

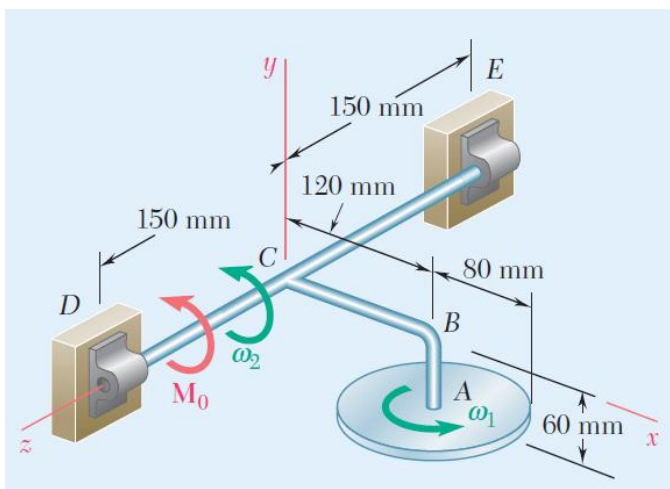
Statement of the problem

A **2.5-kg homogeneous disk** of **80 mm radius** is free to rotate with respect to **arm ABC**, which is welded to a **shaft DCE** supported by bearings at **D** and **E**. Both the arm and the shaft have **negligible mass**. At time **$t = 0$** , a couple **$\mathbf{M}_0 = (0.5 \text{ N} \cdot \text{m}) \mathbf{k}$** is applied to shaft **DCE**. It is known that at **$t = 0$** the angular velocity of the disk is **$\boldsymbol{\omega}_1 = (60 \text{ rad/s}) \mathbf{j}$** , and that friction in the bearing at **A** causes the magnitude of **$\boldsymbol{\omega}_1$** to decrease at a rate of **15 rad/s^2** .

Determine the **dynamic reactions** exerted on the shaft by the bearings at **D** and **E** at any time **t** . Resolve these reactions into components directed along the **x** and **y** axes rotating with the shaft.

Using computational software:

- calculate the components of the reactions for **$0 \leq t \leq 4 \text{ s}$** ;
- determine the times **t_1** and **t_2** at which the **x** and **y** components of the reaction at **E** are respectively equal to zero.



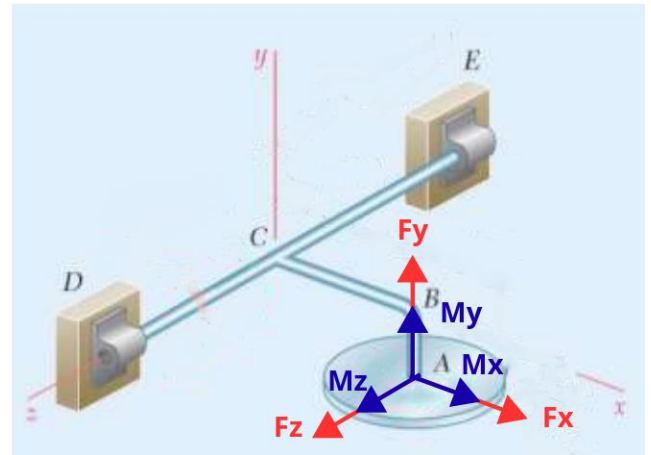
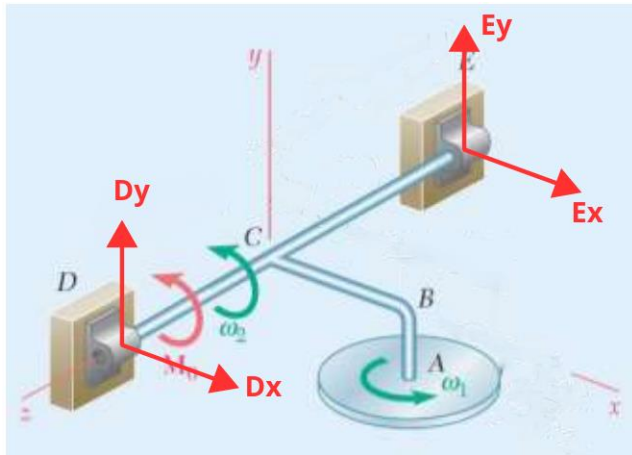
**Beer, F. P.; Johnston Jr., E. R.; Mazurek, D. F.;
Cornwell, P. J.; Self, B. P.**

*Vector Mechanics for Engineers: Statics and
Dynamics.*

McGraw-Hill Education, **11th Edition**, 2016.
Problems **18.C4** (Dynamics, 9th Edition) and
18.C5 (Dynamics, 7th Edition).

Analytical solution

To find the reactions at points D and E, one must first establish an equivalence between the forces at D and E and the forces and moments at the center of mass of the body.



1) Angular Momentum at A

Angular Momentum Equation in a Rotating Reference Frame

$$\sum \vec{M}_A = \overrightarrow{(\dot{H}_A)_{xyz}} + \vec{\Omega} \times \vec{H}_A$$

Angular momentum expression

$$\vec{H}_A = H_x i + H_y j + H_z k$$

$$\vec{H}_A = I_x \omega_x i + I_y \omega_y j + I_z \omega_z k$$

Moments of inertia of the disk

$$I_x = \frac{1}{4} m R^2 \rightarrow \text{Moment of the disk around the } x - \text{axis.}$$

$$I_y = \frac{1}{2} m R^2 \rightarrow \text{Moment of the disk around the } y - \text{axis.}$$

$$I_z = \frac{1}{4} m R^2 \rightarrow \text{Moment of the disk around the } z - \text{axis.}$$

Angular velocity components

$$\omega_x = 0$$

$$\omega_y = \omega_1$$

$$\omega_z = \omega_2$$

$$\vec{H}_A = \frac{1}{4} m R^2 0 i + \frac{1}{2} m R^2 \omega_1 j + \frac{1}{4} m R^2 \omega_2 k$$

$$\vec{H}_A = \frac{1}{2} m R^2 \omega_1 j + \frac{1}{4} m R^2 \omega_2 k$$

$$\vec{\dot{H}}_A = \frac{1}{2} m R^2 \dot{\omega}_1 j + \frac{1}{4} m R^2 \dot{\omega}_2 k$$

Angular velocity of the rotating reference frame

$$\vec{\Omega} = \omega_2 k$$

Final moment equation

$$\vec{M}_A = \left(\frac{1}{2} m R^2 \dot{\omega}_1 j + \frac{1}{4} m R^2 \dot{\omega}_2 k \right) + (\omega_2 k) \times \left(\frac{1}{2} m R^2 \omega_1 j + \frac{1}{4} m R^2 \omega_2 k \right)$$

$$\vec{M}_A = -\frac{1}{2}mR^2\omega_1\omega_2i + \frac{1}{2}mR^2\dot{\omega}_1j + \frac{1}{4}mR^2\dot{\omega}_2k$$

2) Forces in A

$$m\vec{a}_a = m(\vec{a}_c + \vec{a}_{a/c})$$

Since point C is fixed,

$$a_c = 0$$

$$\begin{aligned} m\vec{a}_a &= m\vec{a}_{a/c} \\ m\vec{a}_a &= m(\dot{\omega}_2 \times \vec{r}_{a/c} - \omega_2^2 \vec{r}_{a/c}) \end{aligned}$$

$$\vec{r}_{a/c} = -d_{AB}j + d_{BC}i$$

$$\begin{aligned} m\vec{a}_a &= m(\dot{\omega}_2 k \times (-d_{AB}j + d_{BC}i) - \omega_2^2(-d_{AB}j + d_{BC}i)) \\ m\vec{a}_a &= m(\dot{\omega}_2 k \times (-d_{AB}j + d_{BC}i) - \omega_2^2(-d_{AB}j + d_{BC}i)) \\ m\vec{a}_a &= m\dot{\omega}_2 d_{AB}i + m\dot{\omega}_2 d_{BC}j + m\omega_2^2 d_{AB}j - m\omega_2^2 d_{BC}i \\ \vec{F}_A &= (m\dot{\omega}_2 d_{AB} - m\omega_2^2 d_{BC})i + (m\dot{\omega}_2 d_{BC} + m\omega_2^2 d_{AB})j \end{aligned}$$

3) Moment in D

Note: Here, it is also possible to calculate the moments at point E with the aim of nullifying the moments generated by the forces E_x and E_y , but it has been opted to do this at point D, nullifying the moments generated by the forces D_x and D_y . Thus:

$$\vec{r}_{d/e} \times \vec{F}_E + \vec{M}_0 = \vec{r}_{d/a} \times \vec{F}_A + \vec{M}_A$$

$$\vec{r}_{d/e} = -d_{ED}k$$

$$\vec{F}_E = E_y j + E_x i$$

$$\vec{M}_0 = M_0 j$$

$$\vec{r}_{d/a} = d_{BC}i + d_{AB}j + d_{CD}k$$

$$\vec{F}_A = (m\dot{\omega}_2 d_{AB} - m\omega_2^2 d_{BC})i + (m\dot{\omega}_2 d_{BC} + m\omega_2^2 d_{AB})j$$

$$\vec{M}_A = -\frac{1}{2}mR^2\omega_1\omega_2i + \frac{1}{2}mR^2\dot{\omega}_1j + \frac{1}{4}mR^2\dot{\omega}_2k$$

Determination of $\vec{r}_{d/e} \times \vec{F}_E + \vec{M}_0$

$$\begin{aligned} &\vec{r}_{d/e} \times \vec{F}_E + \vec{M}_0 \\ &[-d_{ED}k \times (E_y j + E_x i) + M_0 k] \\ &\begin{bmatrix} d_{ED}E_y i - d_{ED}E_x j + M_0 k \\ d_{ED}E_y i - d_{ED}E_x j + M_0 k \end{bmatrix} \end{aligned}$$

Determination of $\vec{r}_{d/a} \times \vec{F}_A + \vec{M}_A$

$$\begin{aligned} &\vec{r}_{d/a} \times \vec{F}_A + \vec{M}_A \\ &(d_{BC}i - d_{AB}j - d_{CD}k) \times ((m\dot{\omega}_2 d_{AB} - m\omega_2^2 d_{BC})i + (m\dot{\omega}_2 d_{BC} + m\omega_2^2 d_{AB})j) + \vec{M}_A \end{aligned}$$

$$\begin{aligned} &\begin{bmatrix} md_{CD}(\dot{\omega}_2 d_{BC} + \omega_2^2 d_{AB})i - \frac{1}{2}mR^2\omega_1\omega_2i \\ -md_{CD}(\dot{\omega}_2 d_{AB} - \omega_2^2 d_{BC})j + \frac{1}{2}mR^2\dot{\omega}_1j \\ m\dot{\omega}_2(d_{BC}^2 + d_{AB}^2)k + \frac{1}{4}mR^2\dot{\omega}_2k \end{bmatrix} \end{aligned}$$

By equating each component of k

$$M_0 = m\dot{\omega}_2(d_{BC}^2 + d_{AB}^2) + \frac{1}{4}mR^2\dot{\omega}_2$$

$$M_0 = \dot{\omega}_2 m \left((d_{BC}^2 + d_{AB}^2) + \frac{1}{4}R^2 \right)$$

$$\dot{\omega}_2 = \frac{M_0}{\left((d_{BC}^2 + d_{AB}^2) + \frac{1}{4}R^2 \right)}$$

By equating each component of j

$$-d_{ED}E_x = -md_{CD}(\dot{\omega}_2 d_{AB} - \omega_2^2 d_{BC}) + \frac{1}{2}mR^2\dot{\omega}_1$$

$$E_x = \frac{-md_{CD}(\dot{\omega}_2 d_{AB} - \omega_2^2 d_{BC}) + \frac{1}{2}mR^2\dot{\omega}_1}{-d_{ED}}$$

By equating each component of i

$$d_{ED}E_y = md_{CD}(\dot{\omega}_2 d_{BC} + \omega_2^2 d_{AB}) - \frac{1}{2}mR^2\omega_1\omega_2$$

$$E_y = \frac{md_{CD}(\dot{\omega}_2 d_{BC} + \omega_2^2 d_{AB}) - \frac{1}{2}mR^2\omega_1\omega_2}{d_{ED}}$$

$$4) \sum \mathbf{F} = m\mathbf{a}_A$$

Note: Similarly to what was done in the previous item, the moments could also be taken about point **E** to determine the reactions at **D**. However, once the reactions at point **E** are known, it is simpler to compute the sum of forces; therefore, this approach was adopted.

$$\sum F = ma_A$$

$$E_x i + D_x i + E_y j + D_y j = (m\dot{\omega}_2 d_{AB} - m\omega_2^2 d_{BC})i + (m\dot{\omega}_2 d_{BC} + m\omega_2^2 d_{AB})j$$

By equating each component of i

$$E_x + D_x = m\dot{\omega}_2 d_{AB} - m\omega_2^2 d_{BC}$$

$$D_x = m\dot{\omega}_2 d_{AB} - m\omega_2^2 d_{BC} - E_x$$

By equating each component of j

$$E_y + D_y = m\dot{\omega}_2 d_{BC} + m\omega_2^2 d_{AB}$$

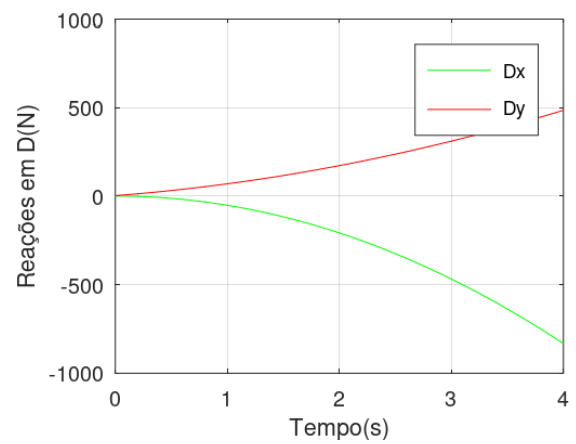
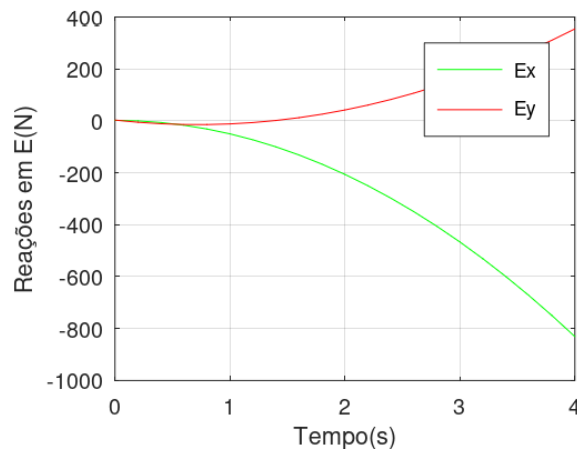
$$D_y = m\dot{\omega}_2 d_{BC} + m\omega_2^2 d_{AB} - E_y$$

Reactions as Functions of Time

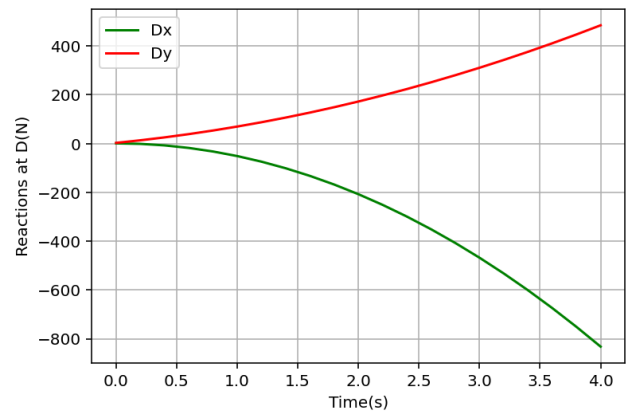
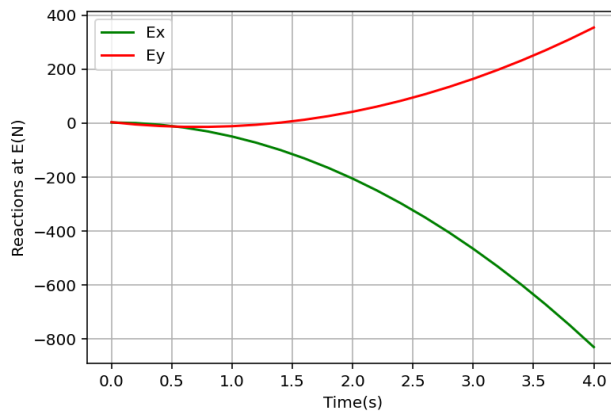
To obtain the reactions as functions of time, it is sufficient to express the angular velocities as functions of time, that is, by replacing ω_2 with $\dot{\omega}_2 t$ and ω_1 with $\omega_{1,\text{initial}} + \dot{\omega}_1 t$.

Computational Implementation

1) Matlab Graphs



2) Python Graphs



3) Time at Which the Reactions at Point E Are Equal to Zero

Having the equations $E_x(t)$ and $E_y(t)$, computational numerical methods can be used to determine the points at which $E_x(t)$ and $E_y(t)$ are equal to zero. In this case, the **bisection method** was employed to find the roots of the equations, leading to the following times.

Equation	Time (from 0s to 4s)
$E_x(t)$	0.19651931s
$E_y(t)$	0.06549466s
	1.36690485s

Simulation

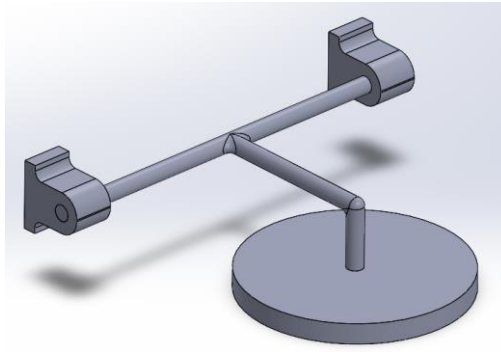
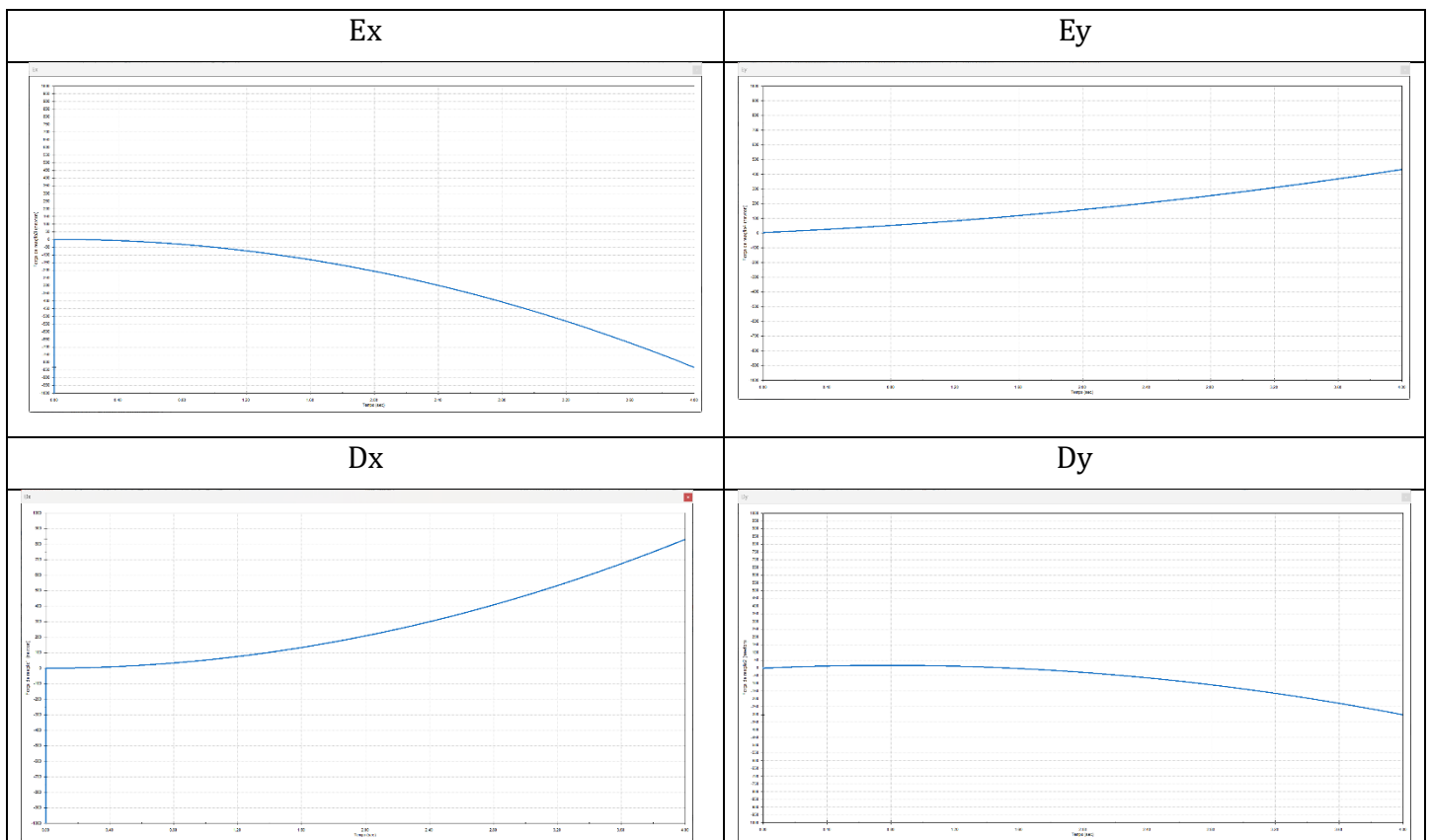


Illustration of the component modeled in SolidWorks

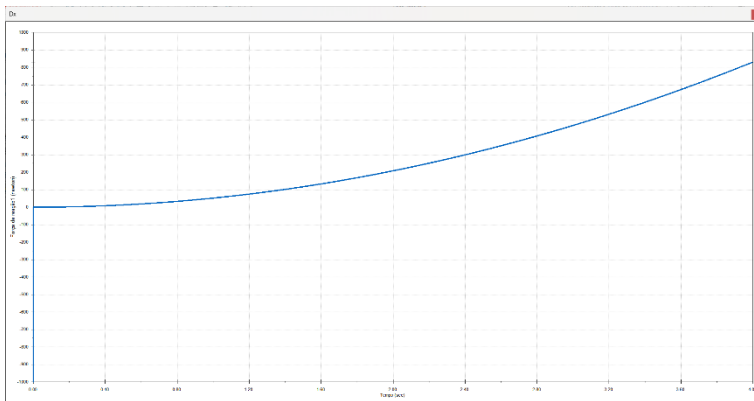
The plots generated using SolidWorks are shown below.



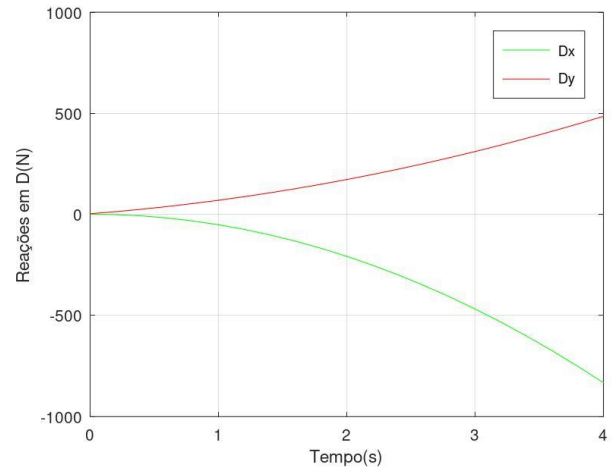
Results

The results obtained from the analytical/programming approach and from the simulation are consistent with each other. This can be observed by comparing the graphs from both approaches. It is worth noting that, due to a convention adopted by the software, the D_x and D_y values in the SolidWorks graphs have the opposite sign compared to those adopted in the MATLAB and Python graphs.

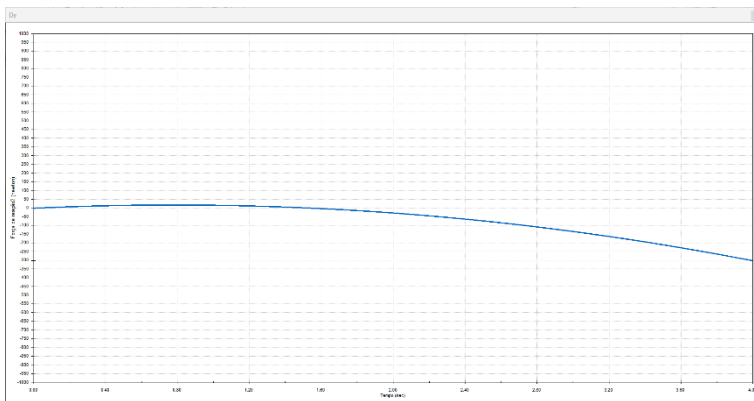
1) Reaction of D



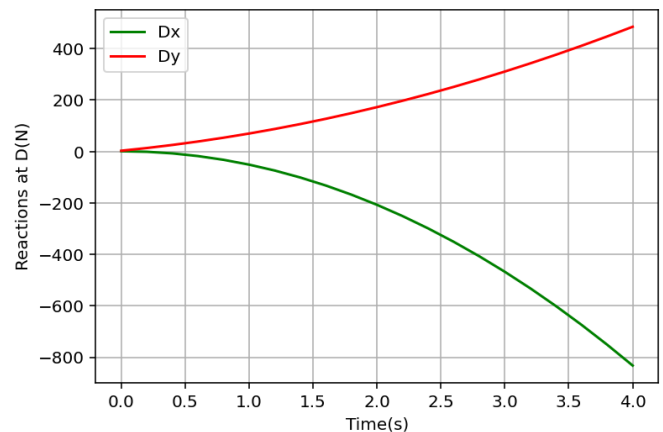
Graph of the reaction force at D in the x-direction (SolidWorks)



Graphs of the reaction force at D (MATLAB)

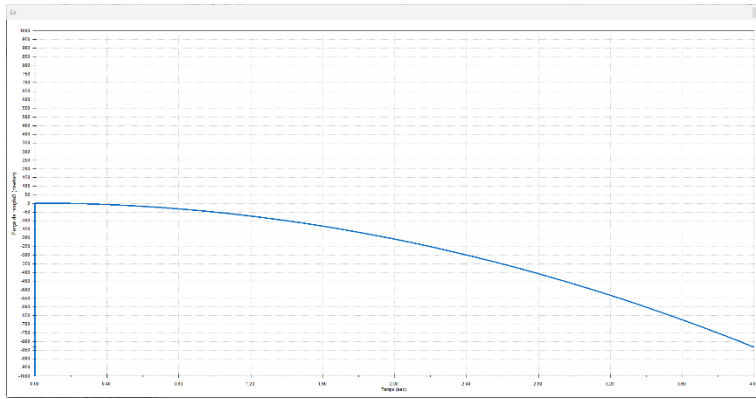


Graph of the reaction force at D in the y-direction (SolidWorks)

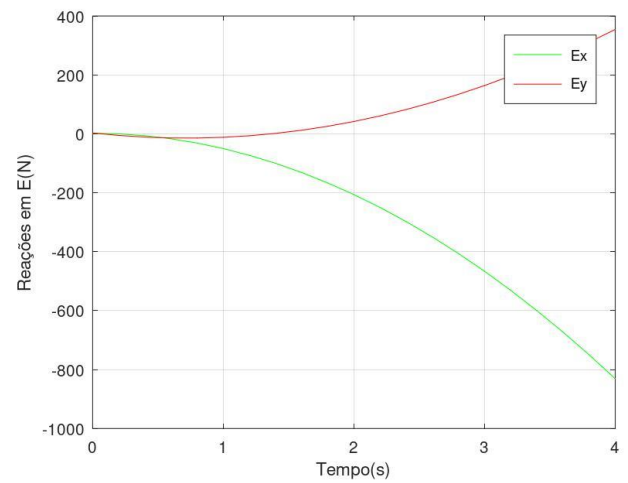


Graphs of the reaction force at D (Python)

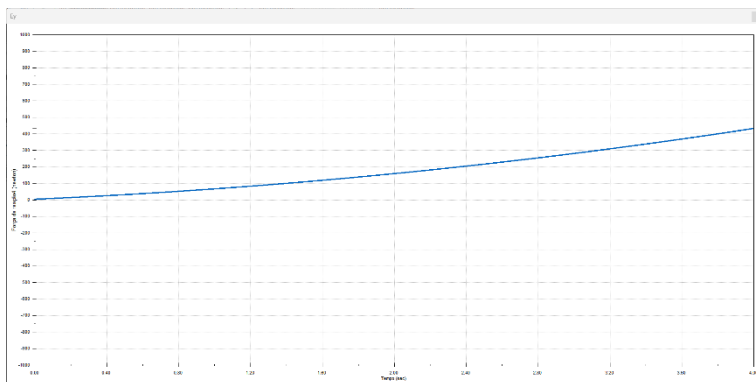
2) Reaction of E



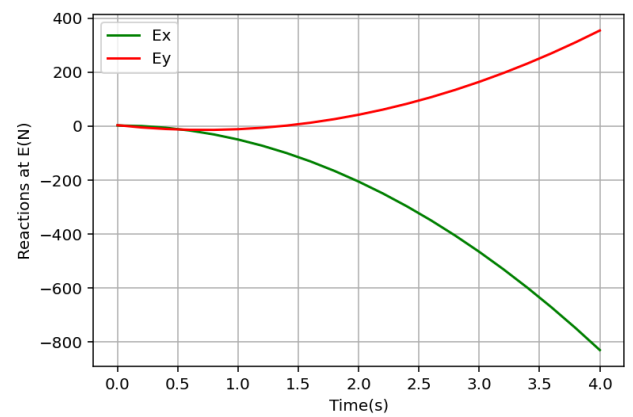
Graph of the reaction force at E in the x-direction (SolidWorks)



Graphs of the reaction force at D (MATLAB)



Graph of the reaction force at E in the y-direction (SolidWorks)



Graphs of the reaction force at E (Python)