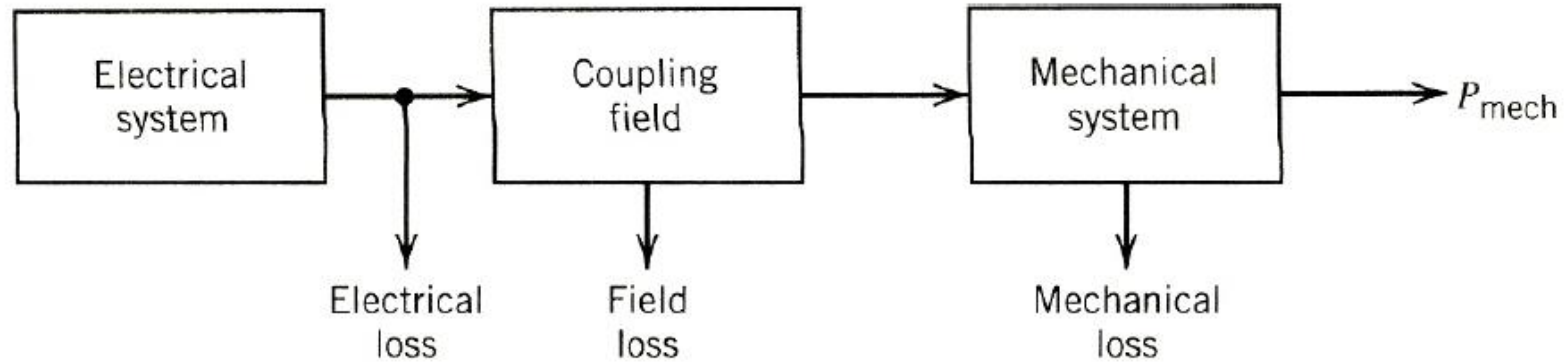


# Chapter 2 Electromechanical Energy Conversions

## Learning Objectives

- ▶ Analyze electromechanical energy conversion based on concepts of energy and coenergy
- ▶ Understand operating principles of rotating and cylindrical machines

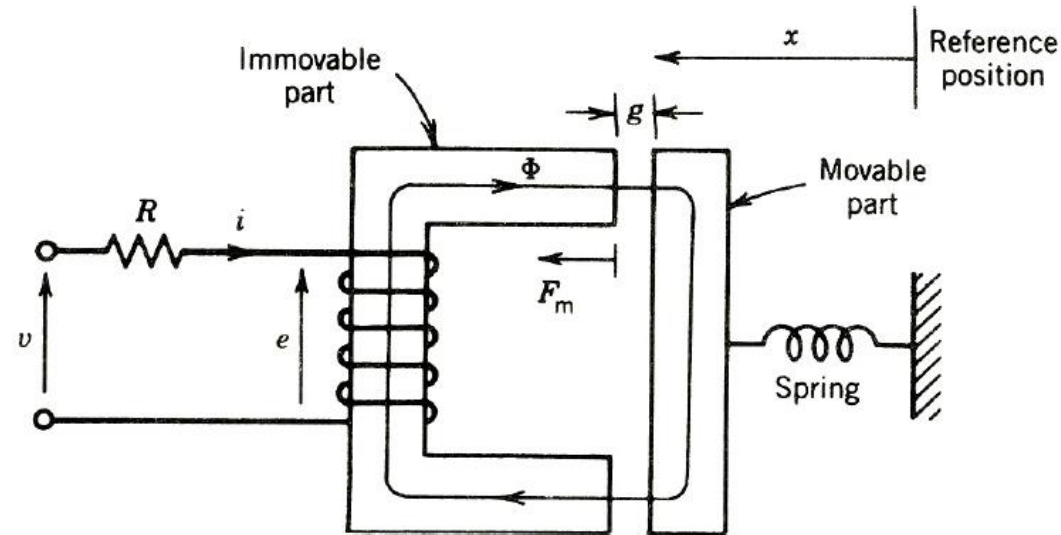
## 2.1 Fundamentals



- Based on the principle of conservation of energy, energy can neither be created nor destroyed but changed from one form to another
- Consider a differential time interval

$$dW_e = dW_m + dW_f$$

## 2.1 Fundamentals



- ▶ Consider if the movable part is held stationary at some air gap with current is increased from zero to a value  $i$

$$dW_e = dW_f$$

- ▶ If core loss is neglected, all incremental electrical energy input is stored as field energy

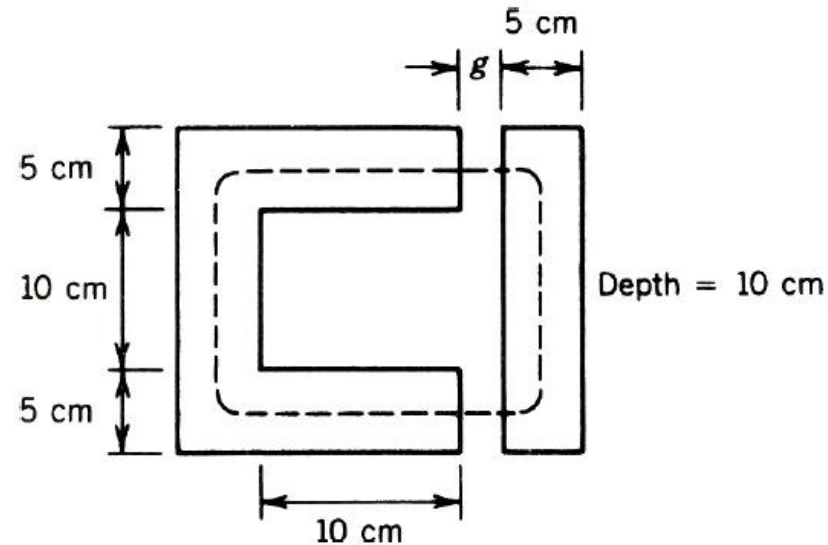
$$dW_e = e i dt \qquad dW_f = i d\lambda$$

## 2.1 Fundamentals

- ▶ Energy stored in the field

$$\begin{aligned}W_f &= \int_0^\lambda i d\lambda \\&= \int \frac{H_c l_c + H_g l_g}{N} N A dB \\&= \int \left( H_c dBA l_c + \frac{B}{\mu_0} dB l_g A \right) \\&= w_{fc} \times V_c + w_{fg} \times V_g \\&= W_{fc} + W_{fg}\end{aligned}$$

## Concept Check 2.1



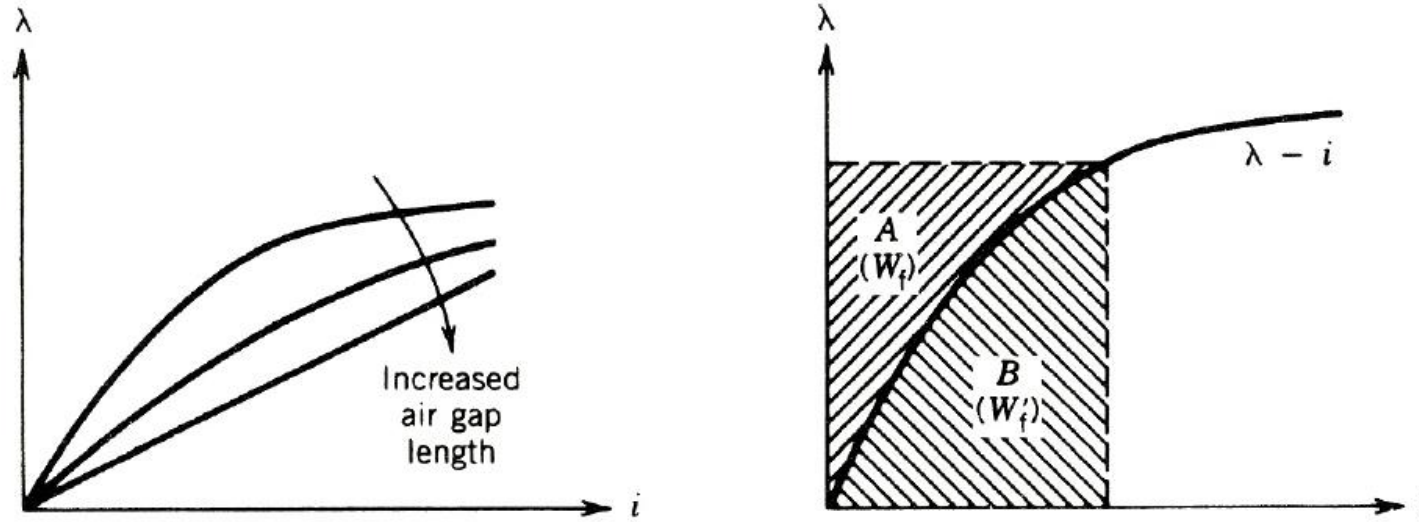
Consider a actuator system as shown above. It consists of coil of 250 turns and coil resistance of  $5\ \Omega$ . For a fixed air gap length of 5 mm, a dc source is connected to the coil to produce a flux density of 1.0 T in the air gap. Assume the magnetic field intensity of core is a cast steel with flux density of 1.0 T is 670 At/m.

- (a) Find the voltage of the dc source (Ans: 167.2 V)
- (b) Find the stored field energy (Ans: 20.9 J)

# Concept Check 2.1

# Concept Check 2.1

## 2.2 Mechanical Force



- ▶ For larger air gap length, the  $\lambda - i$  characteristic will become more linear
- ▶ The area  $B$  is known as coenergy

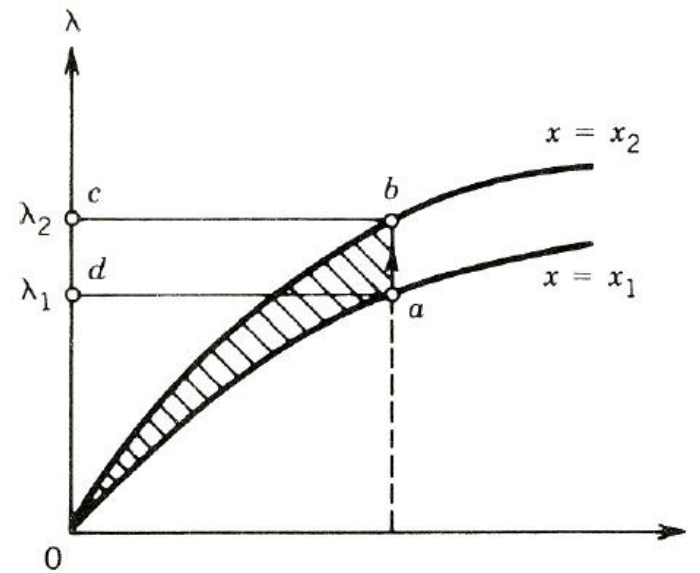
$$W'_f = \int_0^\lambda i d\lambda$$

- ▶ If it is linear

$$W'_f = W_f = \lambda i$$



## 2.2 Mechanical Force



- If the movable part has moved slowly with current remained constant, the operating point will move upward from point  $a$  to  $b$

$$dW_e = \int e i dt = \int_{\lambda_1}^{\lambda_2} i d\lambda = \text{area } abcd$$

$$dW_f = \text{area } Obc - \text{area } Oad$$

$$dW_m = dW_e - dW_f = \text{area } Oab$$

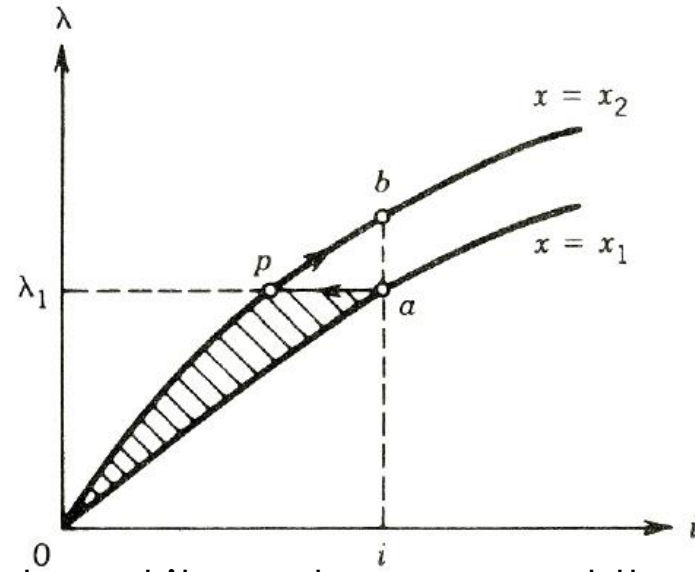
## 2.2 Mechanical Force

- ▶ If the motion is under constant-current conditions, the mechanical work done is the incremental part in the coenergy and the mechanical force is

$$f_m dx = dW_m = W_f'$$

$$f_m = \left. \frac{\partial W_f'(i, x)}{\partial x} \right|_{i=\text{constant}}$$

## 2.2 Mechanical Force



- If the movement is very quick and it can be assumed the flux linkage is constant
- The mechanical work done is shown in area  $0ap$ , which is decreased part in field energy

$$f_m dx = dW_m = W_f$$

$$f_m = \left. \frac{\partial W_f(\lambda, x)}{\partial x} \right|_{\lambda=\text{constant}}$$

- If the displacement is small, areas  $0ab$  of both cases are equal so as the force

## Concept Check 2.2

The  $\lambda - i$  relationship of an electromagnetic system is given as

$$i = \left( \frac{\lambda g}{0.09} \right)^2$$

Given that it is valid for the limits  $0 < i < 4$  A and  $3 < g < 10$  cm. For current  $i = 3$  A and air gap length  $g = 5$  cm. Find the mechanical force on the moving part, by using energy and coenergy of the field (Ans: - 124.7 Nm; - 124.7 Nm)

# Concept Check 2.2

## Concept Check 2.2

## 2.2 Mechanical Force

- ▶ In the reluctance of the magnetic core path is negligible as compared to that of the air gap path, the  $\lambda - i$  relation becomes linear

$$\lambda = L(x)i$$

$$W_f = \int_0^\lambda \frac{\lambda}{L(x)} d\lambda$$

$$= \frac{1}{2} L(x) i^2$$

$$f_m = - \frac{\partial}{\partial x} \left( \frac{\lambda^2}{2L(x)} \right) \Big|_{\lambda=\text{constant}}$$

$$= \frac{1}{2} i^2 \frac{dL(x)}{dx}$$

## 2.2 Mechanical Force

- ▶ For linear system

$$W_f = W_f' = \frac{1}{2} L(x) i^2$$

$$f_m = \frac{\partial}{\partial x} \left( \frac{1}{2} L(x) i^2 \right) \Big|_{i=\text{constant}}$$

$$= \frac{1}{2} i^2 \frac{dL(x)}{dx}$$

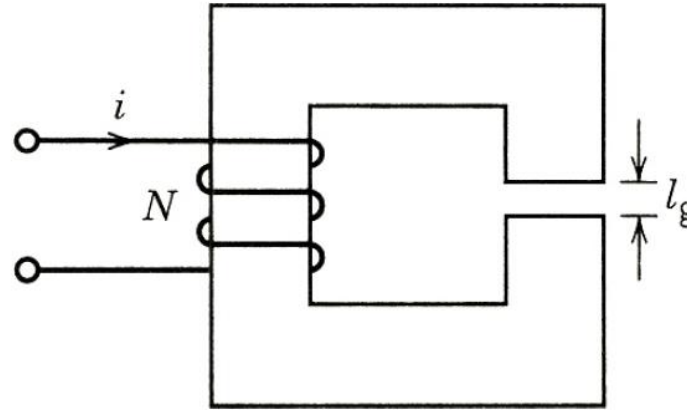
- ▶ If the reluctance of the magnetic core path is negligible

$$Ni = H_g 2g = \frac{B_g}{\mu_0} 2g$$

$$f_m = \frac{B_g^2}{2\mu_0} (2A_g)$$



## Concept Check 2.3



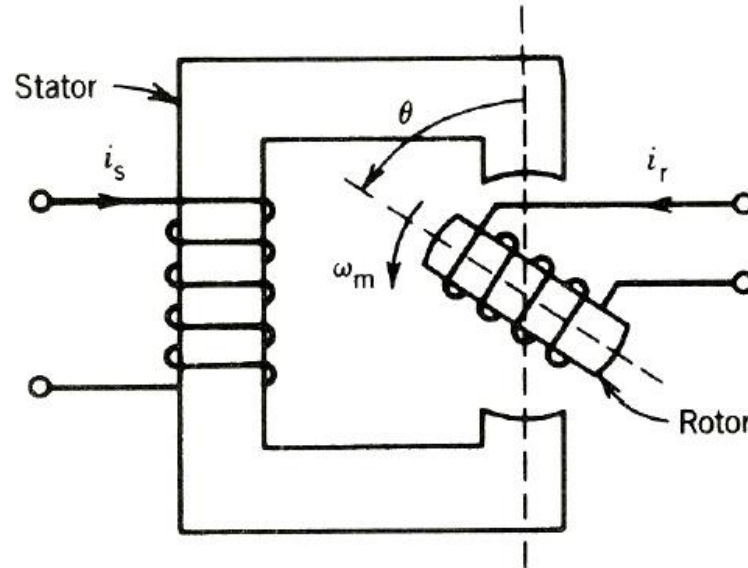
Consider a magnetic system as shown above. It consists of coil of 500 turns, current of 2 A, width of air gap of 2.0 cm, depth of air gap of 2.0 cm and length of air gap of 1 mm. Neglect the reluctance of the core, leakage flux and fringing flux.

- (a) Find the force of attraction between both sides of the air gap (Ans: 251.3 N)
- (b) Find the energy stored in the air gap (Ans: 0.251 J)

# Concept Check 2.3

# Concept Check 2.3

## 2.3 Rotating Machine



- ▶ Consider a rotating electromagnetic system that consists of both stator and rotor with winding carrying currents
- ▶ Assume the stored field energy is kept as static, i.e., no mechanical output

$$\begin{aligned} dW_f &= e_s i_s dt + e_r i_r dt \\ &= i_s d\lambda_s + i_r d\lambda_r \end{aligned}$$

## 2.3 Rotating Machine

- ▶ For a linear magnetic system

$$\lambda_s = L_{ss}i_s + L_{sr}i_r$$

$$\lambda_r = L_{rs}i_s + L_{rr}i_r$$

- ▶ As a matrix form

$$\begin{bmatrix} \lambda_s \\ \lambda_r \end{bmatrix} = \begin{bmatrix} L_{ss} & L_{sr} \\ L_{sr} & L_{rr} \end{bmatrix} \begin{bmatrix} i_s \\ i_r \end{bmatrix}$$

- ▶ Hence

$$\begin{aligned} dW_r &= i_s d(L_{ss}i_s + L_{sr}i_r) + i_r d(L_{sr}i_s + L_{rr}i_r) \\ &= L_{ss}i_s di_s + L_{rr}i_r di_r + L_{sr}d(i_s i_r) \end{aligned}$$

## 2.3 Rotating Machine

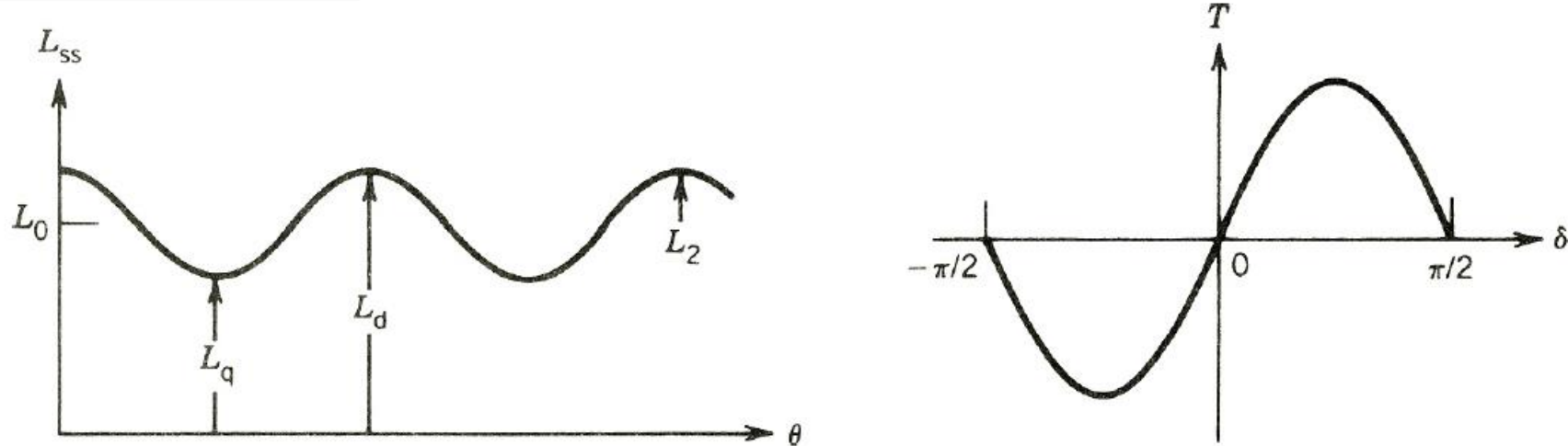
- ▶ The field energy

$$\begin{aligned} W_f &= L_{ss} \int_0^{i_s} i_s di_s + L_{rr} \int_0^{i_r} i_r di_r + L_{sr} \int_0^{i_s, i_r} d(i_s i_r) \\ &= \frac{1}{2} L_{ss} i_s^2 + \frac{1}{2} L_{rr} i_r^2 + L_{sr} i_s i_r \end{aligned}$$

- ▶ In a linear magnetic system, energy and coenergy are the same

$$\begin{aligned} T &= \left. \frac{\partial W_f'(i, \theta)}{\partial \theta} \right|_{i=\text{constant}} \\ &= \frac{1}{2} i_s^2 \frac{dL_{ss}}{d\theta} + \frac{1}{2} i_r^2 \frac{dL_{rr}}{d\theta} + i_s i_r \frac{dL_{sr}}{d\theta} \end{aligned}$$

## Concept Check 2.4



Consider an electromagnetic system whose rotor consists of no winding, i.e., it is a reluctance motor. Its stator current is  $i_s = I_{sm} \sin \omega t$  with stator inductance is as a function of the rotor position as  $L_{ss} = L_0 + L_2 \cos 2\theta$ , as shown above.

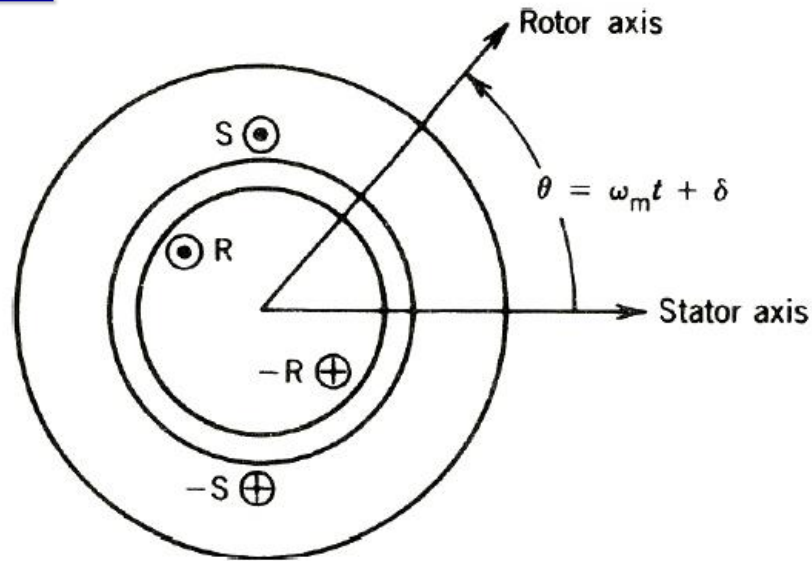
- Find an expression for the torque acting on the rotor (Ans:  $T = -I_{sm}^2 L_2 \sin 2\theta \sin^2 \omega t$ )
- Let  $\theta = \omega_m t + \delta$ , find the condition for nonzero average torque and also an expression for the torque (Ans: 0;  $T_{avg} = -1/4 I_{sm}^2 (L_d - L_q) \sin 2\delta$ ;  $\pm \omega$ ;  $T_{avg} = 1/8 I_{sm}^2 (L_d - L_q) \sin 2\delta$ )

# Concept Check 2.4



# Concept Check 2.4

## 2.4 Cylindrical Machine



- ▶ If the effects of the slots are neglected, the reluctance of the magnetic path is independent of the position of the rotor
- ▶ Self-inductances are constant and no reluctance torque is produced
- ▶ The mutual inductance varies with position, and the produced torque becomes

$$T = i_s i_r \frac{dL_{sr}}{d\theta}$$

## 2.4 Cylindrical Machine

➤ Assume

$$L_{sr} = M \cos \theta$$

$$i_r = I_{rm} \cos(\omega_r t + \alpha)$$

$$i_s = I_{sm} \cos \omega_s t$$

$$\theta = \omega_m t + \delta$$

➤ Torque becomes

$$\begin{aligned} T &= -I_{sm} I_{rm} \cos(\omega_s t) \cos(\omega_r t + \alpha) \sin(\omega_m t + \delta) \\ &= -\frac{I_{sm} I_{rm} M}{4} \left[ \sin\{(\omega_m + (\omega_s + \omega_r))t + \alpha + \delta\} \right. \\ &\quad \left. + \sin\{(\omega_m - (\omega_s + \omega_r))t - \alpha + \delta\} \right. \\ &\quad \left. + \sin\{(\omega_m + (\omega_s - \omega_r))t - \alpha + \delta\} \right. \\ &\quad \left. + \sin\{(\omega_m - (\omega_s - \omega_r))t + \alpha + \delta\} \right] \end{aligned}$$

## 2.4 Cylindrical Machine

- ▶ Average torque becomes nonzero when

$$\omega_m = \pm(\omega_s \pm \omega_r)$$

- ▶ Consider when  $\omega_r = 0$ ,  $\alpha = 0$ ,  $\omega_m = \omega_s$

$$T = -\frac{I_{sm}I_R M}{2} \{\sin(2\omega_s t + \delta) + \sin\delta\}$$

$$T_{avg} = -\frac{I_{sm}I_R M}{2} \sin\delta$$

- ▶ When the machine is operated under synchronous speed, it can develop an average unidirectional torque
- ▶ Even it can develop an average torque, it produce a pulsating value

## 2.4 Cylindrical Machine

- ▶ Consider when  $\omega_m = \omega_s - \omega_r$ , the machine is operated at an asynchronous speed

$$T = -\frac{I_{sm}I_{rm}M}{4}\sin(2\omega_s t + \alpha + \delta) + \sin(-2\omega_r t - \alpha + \delta) \\ + [\sin(2\omega_s t - 2\omega_r t - \alpha + \delta) + \sin(\alpha + \delta)]$$

$$T_{avg} = -\frac{I_{sm}I_{rm}M}{4}\sin(\alpha + \delta)$$

- ▶ This is the fundamental operation of an induction machine
- ▶ No average torque is produced at  $\omega_m = 0$
- ▶ It can produce average torque when speed is brought up to  $\omega_m = \omega_s - \omega_r$