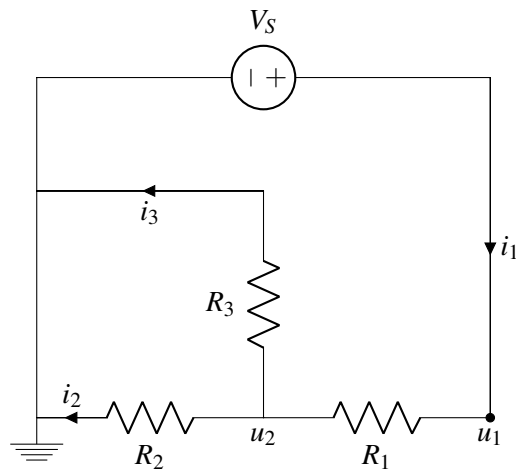




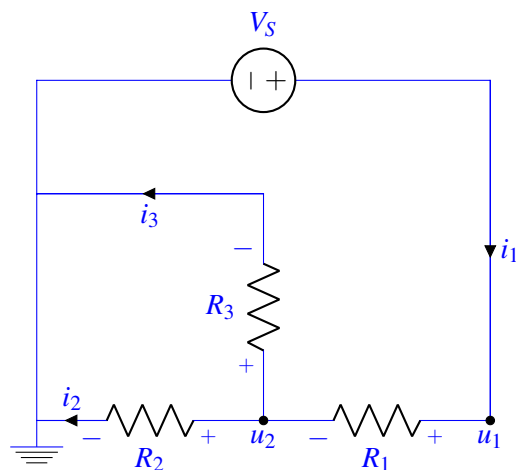
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### 3. Seven Steps of Highly Resistive Circuits (10 points)

- (a) (3 point) Label the +/- polarity of voltage across each resistor element on the following circuit. Be sure to follow passive sign convention using the labeled currents.



**Solution:** Label polarity as shown.



- (b) (7 points) Fill in the following matrix and unknown vector, such that they represent linearly independent equations for the circuit given above. Assume the resistor and voltage source values are known constants. **You do not need to solve this matrix.**

$$\begin{bmatrix} & & & & & \\ & & & & & \\ & & & & & \\ & & & & & \\ & & & & & \\ & & & & & \end{bmatrix} \begin{bmatrix} i_1 \\ i_2 \\ i_3 \\ u_1 \\ u_2 \end{bmatrix} = \begin{bmatrix} \\ \\ \\ \\ \end{bmatrix}$$

**Solution:**

$$i_1 = i_2 + i_3$$

$$u_1 - u_2 = i_1 R_1$$

$$u_2 - 0 = i_2 R_2$$

$$u_2 - 0 = i_3 R_3$$

$$u_1 - 0 = V_s$$

$$\begin{bmatrix} 1 & -1 & -1 & 0 & 0 \\ -R_1 & 0 & 0 & 1 & -1 \\ 0 & -R_2 & 0 & 0 & 1 \\ 0 & 0 & -R_3 & 0 & 1 \\ 0 & 0 & 0 & 1 & 0 \end{bmatrix} \begin{bmatrix} i_1 \\ i_2 \\ i_3 \\ u_1 \\ u_2 \end{bmatrix} = \begin{bmatrix} 0 \\ 0 \\ 0 \\ 0 \\ V_s \end{bmatrix}$$

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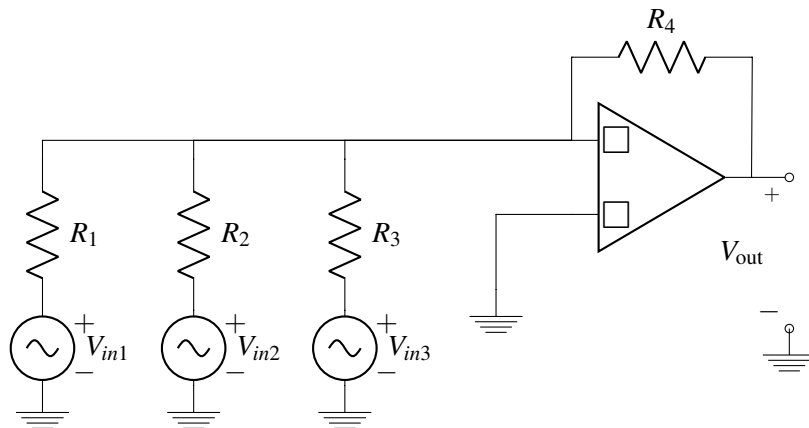
#### 4. "Operational" Amplifiers (12 points)

“As an amplifier so connected can perform the mathematical operations of arithmetic and calculus on the voltages applied to its inputs, it is hereafter termed an ‘operational amplifier’.”

John Ragazzini, Robert Randall and Frederick Russell  
Proceedings of IRE, Vol. 35, May 1947

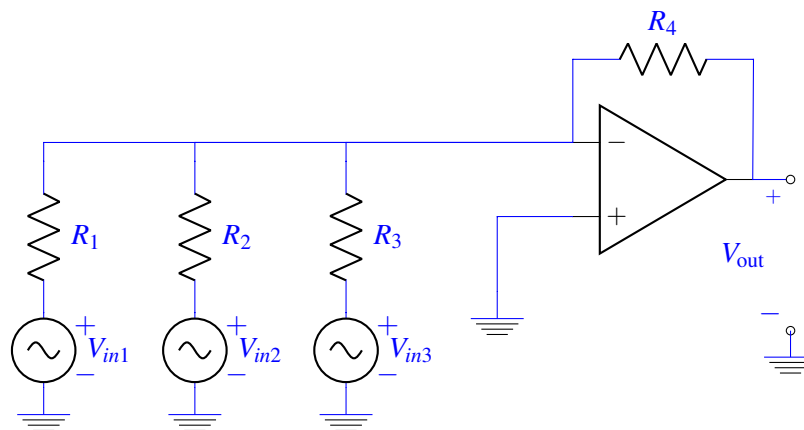
In this problem we will explore some of the mathematical operations an op amp can perform.

(a) (5 points)



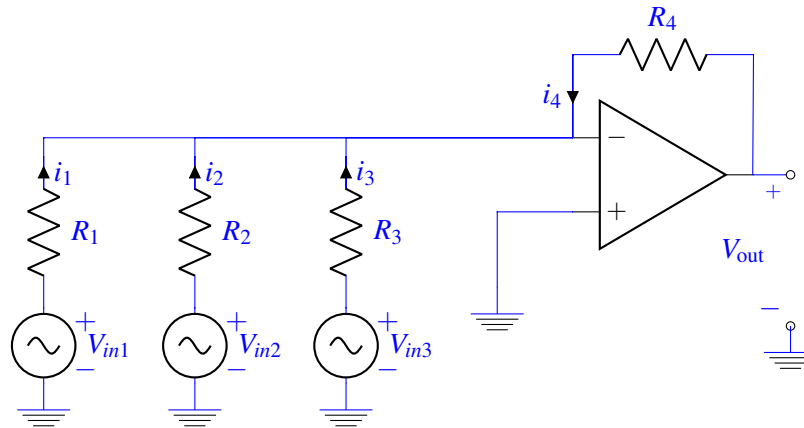
i. Label the '+' and '-' terminals of the op amp above so that it is in negative feedback.

**Solution:**



ii. Derive an expression for  $V_{out}$  as a function of  $V_{in1}$ ,  $V_{in2}$ , and  $V_{in3}$ .

**Solution:**



Since no current enters the op amp, we get the following equation from KCL:

$$i_1 + i_2 + i_3 + i_4 = 0$$

By the Golden Rules  $V_- = V_+ = 0V$ . We use  $V_-$  to calculate the current in each branch:

$$i_1 = \frac{V_{in1}}{R_1} \quad i_2 = \frac{V_{in2}}{R_2}$$

$$i_3 = \frac{V_{in3}}{R_3} \quad i_4 = \frac{V_{out}}{R_4}$$

Putting this together with the KCL equation above yeilds

$$\frac{V_{in1}}{R_1} + \frac{V_{in2}}{R_2} + \frac{V_{in3}}{R_3} + \frac{V_{out}}{R_4} = 0$$

$$v_{out} = -\left(\frac{R_4}{R_1}V_{in1} + \frac{R_4}{R_2}V_{in2} + \frac{R_4}{R_3}V_{in3}\right)$$

iii. Mark the operation below that is best represented by this configuration.

☐ Subtraction

☐ Inner Product

☐ Differentiation

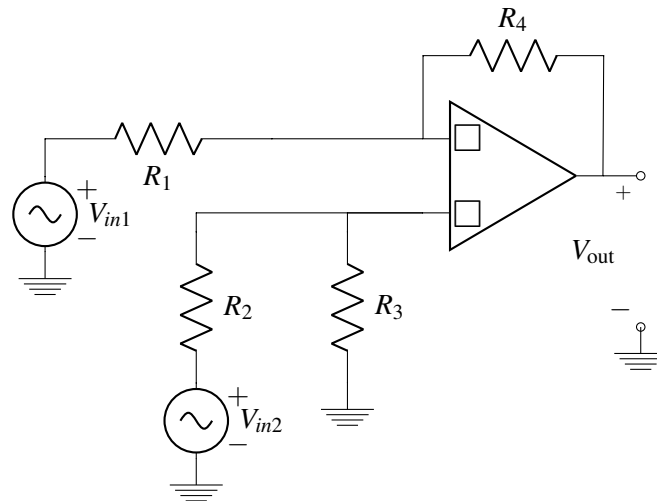
☐ Integration

**Solution:** This operation is the **inner product** between the following two vectors:

$$\begin{bmatrix} V_{in1} & V_{in2} & V_{in3} \end{bmatrix}^T$$

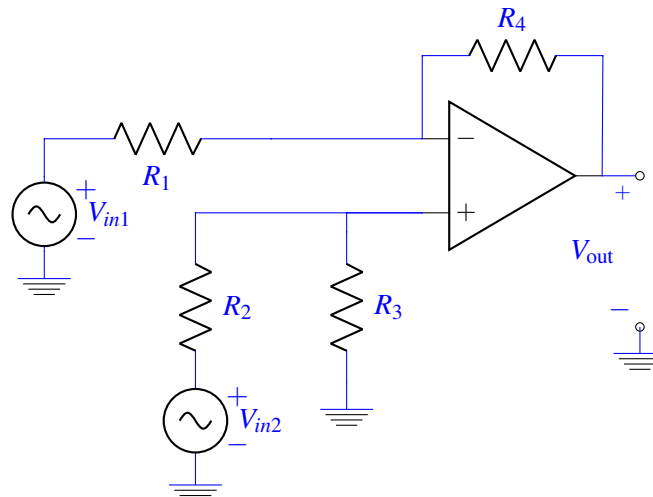
$$\begin{bmatrix} -\frac{R_4}{R_1} & -\frac{R_4}{R_2} & -\frac{R_4}{R_3} \end{bmatrix}^T$$

(b) (7 points)



- i. Label the '+' and '-' terminals of the op amp above so that it is in negative feedback.

**Solution:**



- ii. Derive an expression for  $V_{out}$  as a function of  $V_{in1}$  and  $V_{in2}$ .

**Solution:**

Using superposition:

Nulling  $V_{in1}$ , we see that  $V_+$  is formed by a voltage divider:

$$V_+ = V_{in2} \left( \frac{R_3}{R_2 + R_3} \right)$$

The output amplifies  $V_+$  like a non-inverting amplifier:

$$V_{out2} = V_{in2} \left( \frac{R_3}{R_2 + R_3} \right) \left( 1 + \frac{R_4}{R_1} \right)$$

Nulling  $V_{in2}$ , we see that  $V_+$  must be 0 V. By the golden rules,  $V_- = V_+$ , and we can treat this like an inverting amplifier:

$$V_{out1} = -V_{in1} \left( \frac{R_4}{R_1} \right)$$

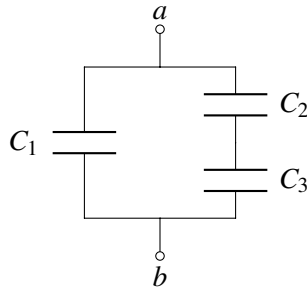
By superposition, we add the intermediate output voltages to determine the final output voltage:

$$V_{out} = V_{in2} \left( \frac{R_3}{R_2 + R_3} \right) \left( 1 + \frac{R_4}{R_1} \right) - V_{in1} \left( \frac{R_4}{R_1} \right)$$

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### 5. Equivalent Capacitance (9 points)

- (a) (4 points) Find the equivalent capacitance between terminals  $a$  and  $b$  of the following circuit in terms of the given capacitors  $C_1$ ,  $C_2$ , and  $C_3$ . Leave your answer in terms of the addition, subtraction, multiplication, and division operators **only**.



**Solution:**

$$C_{eq} = C_1 + (C_2 || C_3)$$

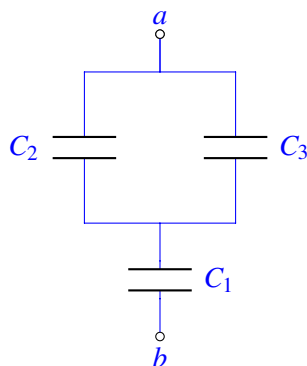
$$C_{eq} = C_1 + \frac{C_2 C_3}{C_2 + C_3}$$

Here,  $||$  represents the mathematical parallel operator ( $a || b = \frac{ab}{a+b}$ ).

- (b) (5 points) Find and draw a capacitive circuit using three capacitors,  $C_1$ ,  $C_2$ , and  $C_3$ , that has equivalent capacitance of

$$\frac{C_1(C_2 + C_3)}{C_1 + C_2 + C_3}$$

**Solution:** This expression is the same as  $C_1 || (C_2 + C_3)$ , so  $C_2$  and  $C_3$  are in parallel with each other, and  $C_1$  is series with both of them:

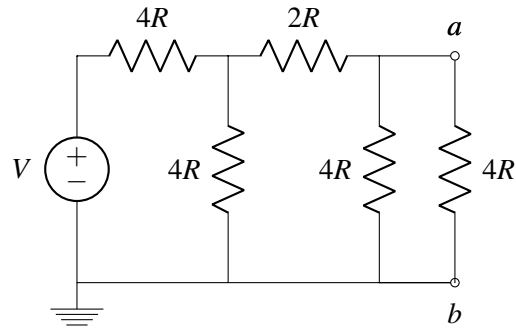




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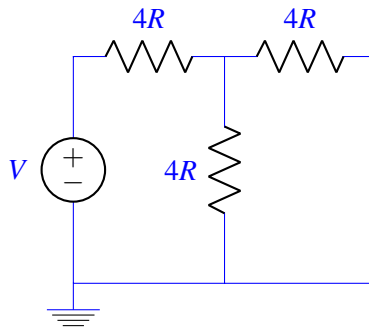
### 6. Power to Resist (6 points)

Find the power dissipated by the voltage source in the circuit below. Be sure to use passive sign convention.



#### Solution:

This circuit can be reduced using techniques similar to those used to analyze the R-2R ladder from homework. We want to find the equivalent resistance across the voltage source in Figure 6.2. Start by reducing the two resistors on the right to  $4R \parallel 4R = 2R$ . Then combine the other  $2R$  resistor with this to get a new resistor of value  $4R$  as in the circuit below.



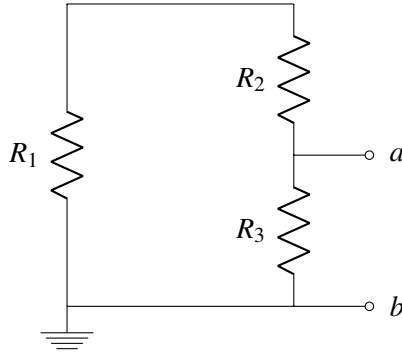
Once again we have  $4R \parallel 4R = 2R$ . This is finally in series with  $4R$  giving us a total resistance of  $4R + 2R = 6R$

$$P = VI = V \frac{-V}{6R} = -\frac{V^2}{6R}$$

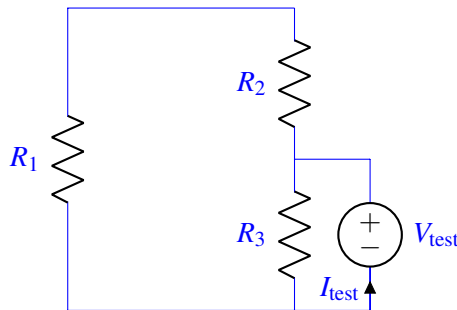
The negative sign is present because the voltage source actually provides power, which can also be seen by using passive sign convention.

## 7. Mechanical Thevenin and Norton Equivalents (10 points)

- (a) (4 points) Find and draw the **Thevenin** equivalent circuit between terminals  $a$  and  $b$  in the circuit below. Clearly label the Thevenin equivalent voltage,  $V_{th}$ , and the Thevenin equivalent resistance  $R_{th}$ .



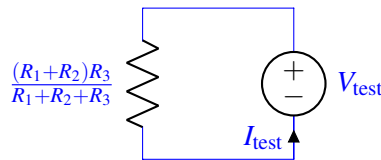
**Solution:** Start by finding  $V_{oc}$ , which is the voltage dropped across  $R_3$ . Since there are no sources in this circuit, the voltage across  $R_3$ ,  $V_{R_3} = 0$  and therefore  $V_{th} = 0$ . To find  $R_{th}$ , first null all independent sources (there are none). Then apply a test voltage to the terminals like so:



And calculate the current exiting the voltage source with Nodal Analysis or Resistor Equivalences. This solution uses resistive equivalences.  $R_{eq}$  as seen from the voltage source is

$$R_{eq} = (R_1 + R_2) || R_3 = \frac{(R_1 + R_2)R_3}{R_1 + R_2 + R_3}$$

Collapsing the resistors down into this  $R_{eq}$  turns the circuit into the one below:

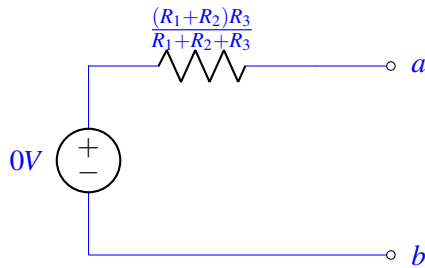


We can solve for the value of  $I_{test}$  with Ohm's Law.

$$V = IR \rightarrow I = \frac{V_{test}}{R_{eq}} = \frac{V_{test}}{\frac{(R_1+R_2)R_3}{R_1+R_2+R_3}} = V_{test} \frac{R_1 + R_2 + R_3}{(R_1 + R_2)R_3}$$

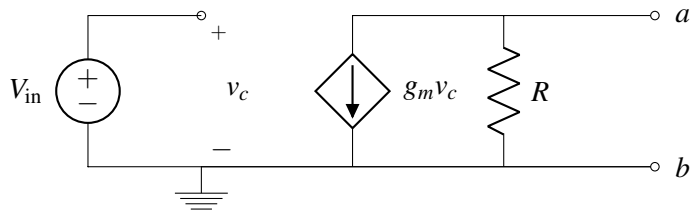
$$R_{th} = \frac{V_{test}}{I_{test}} = \frac{V_{test}}{V_{test} \frac{R_1+R_2+R_3}{(R_1+R_2)R_3}} = \frac{(R_1 + R_2)R_3}{R_1 + R_2 + R_3}$$

Therefore, the Thevenin Equivalent circuit is as follows:

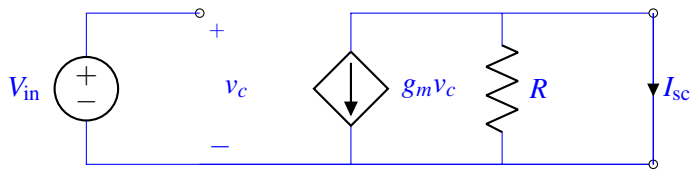


Circuits omitting the voltage source are also fine.

- (b) (6 points) Find and draw the **Norton** equivalent circuit between terminals  $a$  and  $b$  in the circuit below. Clearly label the Norton equivalent current,  $I_{no}$ , and the Norton equivalent resistance  $R_{no}$ .



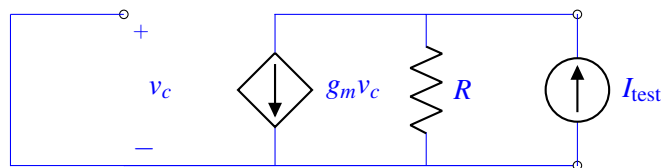
**Solution:** Begin by finding the short circuit current,  $I_{sc}$  which is equal to  $I_{no}$ , by shorting the terminals  $a$  and  $b$ .



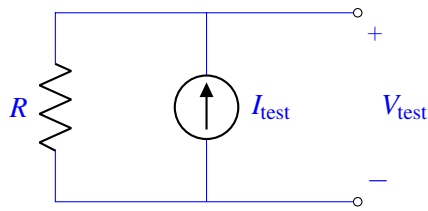
This sets the voltage across  $R$  to be 0V, since it is in parallel with an ideal wire. Therefore, the current from current source  $g_m v_c$  will be what flows through the short, where  $v_c = V_{in}$ . Be careful, however: the current is flowing from the *negative* terminal to the *positive* terminal, so  $I_{sc}$  is actually  $-g_m V_{in}$ .

$$I_{no} = I_{sc} = -g_m V_{in}$$

Now, onto finding  $R_{no}$ . Null all independent sources, and apply a test current to the circuit as shown:



When the voltage source is nulled,  $v_c = 0$ , so the dependent current source  $g_m v_c$  will output *zero* current and behave as an open circuit. So what is left is essentially a loop with the resistor  $R$  and  $I_{test}$ :



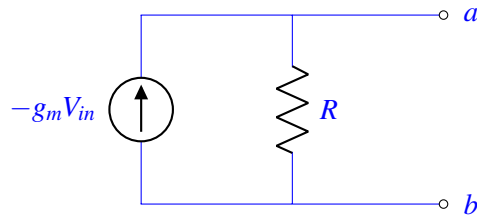
Because the resistor and current source are in a simple loop, the voltage across the resistor (and therefore  $V_{\text{test}}$ ) can be calculated with Ohm's Law:

$$V_{\text{test}} = I_{\text{test}}R$$

And  $R_{\text{no}}$  can be calculated with:

$$R_{\text{no}} = \frac{V_{\text{test}}}{I_{\text{test}}} = \frac{I_{\text{test}}R}{I_{\text{test}}} = R$$

The Norton Equivalent circuit is as follows:

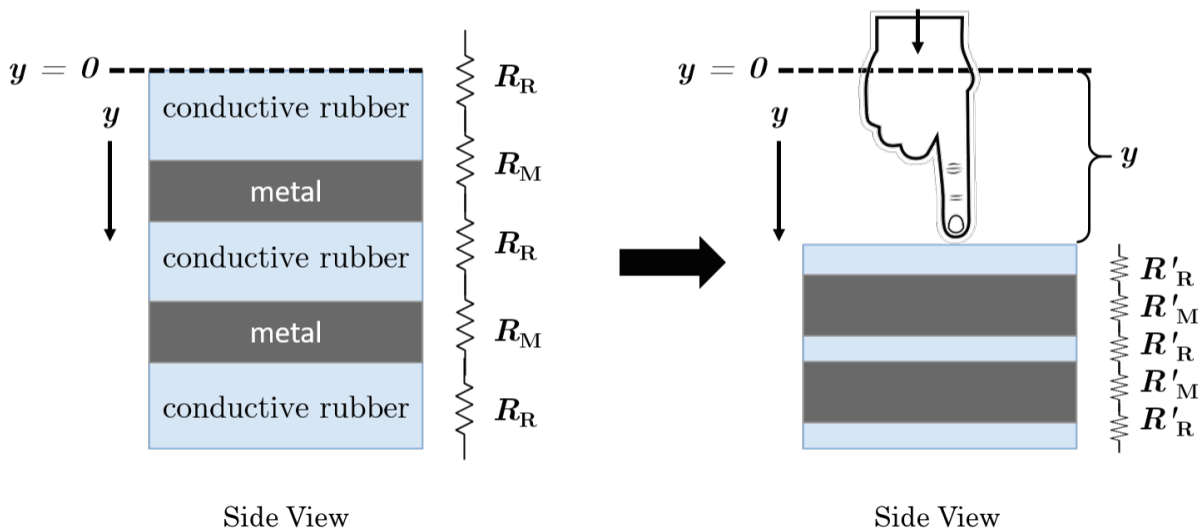


### 8. Midterms are a lot of Pressure (16 points)

In our labs, we used our resistive touchscreen to figure out where we were pressing in a 2D space. Now we'll use a new setup to determine how hard we're pressing! For this we'll use something called "pressure sensitive rubber," which incorporates conductive rubber and metal into one system. As the rubber is pressed, the conductive rubber portions are compressed, which changes the resistance. The metal plates do not change, but they assist in conduction through the material.

The pressure sensitive rubber system is shown below, with a resistive model next to the diagram. The resistivity of rubber and metal are represented by  $\rho_R$  and  $\rho_M$  respectively. When the system is at rest (no touch), the resistances of the rubber and metal are represented by  $R_R$  and  $R_M$ . The area of the sensor, as seen from above, is  $A$ .

To use the material, a finger presses on top of the system, compressing the rubber regions, creating a change in resistance, also shown below. Please answer the following questions related to the system.



- (a) (2 point) Is the resistor model implementing resistors in series or parallel?

**Solution:** The resistors are in series.

- (b) (3 points) If the values are  $R_R = 1 \text{ k}\Omega$  and  $R_M = 10 \Omega$ , what is the total resistance before pressing the system?

**Solution:** There are three  $R_R$  resistors and two  $R_M$ , so  $R_{total} = 3 \text{ k}\Omega + 20 \Omega = 3.02 \text{ k}\Omega$ .

- (c) (4 points) During the press, the length of each rubber portion is reduced by a factor of 5. (Its length is now 1/5 of its original value.) The size of the metal plates does not change. What is the new total resistance during a press?

**Solution:** If the length is reduced by a factor of 5, our  $R_R$  is reduced by a factor of 5:

$$R_R = \rho_R \frac{l}{A} \rightarrow R'_R = \rho_R \frac{l/5}{A} = \frac{R_R}{5}$$

$$R'_{total} = \frac{3 \text{ k}\Omega}{5} + 20 \Omega = 620 \Omega$$

- (d) (5 points) The force required to compress the rubber is  $F = ky$ , where  $k$  is a constant and  $y$  is the distance compressed (from the origin). Derive an expression for the resistance as a function of the pressing force  $F$ .

Write your answer in terms of the initial resistances ( $R_R$  and  $R_M$ ), the resistivities ( $\rho_R$  and  $\rho_M$ ), the area of the sensor,  $A$ , and the constant,  $k$ . Assume all rubber layers compress the same amount and uniformly.

**Solution:** First, let's consider the total resistance of just the rubber. If we press the rubber such that the rubber compresses by an amount  $y$ , this means we've reduced the length of our conductive rubber region to  $l - y$ , making our resistance of the rubber region:

$$\begin{aligned} R_{R-press} &= \rho_R \frac{l-y}{A} \\ &= \rho_R \frac{l-F/k}{A} \\ &= \rho_R \frac{l}{A} - \rho_R \frac{F/k}{A} \end{aligned}$$

The first term is equivalent to the initial (no press) resistance of one segment of rubber,  $3R_R$ .

$$R_{R-press} = 3R_R - \rho_R \frac{F}{kA}$$

To get the total resistance of the sensor, we can add the resistance of the metal portions. Since the metal portions do not change, their resistance is still  $2R_M$ .

$$R_{total}(F) = 3R_R - \rho_R \frac{F}{kA} + 2R_M$$

- (e) (2 points) For a particular sensor, we find that the resistance is:

$$R(F) = \frac{8k\Omega \cdot mm^2}{A} - \left(100 \frac{\Omega \cdot m^2}{N}\right) \frac{F}{A}$$

We define the sensitivity of the sensor,  $S$ , to be the change in resistance per unit of force:

$$S = \left| \frac{dR}{dF} \right|$$

If we want to increase sensitivity, how should we change the area of the sensor? Justify your answer in 1-2 sentences.

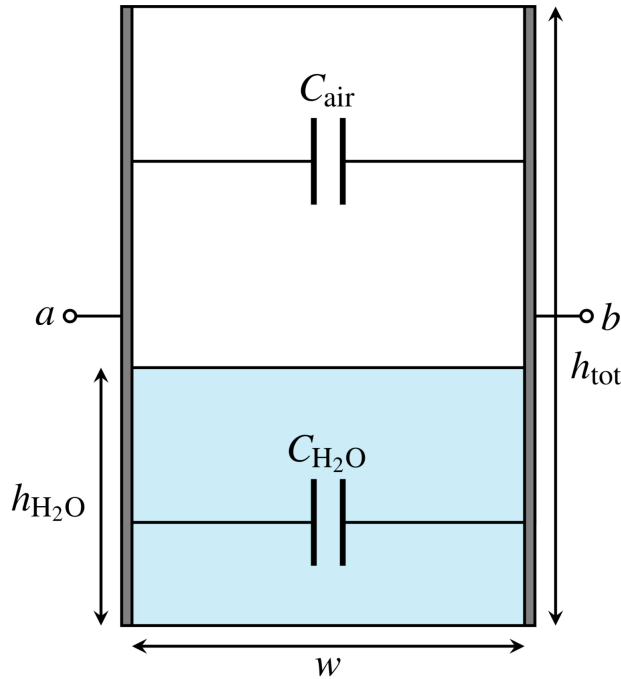
**Solution:** We can calculate the sensitivity:

$$S = \left| \frac{d}{dF} \left( \frac{8k\Omega \cdot mm^2}{A} - \left(100 \frac{\Omega \cdot m^2}{N}\right) \frac{F}{A} \right) \right| = 100 \frac{\Omega \cdot m^2}{N} \left| \frac{1}{A} \right|$$

Sensitivity is inversely proportional to  $A$ , so we should **decrease** the area of the sensor if we want to increase sensitivity.

### 9. Rain Sensor (20 points)

A capacitive sensor can be used to measure how much rain water is in a tank. To do this, two capacitor plates are attached to a rectangular tank. The idea is to make a capacitor whose capacitance varies with the amount of water inside. The width and length of the tank are both  $w$  (i.e. the base is square), and the height of the tank is  $h_{\text{tot}}$ . The permittivity of air is  $\epsilon$ , and the permittivity of rainwater is  $81\epsilon$ .



- (a) (5 points) Derive an expression for the total capacitance,  $C_{\text{tank}}$ , between terminals  $a$  and  $b$  as a function of  $h_{\text{tot}}$ ,  $w$ ,  $h_{\text{H}_2\text{O}}$ , and  $\epsilon$ .

**Solution:** The total capacitance  $C_{\text{tank}}$  contains two components: the capacitance due to water, and the capacitance due to air. Because these capacitors are parallel to each other, the total capacitance is the sum of  $C_{\text{air}}$  and  $C_{\text{H}_2\text{O}}$ .

The capacitance of the two plates due to water is:

$$C_{\text{H}_2\text{O}} = \frac{81\epsilon h_{\text{H}_2\text{O}} w}{w} = 81\epsilon h_{\text{H}_2\text{O}}$$

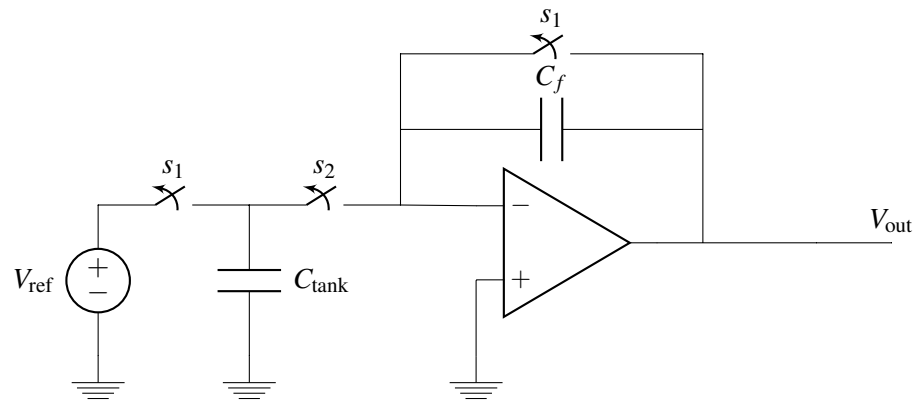
The capacitance of the two plates separated by air:

$$C_{\text{air}} = \frac{\epsilon (h_{\text{tot}} - h_{\text{H}_2\text{O}}) w}{w} = \epsilon (h_{\text{tot}} - h_{\text{H}_2\text{O}})$$

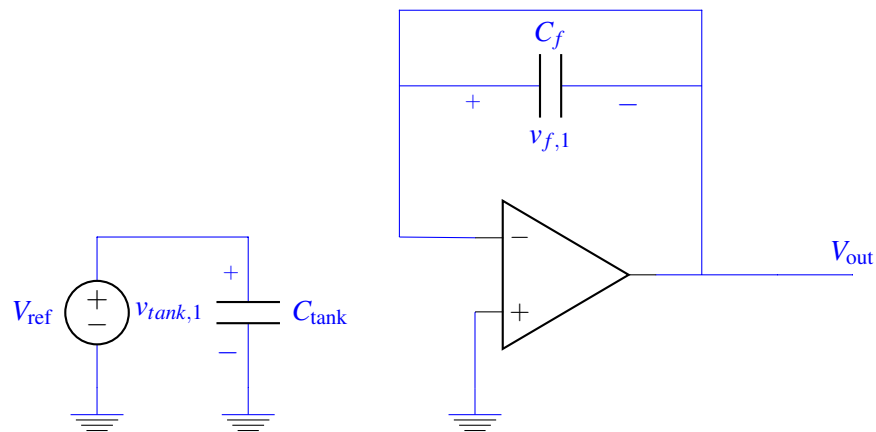
The equivalent total capacitance is then:

$$C_{\text{tank}} = C_{\text{H}_2\text{O}} + C_{\text{air}} = \epsilon (h_{\text{tot}} + 80h_{\text{H}_2\text{O}})$$

- (b) (2 points) You would like to measure changes in  $C_{\text{tank}}$  as changes in voltage, so you design the following circuit. Draw the equivalent circuit when  $s_1$  is on and  $s_2$  is off.



**Solution:**



- (c) (3 points) Find expressions for charge across each capacitor when  $s_1$  is on and  $s_2$  is off.

**Solution:** The charge across  $C_{\text{tank}}$  is:

$$Q_{C_{\text{tank}},1} = v_{\text{tank},1} C_{\text{tank}} = V_{\text{ref}} C_{\text{tank}}$$

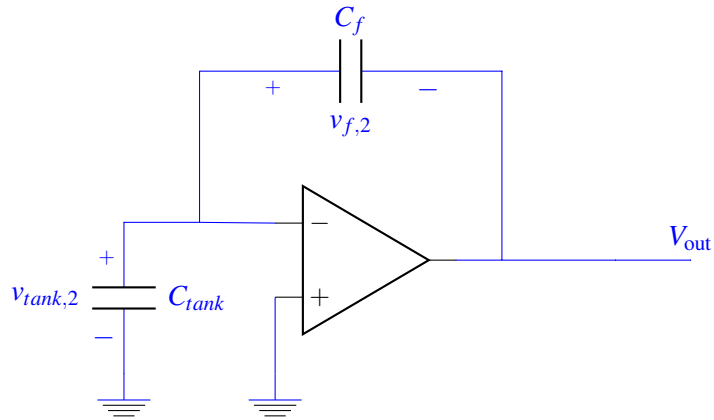
The two terminals of  $C_f$  are shorted, so there is no charge across it:

$$Q_{C_f,1} = C_f V_{f,1} = 0$$

- (d) (2 points) Draw the equivalent circuit when  $s_2$  is on and  $s_1$  is off.

**Solution:**





- (e) (3 points) Find expressions for charge across each capacitor when  $s_2$  is on and  $s_1$  is off.

**Solution:** Since the voltage on the positive terminal of this op amp in negative feedback is zero, the voltage on the negative terminal must also be zero. The charge across  $C_{\text{tank}}$  is given by:

$$Q_{\text{ctank},2} = C_{\text{tank}} v_{\text{tank},2} = 0$$

The charge across  $C_f$  is given by

$$Q_{f,2} = C_f v_{f,2} = C_f (0 - V_{\text{out}}) = -C_f V_{\text{out}}$$

- (f) (5 points) Express  $V_{\text{out}}$  as a function of  $V_{\text{ref}}$  and the capacitances. What happens to  $V_{\text{out}}$  when the amount of water in the tank increases?

**Solution:** Using the fact that the charge on a node is conserved, we can write the following expression

$$Q_{\text{ctank},1} + Q_{Cf,1} = Q_{\text{ctank},2} + Q_{Cf,2}$$

After plugging in the expressions in the previous parts:

$$V_{\text{ref}} C_{\text{tank}} = -C_f V_{\text{out}}$$

$$V_{\text{out}} = -\frac{C_{\text{tank}}}{C_f} V_{\text{ref}}$$

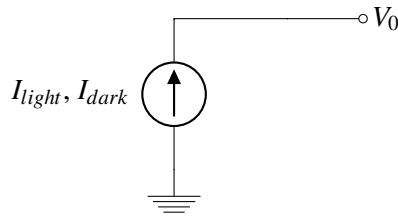
As the amount of water increases, the capacitance  $C_{\text{tank}}$  increases, causing the voltage at the output to decrease.

PRINT your name and student ID: \_\_\_\_\_

**10. A Light Design Problem, So to Speak... (15 points)**

Your pet cactus needs a lot of light every day, and you're not sure your room is sunny enough. You decide to use your knowledge from 16A to build a device to detect if the sun is shining in your room.

- (a) (8 points) Assume you just finished the Imaging Lab, where you build a light sensor, which can be modeled as a current source as shown below. When the light is on, the current source produces 5 mA. When the light is off, 1 mA.



$$I_{light} = 5 \text{ mA}, I_{dark} = 1 \text{ mA}$$

Using this knowledge, **design a circuit that outputs 10 V when the light is on and 0 V when the light is off**. In addition to the model of the light sensor above, you may use the following components (only!):

- **one** op amp
- **one** resistor
- **two** voltage sources

You must explicitly note the power supplies used on the op amp. Clearly label values of resistors and voltage sources that you use.

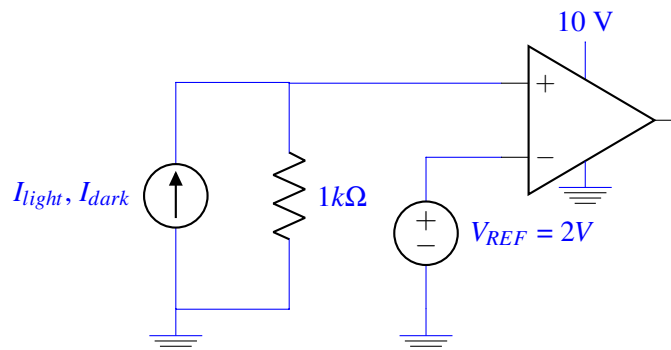
**Solution:**

We want to utilize the fact that the light being on and off will produce different voltages in our sensor. Picking a resistor value of  $R = 1k\Omega$ , we can see the voltages for light being on and off would be:

$$V_{light} = (1k\Omega)(5mA) = 5V$$

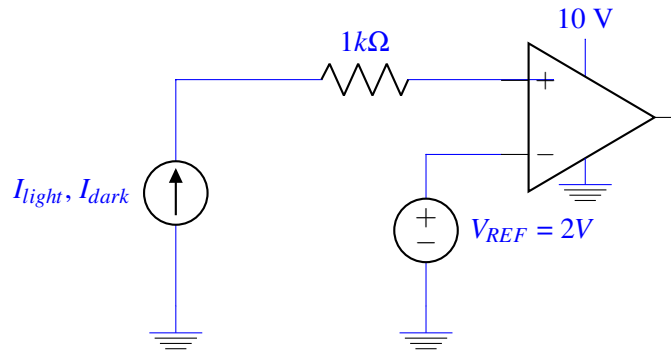
$$V_{dark} = (1k\Omega)(1mA) = 1V$$

Now that we have two separate voltage values, we can run our sensor into a comparator, whose  $V_{REF}$  value is between  $V_{light}$  and  $V_{dark}$ , as shown. Note that the op amp's power supply rails have been chosen to be  $V_{DD} = 10V$  and  $V_{SS} = 0V$  to match our desired output.



### Common Mistakes:

The following circuit design is incorrect because the current source is feeding directly into the op amp, but no current can enter the op amp. Therefore, this circuit will not output the desired voltages.



- (b) (4 points) You realize that the light sensor can only provide a maximum of  $P_{max} = 40mW$  of power. Does this affect your design from part (a)? If so, how should it change? If not, why does it not affect it?

(Do not use additional components beyond those specified in the problem statement.)

**Solution:** The max power provided by the sensor will happen when the light is on,  $I = 5mA$ . In the design above, this creates a voltage drop over the sensor of  $-IR = -(5mA)(1k\Omega) = -5V$  (using passive sign convention). The power dissipated by the sensor is

$$P = IV = (5mA)(-5V) = -25mW$$

The power *dissipated* negative, so the power *provided* to the circuit is positive  $25mW$  which is less than  $P_{max}$ . Therefore this circuit does not need to be altered.

Let's calculate what resistance values meet the maximum power requirement:

$$|P| \leq 40mW$$

$$|IV| \leq 40mW$$

$$|I^2V| \leq 40mW$$

$$|(5mA)^2R| \leq 40mW$$

$$R \leq 1.6k\Omega$$

- (c) (3 points) You notice that there is noise in both  $I_{light}$  and  $I_{dark}$  (ie. sometimes the currents are higher or lower than expected). Assuming that there is the same amount of noise in both  $I_{light}$  and  $I_{dark}$ , modify your design to be as robust as possible to these fluctuations. Justify your design choices in 1-2 sentences. If you believe your design does not need modification, explain why.

(Do not use additional components beyond those specified in the problem statement.)

**Solution:** The reference voltage should be exactly **in between**  $V_{light}$  and  $V_{dark}$  to be most robust to noise in the inputs. Specifically,

$$V_{ref} = \frac{I_{light} + I_{dark}}{2} R$$

. Using the values for  $I_{light}$  and  $I_{dark}$ , the expression then becomes:

$$V_{ref} = \frac{6mA}{2} R = \frac{6mA}{2} 1k\Omega = 3V$$

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