

# Simulation of Engineering System 3 (ENG3036)

## Assignment Report Template Part 2

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Assignment Topic: Position Control for a Robot Arm

### 2.0 Introduction for Part 2

After developing models and simulating the robot arm control system in part 1, it became clear that the system should be improved with further tuning. While the final forearm deflection angle did settle at the desired  $55^\circ$  there was a lot of oscillation within the gear and actuator.

Hence, in this part of the assignment the existing control system was tuned by changing the proportional gain value  $G_c$ . The effects of varying the value of  $G_c$  were then analysed to fine an optimal value. In addition to tuning the proportional control system, an integral term ( $K_i$ ) was added to then change it into a proportional integral controller. Once this had been implemented, the value of  $K_i$  was altered and its effects on the system could be analysed.

Furthermore, the redesigned control system was then tested by varying a key parameter which had previously remained constant, in this case the deflection of the upper arm ( $\theta_U$ ). The varying values of  $\theta_U$  were found by interpolating data points of the upper arm angle at specific times. This data was then implemented into MATLAB to show how the system responds.

Proper tuning of control systems is crucial as it optimizes the response of a system, ensuring stability and efficiency. Implementing dynamic parameters (e.g. varying  $\theta_U$  over time) into the model reflects real-world scenarios where system dynamics change over time. This in turn enhances the adaptability of the model making it more useful in industry applications.

### Control System Design & Implementation

#### 2.1 $G_c$ Control Gain Variation Results & Analysis

The first attempt to improve the control system was by altering the  $G_c$  value which had already been implemented withing the MATLAB script. The aim is to reach the desired deflection angle of  $55^\circ$  as quickly as possible without overshoot. Initially the value of  $G_c$  was increased from 3 to 4. This caused the forearm deflection to oscillate with increasing amplitude each period meaning the system is unstable (figure 1). Hence, the value of  $G_c$  was decreased.

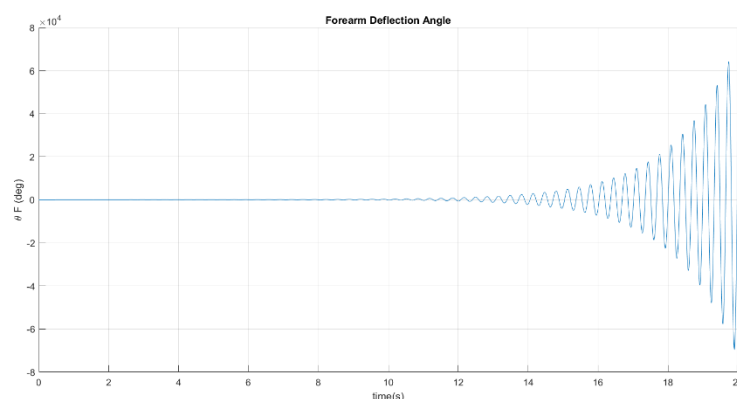


Figure 1 - Forearm deflection using a value of  $G_c = 4$

After testing multiple values, it was found that values between 0.1 and one produced the most desirable results and so these values were plotted against each other to find a final optimal value (figure 2).

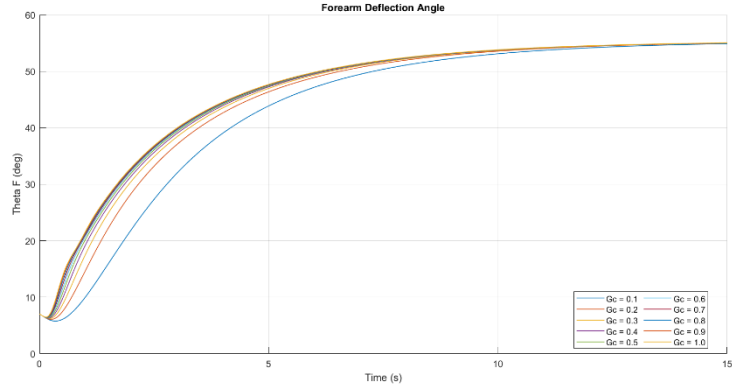


Figure 2 - Comparison of forearm deflection using values  $G_c = 0.1, 1$

While figure 2 shows that larger values closer to 1 provide shorter settling times, figure 3 shows that values over 0.2 cause overshoot within the gear and actuator. Although a fast settling time is desirable, accuracy in movement is paramount in robotic applications. Hence, a value of  $G_c = 0.2$  was chosen to give the shortest settling time whilst removing overshoot from the system.

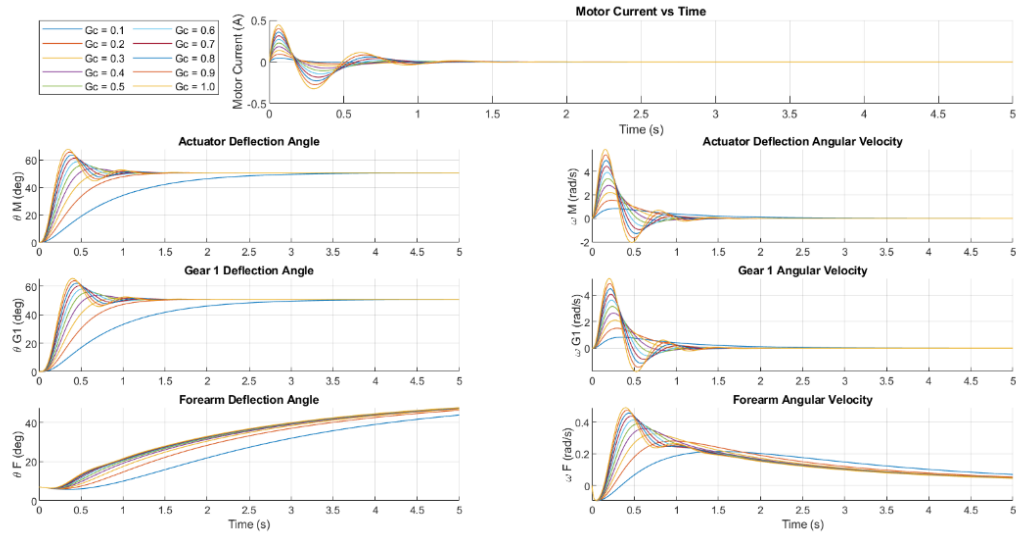


Figure 3 - System results using values  $G_c = 0.1, 1$

The final response of the system using a value of  $G_c = 0.2$  can be seen in figure 4.

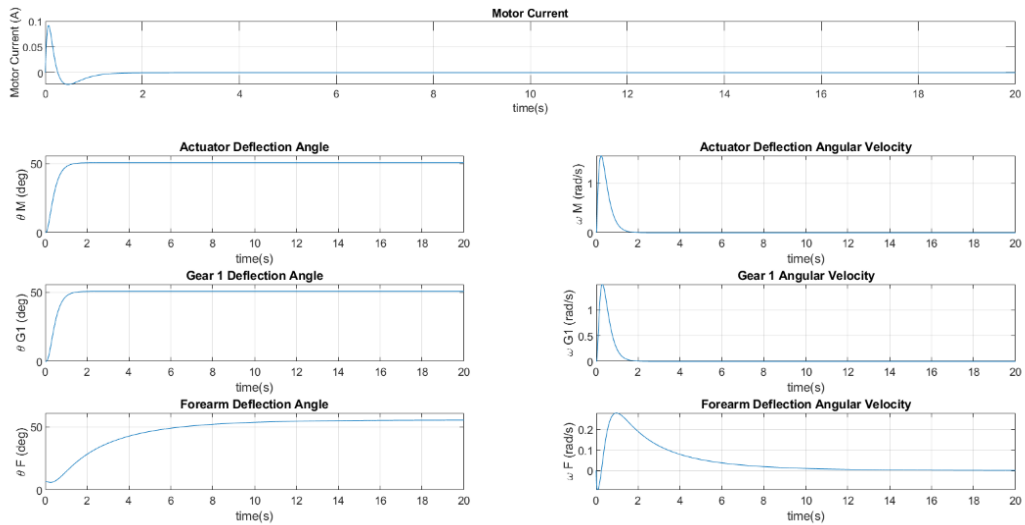


Figure 4 - State variables when implementing  $G_c = 0.2$

## 2.2 Integration Implementation in Control System in MATLAB Code $K_i$ Control Gain Variation Results & Analysis

After finding an optimal value for  $G_c$ , an integral term was introduced into the controller to try and further improve the system. The addition of this term creates a proportional-integral (PI) controller. Using equation 2 from the assignment brief, the MATLAB script was altered (figure 5). The integral term of the PI controller reacts to the accumulation of past errors to eliminate steady-state errors which lead to offset in the final settled value.

```
Delta_Theta = (Theta_Ref * Kr) - (x(2) * Ks);  
Integral_DTheta = Integral_DTheta + (stepsize * Delta_Theta);  
Ve = (Gc * Delta_Theta) + (Gc*Ki*Integral_DTheta);  
Va = (Ve * Kg);
```

Figure 5 - Implementing PI controller into MATLAB code

Multiple values of  $K_i$  were tested while keeping  $G_c$  at 0.2. It was found that increasing the value of  $K_i$  reduces the settling time of the forearm deflection angle (figure 6).

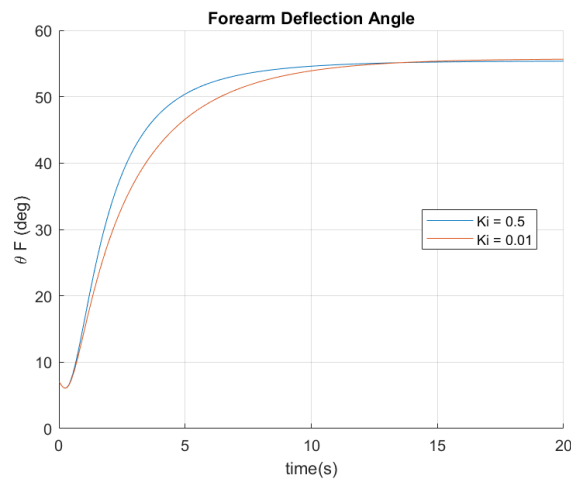


Figure 6 - Comparison of forearm deflection when using  $K_i$  values of 0.5 vs 0.01

However, this higher value of  $K_i$  introduces overshoot within the gear and the actuator (figure 7). Thus, it was judged that the PI controller had a negative impact on the system as although it reduces settling time, the accuracy of the system is compromised. Due to this a small value of  $K_i$  (0.01) was chosen.

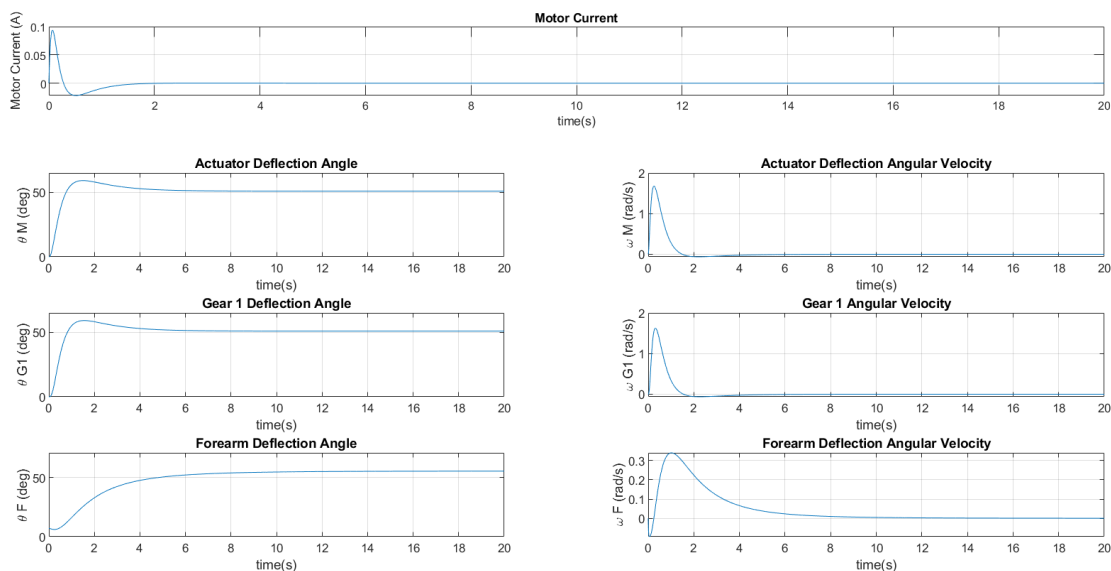


Figure 7 - State variables when implementing  $K_i = 0.5$

To further improve the system, a proportional-integral-derivative (PID) controller could be implemented. Adding a derivative term predicts future errors which reduces the response time and overshoot in the system. This would allow for a shorted settling time without compromising on the accuracy of the movement of the forearm. These characteristics make PID controllers good for high speed, high accuracy applications.

## Interpolation

### 2.3 Interpolation Algorithm Calculation

To take the motion of the upper arm into consideration, the system was altered to include a varying value of  $\theta_U$ . This allows us to examine the forearm control system in a dynamic environment. The values of  $\theta_U$  interpolated from the given data points in Appendix B of the assignment brief. This was done using Newton's divided difference (figure 8).

t(time)	$\theta_U[ ]$	$\theta_U[ , ]$	$\theta_U[ , , ]$	$\theta_U[ , , , ]$	$\theta_U[ , , , , ]$	$\theta_U[ , , , , , ]$
0	3.0	$\theta_U(t_0, t_1) = \frac{10.5-3.0}{2.5-0} = 3$				
2.5	10.5	$\theta_U(t_1, t_2) = \frac{25.5-10.5}{6.5-2.5} = \frac{15}{4}$	$\theta_U(t_0, t_1, t_2) = \frac{15/4 - 3}{6.5-0} = \frac{3}{26}$			
6.5	25.5	$\theta_U(t_2, t_3) = \frac{30-25.5}{17-6.5} = \frac{4.5}{10.5}$	$\theta_U(t_1, t_2, t_3) = \frac{25.5-10.5}{6.5-2.5} - \frac{3}{26} = \frac{93}{406}$	$\theta_U(t_0, t_1, t_2, t_3) = \frac{93/406 - 3/26}{17-0} = -\frac{909}{44863}$		
17	30	$\theta_U(t_3, t_4) = \frac{37-30}{22.5-17} = \frac{7}{5.5}$	$\theta_U(t_2, t_3, t_4) = \frac{30-25.5}{6.5-2.5} - \frac{93}{406} = \frac{65}{1251}$	$\theta_U(t_1, t_2, t_3, t_4) = \frac{65/1251 - (-93/406)}{22.5-2.5} = 0.01409$	$\theta_U(t_0, t_1, t_2, t_3, t_4) = \frac{0.01409 - (-909/44863)}{22.5-0} = 1.5267 \times 10^{-3}$	
22.5	37	$\theta_U(t_4, t_5) = \frac{50.5-37}{28-22.5} = \frac{13.5}{5.5}$	$\theta_U(t_3, t_4, t_5) = \frac{37-30}{5.5} - \frac{7}{5.5} = \frac{65}{1251}$	$\theta_U(t_2, t_3, t_4, t_5) = \frac{13.5/5.5 - 65/1251}{28-6.5} = \frac{741}{291363}$	$\theta_U(t_1, t_2, t_3, t_4, t_5) = \frac{741/291363 - 0.01409}{28-2.5} = -4.5282 \times 10^{-4}$	$\theta_U(t_0, t_1, t_2, t_3, t_4, t_5) = \frac{-4.5282 \times 10^{-4} - 1.5267 \times 10^{-3}}{28-0} = -7.0697 \times 10^{-5}$
28	50.5					

Figure 8 – Newton's divided difference table

The final values of the divided differences can be seen in table 1.

t (Time)	$\theta_U[ ]$	$\theta_U[ , ]$	$\theta_U[ , , ]$	$\theta_U[ , , , ]$	$\theta_U[ , , , , ]$	$\theta_U[ , , , , , ]$
0	3					
		3				
2.5	10.5		0.115			
		3.75		-0.0203		
6.5	25.5		-0.229		0.00153	
		0.429		0.0141		-0.0000707
17.0	30		0.0528		-0.000453	
		1.273		0.00254		
22.5	37		0.107			
		2.455				
28.0	50.5					

Table 1 - Final divided difference table

Once the divided differences had been calculated, they were put into the nested form to give the final polynomial (figure 9). This expression can be used to approximate  $\theta_U$  at the times between the data points.

$$P(t) = 3 + 3(t-0) + 0.115(t-0)(t-2.5) - 0.0203(t-0)(t-2.5)(t-6.5) + 0.00153(t-0)(t-2.5)(t-6.5)(t-17) - 0.0000707(t-0)(t-2.5)(t-6.5)(t-17)(t-22.5)$$

Figure 9 - Interpolated polynomial derived from Newton's Divided Differences

### 2.4 Interpolation MATLAB Code, Results & Analysis

The polynomial was implemented into MATLAB as shown in figure 10.

```

% Interpolation data
t = [0, 2.5, 6.5, 17, 22.5, 28]; % Time data points
Theta_U_values = deg2rad([3, 10.5, 25.5, 30, 37, 50.5]); % Convert to radians
interpol = [3, 3, 0.115, -0.0203, 0.00153, -0.0000707]; % Coefficients

% Dynamic Simulation Loop
for time = 0:stepsize:EndTime

    % Interpolated Theta_U using nested polynomial form
    Theta_U = interpol(1) + ...
        interpol(2) * (time - t(1)) + ...
        interpol(3) * (time - t(1)) * (time - t(2)) + ...
        interpol(4) * (time - t(1)) * (time - t(2)) * (time - t(3)) + ...
        interpol(5) * (time - t(1)) * (time - t(2)) * (time - t(3)) * (time - t(4)) + ...
        interpol(6) * (time - t(1)) * (time - t(2)) * (time - t(3)) * (time - t(4)) * (time - t(5));

```

Figure 10 - Implementing polynomial in MATLAB code

Plotting the varying value of  $\theta_U$  against time shows the movement of the upper arm (figure 11). The response of the system to the varying value of  $\theta_U$  can be seen in figure 12.

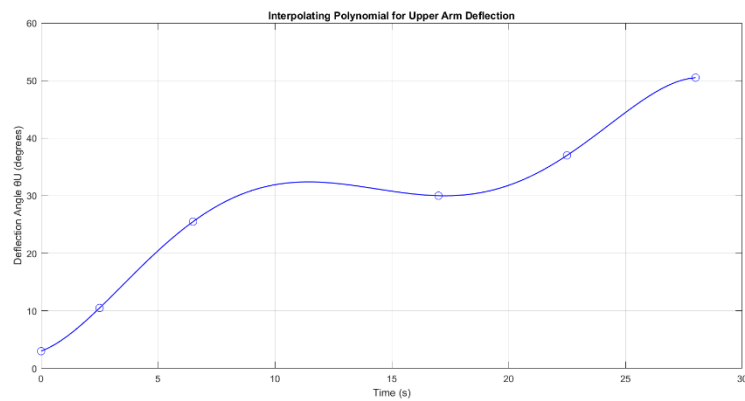


Figure 11 - Interpolated  $\theta_U$  against time

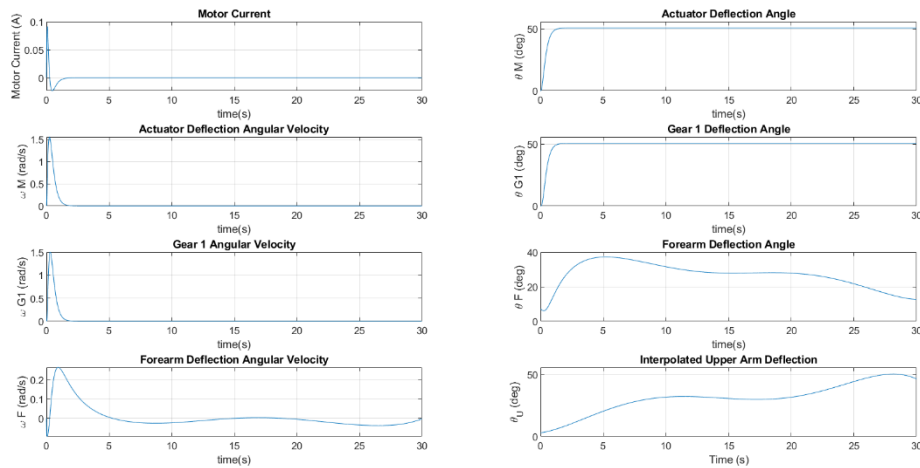


Figure 12 - State variables when implementing a variable value of  $\theta_U$

## 2.5 Conclusions

In conclusion, the control system was significantly improved by tuning  $G_c$  with the optimal value of 0.2 balancing a reduced settling time with stability. The addition of an integral term to the control system allowed for faster settling times for the forearm deflection however, as the value of  $K_I$  is increased, overshoot is introduced to the system and thus it was kept small at 0.01. The control system could be further improved by implementing a PID controller for faster responses whilst reducing overshoot. The implementation of a varying value of  $\theta_U$  improves the realism of the system allowing it to adapt to dynamic environments. Implementing other dynamic parameters could further enhance the model.