JULES.jl

Tristan Abbott, Ali Ramadhan, and Raphael Rousseau-Rizzi

June 19, 2019

1 Equation Set

The equation set is written in terms of five prognostic conservative variables: three momenta, mass density, and specific entropy. While defining and deriving these equations, it will prove convenient to define a 4-vector $u^{\alpha} = (1, u, v, w)$ for $\alpha = (t, x, y, z)$. This allows us to write a conservation law for a variable ϕ as

$$\partial_t \rho \phi + \partial_i \rho u_i \phi = \partial_\alpha \rho u^\alpha \phi = \text{ sources and sinks.}$$

Because mass conservation written in this form is just

$$\partial_{\alpha}\rho u^{\alpha} = 0, \tag{1}$$

this immediately provides some useful properties, namely that

$$\partial_{\alpha}\rho u^{\alpha}\phi = \rho u^{\alpha}\partial_{a}\phi$$

and

$$u^{\alpha}\partial_{\alpha}\rho = -\rho\partial_{\alpha}u^{\alpha}.$$

Written with this notation, and using $\tau^{(i)}$ to denote the stress tensor for component i, the momentum equations are

$$\partial_{\alpha}\rho u^{\alpha}u = -\partial_{x}p - \boldsymbol{\nabla}\cdot\boldsymbol{\tau}^{(x)} \tag{2}$$

$$\partial_{\alpha}\rho u^{\alpha}v = -\partial_{y}p - \boldsymbol{\nabla} \cdot \boldsymbol{\tau}^{(y)} \tag{3}$$

$$\partial_{\alpha}\rho u^{\alpha}w = -\partial_{z}p - \rho g - \boldsymbol{\nabla}\cdot\boldsymbol{\tau}^{(z)} \tag{4}$$

(5)

To derive an equation for specific entropy

$$s = s_0 + c_v \ln \left(\frac{T}{T_0}\right) - R \ln \left(\frac{\rho}{\rho_0}\right),$$

we can write its conservation law as

$$\partial_{\alpha}\rho u^{\alpha}s = \partial_{\alpha}\rho u^{\alpha}c_{v}\ln\left(\frac{T}{T_{0}}\right) - \partial_{\alpha}\rho u^{\alpha}R\ln\left(\frac{\rho}{\rho_{0}}\right)$$
$$= \frac{1}{T}\partial_{\alpha}\rho u^{\alpha}c_{v}T - \frac{R}{\rho}\partial_{\alpha}\rho u^{\alpha}\rho.$$

The first law of thermodynamics allows us to express $\partial_{\alpha}\rho u^{\alpha}c_{v}T$ (a conservation law for the internal energy) in terms of a heating rate $Q - \nabla \cdot J + \epsilon$ (which includes contributions from diabatic heating Q, convergence of conductive heat fluxes J, and dissipation ϵ) and a work rate $-p\nabla \cdot \mathbf{u}$. Substituting this back into the entropy equation gives

$$\partial_{\alpha}\rho u^{\alpha}s = \frac{1}{T}(Q - \nabla \cdot J + \epsilon - p\nabla \cdot \mathbf{u}) - \frac{R}{\rho}\partial_{\alpha}\rho u^{\alpha}\rho$$

$$= \frac{1}{T}(Q - \nabla \cdot J + \epsilon - p\nabla \cdot \mathbf{u}) - Ru^{\alpha}\partial_{\alpha}\rho$$

$$= \frac{1}{T}(Q - \nabla \cdot J + \epsilon - p\nabla \cdot \mathbf{u}) + R\rho\partial_{\alpha}u^{\alpha}$$

$$= \frac{1}{T}(Q - \nabla \cdot J + \epsilon - p\nabla \cdot \mathbf{u}) + \frac{p}{T}\nabla \cdot \mathbf{u}$$

$$= \frac{1}{T}(Q - \nabla \cdot J + \epsilon).$$

We probably could have written this equation down without going through the derivation, but the derivation might be a useful starting point when we eventually try to derive equations for moist entropy (which will be much more complicated).

In summary, our equation set is

$$\partial_{\alpha}\rho u^{\alpha} = 0 \tag{6}$$

$$\partial_{\alpha}\rho u^{\alpha}u = -\partial_{x}p - \boldsymbol{\nabla}\cdot\boldsymbol{\tau}^{(x)} \tag{7}$$

$$\partial_{\alpha}\rho u^{\alpha}v = -\partial_{\nu}p - \nabla \cdot \tau^{(y)} \tag{8}$$

$$\partial_{\alpha}\rho u^{\alpha}w = -\partial_{z}p - \rho g - \boldsymbol{\nabla}\cdot\boldsymbol{\tau}^{(z)} \tag{9}$$

$$\partial_{\alpha}\rho u^{\alpha}s = \frac{1}{T}(Q - \nabla \cdot J + \epsilon) \tag{10}$$

In addition to these prognostic equations, we need a set of diagnostic equations that relate $T, p, \tau, Q, \mathbf{J}$, and ϵ to prognostic fields. Diagnostic equations for p and T can be obtained from the definition of s and the ideal gas law, Q is typically provided by model "physics", and \mathbf{J} , τ , and ϵ are provided by a sub-grid-scale turbulence closure.

2 Time integration