Wind Farm Control

Active Power Control and Minimizing Loads by Yaw Control and Axial Induction

Niels van Duijn, Jurriaan Govers, Luuk van Hagen
Jochem Hoorneman, Max van Leeuwen
TU Delft

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Abstract

This will be the abstract of our paper. We will show how cool our research is and how important we are. Blabla Lorem impsum.

I. Introduction

To minimize cost of wind energy and to efficiently use resource rich locations, wind farms are constructed, characterized by a large concentration of wind turbines. An inherent side effect of wind turbine however is a wake. When wind turbines are placed in close proximity of each other in a wind farm, a wake can have negative effects. A wake forms behind an upwind wind turbine and can have severe effects on the power production and loads of the downwind turbine.

With an increasing role of wind energy in Europe's energy production [1], it is important for wind farms to be able to meet the demands of the power system [2]. Controlling the power output of a wind farm is essential because an overload of energy can decrease the stability of the power system [2]. Currently, most wind farms operate based on 'greedy control', meaning that the individual turbines always try to deliver maximum power. This causes a problem when the power demand is low and the dependency on the wind energy is high, resulting in an overload of the power system. Active power control can solve this problem, by regulating the power output of a wind farm.

There are several methods of active power control in a wind farm, two of which will be discussed in this paper, that is, yaw control and axial induction control. Yaw control can be used as a method to reduce the power output of a single wind turbine and as a method to increase power output and reduce loads of a wind farm (verwijzing). A disadvantage of yawing is an increase of the load on individual turbines, and thus reducing its lifespan [3, 4]. In addition, yawing a turbine can deflect a wake. This can be used as a method to redirect a wake from a downwind turbine, this would reduce the loads and increase power output of the downwind turbine(verwijzing). However, under unfavorable conditions it can result in an asymmetrical overlap of the wake on the downwind turbine. This can significantly increase the loads of the downwind turbine [5, 6](nog meer verwijzingen). Therefore, it is necessary to understand the effects of yawing a turbine with respect to wake propagation. Axial induction can control the power output by varying the axial induction factor during the optimization. Loads that are introduced by axial induction will not be discussed in this paper. As yawing of the turbine and the deflection of a wake can cause additional loads on the turbines of a wind farm, a trade of must be made between active power control and loads minimization.

Previous studies have mainly focused on optimizing the power output, rather than controlling the power output (verwijzingen naar studies die dit hebben gedaan). Other studies focus on power optimization, while also taking the loads into account, so that an optimum is found between the two (verwijzing naar wie dit heft gedaan). The use of axial induction in optimizing power control has been marginally studied(heb hier nog geen goede bron voor kunnen vinden). Active power control through a combination of yaw control and axial induction control while minimizing loads is still novel.

This paper will focus on the optimization of active power control and loads, by means of yaw control and axial induction control. In addition, a method is developed so that on-site power control can be realized.

Hier nog een overzicht van wat er in paper te vinden is. Moet later geschreven worden als de rest af is.

II. Method

To realize active power control and minimizing loads by yaw control and axial induction, it is necessary to know the effect of different flow conditions on the total power of the wind farm and the effect of different flow conditions on the loads for each of the turbine. Moreover, there need to be an optimizer which executes the optimization to approach a set value for the power and to minimize the loads.
The total power of the wind farm is calculated with the FLORIS-model. Besides, FLORIS is able to adjust the turbine configurations, the axial induction and yaw position. The effect of the wind flow on a turbine, regarding the loads, are given by the programs FAST and MLife. The output of these programs are Damage Equivalent Load values (DELs), which are a measure of equivalent load damage to the turbine concerning the material properties.[11] These DELs are calculated for a different set of wind and turbine conditions and are stored in a look-up table(LUT).

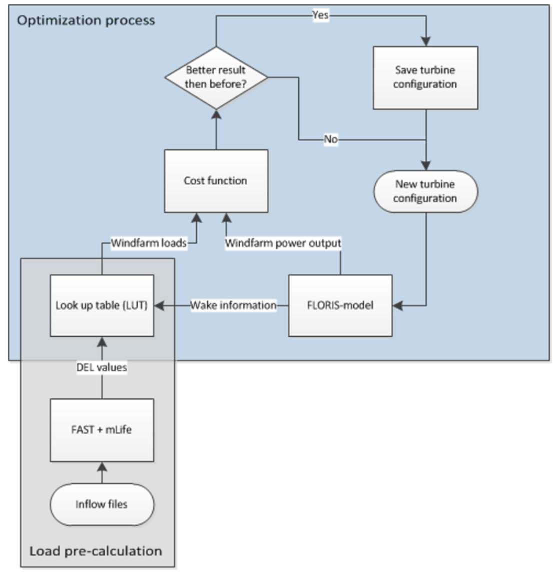


Figure 1: *Overview of the optimization procedure.*

The optimizer takes the desired power production of the wind farm as an input and uses the configurations of the turbines from FLORIS to find in the look-up table the DEL values coupled to this configurations. If the configurations of the turbines are an improvement compared to the previous one, i.e. a improved power control or a reduce in the loads, FLORIS will save the changes in turbine configurations. An overview of the optimization procedure is shown in Figure 1.

In the following sections, different models and model steps, used to perform the optimization, are explained:

i. FLORIS

The FLOw Redirection and Induction in Steady state (FLORIS) model calculates the power of

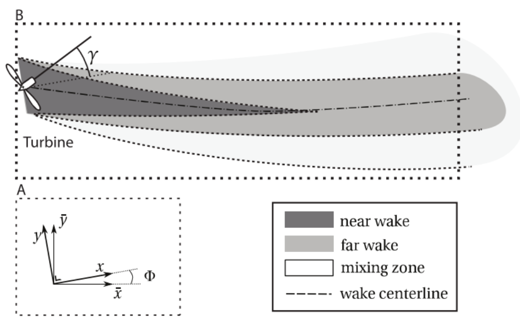


Figure 2: *Simplified top view representation of a wake of a turbine by FLORIS.[8]*

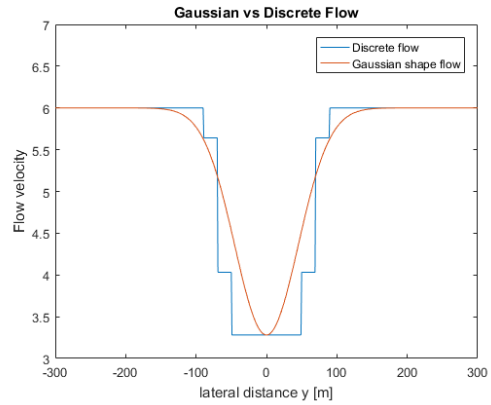


Figure 3: *Discrete wake versus Gaussian wake*

the wind farm as a function of the yaw misalignment and the axial induction. [8] FLORIS is a relative accurate[6] and a low computation model, due to the fact that it uses high-fidelity data from a computational fluid dynamics simulation.

i.1 Wake modelling

As can be seen in Figure 2, FLORIS contains a wake model which divides the wake in different zones: the near wake, the far wake, and the mixing zone, $q = 1$, $q = 2$, and $q = 3$ respectively. Each zone has its own diameter and wind speed, which are calculated by FLORIS.(1 to 2).

Let D_i denote the rotor diameter of the i^{th} turbine, k_e a coefficient that describes expansion of the zones , and $m_{e,q}$ the expansion factor which are calculated by Gebraad.[8]. The size of the wake diameter $D_{w,q,i}$ increases proportionally to the downwind distance (x). The diameter of the wake diameter is computed by,

$$D_{w,i,q}(x) = max(D_i + 2k_e m_{e,q}([x - X_i], 0) \quad (1)$$

Also the velocity depends on the downwind distance (x), which is an argument of the wake decay coefficient $c(x, y)$.2. This wake decay coefficient is multiplied by the axial induction factor and subtracted from the free stream velocity U_i. The axial induction factor is a value for the decrease in wind velocity behind a turbine relative to its own rotor speed. The wake decay coefficient describes the decay of velocity for each wake zone and is defined in 3. The model parameter $M_{U,q}$, which depends on the wake zone and the yaw angle, is calculated by Gebraad.[8]

$$U_{w,i}(x, y) = U_i \left(1 - 2a_i c_i(x, y)\right) \quad (2)$$

$$c_{i,q}(x) = \left[\frac{D_i}{D_i + 2k_e m_{U,q}(\gamma_i)[x - X_i]}\right]^2 \quad (3)$$

ii. FAST & MLife

FAST is a programming tool for the simulation of dynamic (load) responses of wind turbines (by NREL) [9]. It uses wind turbine specifications as well as wind flow situations. By evaluating a flow field, FAST computes the bending moment of a blade. Since the bending moment of a blade does not give direct information about the effect on the life-cycle time of a turbine, the program MLife is used to convert the bending moment to damage equivalent loads (DELs).

iii. Inflow files, Flow field

FLORIS describes a discrete flow field of a wake, with three zones. The flow field of the wake in FLORIS is calculated with equations ((1 to 2)). The wake is divided into three zones as described in paragraph i.1. A real wake will not have discrete zones, but a more fluent transition between the wake zones. To create a more fluent transition between the different wake-zones a Gaussian distribution of the flow field is preferred [7].The difference of wake shape between a Gaussian and discrete shape can be seen in Figure 3. The Gaussian distribution is calculated as followed,

$$G(y,z) = A[e^{-(\frac{y^2}{2\sigma_y}+\frac{z^2}{2\sigma_z})}] \tag{4}$$

where the amplitude of the Gaussian, A, is equal to the velocity loss of the inner wake zone, $U_{w,1}$, which is calculated with equation 2. σ_y and σ_z reflect the Gaussian standard deviation in horizontal and vertical direction, respectively. The standard deviations are related to the outer wake zone $D_{w,i,q=3}$ which is given in 5,

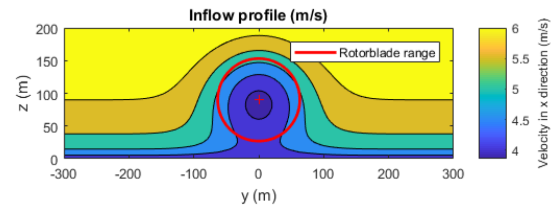
$$\sigma_y, \sigma_z = D_{w,i,q=3}/n \tag{5}$$

Where n can be modified to change the width of the Gaussian. Consequently, it is possible to fit the Gaussian to the wake zones of Gebraad. (Figure 3)

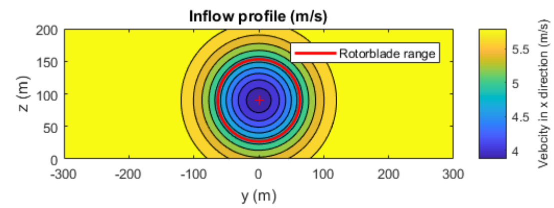
iv. Wind shear

Wind shear can cause an important difference in velocity speeds between the rotor hub height, the end of the rotor blades at their highest points and the end of the rotor blades at their lowest point [10]. The velocity distribution is calculated with,

$$v = v_{ref}\left[\frac{h}{h_{ref}}\right]^{\alpha} \tag{6}$$



(a) *Flow field with wind shear.*



(b) *Flow field without wind shear*

Figure 4: *Gaussian wind fields with a free stream velocity of 6 m/s at a height of 90 m. The outer diameter of de wake is 220 m and the diameter of the rotor blades is 126.4 m.*

where v and v_{ref} are the velocity at heights h, and h_{ref} respectively. Value α is the wind shear coefficient which depends on different factors. Coefficient α is fixed at value 0.1, reflecting a terrain type close to ocean and smooth ground [10]. The wind shear is implemented in the flow field. The difference between a flow field with and without wind shear can be seen in Figure 4

Table 1: *Overview of the minimum value, maximum value, and step size of the parameters, diameter of outer wake zone (Dwake), free stream wind speed (U), yaw of the turbine (yaw), and the center to center distance between the center of the turbine and the center of the wake (y wake).*

	Minimum	Maximum	Step-size
Dwake	180	330	25
U	6	8	2
yaw	-30	30	20, 10, 5
y wake	-250	250	10

Note: Input values for yaw are [-30, -10, -5, 0, 5, 10, 30].

v. LUT

To reduce computational time during optimization a look-up table (LUT) is created. The LUT is created using FAST and MLife, and it contains a a large number of DEL values for a wide variety of wind field conditions on a wind turbine. These different conditions are described by the ranges of the parameters, which can be seen in Table 1. The parameters are wake characteristics which can be extracted from FLORIS. The parameters chosen for the LUT are:

- the free stream wind speed, U
- the outer diameter of the wake, Dwake
- the yaw of the turbine, yaw
- the center to center distance between the turbine and the wake, y wake

To save calculation time, the LUT parameters are discretized, given each parameter a certain step-size. This step-size is chosen such that interpolation will give a representative result. For each parameters step-sizes are selected, as shown in Table 1. With the use of the pre-calculated LUT, online optimization can be realized.

vi. Optimization

To optimize for power reference tracking and load minimization, a game-theoretic approach was used.[12] The optimization algorithm searches for the optimal yaw and axial induction settings of each individual turbine. These can influence the power and loads significantly, so both are combined in a cost function. [12][6]

vi.1 Cost Function

The cost function depends on two variables: a normalized power and a normalized load variable. To achieve the optimal yaw and axial induction settings a mixed-objective cost function is defined as follows:

$$J(P, DEL) = c * ((P_{ref} - P(a_i, \gamma_i))/P_{bw})^2 + (1-c) * DEL(a_i, \gamma_i)/DEL_{base} \tag{7}$$

Where c is the tuning parameter for the optimization between power and loads and P_{ref} is the desired power output of the wind farm. P_{bw} and DEL_{base} are the power and loads baselines respectively, to create normalized variables.
To execute the optimization, the cost function has to be minimized. To obtain power production close to the reference, the power part of the cost function is a quadratic difference. As a result values much larger than the reference are heavily penalized, whereas the power crosses P_{bw} the emphasis shifts to the loads.

vi.2 Game Theory

The game-theoretic approach uses random perturbations for the yaw angles and the axial induction to optimize the cost function. When new values for yaw and axial induction settings give an improvement regarding the cost function, the settings are saved and the process will be repeated with this new settings. Because of the fact it uses random perturbations, the game theoretic approach is an adequate optimizer to find the global minimum of the settings.[6]

III. Results

Figures, tables with results and explanation.

the aimed outputs are the optimal variable settings of yaw and axial induction, at which the DELs are minimised for a set power output.

as discused in the capter on optimalisation, is the optimalisation caracterised by certine input settings. a better understanding of the optimalisation can be achived(?) by experimenting with these settings. this chapter will show some of the more significant cases. ——————————————————- - a realistic run (4MW ?)

- one with a ref power above the max, making it also optimize for power

-one extreme(0 power), validation the optimalisation methode for the extremes, relating it to the axial induction?

-one with more/less iterations, evaluating accuracy and computation time.

– bandwith -jurriaan? experimenting with relevance – optimalisation factor -only loads? -only power? ——————————————————

IV. Discussion

What have we done and how to interpret the results

Recommendations for further studies

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