

# Progress Report

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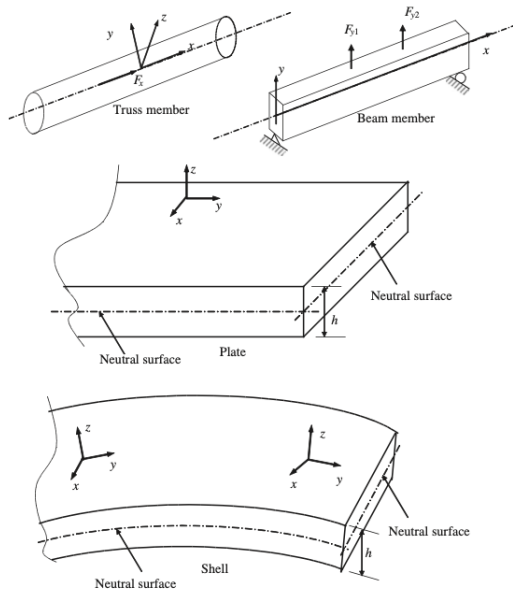
# What to Solve

We seek to solve dynamic equilibrium equations. The formulation from Liu and Quek assumes among other things:

- ① *Linear Elastic* Deformation grows proportionally with external force.
- ② *Isotropic* Material property is direction independent.

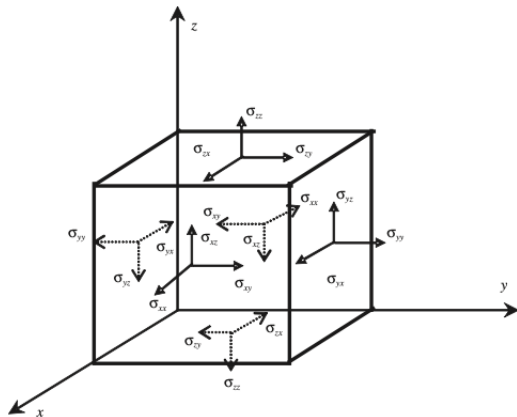
We distinguish between four kinds of objects: beams, trusses, plates and shells.

# What to Solve



# What to Solve

Taking a queue from Liu and Quek, we start off by defining DEE for an idealized infinitesimal, linearly elastic, isotropic material.



Observe that because of equilibrium  $\sigma_{xy} = \sigma_{yx}$ ;  $\sigma_{xz} = \sigma_{zx}$ ;  $\sigma_{yz} = \sigma_{zy}$   
 Which give us the stress tensors:  $\sigma^T = \{\sigma_{xx}, \sigma_{yy}, \sigma_{zz}, \sigma_{yz}, \sigma_{xz}, \sigma_{xy}\}$

# What to Solve

We also get six strain components  $\epsilon^T = \{\epsilon_{xx}, \epsilon_{yy}, \epsilon_{zz}, \gamma_{yz}, \gamma_{xz}, \gamma_{xy}\}$  Where:

$$\epsilon_{xx} = \frac{\partial u}{\partial x}; \quad \epsilon_{yy} = \frac{\partial v}{\partial y}; \quad \epsilon_{zz} = \frac{\partial w}{\partial z};$$

$$\gamma_{xy} = 2\epsilon_{xy} = \frac{\partial u}{\partial y} + \frac{\partial v}{\partial x};$$

$$\gamma_{xz} = 2\epsilon_{xz} = \frac{\partial u}{\partial z} + \frac{\partial w}{\partial x};$$

$$\gamma_{yz} = 2\epsilon_{yz} = \frac{\partial v}{\partial z} + \frac{\partial w}{\partial y};$$

# What to Solve

Provided  $\mathbf{U} = \begin{pmatrix} u \\ v \\ w \end{pmatrix}$  the displacement matrix we get the system  $\epsilon = \mathbf{L}\mathbf{U}$

Where the differential operator is:  $\mathbf{L} = \begin{pmatrix} \frac{\partial}{\partial x} & 0 & 0 \\ 0 & \frac{\partial}{\partial y} & 0 \\ 0 & 0 & \frac{\partial}{\partial z} \\ 0 & \frac{\partial}{\partial z} & \frac{\partial}{\partial y} \\ \frac{\partial}{\partial z} & 0 & \frac{\partial}{\partial x} \\ \frac{\partial}{\partial y} & \frac{\partial}{\partial x} & 0 \end{pmatrix}$

# What to solve

For an external force in the  $y$  direction the equilibrium forces are:

$$(\sigma_{xx} + d\sigma_{xx})dydz - \sigma_{xx}dydz + (\sigma_{yx} + d\sigma_{yx})dxdz - \sigma_{yx}dxdz + (\sigma_{zx} + d\sigma_{zx})dxdy - \sigma_{zx}dxdy + f_x dxdydz = \rho \ddot{u} dxdydz \quad (1)$$

But since:

$$d\sigma_{xx} = \frac{\partial \sigma_{xx}}{\partial x} dx, d\sigma_{yx} = \frac{\partial \sigma_{yx}}{\partial y} dy, d\sigma_{zx} = \frac{\partial \sigma_{zx}}{\partial z} dz \quad (2)$$

Substituting (2) into (1) gives us:

$$\frac{\partial \sigma_{xx}}{\partial x} + \frac{\partial \sigma_{yx}}{\partial y} + \frac{\partial \sigma_{zx}}{\partial z} + f_x = \rho \ddot{u} \quad (3)$$



# What to solve

Using analogous equations for different directions,  $y$  and  $z$ , we get:

$$\begin{aligned}\frac{\partial \sigma_{xy}}{\partial x} + \frac{\partial \sigma_{yy}}{\partial y} + \frac{\partial \sigma_{zy}}{\partial z} + f_y &= \rho \ddot{v} \\ \frac{\partial \sigma_{xz}}{\partial x} + \frac{\partial \sigma_{yz}}{\partial y} + \frac{\partial \sigma_{zz}}{\partial z} + f_z &= \rho \ddot{w}\end{aligned}$$

Yielding the linear system:

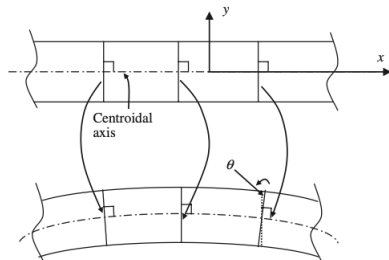
$$L^T \sigma + f_b = \rho \ddot{U} \quad (4)$$

And since Hooke's Law states  $\sigma = c\epsilon$  we can further simplify to:

$$L^T c L U + f_b = \rho \ddot{U}$$

# What to Solve

For beams, the ruling paradigm is *Euler-Bernoulli* beam theory. This assumes that transverse sections of the beam remain normal to the centroidal axis.



Leads to assumption:  $\gamma_{xy} = 0, u = -y\theta, \theta = \frac{\partial v}{\partial x}$

# What to Solve

Leading us to conclude

$$\epsilon_{xx} = \frac{\partial u}{\partial x} = \frac{\partial(-y\theta)}{\partial x} = -y \frac{\partial \theta}{\partial x} = -y \frac{\partial^2 v}{\partial x^2} = -yLv \quad (5)$$

With differential operator:  $L = \frac{\partial^2}{\partial x^2}$

Recall that Hooke's Law then says  $\sigma_{xx} = E\epsilon_{xx}$

Substituting (5) into Hooke's Law then gives:

$$\sigma_{xx} = -yELv \quad (6)$$

Following further moment derivations from Liu and Quek, the dynamic equilibrium equations for beam is then:

$$EI \frac{\partial^4 v}{\partial x^4} = F_y \quad (7)$$

General structure of a deal.ii step.

- 1 include deal.ii headers
- 2 Create class `StepN` with public methods `StepN()`, `run()` and private methods `make_grid()`, `setup_system()`, `assemble_system()`, `solve()`, `output_results()`, and attributes often `Triangulation<dim>`, `FE_Q <dim>`, `DoFHandler<dim>`
- 3 Define the methods outside, sometimes all encapsulated in a template for dimension independent programming.

# How to Solve It

```
23 > #include <deal.II/grid/tria.h> --  
48  
49 using namespace dealii;  
50  
51  
52  
53 > class Step3 --  
78  
79 > Step3::Step3() --  
83  
84 > void Step3::make_grid() --  
91  
92 > void Step3::setup_system() --  
107  
108 > void Step3::assemble_system() --  
166  
167 > void Step3::solve() --  
174  
175 > void Step3::output_results() const --  
185  
186 > void Step3::run() --  
194  
195 > int main() --  
204
```

# How to Solve It

Results of solving Laplace Equation on Different Domains:

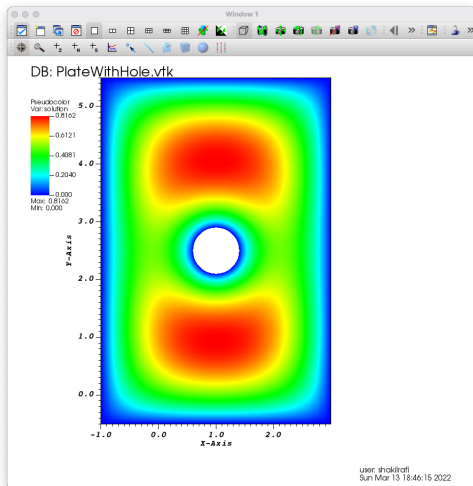


Figure: Plate with one hole

# How to Solve It

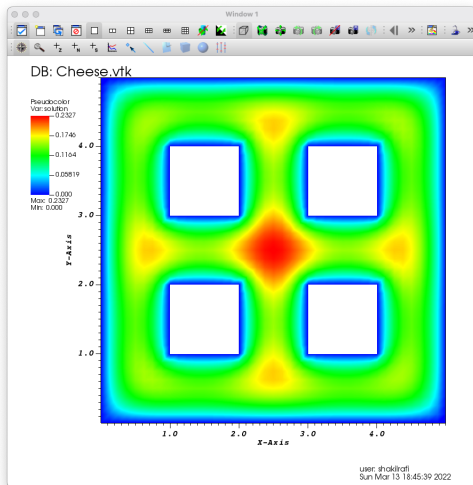


Figure: Cheese domain

