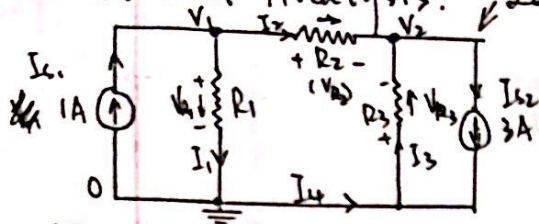


1. Circuit Analysis. Labeling. So  $A\vec{x} = \vec{b}$  where



Using KCL, so:

$$\vec{x} = [I_1 \ I_2 \ I_3 \ I_4 \ V_{R1} \ V_{R2} \ V_{R3} \ V_1 \ V_2]^T$$

$$\begin{cases} I_1 = 1A = I_4 + I_2 \\ I_2 + I_3 = I_{S2} = 3A \\ I_1 = I_4 + I_{S1} = I_4 + 1A \\ (I_3 = I_4 + I_{S2} = I_4 + 3A) \end{cases} \Rightarrow \begin{cases} I_1 + I_2 = 1A \quad (1) \\ I_2 + I_3 = 3A \quad (2) \\ I_1 - I_4 = 1A \quad (3) \end{cases}$$

Then, using Ohm's Law, so:

and also:

$$\begin{cases} V_{R1} = R_1 \cdot I_1 = 10I_1 \\ V_{R2} = R_2 \cdot I_2 = 20I_2 = 20 - 20I_1 \\ V_{R3} = R_3 \cdot I_3 = 50I_3 = 50I_1 + 100 \\ V_1 - 0 = V_{R1} \\ V_1 - V_2 = V_{R2} \Rightarrow V_2 = 30I_1 + 20 \\ V_2 - 0 = -V_{R3} \Rightarrow V_2 = -50I_1 - 100 \end{cases} \Rightarrow \begin{cases} V_{R1} - R_1 \cdot I_1 = 0 \quad (4) \\ V_{R2} - R_2 \cdot I_2 = 0 \quad (5) \\ V_{R3} - R_3 \cdot I_3 = 0 \quad (6) \\ V_1 - V_{R1} = 0 \quad (7) \\ V_1 - V_2 - V_{R2} = 0 \quad (8) \\ V_2 + V_{R3} = 0 \quad (9) \end{cases}$$

Using Equations (1)-(9), we can setup  $A\vec{x} = \vec{b}$  as:

$I_1 = 1A$   
 $I_2 = I_{S2}$   
 $I_3 = I_{S1}$   
 $V_{R1} = 10I_1$   
 $V_{R2} = 20I_2$   
 $V_{R3} = 50I_3$   
 $I_1 = 1A$

$$\begin{bmatrix} 1 & 1 & 0 & 0 & 0 & 0 & 0 & 0 & 0 \\ 0 & 1 & 1 & 0 & 0 & 0 & 0 & 0 & 0 \\ 1 & 0 & 0 & -1 & 0 & 0 & 0 & 0 & 0 \\ -R_1 & 0 & 0 & 0 & 1 & 0 & 0 & 0 & 0 \\ 0 & -R_2 & 0 & 0 & 0 & 1 & 0 & 0 & 0 \\ 0 & 0 & -R_3 & 0 & 0 & 0 & 1 & 0 & 0 \\ 0 & 0 & 0 & 0 & -1 & 1 & 0 & 0 & 0 \\ 0 & 0 & 0 & 0 & 0 & -1 & 0 & 1 & -1 \\ 0 & 0 & 0 & 0 & 0 & 0 & 1 & 0 & 1 \end{bmatrix} \begin{bmatrix} I_1 \\ I_2 \\ I_3 \\ I_4 \\ V_{R1} \\ V_{R2} \\ V_{R3} \\ V_1 \\ V_2 \end{bmatrix} = \begin{bmatrix} 1 \\ 3 \\ 1 \\ 0 \\ 0 \\ 0 \\ 0 \\ 0 \\ 0 \end{bmatrix}$$

With  $R_1 = 10\Omega$   
 $R_2 = 20\Omega$   
 $R_3 = 50\Omega$

So,

$$\begin{bmatrix} I_1 \\ I_2 \\ I_3 \\ I_4 \\ V_{R1} \\ V_{R2} \\ V_{R3} \\ V_1 \\ V_2 \end{bmatrix} = \begin{bmatrix} -1 & A \\ 2 & A \\ -1 & A \\ -2 & A \\ -10 & V \\ 40 & V \\ 50 & V \\ -10 & V \\ -50 & V \end{bmatrix}$$

## 2. Cell Phone Battery

(a) 35.1 hours

Since  $P = I \cdot V$ , so we have

$$I = \frac{P}{V} = \frac{0.3W}{3.8V} = 7.89 \cdot 10^{-2} A = 78.9mA$$

Then, with  $C = I \cdot t$ , so we have

$$t = \frac{C}{I} = \frac{2770mAh}{78.9} = 35.1hr$$

Thus, a Pixel's full battery will last 35.1 hours under regular usage conditions.

(b)  $6.22 \cdot 10^{22}$  electrons

Since  $2770 \text{ mAh} = 2770 \text{ mAh} \cdot \frac{3600s}{1h} = 9.972 \cdot 10^6 \text{ mAs}$ , and given that  $1 \text{ mC} = 1 \text{ mAs}$ ,

so  $C_{pixel} = 2770 \text{ mAh} = 9.972 \cdot 10^6 \text{ mAs} = 9.972 \cdot 10^6 \text{ mC}$

So, there are  $\frac{C_{pixel}}{C_{electron}} = \frac{9.972 \cdot 10^3 C}{1.602 \cdot 10^{-19} C} = 6.22 \cdot 10^{22}$  usable electrons worth of charge.

(c)  $3.79 \cdot 10^4 \text{ J}$

Since we could calculate that:

$$E_{discharge} = P \cdot t = 0.3 \text{ W} \cdot 35.1 \text{ hr} \cdot \frac{3600 \text{ s}}{1 \text{ hr}} = 3.79 \cdot 10^4 \text{ Ws} = 3.79 \cdot 10^4 \text{ J}$$

Thus, we have that

$$E_{charge} = E_{discharge} = 3.79 \cdot 10^4 \text{ J}$$

So,  $3.79 \cdot 10^4 \text{ J}$  is the energy necessary for recharging a completely discharged cell phone battery.

(d) \$0.04

The total energy used by recharging for 31 days is:

$$E_{total} = E_{charge} \cdot 31 = 3.79 \cdot 10^4 \text{ J} \cdot 31 = 1.175 \cdot 10^6 \text{ J} = 1.175 \cdot 10^6 \text{ Ws}$$

So, we can transform its unit to get:

$$E_{total} = 1.175 \cdot 10^6 \text{ Ws} \cdot \frac{1 \text{ kW}}{1000 \text{ W}} \cdot \frac{1 \text{ hr}}{3600 \text{ s}} = 0.326 \text{ kWh}$$

Thus, I would need to pay  $0.326 \text{ kWh} \cdot \frac{\$0.12}{1 \text{ kWh}} = \$0.04$  for recharging for the month of October.

(e)

First,  $R = 200m\Omega = 200m\Omega \cdot \frac{1\Omega}{1000m\Omega} = 0.2\Omega$ . We consider  $R_{bat} = 1m\Omega, 1\Omega, 10k\Omega$  separately below.

Case 1 ( $R_{bat} = 1\ m\Omega$ ): With  $R_{eq} = R + R_{bat} = 200m\Omega + 1m\Omega = 201m\Omega$ , so

$$I_{bat} = I = \frac{V}{R_{eq}} = \frac{5V}{201m\Omega} = 24.88A$$

So the power dissipated across  $R_{bat}$  is:

$$P_{bat} = I_{bat}V_{bat} = I_{bat}^2 R_{bat} = (24.88A)^2 \cdot 1m\Omega = 0.62\ W$$

Thus, using the results we got from part (d), so it takes the battery

$$t = \frac{E_{total}}{P} = \frac{3.79 \cdot 10^4\ Ws}{0.62W} = 6.11 \cdot 10^4 s = 6.11 \cdot 10^4 s \cdot \frac{1hr}{3600s} = 16.98\ hr$$

Case 2 ( $R_{bat} = 1\ \Omega$ ): With  $R_{eq} = R + R_{bat} = 0.2\Omega + 1m\Omega = 1.2m\Omega$ , so

$$I_{bat} = I = \frac{V}{R_{eq}} = \frac{5V}{1.2\Omega} = 4.17A$$

So the power dissipated across  $R_{bat}$  is:

$$P_{bat} = I_{bat}V_{bat} = I_{bat}^2 R_{bat} = (4.17A)^2 \cdot 1\Omega = 17.39\ W$$

Thus, using the results we got from part (d), so it takes the battery

$$t = \frac{E_{total}}{P} = \frac{3.79 \cdot 10^4\ Ws}{17.39W} = 2.18 \cdot 10^3 s = 2.18 \cdot 10^3 s \cdot \frac{1hr}{3600s} = 0.605\ hr = 36.3\ min$$

Case 3 ( $R_{bat} = 10\ k\Omega$ ): With  $R_{eq} = R + R_{bat} = 0.2\Omega + 10k\Omega = 10000.2\ \Omega$ , so

$$I_{bat} = I = \frac{V}{R_{eq}} = \frac{5V}{10000.2\Omega} = 5.00 \cdot 10^{-4}\ A$$

So the power dissipated across  $R_{bat}$  is:

$$P_{bat} = I_{bat}V_{bat} = I_{bat}^2 R_{bat} = (5.00 \cdot 10^{-4}A)^2 \cdot 10k\Omega = 2.5 \cdot 10^{-3}\ W$$

Thus, using the results we got from part (d), so it takes the battery

$$t = \frac{E_{total}}{P} = \frac{3.79 \cdot 10^4\ Ws}{2.5 \cdot 10^{-3}W} = 1.52 \cdot 10^7 s = 1.52 \cdot 10^7 s \cdot \frac{1hr}{3600s} = 4.22 \cdot 10^3\ hr$$

### 3. Fruity Fred

(a)  $R_{AB} = \rho \frac{L-kF}{A_c} + \rho \frac{L-kF}{A_c} = \frac{2\rho(L-kF)}{A_c}$

(b)  $F = \frac{A_c V_{out} + 2\rho L(V_{out} - 1)}{2\rho k(V_{out} - 1)}$

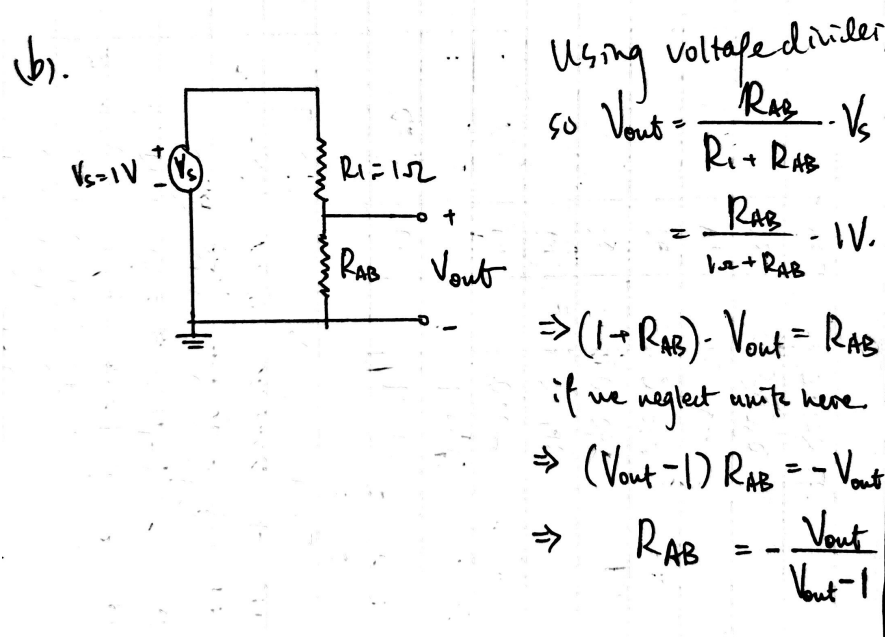


Figure 1: Circuit Designed

As deduced from the process on the picture, so  $R_{AB} = -\frac{V_{out}}{V_{out} - 1}$ . Also, as we derived from part (a), which gives  $R_{AB} = \frac{2\rho(L-kF)}{A_c}$ . Thus, we have that:

$$\begin{aligned} R_{AB} &= \frac{2\rho(L-kF)}{A_c} = -\frac{V_{out}}{V_{out} - 1} \\ \Rightarrow 2\rho(L-kF) \cdot -(V_{out} - 1) &= A_c \cdot V_{out} \\ \Rightarrow (2\rho L - 2\rho kF) \cdot -(V_{out} - 1) &= A_c \cdot V_{out} \\ \Rightarrow -2\rho L(V_{out} - 1) + 2\rho k(V_{out} - 1)F &= A_c \cdot V_{out} \\ \Rightarrow 2\rho k(V_{out} - 1)F &= A_c \cdot V_{out} + 2\rho L(V_{out} - 1) \\ \Rightarrow F &= \frac{A_c V_{out} + 2\rho L(V_{out} - 1)}{2\rho k(V_{out} - 1)} \end{aligned}$$

#### 4. Temperature Sensor

(a)  $V_{out} = \frac{V_s R_2}{R_1 + R_2}$

The current through the circuit is  $I = \frac{V_s}{R_{eq}}$ , where  $R_{eq} = R_1 + R_2$ , so  $I = \frac{V_s}{R_1 + R_2}$

So,  $V_{out}$ , which measures the voltage drop over  $R_2$ , is equal to (or we could've used the Voltage Divider formula directly to obtain):

$$V_2 = I_2 \cdot R_2 = I \cdot R_2 = \frac{V_s}{R_1 + R_2} \cdot R_2 = \frac{V_s R_2}{R_1 + R_2}$$

Thus,  $V_{out} = V_2 = \frac{V_s R_2}{R_1 + R_2}$

(b)  $T = \frac{V_s R_o - V_{out} R_1 - V_{out} R_o}{(V_{out} - V_s) R_o \alpha}$

Similarly, the current through the circuit is  $I = \frac{V_s}{R_{eq}}$ , where  $R_{eq} = R_1 + R_2 = R_1 + R_o(1 + \alpha T)$ , so  $I = \frac{V_s}{R_1 + R_o(1 + \alpha T)}$

So,  $V_{out}$ , which measures the voltage drop over  $R_2$ , is equal to:

$$V_2 = I_2 \cdot R_2 = I \cdot R_2 = \frac{V_s}{R_1 + R_o(1 + \alpha T)} \cdot R_o(1 + \alpha T) = \frac{V_s R_o(1 + \alpha T)}{R_1 + R_o(1 + \alpha T)}$$

Thus,  $V_{out} = V_2 = \frac{V_s R_o(1 + \alpha T)}{R_1 + R_o(1 + \alpha T)}$ , which gives us that:  $V_{out} \cdot (R_1 + R_o(1 + \alpha T)) = V_s R_o(1 + \alpha T)$

So,  $V_{out} R_1 + V_{out} R_o + V_{out} R_o \alpha T = V_s R_o + V_s R_o \alpha T$ , which gives:

$$\begin{aligned} V_{out} R_o \alpha T - V_s R_o \alpha T &= V_s R_o - V_{out} R_1 - V_{out} R_o \\ \implies (V_{out} - V_s) R_o \alpha \cdot T &= V_s R_o - V_{out} R_1 - V_{out} R_o \\ \implies T &= \frac{V_s R_o - V_{out} R_1 - V_{out} R_o}{(V_{out} - V_s) R_o \alpha} \end{aligned}$$

(c)  $T = \frac{V_s R_o - V_{out} R_1 - V_{out} R_o}{-V_s R_o \alpha + V_{out} R_1 \beta + V_{out} R_o \alpha}$

Again, similarly, the current through the circuit is  $I = \frac{V_s}{R_{eq}}$ , where  $R_{eq} = R_1' + R_2 = R_1(1 + \beta T) + R_o(1 + \alpha T)$ , so  $I = \frac{V_s}{R_1(1 + \beta T) + R_o(1 + \alpha T)}$

So,  $V_{out}$ , which measures the voltage drop over  $R_2$ , is equal to:

$$V_2 = I_2 \cdot R_2 = I \cdot R_2 = \frac{V_s}{R_1(1 + \beta T) + R_o(1 + \alpha T)} \cdot R_o(1 + \alpha T) = \frac{V_s R_o(1 + \alpha T)}{R_1(1 + \beta T) + R_o(1 + \alpha T)}$$

Thus,  $V_{out} = V_2 = \frac{V_s R_o(1 + \alpha T)}{R_1(1 + \beta T) + R_o(1 + \alpha T)}$ , which gives us that:

$$\begin{aligned} V_{out} \cdot (R_1(1 + \beta T) + R_o(1 + \alpha T)) &= V_s R_o(1 + \alpha T) \\ \implies V_{out} R_1 + V_{out} R_1 \beta T + V_{out} R_o + V_{out} R_o \alpha T &= V_s R_o + V_s R_o \alpha T \\ \implies (V_{out} R_1 \beta + V_{out} R_o \alpha - V_s R_o \alpha) \cdot T &= V_s R_o - V_{out} R_1 - V_{out} R_o \end{aligned}$$

$$\Rightarrow T = \frac{V_s R_o - V_{out} R_1 - V_{out} R_o}{-V_s R_o \alpha + V_{out} R_1 \beta + V_{out} R_o \alpha}$$

(d) No, it can't.

Here, we use the derived formula of voltage dividers directly to obtain the voltage drop over  $R_2$ :

$$V_2 = \frac{V_s \cdot R_{o2} \cdot (1 + \alpha T)}{(R_{o1} + R_{o2}) \cdot (1 + \alpha T)} = \frac{V_s R_{o2}}{R_{o1} + R_{o2}}$$

Thus,  $V_{out} = V_2 = \frac{V_s R_{o2}}{R_{o1} + R_{o2}}$ , which is independent of the variable  $T$ , which implies that we cannot express the temperature  $T$  as an equation in terms of the measurable variables. Therefore, this circuit (specifically the measurements of  $V_{out}$ ) cannot be used to measure temperature.

## 5. Multitouch Resistive Touchscreen

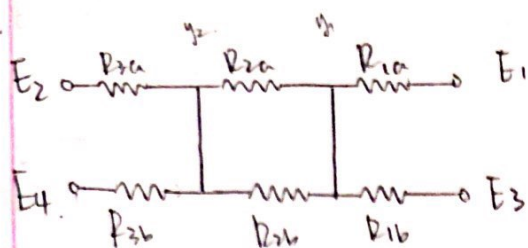
(a)  $4k\Omega$

Since  $W = 3cm = 0.03m$ ,  $H = 12cm = 0.12m$ ,  $T = 1mm = 1 \cdot 10^{-3}m = 0.001m$ , so we can calculate the resistance between  $E_1$  and  $E_2$  as:

$$R = \rho \cdot \frac{L}{A} = \rho \cdot \frac{H}{W \cdot T} = 1\Omega m \cdot \frac{0.12m}{0.03m \cdot 0.001m} = 4000\Omega = 4 \text{ k}\Omega$$



1b).

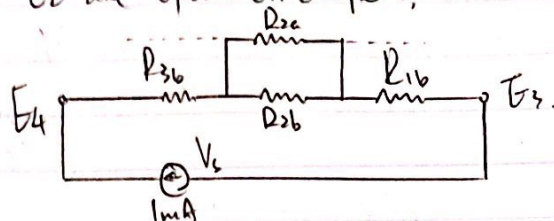


Given that  $R_{total} = l \frac{H}{W \cdot T} = 8 \text{ k}\Omega$ ,  $y_1 = 3 \text{ cm}$ ,  $y_2 = 7 \text{ cm}$ ,  $H = 12 \text{ cm}$   
 with  $R_{total} = 8 \text{ k}\Omega$ ,  
 so  $R_{1a} = R_{1b} = R_{total} \cdot \frac{y_1}{H} = 2 \text{ k}\Omega$ .

$$R_{2a} = R_{2b} = R_{total} \cdot \frac{y_2 - y_1}{H} = 2.667 \text{ k}\Omega.$$

$$R_{3a} = R_{3b} = R_{total} \cdot \frac{H - y_2}{H} = 3.333 \text{ k}\Omega$$

(c). Using the given conditions, since  $E_1$  and  $E_2$  are open-circuited, so no current flow through resistors  $R_{2a}$  and  $R_{1a}$ , which means that the circuit diagram is equivalent to:



We can calculate using methods that the resistance between  $E_4$  and  $E_3$  is:

$$R_{eq} = R_{3b} + \frac{1}{\frac{1}{R_{2a}} + \frac{1}{R_{2b}}} + R_{1b} = R_{total} \cdot \frac{H - y_2}{H} + \frac{1}{2} \cdot R_{total} \cdot \frac{y_2 - y_1}{H} + R_{total} \cdot \frac{y_1}{H}$$

with  $y_1 = 3 \text{ cm}$ ,  $y_2 = 7 \text{ cm}$ ,  $H = 12 \text{ cm}$ , so  $= R_{total} \cdot \frac{H - y_2/2 + y_1/2}{H} = \frac{20}{3} \text{ k}\Omega = 6.667 \text{ k}\Omega$

Thus,  $V_s = I_s \cdot R_{eq} = 1 \text{ mA} \cdot 6.667 \text{ k}\Omega = 6.667 \text{ V}$ .

which means that  $V_{E_4 - E_3} = V_s = \boxed{6.667 \text{ V}}$ .

(d) Using what we've deduced in the steps of part (c), we have that:

$$R_{eq} = R_{total} \cdot \frac{H - y_2/2 + y_1/2}{H}$$

So,  $V_{E_4 - E_3} = V_s = I_s \cdot R_{eq} = 1 \text{ mA} \cdot 8 \text{ k}\Omega \cdot \frac{H - y_2/2 + y_1/2}{H} = 8 \text{ V} \cdot \left(1 - \frac{y_2}{24} + \frac{y_1}{24}\right)$

So,  $\boxed{V_{E_4 - E_3} = \left(8 - \frac{1}{3}y_2 + \frac{1}{3}y_1\right) \text{ V}}$

(e) Using similar logic from part (c) and (d), so we can drive  $E_2, E_4$  with a  $1 \text{ mA}$  current source and measure  $V_{E_4 - E_2} = I_s \cdot R_{eq_{2,4}}$  where

$$R_{eq_{2,4}} = R_{3a} + \frac{1}{\frac{1}{R_{2a}} + \frac{1}{R_{3b}}} + R_{3b} = R_{total} \cdot \left(\frac{H - y_2}{H} + \frac{1}{2} \cdot \frac{y_2 - y_1}{H} + \frac{H - y_2}{H}\right)$$

$$= 8 \text{ k}\Omega \cdot \frac{2H - \frac{3}{2}y_2 - \frac{1}{2}y_1}{H}$$

So,  $V_{E_4 - E_2} = 1 \text{ mA} \cdot 8 \text{ k}\Omega \cdot \left(2 - \frac{3}{24}y_2 - \frac{1}{24}y_1\right) = \left(16 - y_2 - \frac{1}{3}y_1\right) \text{ V}$ .



Similarly,  $R_{eq1,3} = R_{1a} + \frac{1}{\frac{1}{R_{2a}} + \frac{1}{R_{2b}}} + R_{1b} = R_{total} \cdot \left( \frac{y_1}{H} + \frac{1}{2} \cdot \frac{y_2 - y_1}{H} + \frac{y_1}{H} \right)$

$$= 8k\Omega \cdot \left( \frac{y_1 + \frac{1}{2}y_2 - \frac{1}{2}y_1 + y_1}{H} \right) \text{ where } H = 12 \text{ cm}$$

$$= 8k\Omega \cdot \left( \frac{1}{8}y_1 + \frac{1}{24}y_2 \right)$$

And, providing/driving  $E_1, E_3$  with a 1mA current source gives:

$$V_{E_1 - E_3} = I_s R_{eq1,3} = 1mA \cdot 8k\Omega \left( \frac{1}{8}y_1 + \frac{1}{24}y_2 \right)$$

$$\text{So } V_{E_1 - E_3} = \left( y_1 + \frac{1}{3}y_2 \right) V$$

Thus, we have two (plus one) equations:

$$V_{E_4 - E_2} = \left( 16 - \frac{1}{3}y_1 - y_2 \right) V$$

$$V_{E_1 - E_3} = \left( y_1 + \frac{1}{3}y_2 \right) V$$

$$[\text{from (1)}] \quad V_{E_4 - E_3} = \left( 8 + \frac{1}{3}y_1 - \frac{1}{3}y_2 \right) V$$

## **6. Homework Process and Study Group**

I worked alone without getting any help, except asking questions and reading posts (especially answers from the GSIs) on Piazza as well as reading the Notes of the course.