

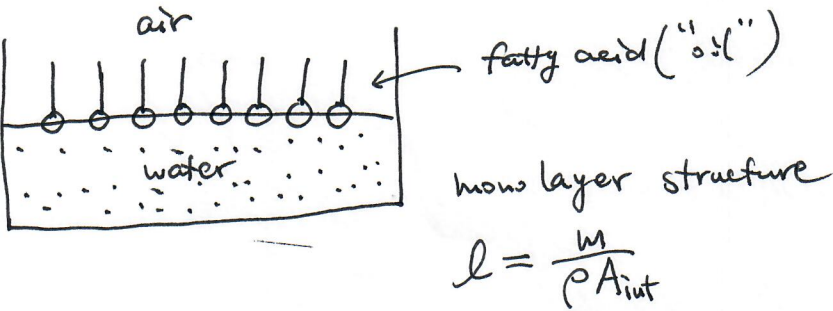
Lecture VI Lipids

1. Why lipids?

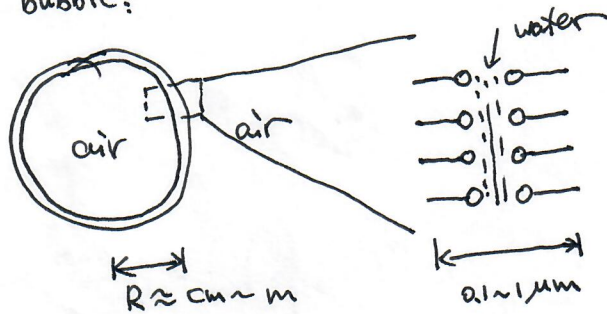
Biologically, extremely important, form bilayer membranes

2. Self-assembly

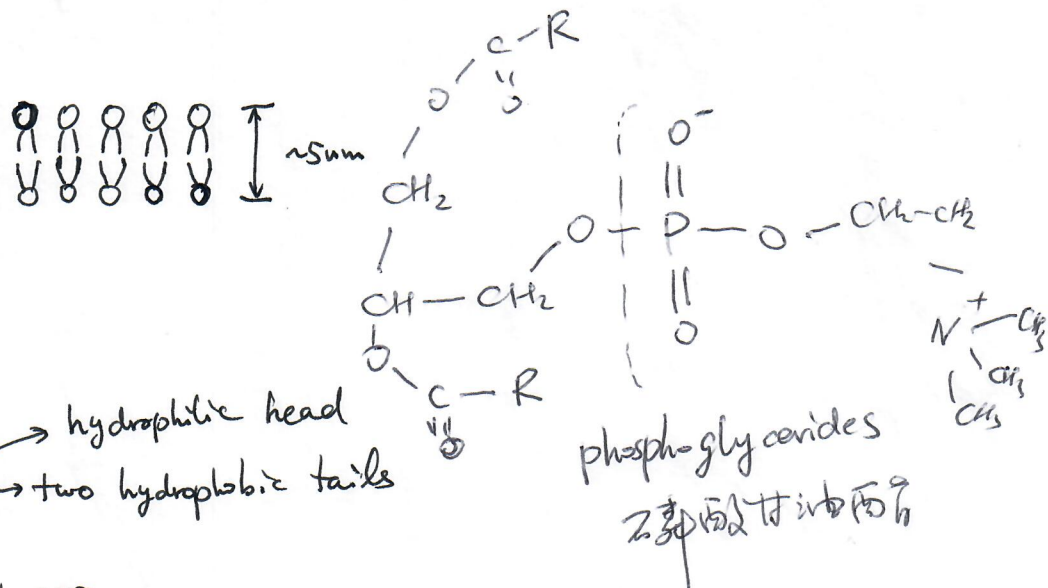
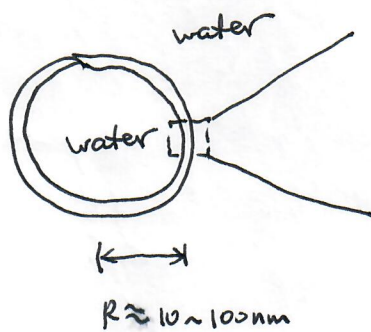
Middle-school physics



soap bubble:



lipid vesicle



lipid → phospholipid

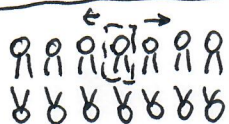
hydrophilic head
two hydrophobic tails

3. Motions in a lipid bilayer

Question: Which state, fluid or solid, do you expect cell membrane to be?

Answer: fluid (flexibility, Material exchange between the inside and the outside of cells)

1) lateral diffusion

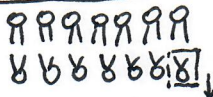


Diff. coeff. $D \sim 1 \mu\text{m}^2/\text{s}$ (fluorescent microscope)

water self diff. coeff. : $D \sim 0.1 \text{ cm}^2/\text{s}$

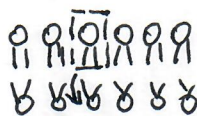
lipid bilayer is very viscous

2) protrusion (thermal excitation)



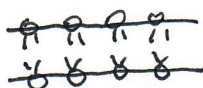
- single molecule or a few molecules relative to the membrane plane
- exposure of hydrophobic cores to water, associated with an energy penalty $\sim \sigma_{pr} A_L$ with σ_{pr} protrusion tension, A_L : area per lipid
- length scales of protrusion, ① amplitude: $\sim 0.1 \text{ nm}$
② length scale at which the protrusion mode can be seen or measured

3) flip-flop: migration of a lipid molecule from one leaflet to the other.



- involves local rearrangement of neighboring molecules and energetically unfavorable contact of head and tails.
- rare event in real cellular membranes, or synthetic bilayers.
rate: $\sim 1/\text{hour}$
- on a not very long time scale the two leaflets are asymmetric
- proteins can catalyze the flip-flop of lipids

4) shape fluctuations (thermal excitation)



"bending"

4. Mechanical deformation of lipid membranes

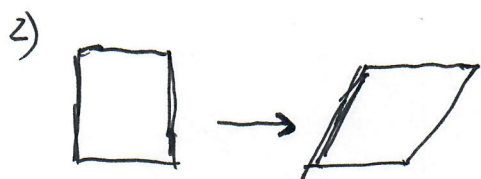


stretching

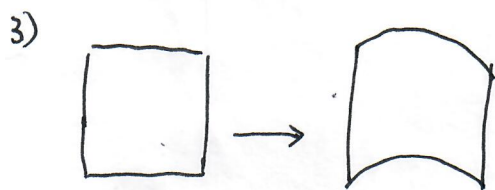
$$E_{st} = \frac{1}{2} \frac{K_A}{A_0} (A - A_0)^2$$

A, A_0 : area per lipid
 K_A : area compressibility modulus. $0.1 \text{ to } 0.2 \text{ J/m}^2$
 $A_0 \sim 0.5 \text{ nm}^2$

- A lipid bilayer ruptures once its area is stretched by 2% - 5%.



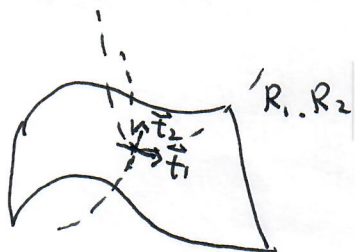
shearing, fluid, no shear resistance



bending, main contribution

5. Curvature and bending energy

- lateral extension \gg membrane thickness ($\sim 5 \text{ nm}$). lipid membrane, viewed as a thin elastic sheet
- parameterization (differential geometry)



$$c_1 = \frac{1}{R_1} \quad c_2 = \frac{1}{R_2} \quad \text{curvature}$$

energy density (E_{be}/A) independent of parameterization, depends on

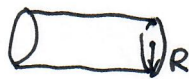
$$\underline{\underline{c}} = \frac{c_1 + c_2}{2} \equiv M \text{ (mean curvature)}$$

$$\underline{\underline{c}} = \frac{c_1 c_2}{2} \equiv G \text{ (Gaussian curvature)}$$



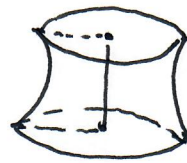
$$M = \frac{1}{R}$$

$$G = \frac{1}{R^2}$$



$$M = \frac{1}{2R}$$

$$G = 0$$



catenoid
 $\frac{1}{2} \text{ sphere}$

$$M = 0$$

$$G = -\frac{1}{R^2}$$

curvature energy

$$E_{be} = \oint \left(2K_{be}(M-M_0)^2 + K_G G + \Sigma \right) dA$$

↑
tension

material parameters:

K_{be} : bending modulus, $\sim 10 k_B T$


M_0 : spontaneous curvature

K_G : Gaussian modulus, for a membrane without topological transformation, $\oint G dA = \text{const}$

rather difficult to measure

How to measure K_{be} ?

In limiting case of infinite large K_{be} , the lipid membrane prefers a planar shape. This means, the larger K_{be} the less deviation of the membrane from the reference planar shape. By looking at the fluctuations, one can measure K_{be} .

 \rightarrow midplane $h(\vec{r})$: height field w.r.t. reference state

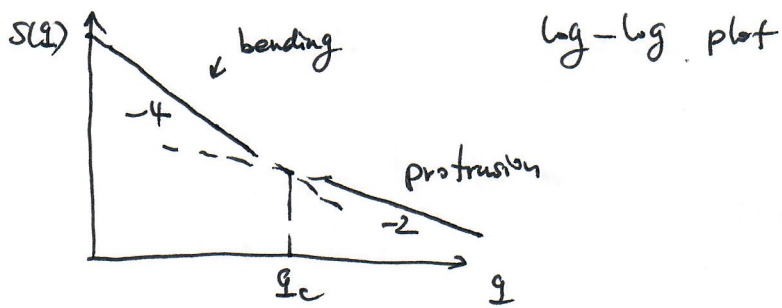
Fourier transform: $\tilde{h}(\vec{q}) = \int h(\vec{r}) e^{i\vec{q} \cdot \vec{r}} d\vec{r}$

fluctuation spectrum: $S(q) = \langle |\tilde{h}(\vec{q})|^2 \rangle$

For a tensionless bilayer ($\Sigma=0$) $E = \oint [2K_{be}(M-M_0)^2 + \sigma_{pr}] dA$

$$S(q) \sim \frac{k_B T}{K_{be} q^4} + \frac{k_B T}{\sigma_{pr} q^2}$$

for large q , i.e. small length scale, $\frac{k_B T}{\sigma_{pr} q^2}$ dominates, protrusion mode
 for small q , i.e. large length scale, $\frac{k_B T}{K_{be} q^4}$ dominates bending, etc

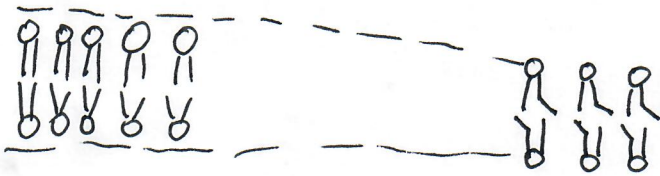
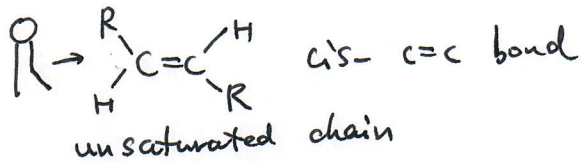
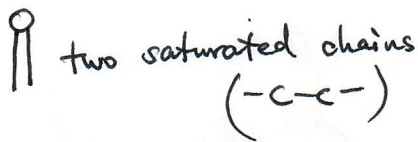


$q_c \rightarrow L_c \approx \text{membrane thickness (nm)}$

characteristic length scale beyond which bending mode dominates.

6. Multicomponent membranes

- Two types of phospholipids



dense packing

- high order of the tails
- Liquid-ordered phase
- high K_{be}

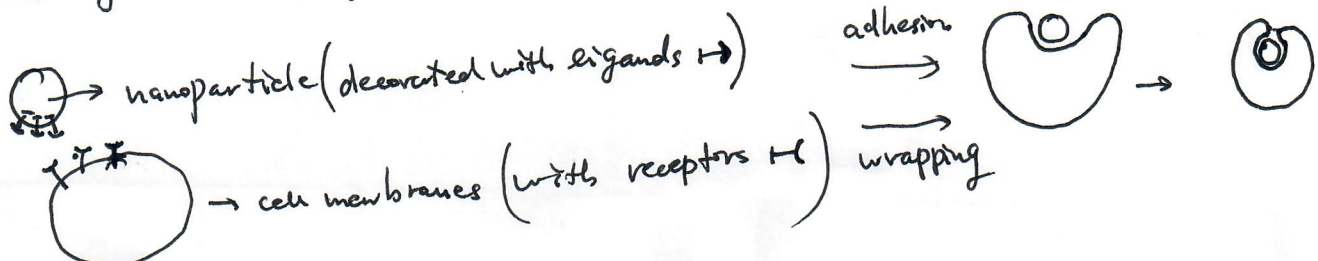
loose packing

- low order of the tails
- liquid-disordered phase
- low K_{be}

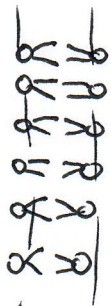
- lipid-raft picture of cellular membrane hypothesis
- separated L_o and L_d domains due to hydrophobic mismatch
- L_o domains: platforms for protein functioning

7. Material exchange (transport) via membranes

endocytosis, exocytosis



exocytosis



attachment
→



fusion
→



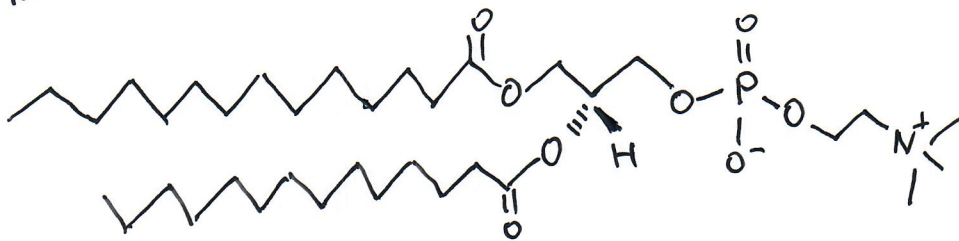
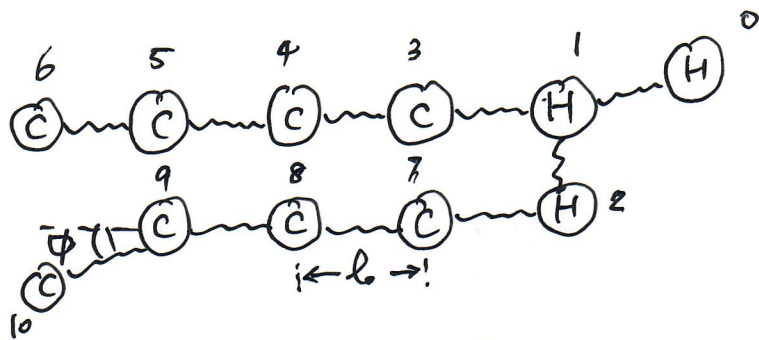
fusion
→



Lecture VI Lipids

Case study:

coarse grained DMPC



1 tail bead $\approx 3.5 -CH_2-$

bonded interactions

$$U_2 = \frac{1}{2} k_2 (|\vec{r}_i - \vec{r}_j| - l_0)^2, \quad k_2 = \frac{128 k_B T}{r_0^2}, \quad l_0 = 0.5 r_0$$

$$U_3 = k_3 [1 - \cos(\phi - \phi_0)], \quad \text{three consecutive tail beads}$$

$$k_3 = 15 k_B T, \quad \phi_0 = 0$$

unbonded interactions (between any two beads)

conservative force + dissipative (frictional) force + random force

$$\vec{F}_{ij}^C + \vec{F}_{ij}^D + \vec{F}_{ij}^R = \left[a_{ij} \left(1 - \frac{r_{ij}}{r_0} \right) - \gamma_{ij} \left(1 - \frac{r_{ij}}{r_0} \right)^2 (\vec{v}_{ij} \cdot \hat{r}_{ij}) + \sigma_{ij} \left(1 - \frac{r_{ij}}{r_0} \right) \zeta_{ij} \delta t^{1/2} \right] \hat{r}_{ij}$$

$$= \left[a_{ij} \left(\frac{1}{r_{ij}} - \frac{1}{r_0} \right) - \gamma_{ij} \left(\frac{1}{r_{ij}} - \frac{1}{r_0} \right)^2 (\vec{v}_{ij} \cdot \vec{r}_{ij}) + \sigma_{ij} \left(\frac{1}{r_{ij}} - \frac{1}{r_0} \right) \delta t^{1/2} \zeta_{ij} \right] \frac{\vec{r}_{ij}}{\sqrt{2 \gamma_{ij} k_B T}}$$

$a_{ij}(\vec{r}_{ij})$	$i=H$	$i=C$	$i=Water$
$j=H$	30(45)	35(90)	30(45)
$j=C$	35(90)	10(45)	75(200)
$j=Water$	30(45)	75(200)	25(45)

bonded forces

$$U_2(\vec{r}) = \frac{1}{2} k_2 (|\vec{r}| - l_0)^2$$

$$\vec{r} \equiv \vec{r}_i - \vec{r}_j, |\vec{r}| = |\vec{r}_i - \vec{r}_j|$$

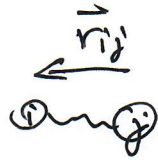
$$\vec{F}_i = - \frac{\partial U_2(\vec{r})}{\partial \vec{r}_i} = - \frac{\partial U_2(\vec{r})}{\partial \vec{r}} \frac{\partial \vec{r}}{\partial \vec{r}_i} = - \frac{\partial U_2(\vec{r})}{\partial \vec{r}}, \quad \vec{F}_j = -\vec{F}_i$$

$$- \frac{\partial U(\vec{r})}{\partial \vec{r}} = - \nabla_{\vec{r}} U(\vec{r}) = - \frac{\partial U}{\partial |\vec{r}|} \frac{\partial |\vec{r}|}{\partial \vec{r}} = -k_2 (|\vec{r}| - l_0) \frac{\partial |\vec{r}|}{\partial \vec{r}}$$

$$= -k_2 (|\vec{r}| - l_0) \frac{\vec{r}}{|\vec{r}|}$$

$$= -k_2 \left(1 - \frac{l_0}{|\vec{r}|}\right) \vec{r}$$

$$\vec{F}_j = k_2 \left(1 - \frac{l_0}{|\vec{r}|}\right) \vec{r}$$



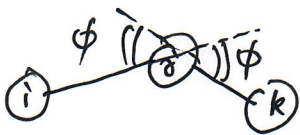
if $|\vec{r}| > l_0$, \vec{F}_i, \vec{r}_{ij} opposite sign
if $|\vec{r}| < l_0$, \vec{F}_i, \vec{r}_{ij} same sign

$$\frac{\partial |\vec{r}|}{\partial \vec{r}} \equiv \frac{\partial [(\vec{r} \cdot \vec{r})^{\frac{1}{2}}]}{\partial \vec{r}} = \frac{\partial (\vec{r} \cdot \vec{r})^{\frac{1}{2}}}{\partial (\vec{r} \cdot \vec{r})} \cdot \frac{\partial (\vec{r} \cdot \vec{r})}{\partial \vec{r}}$$

$$= \frac{1}{2} (\vec{r} \cdot \vec{r})^{-\frac{1}{2}} \cdot \frac{\partial (\vec{r} \cdot \vec{r})}{\partial \vec{r}}$$

$$= \frac{\vec{r}}{|\vec{r}|}$$

$$\frac{\partial |\vec{r}|}{\partial \vec{r}} = \hat{r}$$



$$U_3(\vec{r}_i, \vec{r}_j, \vec{r}_k) = k_3 [1 - \cos(\phi - \phi_0)] \stackrel{\phi_0=0}{=} k_3 (1 - \cos \phi)$$

$$\cos \phi = \frac{\vec{r}_{ji} \cdot \vec{r}_{kj}}{|\vec{r}_{ji}| |\vec{r}_{kj}|}$$

$$\frac{\partial U_3}{\partial \cos \phi} = -k_3$$

$$\vec{F}_i = - \frac{\partial U_3}{\partial \vec{r}_i} = - \frac{\partial U_3}{\partial \cos \phi} \frac{\partial \cos \phi}{\partial \vec{r}_i} = k_3 \frac{\partial \cos \phi}{\partial \vec{r}_i}$$

$$\frac{\partial \cos \phi}{\partial \vec{r}_i} = \frac{\partial \cos \phi}{\partial \vec{r}_{ji}} \frac{\partial \vec{r}_{ji}}{\partial \vec{r}_i} = - \frac{\partial \cos \phi}{\partial \vec{r}_{ji}} = - \frac{\vec{r}_{kj}}{|\vec{r}_{ji}| |\vec{r}_{kj}|} - \frac{\vec{r}_{ji} \cdot \vec{r}_{kj}}{|\vec{r}_{ji}|} \frac{\partial \frac{1}{|\vec{r}_{ji}|}}{\partial \vec{r}_{ji}}$$

vector 3x3 Identity matrix

$$\frac{\partial |\vec{r}_{ji}|}{\partial \vec{r}_{ji}} = \frac{\partial |\vec{r}_{ji}|}{\partial |\vec{r}_{ji}|} \frac{\partial |\vec{r}_{ji}|}{\partial \vec{r}_{ji}} = -|\vec{r}_{ji}|^{-2} \frac{\vec{r}_{ji}}{|\vec{r}_{ji}|} = -\frac{\vec{r}_{ji}}{|\vec{r}_{ji}|^3}$$

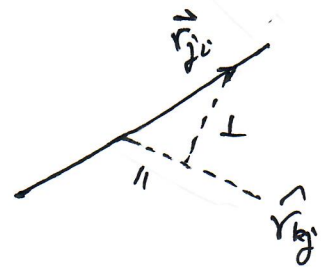
$$\frac{\partial \cos \phi}{\partial \vec{r}_i} = - \frac{\vec{r}_{kj}}{|\vec{r}_{ji}| |\vec{r}_{kj}|} + \frac{(\vec{r}_{kj} \cdot \vec{r}_{ji}) \vec{r}_{ji}}{|\vec{r}_{ji}|^3 |\vec{r}_{kj}|} = \frac{(\vec{r}_{kj} \cdot \vec{r}_{ji}) \hat{r}_{ji} - \vec{r}_{kj}}{|\vec{r}_{ji}| |\vec{r}_{kj}|}$$

$$F_i = K_3 \frac{(\vec{r}_{kj} \cdot \hat{r}_{ji}) \hat{r}_{ji} - \vec{r}_{kj}}{|\vec{r}_{ji}| |\vec{r}_{kj}|} = K_3 \frac{\cos \phi \hat{r}_{ji} - \hat{r}_{kj}}{|\vec{r}_{ji}| |\vec{r}_{kj}|^2}$$



Rewrite $\cos \phi = - \frac{\vec{r}_{ji} \cdot \vec{r}_{kj}}{|\vec{r}_{ji}| |\vec{r}_{kj}|}$ i, k are exchangeable

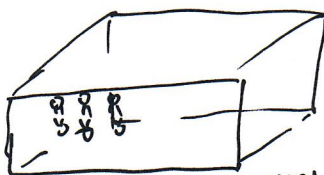
$$F_k = K_3 \frac{(\vec{r}_{ji} \cdot \hat{r}_{kj}) \hat{r}_{kj} - \vec{r}_{ji}}{|\vec{r}_{ji}| |\vec{r}_{kj}|} = K_3 \frac{\vec{r}_{ji} - (\vec{r}_{ji} \cdot \hat{r}_{kj}) \hat{r}_{kj}}{|\vec{r}_{ji}| |\vec{r}_{kj}|} = \frac{\hat{r}_{ji} - \cos \phi \hat{r}_{kj}}{|\vec{r}_{ji}|^2 |\vec{r}_{kj}|}$$



$$F_j = -(F_i + F_k)$$

System II

Simulation setup $L_x \ L_y \ L_z$
20x20x10 r_0^3 box



system I

$L_x = 20$
 $L_y = 10$
 $L_z = 10$

$$N_{\text{lipid}} = 320 \cdot 2 = 640 \quad \bar{A}_L = 1.25 r_0^2$$

$$\rho = 3/r_0^3$$

$$N_{\text{lipid}} \cdot 11 + N_{\text{water}} = \rho V = 12000$$

$$N_{\text{lipid}} = 80 \cdot 2 = 160 \quad \bar{A}_L = 1.25 r_0^2$$

$$\rho V = 3000$$