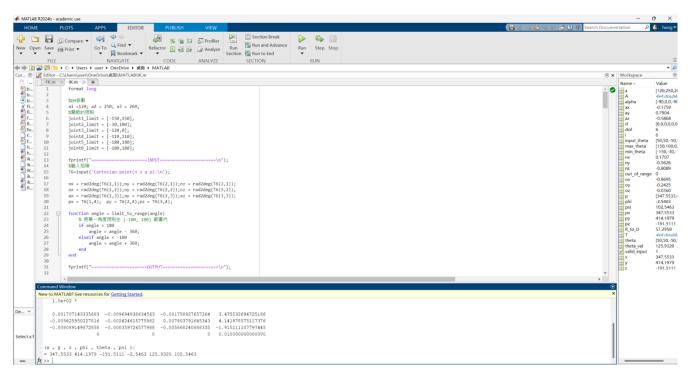
# 機器人學 project1

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# 一、介面說明

開發平台: MATLAB



#### 開啟程式碼後依照下列程序:

- 1. 程式編輯視窗
- 2. 按下 "Run" 執行程式碼
- 3. 在終端機中輸入要執行的程式
- 4. 依照指示輸入變數後按 "Enter"

## 二、程式架構說明

(x , y , z , phi , theta , psi ):

= 577.8388 210.3161 -85.5050 -51.1183 96.7177 91.1183

## Fk. m

```
% DH Model - Puma 560
d = [0, 0, 0, 0, 0, 0];
a = [120, 250, 260, 0, 0, 0];
alpha = [-90, 0, 0, -90, 90, 0];
theta = [0, 0, 0, 0, 0, 0];
max_theta = [150, 100, 0, 110, 180, 180];
min_theta = [-150, -30, -120, -110, -180, -180];
% calculate the transformation matrices
for i = 1:6
   A = [cosd(theta(i)), -sind(theta(i)) * cosd(alpha(i)), sind(theta(i)) * sind(alpha(i)), a(i) * cosd(theta(i)); sind(theta(i)), cosd(theta(i)) * cosd(theta(i)) * sind(alpha(i)), a(i) * sind(theta(i));
       0,
                      sind(alpha(i)),
                                                  cosd(alpha(i)),
   0,
T = T * A;
                      0,
                                                      0,
                                                                                       1];
執行程式後,可以看到
Forward kinematics
Please enter the joint variable (in rad):
theta1, theta2, theta3, theta4, theta5, theta6:
輸入 6 個(角度)來得到轉移矩陣 T6(我自行將弧度轉角度)
測資一:
[20 20 -20 20 20 20]
得到輸出:
[n o a p]:
   1.0e+02 *
   0.007797282437679 \quad -0.006258180148738 \quad -0.000193824180657 \quad 5.778387512885174
  -0.000582222717775 \quad -0.001032939777916 \quad 0.009929453767560 \quad 2.103161056745715
  -0.006234051916208 \quad -0.007730990663630 \quad -0.001169777784405 \quad -0.855050358314172
                                                                  0 0.010000000000000
                     0
                                           0
```

#### 測資二:

[50 50 -50 50 50 50 50]

#### 得到輸出:

## Ik. m

程式架構如程式中註解說明(由於程式過於冗長,故此不附上)

程式執行後,可輸入末端 Cartesian space 座標(n,o,a,p)

按下 enter 後得到 8 組 IK 的解,以及各軸是否超出工作限制的結果:

#### 測資一:

```
Cartesian point(n o a p):
[0.5756 -0.2398 -0.7817 177.8;
0.7738 -0.1494 0.6156 308;
-0.2644 -0.9593 0.0996 -140.1
0 0 0 1.0000;]
```

#### 測資二:

```
Cartesian point(n o a p):
                             _____
[0.1736 0.0000 -0.9848 0.0000;
0.8529 0.5000 0.1504 325.2;
0.4924 -0.8660 0.0868 -158
0 0 0 1.0000;]
======OUTPUT=======
your theta_list1 is:
joint3 is out of range!
joint4 is out of range!
60.003 -28.531 115.004 -121.456 10.005 -49.981
_____
your theta list2 is:
joint3 is out of range!
60.003 -28.531 115.004 58.544 -10.005 130.019
_____
your theta list3 is:
60.003 89.999 -115.004 -9.978 10.005 -49.981
_____
your theta_list4 is:
joint4 is out of range!
60.003 89.999 -115.004 170.022 -10.005 130.019
_____
your theta list5 is:
joint2 is out of range!
joint3 is out of range!
-119.997 149.781 27.071 38.131 169.995 130.019
_____
your theta_list6 is:
joint2 is out of range!
joint3 is out of range!
joint4 is out of range!
-119.997 149.781 27.071 -141.869 -169.995 -49.981
_____
your theta_list7 is:
joint2 is out of range!
-119.997 177.394 -27.071 64.661 169.995 130.019
_____
your theta list8 is:
joint2 is out of range!
joint4 is out of range!
-119.997 177.394 -27.071 -115.339 -169.995 -49.981
```

```
your theta list1 is:
joint3 is out of range!
joint4 is out of range!
90.000 -23.812 119.002 -125.180 10.000 0.008
_____
your theta list2 is:
joint3 is out of range!
90.000 -23.812 119.002 54.820 -10.000 -179.992
_____
your theta_list3 is:
90.000 99.003 -119.002 -9.992 10.000 0.008
_____
your theta list4 is:
joint4 is out of range!
90.000 99.003 -119.002 170.008 -10.000 -179.992
_____
your theta list5 is:
joint2 is out of range!
joint3 is out of range!
-90.000 137.862 44.283 27.846 170.000 -179.992
_____
your theta list6 is:
joint2 is out of range!
joint3 is out of range!
joint4 is out of range!
-90.000 137.862 44.283 -152.154 -170.000 0.008
_____
your theta list7 is:
joint2 is out of range!
-90.000 -176.941 -44.283 71.214 170.000 -179.992
_____
your theta_list8 is:
joint2 is out of range!
-90.000 -176.941 -44.283 -108.786 -170.000 0.008
```

## 三、數學運算說明、推導

	CAn	-Sancoln Cancoln	SânSoan -CânSoa	ancer						
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	0	Sten	CNM							
		0	0	J						
	ردا	0	- S <sub>1</sub>	1x0C,7	C4	0 -54				
A۱۶	51			12051	A4= S+	0 64	0			
	0	-1	0	0	0	-1 0	0			
	Lo	0	D	1	Lo	0 0	) J			
	[42	-52	0,	60C2	A5: S5	0 55 0 -45 1 0	۰٦			
Aı-	52	C2		50 52	A5= S5	0 -45	0			
	0	0	1	0	0	0 0	0			
	Lo	0	0	1 )		0	1.J	_		
	rc3	-53	0 26063	1	r C6	-56	0 4	7		
A3=	0	0	0 26053 1 0		A6 = S6	CG	0 0			
	0		0 1.		1 °	0	) 0			
Į.	_	,	, ,	,	Co	0	0			
		Cx66	(1.0.					J		
		C866	-3665	55	0					
ASA	6=	526	-5556	-45	D					
		SL	-5x56 C6							
	-			Ø	0					
		0	0	0	1					
		,	-C.C	, l			-			
		ſί	200C4-243	56 - 4KS	LS-SXC	SIC4	0			
AFA	5A6€	5	4C2C6 +C45	56 -S456	Lx + L46	SoSK	0			
			-5566							
			- 2006		<u>γ-</u> 2τ	22	0			
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						٥				
			6	, ,	,			C	ascol	
۸	A A		Cofface	-23426	-			C3455	CuSz	
143K	44A:	A6=	C3+656+ S2+656+ -556	456	- 51465	6 + GFCG		53455		
			-550	6	<b>&gt;</b> 5	56		C3	0	
		1	0			0		9	[ ]	
		0								1
			14C5-C6-SD14S		S6-Source	CastSS	250C2 1260C23	A3	C2C3-Q3S2S3+Q2C2	
A2A3	A4A5	A6= S.	otGGCC+GNFS6	-5214C55	6+6446	SayeSs	25052 +260523	ass	52C3+Q3C2S2+Q2S2	
		1.1	-554	555						
						Cs	0		0	
			0	0		0				1

- C 1	
Tb=[noap]	
Mx=4/(C2546666-525456)+S15566	
Mg S1 ( Last Cock - Sast S6) - C1 Sx C6	
Na = - Saay CoC6 - CastS6	
Dx=-C1(C200C556+520+C6)-515556	
0y= 51 (C244C556+5214C6)+45556	
02 = SastCxS6 -CastC6	
Ax=41625455-5165	
ag=5,Cu+55+465	
az=-S24S5	
Px = 120C1+250C1C2+260C1C23	
Py= 12051 +25051C2+26051C3	
R=-250S2-260S25	
Inverse kinematic:	
[ (2,5) 0 - 100 ] [ (2,5) 0 - 200 ] [ (3,5) 0 - 200 ] [ (3,5) 0 - 200 ]	. 0]
A) = (2 5 0 - 10 ) A) = (3 6 0 - 20) A) = (3 5 0 - 20) A) = (3 5 0 - 20) A) = (3 6 0	0 0
, , , , , , , , , , , , , , , , , , , ,	• 1]
[ 2 5 0 0 ] [ (4 5 0 0 ]	
Az = 6 5 4 0 0 Az = 5 6 6 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	
CI SI 0 -120 Mx Ox Ox R	936263-935253+9262
ATITE = -1 0   Mx 0x 0x 0x R	A3 52C3+ A2 C253+ A252
[000]][000]	0
) -P2 = a152C1+a3C2S5+a2S2 - @	
-PXSIT Py4 = 0 -3	
1	

02,52		= 1 81= tan-1 ( F			
() <sup>2</sup> +(2) <sup>2</sup>					
& (PXCI+	Py51-120)2	FLPZ)2 = 2602C32+	+2602532+2502+	2 (260×250624+26	0×2505223)
		= 260²+25	0°+2/250×26	0×43)	
) A	-1 ( CIR-	+519y-120)+ 12-250	- 260 <sup>2</sup>	7	
=) 43=1005	5.   5	+51Py-120)+ Pz2-250° 2 × 250 ×260		_	
				**	
A 3 Az Aix	T = A4A5A	16			
7 CICOS S	51623 -523	-120623-25063-260	[ C4CEC6 -5456	-C4C856-54C6 C458	. 7
-4S23 -	5 S23 -C23	-120C23-250C3-260- 120S23+250S3	SACELLA CASE	-546256+6466 5455	•
		o	× T = -5×C6	SerSL Co	
	0 0	1 ]	•	•	
L1/22/2+C	16,2Pn - 522	B-120CB-250	() -) Ln= 0		
		3P2+120S23+250			
C23 (4PX+S	olfy-120) t	S23(-PZ)=250C	3 +260 - D		
S25 (4 PX+	SIPy-120)-	f C23 (-PZ) = -250	153 - @		
10,40,	= N(CIPX+SI	Py-120)2+ (-PE)2 = (	1 (25013+260) 2+ (	-250Sz)2 = E	
CHA CIPLES	t , co.	50 = -P2			

	(18+51P4-120 , 14Px+51P4-120)	
=) fanø=	-Pt = tan-1 (4/x+5/Py-120)	
645(A2+A3	$s$ ) $s$ in $\phi$ + $s$ in $(42+43)$ $as\phi$ = $s$ in $(42+43+\phi)$ = $\frac{250C_5+240}{E}$	
-sin(02+03	s) sing + cos (92+03) cosp = cos (92+03+0) = -25053	
7 fau(az	+B3+p) = 25063+260 -25083	
7 B2+ B.	$3+\phi = \tan^{-1}\left(\frac{250C_3+260}{-250S_3}\right)$	
=1 A2 = fo	$\frac{250C_3+260}{-250S_3}$ - $\frac{1}{2}$ - $\frac{1}{2}$ - $\frac{1}{2}$ - $\frac{1}{2}$ - $\frac{1}{2}$	
	, , , , , , , , , , , , , , , , , , ,	灰
C16230x	1+51C13Q9-513Q2=C4S5	
	-S1S23Qy-C23Q3=S4S5	
-Sus (cax+	5199)-5262 - CAST  5199)-6262 = S4ST  1	
=) 04 = tan+/	(-523(C192+5194)-C25922 ) or tay- (-523(C192+5194)-C2392)	
	(-33((19x+5194)-6382)  or fant (-33((19x+5194)-6382)  Co3((19x+5194)-53892)	*
ATATATA	1-1- Az-A1	
-4534 0	51C344 -5344 -130C34x-250C34x-260C47	
	51C44 -5244 -120Cas4-250C4x-260C4 -C1 0 0   St C6 -5556 -65 0   St C6 -5556 -65 0   St C6 -5556 -65 0   St C6 0 0 0 0   St C4 0 0 0 0   St C4 0 0 0 0 0   St C4 0 0   St C4 0 0 0   St C4 0	
L1C234ax	+ SIC234ay-S234az=So	
6162740x	( + S1C234ay-5234az = St ay = -Cx	
6162740x	( + S1C234ay-5234az = St ay = -Cx	
CICHYOX SIAX-CI TOMAS = S	4 51C234Ay-5234Az = ST  Ay = -Cx  LS = C1C034Ax+51C034Ay-524Az  -51Ax+41Ay	
CICHYOX SIAX-CI TOMAS = S	( + S1C234ay-5234az = St ay = -Cx	

-LIS234NX-SIS234NY-C234NZ=S6	
-4 S234 Ox -51 S234 Oy - C234 Oz = C6	
fon AL - C15234 Mx + S1523 FNy + C234 M2	
tanab= 452341x+51523419+633413 452340x+51523409+633403	
+ Ob= toun ( C15234 Mx + S15234 My + C234 Mz	)
9 86= four C1S2340x+S1S23404+C23402	

# 四、加分題:討論兩種逆向運動學(代數法,幾何法)的優缺點

## 代數法 (Algebraic Method)

#### 優點:

- 1. 精確性:代數法通常能夠提供較為準確的解,特別是對於複雜的多關節系統。
- 2. 通用性:代數法的應用不受機械結構的特定形狀限制,可以 用於各種機械系統。
- 3. 高效性: 在某些情況下,代數法的計算速度可能比幾何法更快,尤其是當機械結構複雜且需要高精度時。

#### 缺點:

- 1. 複雜性:代數法的數學運算可能變得非常複雜,特別是對於 具有大量關節的系統,導致解的公式難以推導和實現。
- 數學求解困難: 對於一些非線性或特殊機構,代數法的求解可能變得非常困難,並且可能需要使用數值方法。

## 幾何法 (Geometric Method)

#### 優點:

- 簡單直觀:幾何法基於三角學和幾何關係,通常比代數法更容易理解和實現。
- 2. 即時反饋: 幾何法通常可以提供即時的解,這對於需要快速 反應的應用(如機器人的運動控制)是有利的。

3. 易於調整: 對於一些簡單的機械結構,可以較容易地進行手動調整以滿足特定的需求。

#### 缺點:

- 1. 精確度受限: 幾何法的精確度通常比代數法低,特別是在機械結構複雜且需要高精度的情況下。
- 特定機構: 幾何法的適用性可能受到機械結構形狀的限制, 對於某些特定機構可能不夠通用。