一片置知识:

Classical FWI

- 1. Wi = Crike UK.
- 2. Più = fi + trj.j
- 5. Svcf-ein) wdv + Stcu, m). vds = Sv(g-ei). udv + Stcv. m). uds 世而针对方程:

有:(Free boundary. 在S上.G为O) 产生的应为

## 二. 散射设场

对参为个介质有区域以,边界So.对应P°,Ciju,U°(什分的时间)玻璃) 扰动顶带角标"1", 拢动后为;

对体力的时有此似的满足方程,相应地,抗功后也满足方程。

$$\begin{cases} \frac{2}{3\pi_{j}} \left( C_{3j}^{2} pq \frac{3\mu_{i}^{2}}{\pi_{q}^{2}} \right) - e^{\circ} \ddot{u}_{i}^{\circ} = 0 \\ \frac{2}{3\pi_{j}} \left( \left( C_{3j}^{0} pq + C_{3j}^{1} pq \right) \frac{3(u_{i}^{\circ} + u_{p}^{1})}{3\pi_{q}^{2}} \right) - (e^{\circ} + e^{i})(\ddot{u}_{i}^{\circ} + \ddot{u}_{i}^{1}) = 0 \end{cases}$$

担后一式代入前一式有:
「何语": 
$$C^{\circ}U^{\circ} - P^{\circ}\ddot{u}^{\circ} = 0$$
「何语":  $C^{\circ}U^{\circ} - P^{\circ}\ddot{u}^{\circ} = 0$ 
「何语":  $C^{\circ}U^{\circ} + C^{\circ}U^{\circ} + C^{\circ}U^{\circ} - P^{\circ}\ddot{u}^{\circ} + C^{\circ}U^{\circ} + C^{\circ}U^{\circ} - P^{\circ}\ddot{u}^{\circ} - P^{\circ}\ddot{u}$ 

有: 
$$e^{\circ}\ddot{u}_{i} = -e'\ddot{u}_{i} + \frac{\partial}{\partial s_{i}}((\dot{\eta}_{i}r_{i}\frac{\partial u_{p}}{\partial s_{q}}) + \frac{\partial}{\partial s_{i}}((\ddot{\eta}_{i}r_{i}\frac{\partial u_{p}}{\partial s_{q}})$$

(4 为.

此为程介质为 6°. Cing. 波场为 üi 即只要饱加一个特殊付为在均一个质上, 传出的波场 就相当于扰动后的介质中给出的波场, 何可由去计算 非均一个质不的胶动方程, 但此件为 课 显然可求的

根据格林函数,且自由由界上的/多为0.

对其中第二板分部部分:

国Bon / Fredet derivate 有, 把U技成U°

定义:

- 1. ×: 我小二来 mistit function
- 2. Ar: Y=1...N台站位置.
- 3. d(Xnt) 台站Y接收到向三分里数据。
- 4. S(X,t,M) 给定模型是 M后的模拟波形.
- 5. ||A|| = Zij |Avi| C可能是)

$$\mathcal{N}(\mathbf{r}_{m}) = \frac{1}{2} \sum_{r=1}^{N} \int_{0}^{T} || S(x_{r}, t, m) - d(x_{r}, t)||^{2} dt$$

实际探价中如高、没收、加权.

对 Xx Fredst ]:

国係化理化:  $\frac{\chi_{CM+\Sm)} - \chi_{CM}}{\S(\chi_r,t,\, m)+\Sm)} = \frac{\left(-\sqrt{-\chi_{SM}}\right) - \left(-\sqrt{-\chi_{SM}}\right)}{-\sqrt{-\chi_{SM}}} = \frac{\left(-\sqrt{-\chi_{SM}}\right)}{-\sqrt{-\chi_{SM}}} = \frac{\left($ 

M X (s Fredet & x:

$$\&x = \sum_{r=1}^{N} \int_{0}^{T} \left[ S(x_r, t, m) - d(x_r, t) \right] \cdot \&S(x_r, t, m) dt$$

其中65(剂,t, M)即为液场 5时 模型扰动 8M 产生同数射液场、根据乃是后一万有:

\$\$(x1.t.m) = - \int dt \ \d'x [ \( \rangle (x') \) \( \rangle (x,x') \) \( \frac{1}{2} \) \( \rangle (x',t') \)

84jkin(x') 2kGij(xnx'; t-t') 2km(x', t')]

为 [注: G里面为剂, 喜r处的 65 7 现在,只零等出 65、 军出 6x 就能知道模型修改的方向了.

Adjoint :

交换积分顺序

$$\int_{0}^{T} dt \int_{0}^{t} dt' \rightarrow \int_{0}^{T} dt' \int_{t'}^{T} dt$$

$$\downarrow^{t'}$$

$$\downarrow^{t'$$

杉林di牧,

Gik (x, , x'; t-t') = Gri (x', x; t-t')

相气有等-顶、仓含6p. G. 24s. [5-d] 其中8p和24s可拿到dt积分之外, 互可拿到里面.

对后向部分出行分析,①改变积分上下限.用换气 ②引入8(x),这样和作为私分别就一致了.

$$= \int_{0}^{\tau-t'} \int_{0}^{t} dx' G_{ji}(x', x, T-t'-t) = \int_{0}^{\tau-t'} \int_{0}^{t} \int_{0}^{t} (x, t) \int_{0}^{t} \int_{0}^{t} (x, t) \int_{0}^{t} \int_{0}^{t} (x, t) \int_{0}^{t} \int_{0}^{t} (x, t) \int_{0}^{t} \int_{0}^{t} \int_{0}^{t} (x, t) \int_{0}^{t} \int_{$$

$$= \int_{0}^{T-t'} dt \int d'x G_{ji}(x', x, T+t'-t) f_{i}^{t}(x, t)$$

$$\stackrel{\stackrel{>}{=}}{=} S_{j}^{+}(x', T-t')$$

(有时间卷秋: 七类比七 西七类比下七'和干扰 了。如 fct-v)g(v) 一致。 有空间积分)

由此:对Partx有:

对 SX Part Scykin 部分:

如果想用SP类似的思路,建立 Shigklm 就走偏了.

这样反而更复杂了,要避免分母大的吃.

正确思路是直接把SXPatz部分的Scielm展开K和N.

$$|\mathcal{L}| \times_{Cjklm} = -\int_{0}^{T} C_{jklm}(x) \frac{\partial S_{m}(x,t)}{\partial x_{l}} \frac{\partial S_{j}^{\dagger}}{\partial x_{k}} dt = -\int_{0}^{T} C_{jklm}(x) e_{ml} e_{jk}^{\dagger} (x, T-t) dt$$

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$$|\mathcal{L}| \times_{Cjklm} = -\int_{0}^{T} C_{jklm}(x) e_{jklm}(x) e_{jklm}(x) e_{jklm}(x) dt$$

$$|\mathcal{L}| \times_{Cjklm} = -\int_{0}^{T} C_{jklm}(x) e_{jklm}(x) e_{$$

$$-\delta_{j}(x) = -\int_{0}^{T} k(x) \left[ \nabla_{s}(x', t') \cdot \nabla_{s}(x', t') \cdot \nabla_{s}(x', t') \right] dt$$

$$(x, K_{k}(x)) = -\int_{0}^{T} k(x) \left[ \nabla_{s}(x', T-t) \right] \left[ \nabla_{s}(x, t) \right] dt$$

for u:

$$= 8N \left| \frac{38i}{38i} \frac{38i}{38k} + \frac{38i}{38k} \frac{38i}{38k} - \frac{3}{3} \frac{38i}{38i} \frac{38i}{38j} \right|$$

初克:对偏应xe和V

$$\begin{aligned}
e : V &= (e_{ij} - \frac{1}{3} \delta_{ij} e_{mn}) \times V_{ij} - \frac{1}{3} \delta_{ij} e_{mn}) \\
&= e_{ij} V_{ij} - \frac{1}{3} \delta_{ij} e_{ij} V_{nn} - \frac{1}{3} \delta_{ij} V_{ij} e_{mn} + \frac{1}{4} \delta_{ij} \delta_{ij} e_{mm} V_{nn} \\
&= e_{v_{ij}} V_{v_{ij}} - \frac{1}{3} \delta_{v_{ij}} e_{v_{ij}} V_{nn} - \frac{1}{3} \delta_{v_{ij}} V_{v_{ij}} e_{mm} + \frac{1}{3} e_{mm} V_{nn} \\
&= e_{v_{ij}} V_{ij} - \frac{1}{3} e_{v_{ij}} V_{nn} \\
&= e_{v_{ij}} V_{ij} - \frac{1}{3} e_{v_{i}} V_{nn} \\
&= e_{v_{ij}} V_{ij} - \frac{1}{3} e_{v_{i}} V_{nn} \\
&= e_{v_{ij}} V_{ij} + U_{j,v_{i}} + U_{j,v_{i}} + U_{j,v_{i}} + U_{j,v_{i}} \times V_{n}
\end{aligned}$$

of torn: to

K(x)=- 」「W(x) D+(x,T-t); D(x,t)dt. D为偏应变.

注: 85(m+8m)是针对上-步M,不定是构一.

U°. C°. Cin 配 Gy. 但Gy 不定有4析件、Gy 只是一个中间步骤 用来得到反传波均 st. st可立接面过数值计算得到。