

☐ **PHYS115** ☐ **PHYS121** ☒ **PHYS123**
☐ **PHYS116** ☐ **PHYS122** ☐ **PHYS124**
Lab Cover Letter

Author (You) Wolf Mermelstein

Signature: _____



I declare that this assignment is original and has not been submitted for assessment elsewhere, and acknowledge that the assessor of this assignment may, for the purpose of assessing this assignment: (1) reproduce this assignment and provide a copy to another member of faculty; and/or (2) communicate a copy of this assignment to a plagiarism checking service (which may then retain a copy of this assignment on its database for the purpose of future plagiarism checking).

Lab Partner(s) Christopher Richner, Lily Kagy

Date Performed October 25, 2023

Date Submitted October 31, 2023

Lab (such as #1: UNC) #5: RKE

TA: Olivia Green

GRADE (to be filled in by your TA) See your TA for detailed feedback.

An 'x' next to a subcategory means you need to improve this aspect of your work.

Paper Subtotals (points)

() **General (6)**

____ Sig. figs.
 ____ Units
 ____ Clarity of Presentation
 ____ Format

() **Abstract (4)**

____ Quantity or principle
 ____ How measurement was made
 ____ Numerical Results
 ____ Conclusion

() **Intro & Theory (9)**

____ Basic principle
 ____ Main equations to be used
 ____ Apparatus
 ____ What will be plotted
 ____ Fitting parameters related

() **Exp. Procedures (15)**

____ Description
 ____ Stating and justifying uncertainties
 ____ Data Record
 ____ Quality of Lab Work

() **Analysis & Error Analysis (20)**

____ Discussion
 ____ Equations & Calculations
 ____ Presentation inc. Graphs, Tables
 ____ Results Reported & Reasonable
 ____ Underlined items addressed

() **Discussion & Conclusions (6)**

____ Numerical comparison of results
 ____ Logical conclusions
 ____ Discussion of pos. errors
 ____ Suggestions to reduce errors

() **Paper Total (60 points)
(30 points for CME or EPF)**

() **Notebook (10 points)**

____ Format (*proper style, following directions*)
 ____ Apparatus (*brief description of equipment, including sketches*)
 ____ Data (*including computer file names and manually recorded data*)
 ____ Experimental Technique (*describing your procedures; stating & justifying uncersts.*)
 ____ Analysis (*results and errors*)

() **Worksheet(s)/Fill-in-the-Blank-Report (30 points) if applicable**

() **Adjustments** – late submissions, improper procedures, etc. – or bonus points for exceptional work.

() **Total Grade**

Graded by _____ (TA's initial)

Rotational Kinetic Energy Lab

Wolf S. Mermelstein

October 31, 2023

Abstract

content...

Contents

1	Introduction	3
1.1	Moment of Inertia	3
1.2	Conservation of Energy	3
1.3	Working Equation	4
2	Procedure	4
2.1	Taking Measurements	4
2.2	Estimating Moment of Inertia	5
2.3	Monte Carlo Simulation	5
3	Results	6
3.1	Plotting Data	6
4	Analysis	7
4.1	Computing I_1 (w/masses)	7
4.2	Computing I_2 (w/o masses)	8
4.3	Computing I_E (mass loads)	9
4.3.1	Estimating I_E	10
5	Conclusion	10
6	Appendix	11

1 Introduction

1.1 Moment of Inertia

Moment of inertia, often denoted by I , is a function of the specific geometry and mass distribution of an object. Moment of inertia is implicitly relative to the axis of rotation. Where R is the distance from the axis of rotation and M is the mass of the object, for a point mass the moment of inertia, I , is given by

$$I = MR^2 \quad (1)$$

The entire moment of inertia can be computed by thinking of a given object as a collection of tiny masses. As the masses' volumes shrink down to some small volume with some proportionately small mass, they can then be eventually said to be the differential dM . Integrating all the small point masses across the entire object implies that the entire moment of inertia of an object, I_{tot} , is given by

$$I = \sum_{k=1}^{\infty} \frac{m}{k} R^2 \quad (2)$$

$$= \int R^2 dM \quad (3)$$

This is conceptually helpful in understanding moment of inertia for arbitrary shapes, but is not practically useful for non simple (i.e. circles, squares, collections of discrete point masses) shapes, such as the mass-loaded, spoked wheel that we used in our experiment. As a result of such, it is often helpful to actually measure moment of inertia instead of attempting to compute it.

1.2 Conservation of Energy

The translational kinetic energy of an object in motion with mass M moving at speed v is given to be

$$K_T = \frac{1}{2} Mv^2 \quad (4)$$

Since we know that

$$\begin{aligned} \frac{\theta}{2\pi} &= \frac{s}{2\pi R} \\ s &= \theta R \end{aligned} \quad (5)$$

and

$$\begin{aligned} \frac{d}{dt}s &= \frac{d}{dt}\theta R \\ v &= \omega r \end{aligned} \quad (6)$$

We can then derive from equation 4 that the rotational kinetic energy, K_R , is

$$\begin{aligned} K_R &= \frac{1}{2} M(\omega R)^2 \\ &= \frac{1}{2} (MR^2) \omega^2 \\ &= \frac{1}{2} I \omega^2 \end{aligned} \quad (7)$$

where I is defined to be the moment of inertia about the axis of rotation.

For the mass in figure ?? descends downwards due to gravity, it begins to lose its gravitational potential energy, U_W . The total energy of the system is internally conserved, however a small amount of energy is lost due to friction. So, where ΔU_W is the change in the gravitational potential energy of the counterweight, K_T is the translational kinetic energy of the counterweight, and K_R is the rotational kinetic energy of the counterweight, we state that

$$\Delta U_W + K_T + K_R = W_f \quad (8)$$

Which, using equations 7 and 4, implies that

$$\Delta U_W + \left(\frac{1}{2} Mv^2\right) + \left(\frac{1}{2} I\omega^2\right) = W_f \quad (9)$$

ΔU_W should be negative, and K_T & K_R positive because the mass is falling, and, thus, losing gravitational kinetic energy, whilst simultaneously proportionately gaining kinetic energy.

Using the fact that gravitational potential energy for an object at height h of mass m in an environment where gravity can be approximated to g is given to be

$$U_G = (M \cdot g \cdot h) \quad (10)$$

Plugging this in, and renaming h be y , we get the final equation

$$-(M \cdot g \cdot y) + \left(\frac{1}{2}Mv^2\right) + \left(\frac{1}{2}I\omega^2\right) = W_f \quad (11)$$

1.3 Working Equation

Since for our specific experiment we used paperclips attached to the counterweight to cancel out friction, we can instead rewrite equation 11 to be

$$-(M \cdot g \cdot y) + \left(\frac{1}{2}Mv^2\right) + \left(\frac{1}{2}I\omega^2\right) = 0 \quad (12)$$

Carefully noting that we have discluded the energy of the moving paperclips, as it is negligible in comparison to the other energies of the system. And, to further simplify things, we will define y to be vertically positive, so as to make the equation into

$$-(M \cdot g \cdot y) + \left(\frac{1}{2}Mv^2\right) + \left(\frac{1}{2}I\omega^2\right) = 0 \quad (13)$$

Then, using relationship 6, we plug in $\frac{v}{r}$ for ω , resulting in the equation

$$\begin{aligned} -(M \cdot g \cdot y) + \left(\frac{1}{2}Mv^2\right) + \left(\frac{1}{2}I\left(\frac{v}{r}\right)^2\right) &= 0 \\ &= \frac{1}{2} \cdot v^2 \cdot (M + \frac{I}{r^2}) \end{aligned} \quad (14)$$

Or, as will be used later for our computations, the equivalent equation in the form

$$gy = \frac{1}{2}\left(1 + \frac{I}{Mr^2}\right) \cdot v^2 \quad (15)$$

v is a value that is determined by our *Logger Pro*[™] software. It is computed with an advanced proprietary algorithm, but is similar to

$$v \approx \frac{\Delta s}{\Delta T} \quad (16)$$

Figure 1: Visual representation of k and r

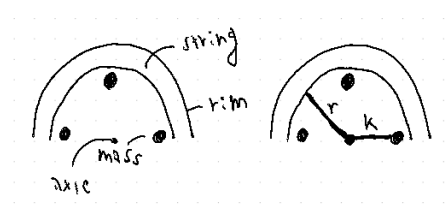
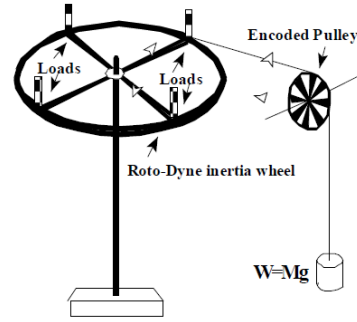


Figure 2: Roto-Dyne wheel Inertia Wheel Apparatus [2]



2 Procedure

2.1 Taking Measurements

Before conducting our experiment, we took measurements of various parts of our setup. First we obtained r from the lab manual, the distance from the axle of the wheel to the string, and then we measured k , the distance from the axle of the wheel to the masses. For r we used the provided uncertainty of $\pm 0.002\text{m}$, whereas for k we measured very carefully and chose the uncertainty to be $\pm 0.01\text{m}$

$$d = 0.200 \pm 0.002 \text{ m} \quad (17)$$

$$r = 0.200 \pm 0.002 \text{ m} \quad (18)$$

$$k = 0.073 \pm 0.001 \text{ m} \quad (19)$$

We used a counterweight with a given mass of 0.06kg to provide a torque to spin our Roto-Dyne wheel, as can be seen in figure ???. To account for friction, we incrementally added paperclips to the bottom of the counterweight. We continued to add paperclips up until the mass would fall at a constant speed to counteract the force of friction, using *Logger Pro*[™] software and

an encoded pulley to monitor acceleration and velocity. Let M_c be the mass of the counterweight and M_p be the mass of the paperclips opposing friction, not used in our computations but still important to the experimental design.

$$M_p = 0.0015 \pm 0.0001 \text{ kg} \quad (20)$$

$$M_c = 0.06 \text{ kg} \quad (21)$$

Also, we were provided with the mass of the Roto-Dyne wheel, M_R and the mass loads, M_L , of which there were 4.

$$M_R = 1.5 \text{ kg} \quad (22)$$

$$M_L = 0.225 \pm 0.002 \text{ kg} \quad (23)$$

For the encoded pulley that we used to measure velocity and length of unrolled string it was given that the gaps between intervals of measurement, Δs , was

$$\Delta s = 0.015 \text{ m}$$

2.2 Estimating Moment of Inertia

Before measuring the moment of inertia, we decided to make a rough approximation. To do this, we used two different common models, the moment of inertia of a disc, $\frac{1}{2}Mr^2$, and the moment of inertia of a ring, Mr^2 . These computations will not be accurate since the actual Roto-Dyne disc is neither a perfect disc nor a hoop. For our rough estimates, we took the radius to be r , and the mass to be

$$\begin{aligned} M_{tot} &= M_R + 4M_L \\ &= 2.4 \text{ kg} \end{aligned} \quad (24)$$

For the disc estimate, we got

$$\begin{aligned} I_{\text{disc}} &= \frac{1}{2}Mr^2 \\ &= 0.048 \text{ kg m}^2 \end{aligned} \quad (25)$$

For the hoop estimate, we got

$$\begin{aligned} I_{\text{hoop}} &= Mr^2 \\ &= 0.096 \text{ kg m}^2 \end{aligned} \quad (26)$$

To determine an overall estimate, I_{est} , we averaged I_{disc} and I_{hoop} , and then set the uncertainty to be that average. Assuming that the wheel is a hoop is an under-estimate, and assuming that the wheel is a disc is an over-estimate, so the actual moment of inertia should be somewhere between the two.

$$\begin{aligned} I_{\text{est}} &= \frac{I_{\text{disc}} + I_{\text{hoop}}}{2} \\ &= 0.072 \pm 0.072 \text{ kg m}^2 \end{aligned} \quad (27)$$

2.3 Monte Carlo Simulation

Before actually measuring the moment of inertia, we performed a Monte Carlo Simulation using our estimated I so that we could compare a graph of data of the estimated value to a graph of data for the actual value later on.

To perform this simulation, we began by creating a new *Origin Pro*TM document, and arranged a table including a column for Δs , the overall displacement (vertical distance it has fallen) of the string, and ΔT_0 , the time elapsed since dropping the counterweight to arrive at that overall displacement. The values for Δs were computed using the equation

$$y_i = i\Delta s \quad (28)$$

Which is simply stating that the total displacement of the rope is equal to the amount of a single displacement, a notch in the encoded pulley, times the number of increments, which is the total number of notches that passed by the laser at a given time point. To compute the ΔT_0 from the Δs we derived the following equation from equations 16 and 15.

First, we manipulated equation 15 by solving for v .

$$\begin{aligned} gy &= \frac{1}{2}\left(1 + \frac{I}{Mr^2}\right) \cdot v^2 \\ v^2 &= \frac{\frac{1}{2}\left(1 + \frac{I}{Mr^2}\right)}{gy} \\ v &= \sqrt{\frac{\frac{1}{2}\left(1 + \frac{I}{Mr^2}\right)}{gy}} \end{aligned} \quad (29)$$

Next we solved equation 16 for t . For our use case here, we will allow ΔT to be ΔT_0 .

$$\begin{aligned} v &\approx \frac{\Delta s}{\Delta T} \\ \Delta T &= \frac{\Delta s}{v} \\ \Delta T_0 &= \frac{\Delta s}{v} \end{aligned} \quad (30)$$

Then, we solved for ΔT_0 by plugging in v from equation 30 and Δs into equation 30.

$$\begin{aligned} \Delta T_0 &= \frac{\Delta s}{v} \\ \Delta T_0 &= \frac{\Delta s}{\sqrt{\frac{\frac{1}{2}(1 + \frac{I}{Mr^2})}{gy}}} \\ \Delta T_0^2 &= \frac{\Delta s^2}{\frac{\frac{1}{2}(1 + \frac{I}{Mr^2})}{gy}} \\ \Delta T_0^2 &= \frac{\Delta s^2(1 + \frac{I}{Mr^2})}{2gy} \\ \Delta T_0 &= \Delta s \sqrt{\frac{(1 + \frac{I}{Mr^2})}{2gy}} \end{aligned} \quad (31)$$

With a simple script we had *Origin Pro*TM apply this equation to each row, utilizing that respective row's Δs value. Now, since this data is purely based on an estimated moment of inertia value, we applied Monte Carlo randomization. To do this, we shifted each ΔT_0 by some ΔT_{0G} obtained from a Gaussian distribution G with the given mean 0 and σ equal to the estimated uncertainty for Δt , $\delta_{\Delta t}$, which was given to be 0.0002s, resulting with a column with values for δt_R . This can be expressed formulaically as

$$\delta T_R = \Delta T_0 + \Delta t \cdot \text{grnd}() \quad (32)$$

After running this computation, for the first three values of ΔT_r we got

Table 1: Samples of random Monte Carlo data generation

trial #	s
1	0.15409
2	0.10925
3	0.08891
1	0.15381
2	0.10883
3	0.08919
1	0.01540
2	0.10891
3	0.08891
1	0.15385
2	0.10918
3	0.08894

of the falling counterweight mass using the encoded pulley and *Logger Pro*TM. We then imported the data into *Origin Pro*TM for analysis and to help us compile plots. To keep our data consistent, we decided to trim the first three rows and all rows after row 44. Data beyond that in either direction was problematic because of us abruptly setting up and stopping the counterweight from hitting the floor.

To visualize our data, we plotted v^2 against displacement for both the system with and without load masses, and did the same for our simulation. For our v^2 column in *Origin Pro*TM we used

$$\begin{aligned} v &= \frac{\Delta s}{\Delta T} \\ v^2 &= \left(\frac{\Delta s}{\Delta T}\right)^2 \\ v^2 &= \left(\frac{0.015}{\Delta T_i}\right)^2 \end{aligned} \quad (33)$$

To include error bars in our *Origin Pro*TM plot, we applied the derivative method row-wise to equation 33, using equation 35. We obtained the value

$$\delta_{\Delta T} = 0.0002s \quad (34)$$

from our lab manual, which is a consequence of the intrinsic inaccuracy of *Logger Pro*TM and our recording hardware. Solving for δ_{v^2} , we got

3 Results

3.1 Plotting Data

For the actual results, we measured the velocity, acceleration, time (duration), and position

$$\begin{aligned}
\delta_{v^2} &= \left| \frac{\partial}{\partial \Delta T_i} \left(\left(\frac{0.015}{\Delta T_i} \right)^2 \right) \cdot \delta_{\Delta t} \right| \\
&= \left| 0.015^2 \cdot \frac{\partial}{\partial \Delta T_i} (\Delta T^2) \cdot \delta_{\Delta t} \right| \\
&= \left| 0.000225 \cdot -2\Delta T^{-3} \cdot \delta_{\Delta t} \right| \\
&= \frac{.00000009}{\Delta T^3} \quad (35)
\end{aligned}$$

Then we used *Origin Pro*TM to compute a line of best fit, of which the regression and slope has been superposed onto our plot figures, figure ??, ??, and ??.

These aforementioned plots can be found in the appendix, section 6. Additionally, tables ?? and ?? contain the actual datatables with raw *Logger Pro*TM data used for generating the plots.

4 Analysis

Objective For the analysis of our data, our objective was to compute I_E , the measured moment of inertia for just the mass loads on the wheel. In order to do this, we took many intermediate steps to prevent mistakes and measurements. This included a Monte Carlo simulation to verify our computation for I_1 , the moment of the Roto-Dyne wheel including the mass loads, and an careful estimate of I_E using the definition of moment of inertia.

4.1 Computing I_1 (w/masses)

The first step towards accomplishing this goal was to determine whether our estimate for the moment of inertia of the Roto-Dyne wheel was reasonably close to our measured moment value. In order to make this determination we first worked to derive a formula for I , the measured value of the moment of inertia. To start, we note the equation for the slope of the Roto-Dyne wheel with the load masses, B_1 and B_2 , the slope without load masses, obtained through *Origin Pro*TM's provided linear fit line.

Using the elementary equation for some slope, m , with a linear function plotted on an x - y graph,

$$m = \frac{\Delta y}{\Delta x} \quad (36)$$

We determined that for our vertical axis v^2 and horizontal axis y ,

$$B_1 = \frac{v^2}{y} \quad B_2 = \frac{v^2}{y} \quad (37)$$

First, we solved equation 15 for v^2 as a function of y

$$gy = \frac{1}{2} \left(1 + \frac{I}{Mr^2} \right) \cdot v^2 \quad (15)$$

$$v^2 = \frac{2gy}{1 + \frac{I}{Mr^2}} \quad (38)$$

Then we plugged this value for v^2 into equation 37, finally solving for I_1

$$\begin{aligned}
B_1 &= \frac{\frac{2gy}{1 + \frac{I_1}{Mr^2}}}{y} \\
&= \frac{\frac{2gy}{1 + \frac{I_1}{Mr^2}}}{y} \cdot \frac{1 + \frac{I_1}{Mr^2}}{1 + \frac{I_1}{Mr^2}} \\
&= \frac{2g}{\left(1 + \frac{I_1}{Mr^2} \right)} \\
By \frac{I_1}{Mr^2} &= 2g - B \\
I_1 &= Mr^2 \cdot \frac{2g - B}{B_1} \\
I_1 &= Mr^2 \cdot \left(\frac{2g}{B_1} - 1 \right) \quad (39)
\end{aligned}$$

Solving for I_1 We then plugged in the values to solve for I_1 for the system including the load masses. Most of the values have already been discussed earlier in our procedure. The two novel values are B_1 and its uncertainty, which will henceforth be denoted as δ_B , provided by *Origin Pro*TM's linear regression model, and g , the generally accepted approximation of near-earth gravity. The more interesting situation, the situation where there are load masses in the Roto-Dyne wheel, is the one we made an estimate and did a Monte Carlo simulation for. We will compute the system without masses for the sake of completion later.

$$r = 0.200 \pm 0.002 \text{ m} \quad (18)$$

$$g = 9.81 \pm 0.01 \text{ ms}^2 \quad (40)$$

$$M = 0.0600 \pm 0.0001 \text{ kg} \quad (21)$$

$$B_1 = 0.68204 \pm 0.00168 \frac{\text{m}}{\text{s}^2} \quad (41)$$

So,

$$\begin{aligned} I_1 &= (.06)(.2)^2 \cdot \left(\frac{2(9.81)}{0.68204} - 1 \right) \\ &\approx 0.06663 \text{ kg m}^2 \end{aligned} \quad (42)$$

Computing Error To compute the error, we applied the derivative method to equation 39, only factoring the error on I_1 due to B as strictly requested by our lab manual. It is, however, worth noting that we believe that the uncertainties due to M and r could be significant, especially given that the r term is squared. These uncertainties will, however, be taken into account for computation of I_E later.

$$\begin{aligned} \delta_I &= \left| \frac{\partial}{\partial B} (Mr^2 \cdot (\frac{2g}{B} - 1)) \cdot \delta_B \right| \\ &= \left| \frac{\partial}{\partial B} (Mr^2 \cdot (2gB^{-1} - 1)) \cdot \delta_B \right| \\ &= 2Mgr^2 \delta_B \cdot \left| \frac{\partial}{\partial B} (B^{-1} - 1) \cdot \delta_B \right| \\ &= 2Mgr^2 \delta_B \cdot \left| \frac{-1}{B^2} \right| \\ &= 2\delta_B \frac{Mgr^2}{B^2} \end{aligned} \quad (43)$$

Plugging in values, we get

$$\delta_I = 2\delta_B \frac{Mgr^2}{B^2} \approx 0.00017 \text{ kg m}^2 \quad (44)$$

So, we can succinctly state

$$I_1 = 0.06663 \pm 0.00017 \text{ kg m}^2 \quad (45)$$

Looking back at our predicted value for I_1 from section 2.2, we chose an estimate of I , denoting it I_{est} . Putting the previously estimated I_1 , " $I_{1,\text{est}}$ " inline with the measured I_1 , " I_1 ", we have

$$I_{1,\text{est}} = 0.072 \pm 0.072 \text{ kg m}^2 \quad (27)$$

$$I_1 = 0.06663 \pm 0.00017 \text{ kg m}^2 \quad (45)$$

It is obvious that the actual value falls within one to two uncertainty intervals of the estimated value. The more important question, however, is whether the estimated value falls within one to two uncertainty intervals of the actual value. Two uncertainty intervals is

$$\begin{aligned} \delta_{I_1} \cdot 2 \\ &= 0.00017 \cdot 2 \\ &= 0.00034 \end{aligned}$$

So, mathematically, we are checking

$$\begin{aligned} 0.07182 &\notin \\ &\notin [0.07182 - 0.00034, 0.07182 + 0.00034] \\ &\notin [0.07148, 0.07216] \end{aligned} \quad (46)$$

Which is false, so our measured indeed value **does not** fall within one to two uncertainty intervals from our estimate. To see how off we are, a percentage value also can be computed, ΔI_{skew}

$$\begin{aligned} \Delta I_{\text{skew}} &= 100 \cdot \left(1 - \frac{I_1}{I_{1,\text{est}}} \right) \\ &\approx 100 \cdot \left(1 - \frac{0.06663}{0.072} \right) \\ &= 100 \cdot (1 - 0.92541) \\ &= 7.45\% \end{aligned} \quad (47)$$

4.2 Computing I_2 (w/o masses)

Solving for I_2 Next we compute the value of I_2 , the moment of inertia of the Roto-Dyne wheel without mass loads, using the same equations for I_1 , equation 39 and for δ_{I_2} , equation 43.

For the system without masses, *Origin Pro*TM produced the linear regression value

$$B_2 = 1.26494 \pm 0.00889 \frac{\text{m}}{\text{s}^2} \quad (48)$$

$$\begin{aligned}
I_2 &= Mr^2 \cdot \left(\frac{2g}{B} - 1\right) \pm 2\delta_B \frac{Mgr^2}{B^2} \\
&= (0.0600)(0.200)^2 \cdot \left(\frac{2(9.81)}{(1.26494)} - 1\right) \\
&\pm 2(0.00889) \frac{(0.0600)(9.81)(0.200)^2}{(1.26494)^2}
\end{aligned}$$

Which evaluates to

$$I_2 = 0.03482 \pm .00026 \text{ kg m}^2 \quad (49)$$

for the massless system. It makes intuitive sense that the moment of inertia is lesser. Inertia is a measure of all the infinite infinitesimally small point masses of an object. There are less masses in the system without mass loads, so the moment of inertia indeed should be notably lesser.

4.3 Computing I_E (mass loads)

We are now very close to being able to find I_E , the moment of just the mass loads. Knowing the experimental moment of inertia for the system with the mass loads and the system without the mass loads, we can compute I_E by subtracting the moment of inertia of the system with the mass loads by the system without the mass loads.

$$I_E = I_1 - I_2 \quad (50)$$

$$\begin{aligned}
&= 0.06663 - 0.03482 \\
&= 0.03181 \text{ kg m}^2 \quad (51)
\end{aligned}$$

We will base the uncertainty of this measurement on the literal, complete equation, subbing I into equation 50 for equation 39.

$$I_E = I_1 - I_2 \quad (50)$$

$$\begin{aligned}
&= Mr^2 \cdot \left(\frac{2g}{B_1} - 1\right) - Mr^2 \cdot \left(\frac{2g}{B_2} - 1\right) \\
&= Mr^2 \left(\left(\frac{2g}{B_1} - 1\right) - \left(\frac{2g}{B_2} - 1\right)\right) \\
&= Mr^2 \frac{2g(B_2 - B_1)}{B_1 B_2} \quad (52)
\end{aligned}$$

Writing the equation like this does not help us solve for I_E , in fact if anything it makes it more convoluted. Rather, the purpose of this literal expression is to allow us to compute an uncertainty based on the values that it is based on. We believe that $\delta_{I_E, M}$ and $\delta_{I_E, g}$ are negligible in comparison to $\delta_{I_E, r}$, δ_{I_E, B_1} , and δ_{I_E, B_2} , since, besides the fact that the actual value for δ_M is 0.0001kg, r is squared which makes its uncertainty even more significant. To start, we recall

$$B_1 = 0.68204 \pm 0.00168 \frac{\text{m}}{\text{s}^2} \quad (41)$$

$$B_2 = 1.26494 \pm 0.00889 \frac{\text{m}}{\text{s}^2} \quad (48)$$

$$r = 0.200 \pm 0.002 \text{ m} \quad (18)$$

$$M = 0.0600 \pm 0.0001 \text{ kg} \quad (21)$$

$$g = 9.81 \pm 0.01 \frac{\text{m}}{\text{s}^2} \quad (40)$$

To compute the overall uncertainty δ_{I_E} , we will first compute $\delta_{I_E, r}$ using the derivative method, and δ_{I_E, B_1} , and δ_{I_E, B_2} using the computational method, and then will add all the uncertainties in quadrature.

$$\begin{aligned}
\delta_{I_E, r} &= \left| \frac{\partial}{\partial r} \left(Mr^2 \frac{2g(B_2 - B_1)}{B_1 B_2} \right) \cdot \delta_r \right| \\
&= \left| 2rM \frac{2g(B_2 - B_1)}{B_1 B_2} \cdot \delta_r \right| \\
&= 0.15907 \text{ kg m}^2 \quad (53)
\end{aligned}$$

$$\begin{aligned}
\delta_{I_E, B_2} &= \left| Mr^2 \frac{2g(B_2 - B_1)}{B_1 B_2} - \right. \\
&\quad \left. Mr^2 \frac{2g((B_2 + \delta_{B_2}) - B_1)}{B_1(B_2 + \delta_{B_2})} \right| \\
&\approx 0.00006 \text{ kg m}^2 \quad (54)
\end{aligned}$$

$$\begin{aligned}
\delta_{I_E, B_1} &= \left| Mr^2 \frac{2g(B_2 - B_1)}{B_1 B_2} - \right. \\
&\quad \left. Mr^2 \frac{2g((B_1 + \delta_{B_1}) - B_1)}{(B_1 + \delta_{B_1}) B_2} \right| \\
&\approx 0.00004 \text{ kg m}^2 \quad (55)
\end{aligned}$$

So, to find the overall uncertainty we add in quadrature, getting

$$\delta_{I_E} = \quad (56)$$

$$\begin{aligned} &= \sqrt{\delta_{I_E,r}^2 + \delta_{I_E,B_1}^2 + \delta_{I_E,B_2}^2} \\ &= \sqrt{0.15907^2 + 0.00006^2 + 0.00004^2} \\ &= 0.15907 \end{aligned} \quad (57)$$

4.3.1 Estimating I_E

Now, like how we came up with an approximate value for the Roto-Dyne wheel with masses and loads by approximating it to be a disc and a ring and averaging the two, we wanted to come up with an estimate in similar fashion for I_E . To do this, we treated the four loads M_L , of 0.225 ± 0.002 kg each, as point masses for computing an estimate for I_E . To do this, we applied equation 1 to all 4 point masses.

$$\begin{aligned} I_{\text{est},E} &= \sum Mr^2 \\ &= 4(M_L r^2) \\ &= 4(0.225 \cdot 0.1^2) \\ &= 0.009 \end{aligned} \quad (58)$$

Computing $\delta_{I_{\text{est},E}}$ is fairly trivial, requiring us to propagate δ_r and δ_{M_L} 's effect on $\delta_{I_{\text{est},E}}$ and then sum in quadrature. For this we used the derivative method.

$$\begin{aligned} \delta_{I_{\text{est},E},r} &= \left| \frac{\partial}{\partial r} (4(M_L r^2)) \cdot \delta_r \right| \\ &= |8M_L r \delta_r| = |8 \cdot 0.225 \cdot 0.1 \cdot 0.002| \\ &= 0.00036 \end{aligned} \quad (59)$$

$$\begin{aligned} \delta_{I_{\text{est},E},M_L} &= \left| \frac{\partial}{\partial M_L} (4(M_L r^2)) \cdot \delta_{M_L} \right| \\ &= |4r^2 \delta_{M_L}| \\ &= |4 \cdot 0.1^2 \cdot 0.002| \\ &= 0.00008 \end{aligned} \quad (60)$$

Adding the uncertainties $\delta_{I_{\text{est},E},M_L}$ and $\delta_{I_{\text{est},E},r}$ in quadrature we get

$$\sqrt{\delta_{I_{\text{est},E},r}^2} \quad (61)$$

5 Conclusion

Acknowledgments

I would like to thank Christopher Richner and Lily Kagy, CWRU Department of Physics, for their help in obtaining the experimental data, collaborating on preparation of the figures, and checking calculations. Additionally, I would like to thank Olivia Green, CWRU Department of Physics, for helping facilitate our lab.

References

- [1] Resnick Halliday and Walker. *Fundamentals of Physics*. Addison-Wesley Professional, 6 edition, 2023.
- [2] D. Schultz. *General Physics I: Mechanics Lab Manual*. CWRU Bookstore, Spring 2004.

6 Appendix

Figure 3: Monte Carlo Simulation of Rotational Kinetic Energy Experiment plot

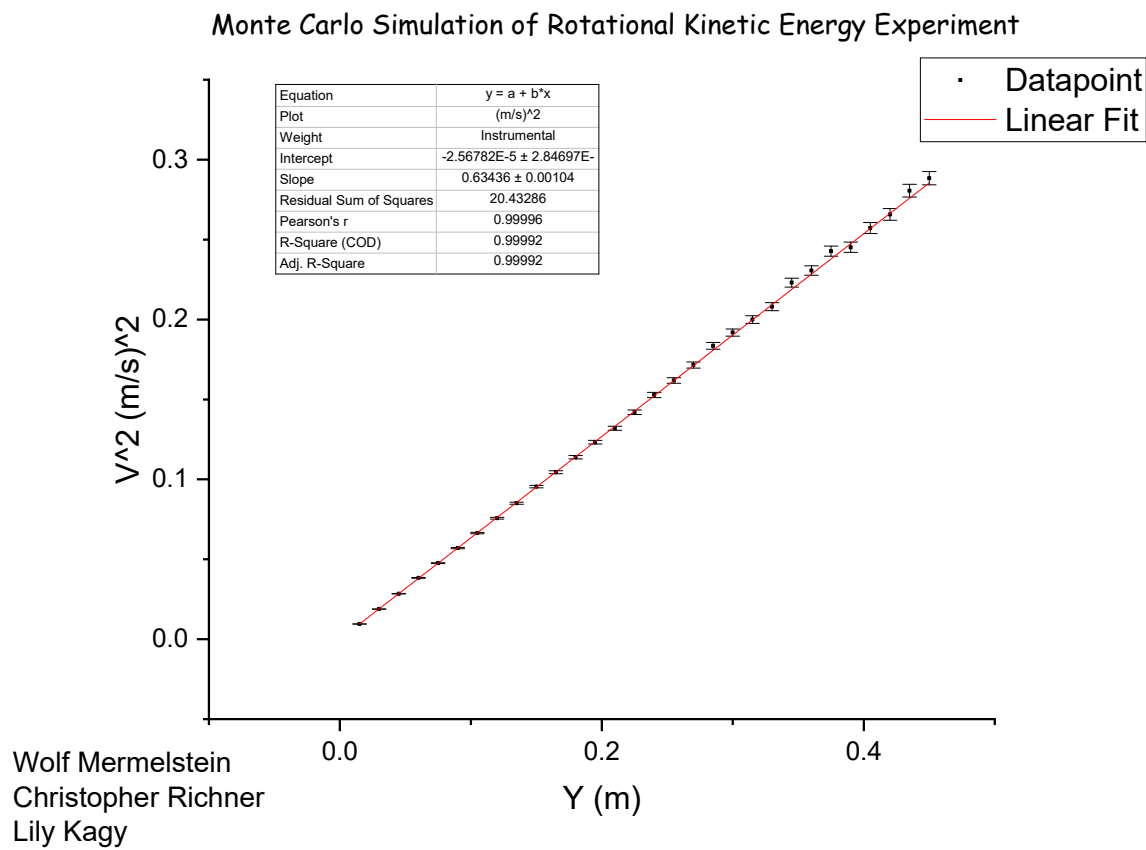


Figure 4: Masses v^2 vs sDist plot

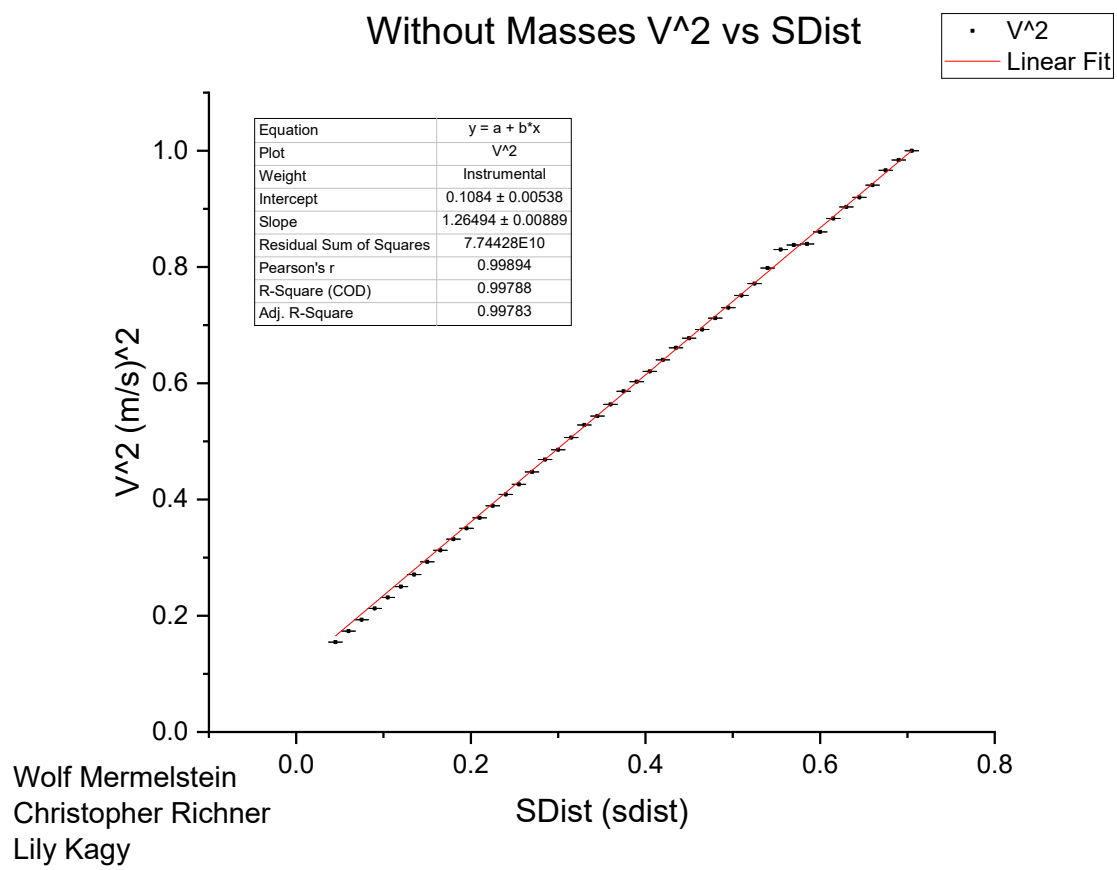


Figure 5: With Masses v^2 vs sDist plot

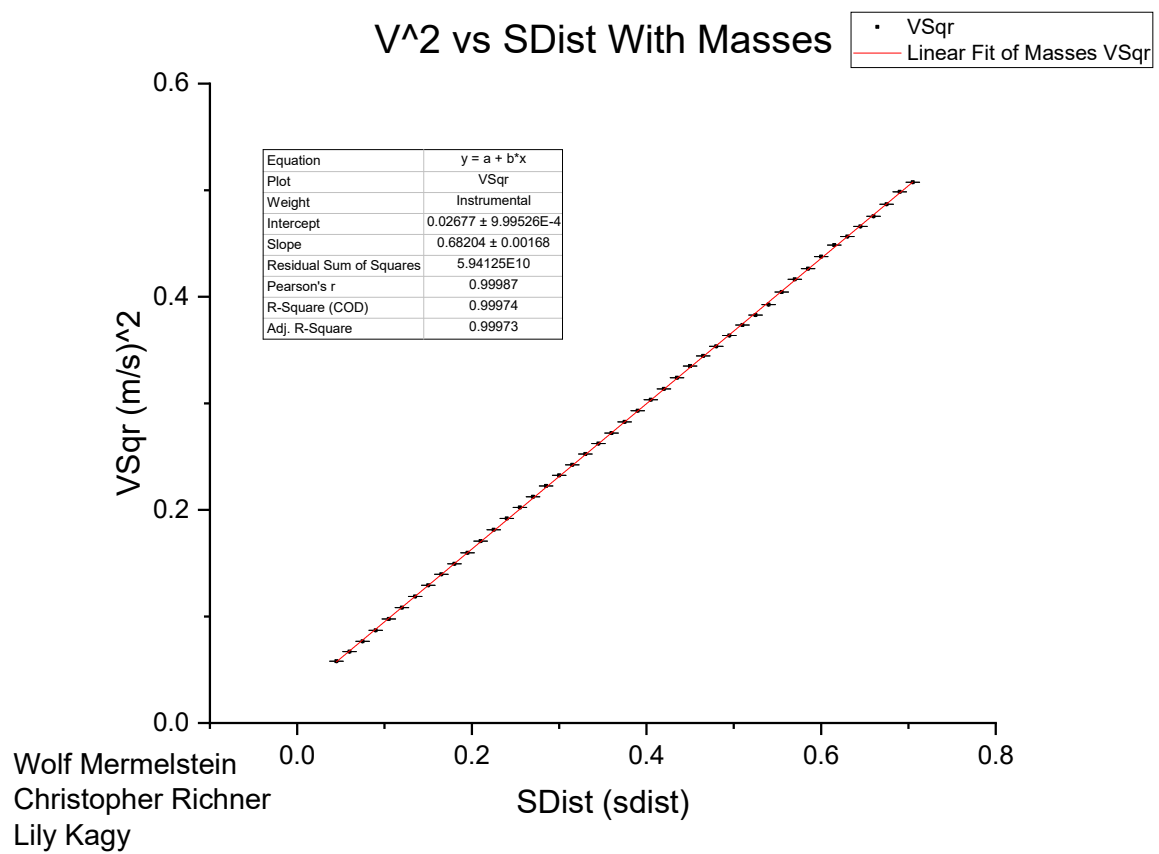


Table 2: Data for falling counterweight **without** mass loads in place

Time	STime	SDist	SVel	SAccel
t	stime	sdist	svel	saccel
s	s	m	m/s	m/s ²
0.2003832	0.3409468	0.045	0.240637469	0.2974361002
0.2421024	0.4010488	0.06	0.2587705469	0.3059740303
0.2727832	0.4571542	0.075	0.2768823709	0.3396616489
0.3099096	0.5096392	0.09	0.2950082819	0.3510465914
0.3375832	0.5590336	0.105	0.3125067287	0.3574728706
0.371984	0.6057826	0.12	0.3289729322	0.3469787101
0.3977972	0.6503324	0.135	0.3445762028	0.3535079613
0.4301136	0.6929332	0.15	0.3594867431	0.3465042602
0.4541972	0.7338524	0.165	0.3734799691	0.3374400019
0.4841948	0.7733118	0.18	0.3866063477	0.3278706007
0.506816	0.8114928	0.195	0.3997294453	0.3595444818
0.5350836	0.8484054	0.21	0.4130797945	0.3638046842
0.5563028	0.8841552	0.225	0.4258449397	0.3503333039
0.5829836	0.9188832	0.24	0.4381633461	0.3590888604
0.6031832	0.9526498	0.255	0.4497965385	0.3299465981
0.6285816	0.9856	0.27	0.4607194593	0.3330491259
0.6478832	1.0177834	0.285	0.4715773455	0.3417015924
0.6720832	1.0492332	0.3	0.4820423673	0.3238048217
0.6905832	1.0800322	0.315	0.492183323	0.3347201767
0.7137832	1.1101992	0.33	0.5023979233	0.3424834134
0.7315832	1.1397582	0.345	0.5121068853	0.3144374509
0.7539216	1.1687902	0.36	0.5216114938	0.3403302933
0.7710904	1.1972824	0.375	0.5315253346	0.355568289
0.792702	1.2252416	0.39	0.5413072074	0.3441565057
0.8092096	1.2527124	0.405	0.5507273167	0.3416705778
0.8302836	1.2797228	0.42	0.559880448	0.3360780896
0.8462136	1.3063022	0.435	0.5692255573	0.3671062769
0.8665272	1.3324336	0.45	0.5787253594	0.359973184
0.8820832	1.358147	0.465	0.5869743702	0.2816386499
0.9017832	1.383547	0.48	0.5946036744	0.3190939627
0.9168836	1.4086054	0.495	0.602973345	0.3489192067
0.9359832	1.4333056	0.51	0.6110845183	0.3078506391
0.9506832	1.4577022	0.525	0.6186489591	0.3122719003
0.9693164	1.481802	0.54	0.6266088147	0.3483025149
0.983612	1.5055832	0.555	0.6359267169	0.4353334838
1.0018836	1.5289834	0.57	0.6452122961	0.3582989806
1.0158992	1.5520834	0.585	0.6529222225	0.3092271113
1.0336832	1.5749334	0.6	0.661597301	0.4500795393
1.0474092	1.5974336	0.615	0.669666613	0.2671862678
1.0647832	1.6197336	0.63	0.6756628186	0.27059002
1.0782148	1.6418362	0.645	0.6826017458	0.3572933224
1.0952812	1.663686	0.66	0.6896131877	0.2844921273
1.1083832	1.6853406	0.675	0.69766979	0.4596086524
1.1251172	1.7066906	0.69	0.7060389196	0.32438475
1.1379832	1.7278332	0.705	0.7123894853	0.2763517435

Table 3: Data for falling counterweight **without** mass loads in place

Time t	STime stime	SDist sdist	SVel svel	SAccel saccel
s	s	m	m/s	m/s ²
0.0942928	0.1784214	0.045	0.3931293508	0.6331416361
0.118666	0.2154714	0.06	0.4167682347	0.6429114748
0.13679	0.2505154	0.075	0.4395279097	0.6560084549
0.1593652	0.2838154	0.09	0.4611842509	0.6446726969
0.1763652	0.3156328	0.105	0.4813227422	0.6212064342
0.1974776	0.3461942	0.12	0.5002408825	0.6168350372
0.2134652	0.375645	0.135	0.5204425281	0.7550560866
0.2334652	0.403888	0.15	0.5411476689	0.7111579009
0.2485668	0.4311196	0.165	0.5590171297	0.6012483335
0.2675656	0.457576	0.18	0.5759222213	0.6767102446
0.2819648	0.4832344	0.195	0.5919181069	0.5701239701
0.3000652	0.5082738	0.21	0.6071150987	0.6437223597
0.3138984	0.5326654	0.225	0.6238645636	0.7296573993
0.3312004	0.5563802	0.24	0.6392812271	0.5705149372
0.3445048	0.5796034	0.255	0.6528166664	0.5951675979
0.361188	0.602345	0.27	0.668869986	0.8166345302
0.3740644	0.624472	0.285	0.6847467198	0.618420718
0.390102	0.6461654	0.3	0.6968292431	0.4955147032
0.4024884	0.6675292	0.315	0.7117831029	0.9044103837
0.417674	0.6883282	0.33	0.7267542228	0.53518959
0.4292784	0.7088134	0.345	0.737173249	0.4820351523
0.4445652	0.7290278	0.36	0.7508551143	0.8716399856
0.4560652	0.7487786	0.375	0.7655336953	0.6147383898
0.4705868	0.768221	0.39	0.7764021555	0.5032779268
0.4818648	0.7874214	0.405	0.7876149561	0.664697796
0.495882	0.8063156	0.42	0.8001386413	0.6609667181
0.5067812	0.8249194	0.435	0.8130346045	0.72541275
0.5206656	0.8432194	0.45	0.8231695853	0.3822354223
0.5311832	0.8613652	0.465	0.8321622217	0.6089180588
0.5446652	0.8792732	0.48	0.8437710657	0.6875800459
0.554982	0.8969236	0.495	0.8544283269	0.520014252
0.5680952	0.9143864	0.51	0.8665462466	0.8678410374
0.5782656	0.931549	0.525	0.8783503608	0.5077214323
0.5911116	0.948543	0.54	0.8933737653	1.260361948
0.6010652	0.965139	0.555	0.9110416678	0.8688140546
0.6135784	0.9814764	0.57	0.915255149	-0.3530060006
0.6232648	0.9979174	0.585	0.9163732773	0.4890230607
0.6353656	1.0142154	0.6	0.9275233967	0.8792576405
0.6447648	1.0302654	0.615	0.9399816885	0.673177482
0.6569652	1.046133	0.63	0.9503827681	0.6378058508
0.6663652	1.0618334	0.645	0.9590269548	0.4633363769
0.6780932	1.0774156	0.66	0.9699853551	0.9431916229
0.6870656	1.0927652	0.675	0.9830297701	0.7564507123
0.6985632	1.1079356	0.69	0.9919658955	0.4216494522
0.7075648	1.1230088	0.705	0.999952488	0.6380581699