Morenet documentation

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November 4, 2020

Abstract

This documentation gathers relevant information pertaining to the modeling and solution of the distributed power flow problem for the morenet project.

1 Problem formulation

Here we present the mathematical formulation of the distributed power flow problem, which simply reads

$$g_i^{\mathrm{pf}}(x_i, z_i) = 0 \tag{1a}$$

$$g_i^{\mathrm{bus}}(x_i) = 0 \tag{1b}$$

$$\sum_{i=1}^{n^{\mathrm{reg}}} A_i \begin{bmatrix} x_i \\ z_i \end{bmatrix} = 0. \tag{1c}$$

In plain words, the first set of equations satisfies the power flow equations in each region i, the second set of equations accounts for the bus specifications, and the third set of equations ensures consensus among the nodes that are shared between regions (will be explained below).

Its advantage is that its solution—supposing it exists—is mathematically equivalent to the original power flow problem. Instead of often done splitting of lines we simply copy neighboring buses within regions.

1.1 Core nodes & copy nodes

Suppose we have a grid that looks like as follows

There are a total of 12 buses in the system. The dashed lines indicate the three different regions: buses $\{1, 2, 3\}$ belong to what we call the master system, buses $\{4, 5, 6, 7\}$ belong to what we call the (first) worker system, and buses $\{8, 9, 10, 11, 12\}$ belong to the (second) worker system. Hence, we distinguish between *master* and *worker* systems; these local or regional systems (or just *subsystems*) make up the overall power system.

For the overall system the power flow problem means to compute the values

$$x_i = \begin{bmatrix} \theta_i \\ v_i \\ p_i \\ q_i \end{bmatrix} \in \mathbb{R}^{4n} \tag{2}$$

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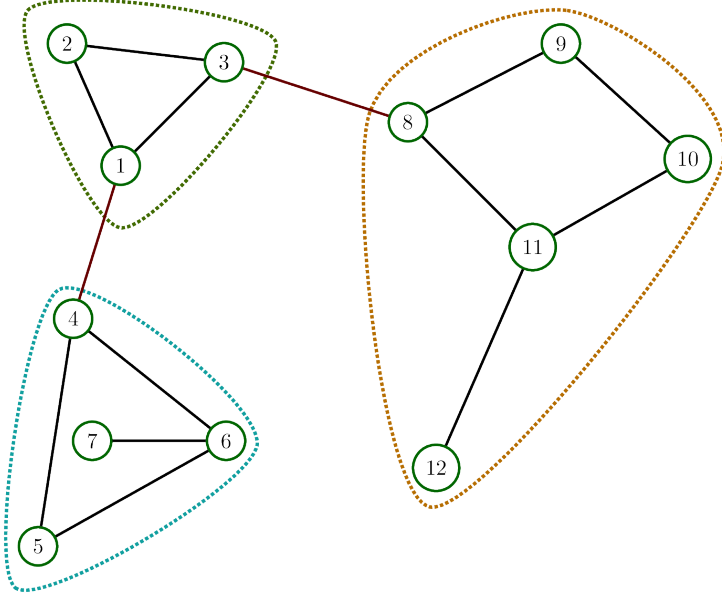
for all $i \in \{1, \ldots, 12\}$. A prototypical power flow problem can be formulated mathematically as a system of nonlinear equations of the form

$$g^{\mathrm{pf}}(x) = 0, \tag{3a}$$

$$g^{\mathrm{bus}}(x) = 0, \tag{3b}$$

where $g^{\mathrm{pf}}(x) = 0$ constitutes the 2×12 power flow equations, and $g^{\mathrm{bus}}(x) = 0$ stands for the remaining 2×12 bus specifications. This yields a total of 4×12 equations for 4×12 unknowns. Arguably, this leads to large systems of nonlinear equations as soon as the number of buses in the power system increases. From here on we call this prototypical power flow problem we just described the *centralized* power flow problem.

The idea of *distributed* power flow is to solve *local* power flow problems within each system (= the master system, and all of the worker systems), independent of each other, and iterate for as long as necessary until the solution of the centralized problem is obtained. Iteration here means to find consensus on the physical values of the exchanged power between the subsystems.

Before making this idea mathematically precise we introduce some more Nomenclature. Suppose we are seated in the master system, the one composed of buses $\{1, 2, 3\}$. From our perspective both worker systems are our *neighbors*. More precisely, we know only that bus 4 (located in the first worker system) is our connection to the first worker system. Likewise, bus 8 (located in the second worker system) is our connection to the second worker system. To distinguish between these different kinds of buses we call the buses $\{1, 2, 3\}$ the *core* nodes of the master system, and buses $\{4, 8\}$ the *copy* nodes. Importantly, all other nodes do not exist for us; they are ignored. Graphically, our world looks as follows.

Why the term *copy*? Because when formulating the power flow equations for the master system we need to know the voltages at the *copy* nodes. And in case we don't know the values (which we really don't because the copy nodes do not belong to our jurisdiction), then we have to *assume*
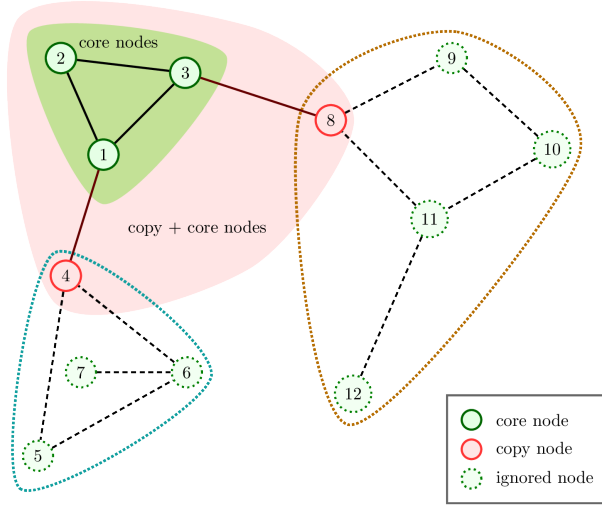
values for them. This can be thought of as copying the buses into the shaded are denoted as "copy + core nodes," hence the name.

Taking on the perspective of the first worker system we see: our core nodes are $\{4, 5, 6, 7\}$, and there is just one copy bus 1, the first bus in the master system. Our world looks as follows.

Being able to distinguish between core nodes and copy nodes allows to formulate the distributed power flow clearer: *solve the power flow problem in each subsystem and attain consensus between the copy nodes and their core node equivalents.* By core node equivalent we mean the following: the first copy bus of the master system has bus 4 as its core node equivalent. It is clear from intuition that if the voltage at the copy node in each subsystem corresponds to the value of its core node equivalent, then the solution of the distributed power flow problem is the same as the solution from the centralized power flow problem.

Let us make these ideas mathematically more precise.

1.2 Local power flow problem

The following table collects symbols and their meanings as they are used throughout.

Symbol	Meaning
n^{reg}	Number of regions
n^{conn}	Number of connecting lines between regions
n_i^{core}	Number of core nodes in region i
n_i^{copy}	Number of copy nodes in region i
x_i	State of core nodes in region i
z_i	State of copy nodes in region i

We compose the set of buses of each region i into a set of *core nodes*, and a set of *copy nodes*. The core nodes are the original nodes that make up the power system. The copy nodes are the nodes that connect the power system to the neighboring power systems. Hence, the copy nodes *do not belong to the power system* but to its neighbors. The sole purpose of the copy nodes is to store
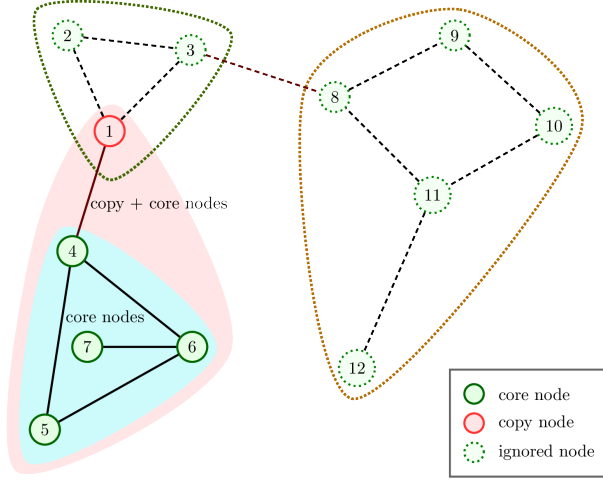
the complex voltage information at the neighboring buses such that power flow equations can be constructed.

The state of the core nodes contains the voltage angles, the voltage magnitudes, the net active power, and the net reactive power of all core nodes

$$x_i = \begin{bmatrix} \theta_i^{\mathrm{core}} \\ v_i^{\mathrm{core}} \\ p_i^{\mathrm{core}} \\ q_i^{\mathrm{core}} \end{bmatrix} \in \mathbb{R}^{4n_i^{\mathrm{core}}}. \tag{4}$$

The state of the copy nodes contains the voltage angles and the voltage magnitudes of all copy nodes

$$z_i = \begin{bmatrix} \theta_i^{\mathrm{copy}} \\ v_i^{\mathrm{copy}} \end{bmatrix} \in \mathbb{R}^{2n_i^{\mathrm{copy}}}. \tag{5}$$

We see: each region i is described by a total of $4n_i^{\mathrm{core}} + 2n_i^{\mathrm{copy}}$ real numbers.

1.2.1 Power flow equations

In region i we formulate a total of $2n_i^{\mathrm{core}}$ power flow equations $g_i^{\mathrm{pf}} \colon \mathbb{R}^{4n_i^{\mathrm{core}}} \times \mathbb{R}^{2n_i^{\mathrm{copy}}} \to \mathbb{R}^{2n_i^{\mathrm{core}}}$ for all core nodes

$$g_i^{\mathrm{pf}}(x_i, z_i) = 0. \tag{6}$$

1.2.2 Bus specifications

In region i we formulate a total of $2n_i^{\mathrm{core}}$ bus specifications $g_i^{\mathrm{bus}} \colon \mathbb{R}^{4n_i^{\mathrm{core}}} \to \mathbb{R}^{2n_i^{\mathrm{core}}}$ for all core nodes

$$g_i^{\mathrm{bus}}(x_i) = 0. \tag{7}$$

1.2.3 Degrees of freedom

Subtracting the number of equations from the number of decision variables gives us a total of

$$\underbrace{4n_i^{\mathrm{core}} + 2n_i^{\mathrm{copy}}}_{\text{Decision variables}} - \underbrace{2n_i^{\mathrm{core}}}_{\text{Power flow equations}} - \underbrace{2n_i^{\mathrm{core}}}_{\text{Bus specifications}} = \underbrace{2n_i^{\mathrm{copy}}}_{\text{Degrees of freedom}} \qquad (8)$$

degrees of freedom for each region i. These degrees of freedom must be fixed globally by the consensus constraints.

1.3 Decentralized power flow problem

$$g_i^{\mathrm{pf}}(x_i, z_i) = 0 \qquad (9a)$$

$$g_i^{\mathrm{bus}}(x_i) = 0 \qquad (9b)$$

$$\sum_{i=1}^{n^{\mathrm{reg}}} A_i \begin{bmatrix} x_i \\ z_i \end{bmatrix} = 0, \qquad (9c)$$

where the consensus matrices $A_i \in \mathbb{R}^{4n^{\mathrm{conn}} \times (4n_i^{\mathrm{core}} + 2n_i^{\mathrm{copy}})}$ enforce equality of the voltage angle and the voltage magnitude at the copy buses and their respective original buses.