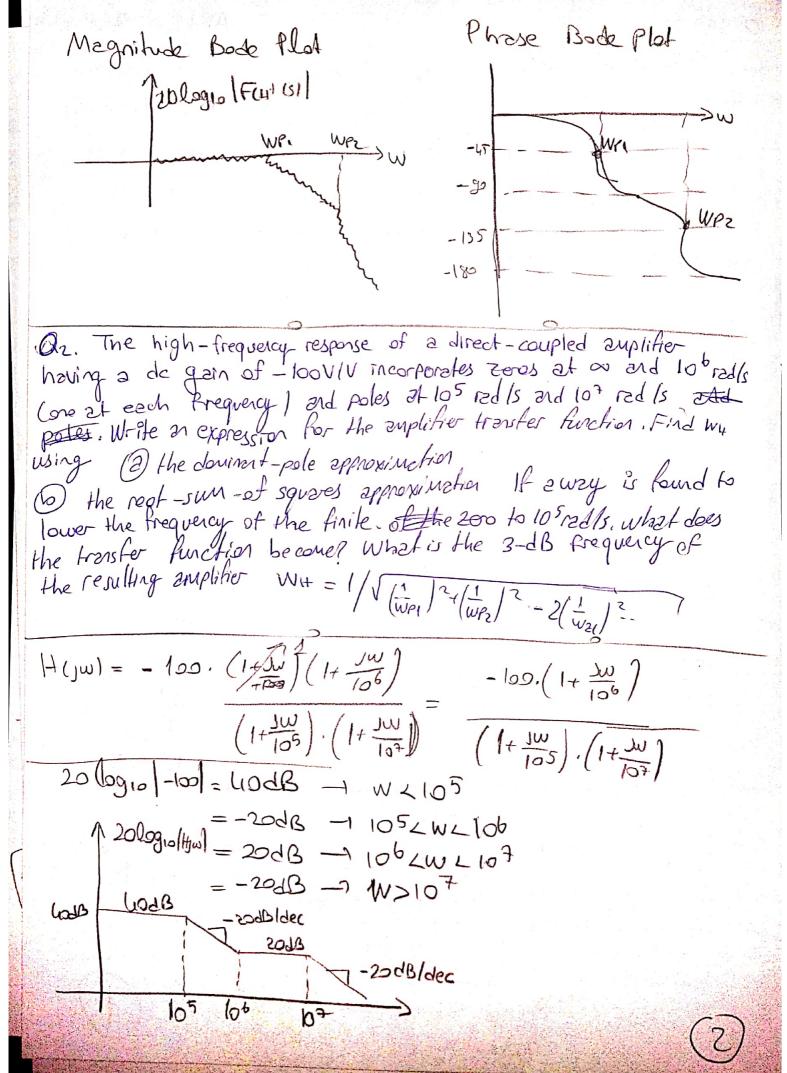
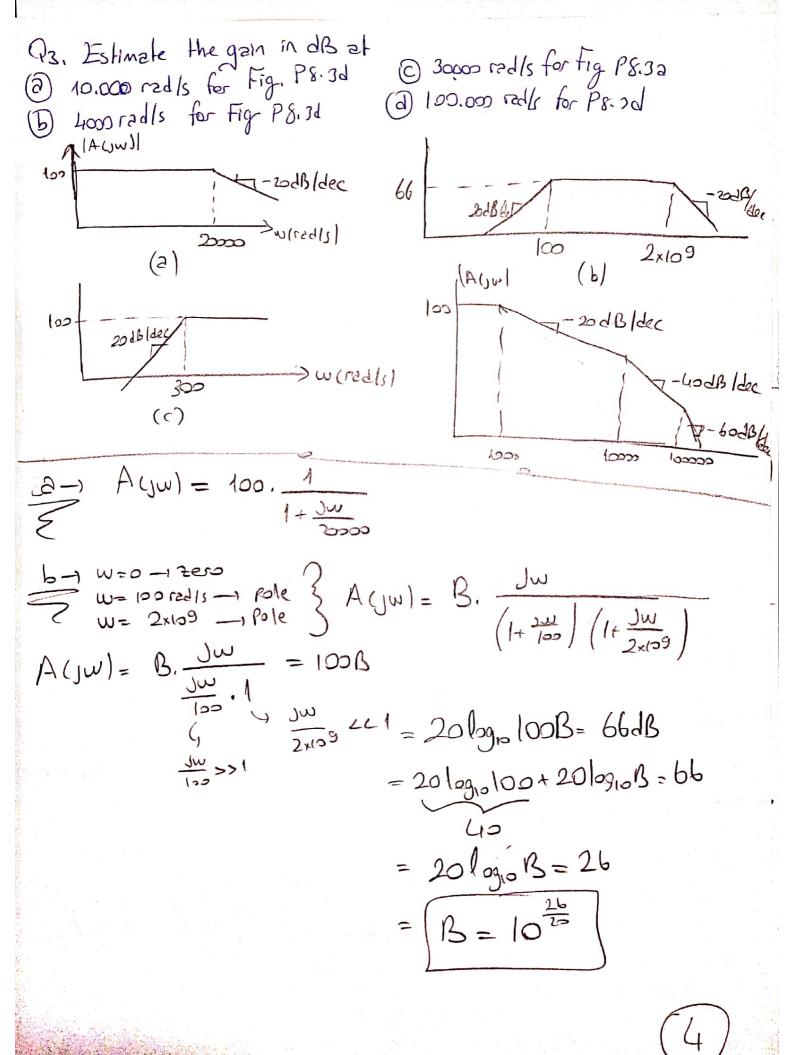
Abdullah MENTSOGLU # HW O4 Q1. Consider 2n amplifier whose  $F_A(S)$  is given by law.  $F_A(S) = \frac{4}{(1+\frac{S}{wp_1})\left(1+\frac{S}{wp_2}\right)} \text{ for which the value of the 3dB frequency}$ wh calculated using the dominant pole approximation differs from that calculated using root sum of squares formula by (2) 10% to 1%  $WW = \left[ \sqrt{\frac{1}{w_{p_1}^2} + \frac{1}{w_{p_2}^2} + \dots} \right] - 2 \cdot \left( \frac{1}{w_{z_1}^2} + \frac{1}{w_{z_{\overline{z}}}} \right) \right]$  $FH (S) = \frac{1}{\left(1 + \frac{S}{WP1}\right) \left(1 + \frac{S}{WP2}\right)} WP1 \times WP2 \longrightarrow WH \approx WP1$ WH = VPA WPA = WPA (WP)2 VI+ (WP)2 WPA)2  $\frac{\Delta W_{H}}{W_{PA}} = 1 - \frac{1}{\sqrt{1 + (\frac{W_{PA}}{W_{PA}})^{2}}} = 1 - \frac{1}{\sqrt{1 + \frac{1}{N^{2}}}} = \frac{1}{\sqrt{1 + \frac{1}{N^{2}}}}} = \frac{1}{\sqrt{1 + \frac{1}{N^{2}}}} = \frac{1}{\sqrt{1 + \frac{1}{N^{2}}}}} = \frac{1}{\sqrt{1 + \frac{1}{N^{2}}}} = \frac{1}{\sqrt{1 + \frac{1}{N^{2}}}} = \frac{1}{\sqrt{1 + \frac{1}{N^{2}}}} = \frac{1}{\sqrt{1 + \frac{1}{N^{2}}}} = \frac{1}{\sqrt{1 + \frac{1}{N^{2}}}}} = \frac{1}{\sqrt{1 + \frac{1}{N^{2}}}} = \frac{1}{\sqrt{1 + \frac{1}{N^{2}}}}} = \frac{1}{\sqrt{1 + \frac{1}{N^{2}}}} = \frac{1}{\sqrt{1 + \frac{1}{N^{2}}}} = \frac{1}{\sqrt{1 + \frac{1}{N^{2}}}}} =$  $\frac{1}{1+\frac{1}{n^2}} = 1.2345$   $\frac{1}{1+\frac{1}{n^2}} = 1.2345$   $\frac{1}{1+\frac{1}{n^2}} = 1.2345$  $V_{1+\frac{1}{02}} = 1.0101$  $n^2 = \frac{1}{0.0203} = 49.251$   $n^2 = 4.2631$  n = 2.064 $1+\frac{1}{n^2}=1.0203$ dolays (-) It ofmor



Lose frelesis Wh =  $\sqrt{\left(\frac{1}{105}\right)^{2} + \left(\frac{1}{105}\right)^{2} - 2\left(\frac{1}{105}\right)^{2}} = 1.01 \times 10^{\frac{5}{105}}$ MH =105159/5 WH = 1.01 x105 red 106 ve 105 zero tes (1+ Ju) = 1+ Ju 105 Hrew (Jw) = -100 1+ Jw WHMEN = 10 red/s FACSI = (1+ 5 WZZZ) . (1+ 5 WZZZ) \_\_\_\_\_ S-JW (1+ 2), (1+ 5) [FH(JW)]= (1+ W2) (1+ W2) (1+ W2) WH 3dB freq. (1+w2). (1+ WZ) DC Power of FA JWZ-1 halved \_1 10 leg10 ( 1 ) = -3dB  $\left| \left[ \operatorname{Fir}(Jw) \right]^{2} = \frac{1}{2} = \left( 1 + \left( \frac{w_{H}}{w_{H}} \right)^{2} \right) \left( 1 + \left( \frac{w_{H}}{w_{H}} \right)^{2} \right)$ (1+(MH)2)(1+(MH)2) WHI V 1 + 1 - 2 ( 1 + 1 ) = 1 general formal



(-) 
$$w=0$$
 ->  $2ero$   $A(yw) = B$   $\frac{Jw}{1+\frac{Jw}{300}}$  for  $w>300$  rad/s

 $A(yw) \stackrel{\sim}{=} B \frac{Jw}{Jw} = 300B$ 
 $20lg_0.300B=100=20lg_0.300+20lg_0.0B$ 
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Stain 100,000 rad/s bu aralleta 1 dec de ددفره ا - دوده A (1000) Godb dusur Mesanyor. Maec/ A ( 100000) = A ( 10000) - 40 ( 10000) 1 dec'lik düsüs. A(JW/100,000) = 60-40 = 20dB Qu. Estimate the radian frequency where the gain is OdB For (c) fig P8.3d (a) Fig P8.3a (b) Fig P8.3c HUWI 5lope = -20dB/dec = 0-100dB / logio Wv - 19102000 logio Wu - 4.301 = -100 4.3010 Wu = 109.301 red/s (C) slope = +20dB | dec = 100dB - 0 = 1 log is 300-log in W1 : 5 10910 (300) - 10910 (Wu) 109,0Wu=-2,522 Wu=10-2,522 rad/5

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A (Ju) = Dolb =) logiow-5 = == -60dB/dec= 0-20dB 10910(w) - 1910(10000) 76 W3=105,33 -10 assume the capacitors are small valued, comparable to the internal capacitances of the transister, Compute the 3dB corner traguercy by the OCTC Method. Cin in gordiges dirence Rinidson ERD Pin = 125/1 1/8m CL NIN gordiguidirena Realson I an RL=ROll[Rp+10 (1+gmro)Rs] W3dB = 1 CIRINT CLRI

W3 dB = 1 Cin.(RS/1/gm) + CL (RD/1/ro(1+gmro)Rs) Q6. Assume the capacitors are small valued, composable to the substance capacitances of the transitor. Compute the 3dB corner frequency by the OCTC Method.

Cin in gardigio direct Rin olson

Cin I 3er

Cin I 4 gmiologo

WadB = 1 0ctc Method

WadB = 1 0ctc Method

Cin Rs + Cl. (2d/1 [loop (1+gmio)Rp]) //