix}^{ig} = RT \sum_i y_i \ln[y_i] & \Delta g_{mix}^{is} = RT \sum_i x_i \ln[x_i] \end{aligned}$$

Ideal Solution

- The gas phase of the solution exhibits properties analogous of ideal gas mixtures
- Ideal gas: $\mu_i^{ig} \equiv \bar{G}_i^{ig} = G_{n,i}^{ig}(T, P) + RT \ln y_i$
- Ideal solution: $\mu_i^{id} \equiv \bar{G}_i^{id} = G_{n,i}(T, P) + RT \ln x_i$
- $\bar{V}_i^{id} = V_{n,i}$
- $\bar{S}_i^{id} = S_{n,i} R \ln x_i$
- $\overline{H}_i^{id} = H_{n,i}$

Ideal Solution

•
$$G_n^{id} = \sum_i x_i G_{n,i} + RT \sum_i x_i \ln x_i$$

•
$$S_n^{id} = \sum_i x_i S_{n,i} - R \sum_i x_i \ln x_i$$

•
$$V_n^{id} = \sum_i x_i V_{n,i}$$

•
$$H_n^{id} = \sum_i x_i H_{n,i}$$

Lewis/Randall Rule

- $\mu_i = \Gamma_i(T) + RT \ln \hat{f}_i$
- $G_i = \Gamma_i(T) + RT \ln f_i$
- $\hat{f}_i^{id} = x_i f_i$
- $\hat{\phi}_i^{id} = \phi_i$

The fugacity of each species in an ideal solution is proportional to its mole fraction.

Excess Properties

- Excess properties: $M^E \equiv M M^{id}$
- Residual properties: $M^R \equiv M M^{ig}$
- $M^E = M^R \sum_i x_i M_i^R$
- $d\left(\frac{G^E}{RT}\right) = \frac{V^E}{RT}dP \frac{H^E}{RT^2}dT + \sum_i \frac{\bar{G}_i^E}{RT}dn_i$

Typical Solution Models

- Regular solution: $S^E = 0$
- Athermal solution: $H^E = 0$
- Ideal solution

Ideal Solution Regular Solution Athernal Solution

$$X - \cancel{f} \qquad 0$$

$$X - \cancel{f} \qquad 0$$

$$S_{mix, m} - k_8(x_1 \ln \phi_1 + x_2 \ln \phi_2) - k_8(x_1 \ln \phi_1 + x_2 \ln \phi_2) - k_8(x_1 \ln \phi_1 + \frac{x_2}{N} \ln \phi_2)$$

$$X_1, X_2 : \text{molar fraction}$$

$$\phi_1, \phi_2 : \text{volume fraction}$$

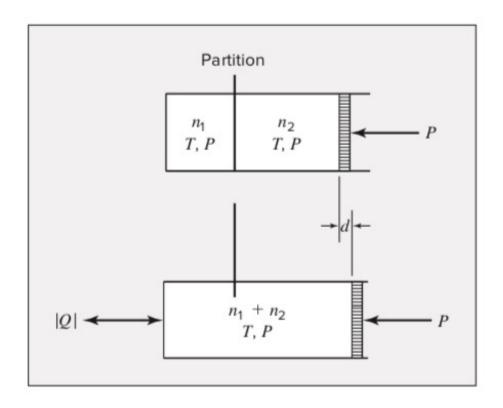
$$\phi_1, \phi_2 : \text{volume fraction}$$

$$\chi_1 = \frac{\phi_1 V_A}{\phi_1 V_A + \phi_2 V_B}$$

$$\chi_2 = \frac{\phi_2 V_B}{\phi_1 V_A + \phi_2 V_B}$$

Mixing Processes

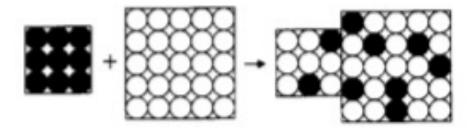
• Standard mixing process: mixing at constant *T* and *P*.



Entropy of Binary Random Mixing

•
$$\Delta \bar{S}_{\text{mix}} = -k \left[\frac{\phi_A}{N_A} \ln \phi_A + \frac{\phi_B}{N_B} \ln \phi_B \right]$$

•
$$\Delta \bar{F}_{\text{mix}} = kT \left[\frac{\phi_A}{N_A} \ln \phi_A + \frac{\phi_B}{N_B} \ln \phi_B \right]$$



Energy of Binary Mixing

Flory interaction parameter:

$$\chi \equiv \frac{z}{2kT} (2u_{AB} - u_{AA} - u_{BB})$$

Free energy of mixing

$$\Delta \bar{F}_{mix} = kT \left[\frac{\phi}{N_A} \ln \phi + \frac{1 - \phi}{N_B} \ln(1 - \phi) + \chi \phi (1 - \phi) \right]$$

χ parameter

•
$$\chi(T) \approx A + \frac{B}{T}$$

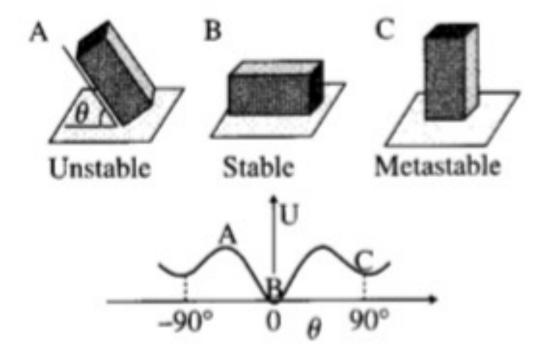
Table 4.3 Temperature dependence of the Flory interaction parameters of polymer blends [Eq. (4.31)] with $v_0 = 100 \text{ Å}^3$

Polymer blend	A	B (K)	T range (°C)
dPS/PS	-0.00017	0.117	150-220
dPS/PMMA	0.0174	2.39	120-180
PS dPMMA	0.0180	1.96	170-210
PS/PMMA	0.0129	1.96	100-200
dPS/dPMMA	0.0154	1.96	130-210
PVME/PS	0.103	-43.0	60-150
dPS/PPO	0.059	-32.5	180-330
dPS/TMPC	0.157	-81.3	190-250
PEO/dPMMA	-0.0021	-	80-160
PP/hhPP	-0.00364	1.84	30-130
PIB/dhhPP	0.0180	-7.74	30-170

dPS—deuterated polystyrene; PS—polystyrene; PMMA—poly(methyl methacrylate); dPMMA—deuterated poly(methyl methacrylate); PVME—poly(vinyl methyl ether); PPO—poly(2,6-dimethyl 1,4-phenylene oxide); TMPC—tetramethylpolycarbonate; PEO—poly(ethylene oxide); PP—polypropylene; hhPP—head-to-head polypropylene; PIB—polyisobutylene; dhhPP—deuterium labelled head-to-head polypropylene (after N. P. Balsara, Physical Properties of Polymers Handbook, AIP Press, 1996, Chapter 19).

Stability

• Unstable, stable, metastable

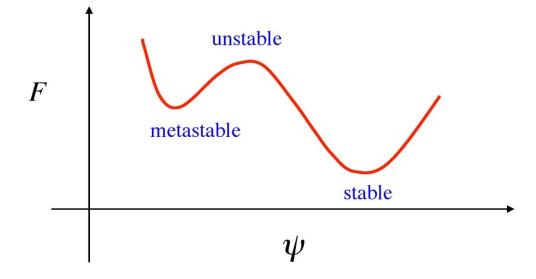


Stable, Metastable and Unstable States

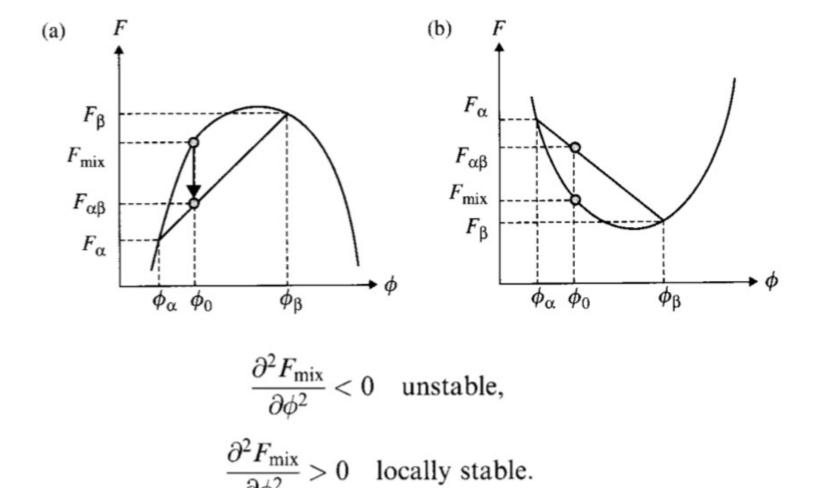
Equilibrium condition:
$$\frac{\partial F}{\partial \psi} = 0$$

Thermodynamic stability (under isothermal condition):

$$\frac{\partial^2 F}{\partial \psi^2} > 0 (a local condition)$$



Stability

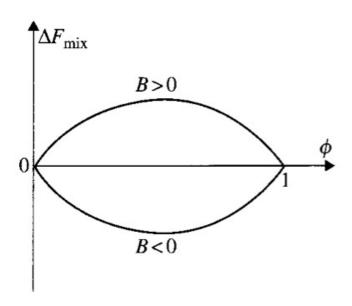


Ideal mixture

- Ideal mixture are stable always
- Entropy always acts to promote mixing
- Principle of entropy increase

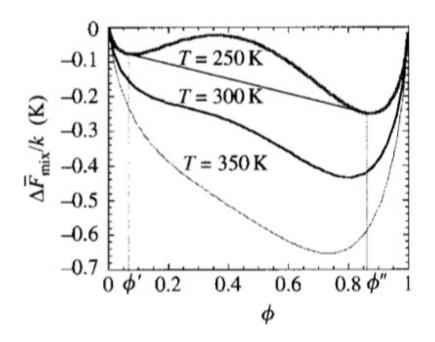
Mixing at T=0 K

- The mixing free energy is determined by the energy of mixing
- $\chi = A + \frac{B}{T}$
- B > 0: mixing is unfavorable
- B < 0: mixing is favorable



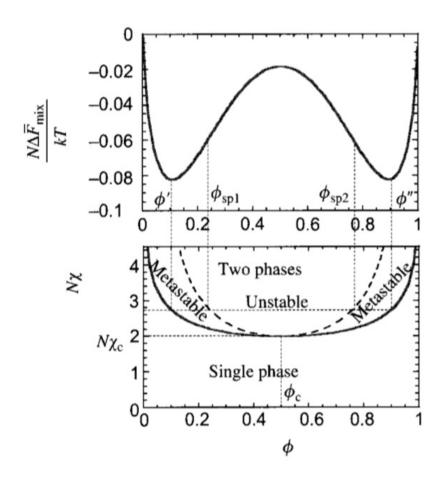
Real Mixture

- Common tangent rule
- Chemical potentials are balanced at equilibrium

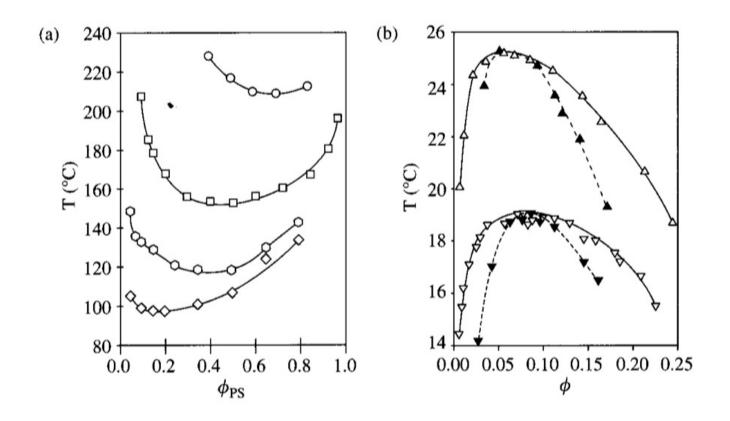


Phase diagram

- Binodal
- Spinodal
- Critical point



UCST and **LCST**



Summary Points

- Partial properties
- Fugacity
- Ideal solution
- Excess properties
- Flory-Huggins theory
- Metastability