

Wind Farm Power Regulation Using Yaw Control and Axial Induction Control

NIELS VAN DUIJN, JURRIAAN GOVERS, LUUK VAN HAGEN
JOCHEM HOORNEMAN, MAX VAN LEEUWEN
TU Delft

June 1, 2017

Abstract

*This will be the abstract of our paper. We will show how cool our research is and how important we are.
Blabla Lorem ipsum.*

I. INTRODUCTION

To efficiently use wind resource rich locations and minimize the cost of wind energy, wind turbines are constructed in close proximity of each other, resulting in a wind farm. A side effect of wind turbine operation is a wake. When wind turbines are placed in close proximity of each other, wakes can have negative effects on downwind turbines. A wake is developed behind a wind turbine and can reduce the power production while increasing the loads of the downwind turbine. A wake can be described by several characteristics, such as a decreased wind velocity caused by the turbine's extraction of energy, an increased turbulent wind flow caused by the rotation of the turbine blades, and a wake deflection can occur which can lead to suboptimal power and load conditions [6, 8, 9, 4, 3].

With an increasing role of wind energy (quantify this) in Europe's energy production new challenges arise[1]. While the electrical power system becomes more dependent on wind energy, it is important for wind farms to be able to meet the demands of the power

system by regulating its power output [2]. Traditionally, the need for power regulation of a wind farm was not necessary, because the wind farms energy production was only a small part of the total energy production. As a result, the wind farms could always perform at maximum capacity, without the risk of overloading the power system. However, because wind energy production has increased in the recent years, and will continue to increase, regulating rather than maximizing power output becomes more important.

Regulating the power output of a wind farm is essential because an under- or overload of energy can decrease the stability of the power system [2]. Instability can lead to suboptimal operation of the power system, such as an energy overload [2, ?]. Currently, most wind farms operate based on 'greedy control', meaning that the individual turbines always try to deliver maximum power for the turbine and not taking additional loads into account introduced by power maximization. This causes a problem when, for example, the power demand is low and the energy dependency of the power

system on wind energy is high. This could then result in an overload of the power system. Power regulation of a wind farm can solve this problem.

There are several methods for power regulation of a wind farm, two of which will be discussed in this paper, that is, yaw control and axial induction control. Yaw control can be used as a method to reduce the power output of a single wind turbine and as a method to increase power output and reduce loads of a wind farm [9, 8, 4, 16]. A disadvantage of yawing is an increase of load on the yawed turbine, and thus reducing its lifespan [3, 7]. In addition, yawing a turbine can deflect a wake. This can be used as a method to redirect a wake from a downwind turbine. This reduces the loads and increases the power output of the downwind turbine (van Dijk, Wilson, Fleming). However, under unfavorable conditions it can result in an asymmetrical overlap of the wake on the downwind turbine. This can significantly increase the loads of the downwind turbine [8, 9]. Therefore, it is necessary to understand the effects of yawing a turbine, what this does with its wake, and how this affects the downwind turbines.

Axial induction control influences the power output of a turbine by means of the blade pitch angle and generator torque. The axial induction factor is denoted by a , and reflects the relation between the decrease in wind velocity of the free stream wind and the wind velocity leaving the rotor. By varying the axial induction factor of a wind turbine, the power output can be controlled. Loads that are introduced by varying a turbine's axial induction factor will not be discussed in this paper. As yawing of the turbine and the deflection of a wake can cause additional loads on the turbines of a wind farm, a trade-off must be made between power regulation and loads minimization.

Previous studies have mainly focused on maximizing the power output while taking

the loads into account, so that an optimum is found between the two [9, 16, 8]. However, increased loading effects on a turbine due to yaw misalignment were not considered. Furthermore, the objective of these studies is power maximization rather than power regulation. Power regulation through a combination of yaw control and axial induction control while minimizing loads is still novel. This paper will focus on the optimization of power regulation, by means of yaw control and axial induction control, while minimizing the loads. In addition, the loading effects on a turbine caused by yaw misalignment is studied.

Hier nog een overzicht van wat er in paper te vinden is. Moet later geschreven worden als de rest af is.

II. METHOD

To realize active power control and minimizing loads by yaw control and axial induction, it is necessary to know the effects of different flow conditions on the total power of the wind farm and the effect of different flow conditions on the loads for each of the turbine. Moreover, there needs to be an optimizer which executes the optimization to approach a set value for the power and to minimize the loads.

The total power of the wind farm is calculated with the FLORIS-model. Besides, FLORIS is able to adjust the turbine configurations, the axial induction and yaw position. The effect of the wind flow on a turbine, regarding the loads, are given by the programs FAST and MLife. The output of these programs are Damage Equivalent Load values (DELs), which are a measure of equivalent load damage to the turbine concerning the material properties.[14] These DELs are calculated for a different set of wind and turbine conditions and are stored in a look-up table (LUT).

The optimizer takes the desired power production of the wind farm as an input. It

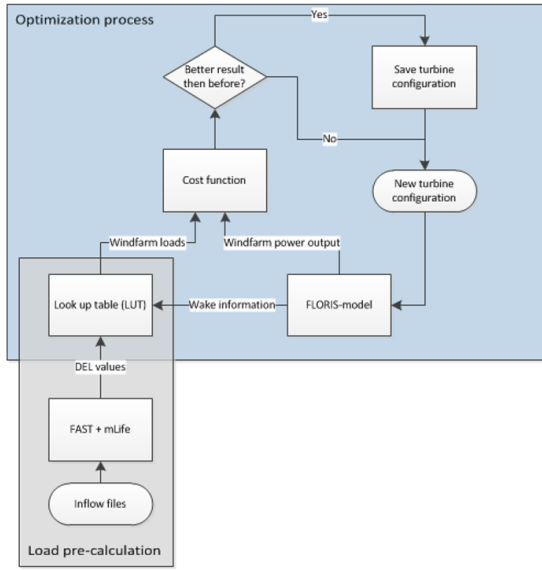


Figure 1: Overview of the optimization procedure.

used the configurations of the turbines from FLORIS to find the corresponding DEL values in the look-up table. If the configurations of the turbines are an improvement compared to the previous one, i.e. a improved power control or a reduce in the loads, FLORIS will save this turbine configurations. An overview of the optimization procedure is shown in Figure 1.

In the following sections, different models and model steps, used to perform the optimization, are explained:

i. FLORIS

The FLOW Redirection and Induction in Steady state (FLORIS) model calculates the power of the wind farm as a function of the yaw misalignment and the axial induction. [11] FLORIS is a relative accurate[9] and a low computation model, due to the fact that it uses high-fidelity data from a computational fluid dynamics simulation.

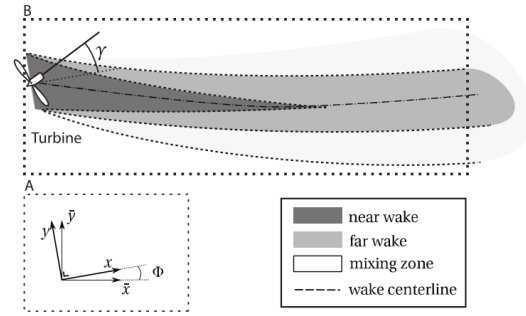


Figure 2: Simplified top view representation of a wake of a turbine by FLORIS.[11]

i.i Wake modelling

As can be seen in Figure 2, FLORIS contains a wake model which divides the wake in different zones: the near wake, the far wake, and the mixing zone, $q = 1$, $q = 2$, and $q = 3$ respectively. Each zone has its own diameter and wind speed, which are calculated by FLORIS.(1 to 2).

Let D_i denote the rotor diameter of the i^{th} turbine, k_e a coefficient that describes expansion of the zones, and $m_{e,q}$ the expansion factor which are calculated by Gebraad.[11]. The size of the wake diameter $D_{w,q,i}$ increases proportionally to the downwind distance (x). The diameter of the wake diameter is computed by,

$$D_{w,i,q}(x) = \max(D_i + 2k_e m_{e,q}([x - X_i], 0), 0) \quad (1)$$

Also the velocity depends on the downwind distance (x), which is an argument of the wake decay coefficient $c(x, y)$.2. This wake decay coefficient is multiplied by the axial induction factor and subtracted from the free stream velocity U_i . The axial induction factor is a value for the decrease in wind velocity behind a turbine relative to its own rotor speed. The wake decay coefficient describes the decay of velocity for each wake zone and is defined in 3. The model parameter $M_{U,q}$, which depends on the wake zone and the yaw angle, is calculated by

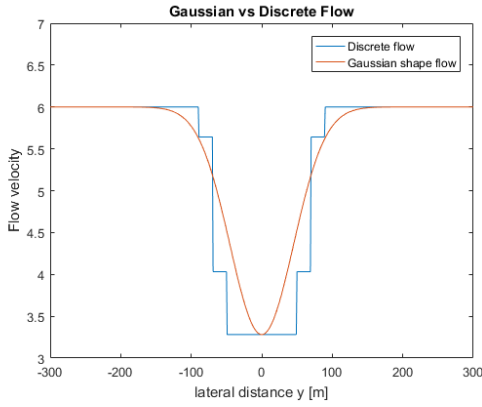


Figure 3: Discrete wake versus Gaussian wake

Gebraad.[11]

$$U_{w,i}(x, y) = U_i (1 - 2a_i c_i(x, y)) \quad (2)$$

$$c_{i,q}(x) = \left[\frac{D_i}{D_i + 2k_e m_{U,q}(\gamma_i) [x - X_i]} \right]^2 \quad (3)$$

ii. FAST & MLife

FAST is a programming tool for the simulation of dynamic (load) responses of wind turbines (by NREL) [12]. It uses wind turbine specifications as well as wind flow situations. By evaluating a flow field, FAST computes the bending moment of a blade. Since the bending moment of a blade does not give direct information about the effect on the life-cycle time of a turbine, the program MLife is used to convert the bending moment to damage equivalent loads (DELs).

iii. Inflow files, Flow field

FLORIS describes a discrete flow field of a wake, with three zones. The flow field of the wake in FLORIS is calculated with Equations ((1 to 2)). The wake is divided into three zones as described in paragraph i.i. A real wake will not have discrete zones, but a more fluent transition between the wake zones. To create a

more fluent transition between the different wake-zones a Gaussian distribution of the flow field is preferred [10]. The difference of wake shape between a Gaussian and discrete shape can be seen in Figure 3. The Gaussian distribution is calculated as followed,

$$G(y, z) = A [e^{-\left(\frac{y^2}{2\sigma_y} + \frac{z^2}{2\sigma_z}\right)}] \quad (4)$$

where the amplitude of the Gaussian, A , is equal to the velocity loss of the inner wake zone, $U_{w,1}$, which is calculated in Equation 2. σ_y and σ_z reflect the Gaussian standard deviation in horizontal and vertical direction, respectively. The standard deviations are related to the outer wake zone $D_{w,i,q=3}$ which is given in 5,

$$\sigma_y, \sigma_z = D_{w,i,q=3} / n \quad (5)$$

Where n can be modified to change the width of the Gaussian. Consequently, it is possible to fit the Gaussian to the wake zones of Gebraad. (Figure 3)

iv. Wind shear

Wind shear can cause an important difference in velocity speeds between the rotor hub height, the end of the rotor blades at their highest points and the end of the rotor blades at their lowest point [13]. The velocity distribution is calculated with,

$$v = v_{ref} \left[\frac{h}{h_{ref}} \right]^\alpha \quad (6)$$

where v and v_{ref} are the velocity at heights h , and h_{ref} respectively. Value α is the wind shear coefficient which depends on different factors. Coefficient α is fixed at value 0.1, reflecting a terrain type close to ocean and smooth ground [13]. The wind shear is implemented in the flow field. The difference between a flow field with and without wind shear can be seen in Figure 4

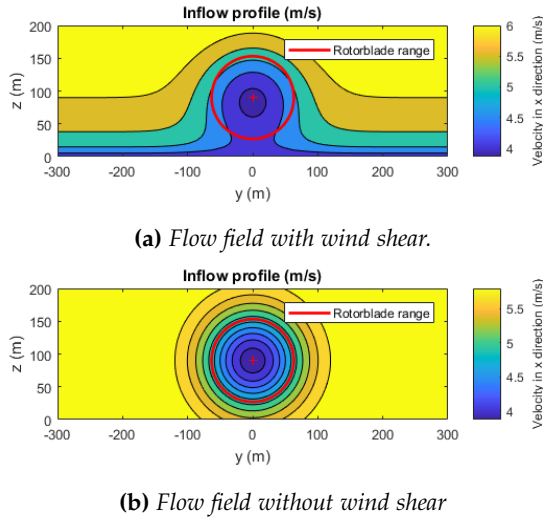


Figure 4: Gaussian wind fields with a free stream velocity of 6 m/s at a height of 90 m. The outer diameter of the wake is 220 m and the diameter of the rotor blades is 126.4 m.

v. LUT

To reduce computational time during optimization a look-up table (LUT) is created. The LUT is with the use of the programs FAST and MLife, and contains a large number of DEL values for a wide variety of wind field conditions on a wind turbine. These different conditions are described by the ranges of the parameters, which can be seen in Table 1. The parameters are wake characteristics which can be extracted from FLORIS. The parameters chosen for the LUT are:

- the free stream wind speed, U
- the outer diameter of the wake, D_{wake}
- the yaw of the turbine, yaw
- the center to center distance between the turbine and the wake, y_{wake}

To save calculation time, the LUT parameters are discretized, given each parameter a certain step-size. This step-size is chosen such that interpolation will give a representative result. For each parameters step-sizes are selected, as

Table 1: Overview of the minimum value, maximum value, and step size of the parameters, diameter of outer wake zone (D_{wake}), free stream wind speed (U), yaw of the turbine (yaw), and the center to center distance between the center of the turbine and the center of the wake (y_{wake}).

	Minimum	Maximum	Step-size
D_{wake}	180	330	25
U	6	8	2
yaw	-30	30	*
y_{wake}	-250	250	10

*Input values for yaw are [-30, -10, -5, 0, 5, 10, 30].

shown in Table 1. With the use of the pre-calculated LUT, online optimization can be realized.

Linear interpolation is used to estimate the DEL values between the data points of the LUT. It is assumed that the DELs as a result of the wind speed (U) could be estimated accurately enough using only the 2 outer bounds. These bound were enough for the goal of this paper, though larger wind farms and different inflow wind velocities would require broadening these ranges.

The DEL effect of the D_{wake} was also found to be accurate enough using fairly large step sizes. the range of this parameter was chosen so all downwind turbines within .. and .. meters could be accurately fitted.

The parameter y_{wake} however, fluctuates over its range, and could not be accurately estimated using linear interpolation over large step sizes. as mentioned in... .A step size of 10 meters, totaling a total of 51 steps, was found to be sufficiently accurate.

The yaw parameter is chosen at a step size of 10 degree, however extra data points were added at ± 5 degree to improve the accuracy in the lower yaw regions. This effect is shown in Figure 5

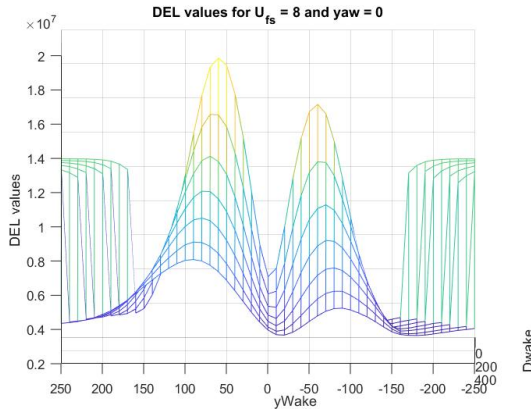


Figure 5: *page filler, not the accurate figure.*

vi. Optimization

To optimize for power reference tracking and load minimization, a game-theoretic approach was used.[15] The optimization algorithm searches for the optimal yaw and axial induction settings of each individual turbine. These settings can influence the power and loads significantly, so both are combined in a cost function. [15][9]

vi.i Cost Function

The cost function depends on two variables: a normalized power and a normalized load variable. To achieve the optimal yaw and axial induction settings a mixed-objective cost function is defined as follows:

$$J(P, DEL) = c * ((P_{ref} - P(a_i, \gamma_i)) / P_{bw})^2 + (1 - c) * DEL(a_i, \gamma_i) / DEL_{mean} \quad (7)$$

Where c is the tuning parameter for the optimization between power and loads and P_{ref} is the desired power output of the wind farm. P_{bw} is the bandwidth of the power in which the power values are acceptable around the reference power. DEL_{mean} is the mean DEL value of the complete LUT.

To execute the optimization, the cost function

has to be minimized. To obtain power production close to the reference, the power part of the cost function is a quadratic difference. As a result values much larger or smaller than the reference are heavily penalized, whereas when the power is within the bandwidth the emphasis shifts to the loads.

vi.ii Game Theory

The game-theoretic approach uses random perturbations for the yaw angles and the axial induction to optimize the cost function. When new values for yaw and axial induction settings give an improvement regarding the cost function, the settings are saved and the process will be repeated with the new settings. Because of the fact it uses random perturbations, the game theoretic approach is an adequate optimizer to find the global minimum of the cost function.[9]

III. RESULTS

This chapter shall describe, compare and evaluate the results of 3 optimisation cases.

- Maximum power production
- Power production at 80 %
- Power production at 60 %

For all these cases was a 9 turbine windfarm used as shown in fig... And were simulated under constant 8 m/s windconditions.

–

Case 1: maximum power production: This, first, case is used to determine the maximum power output that the 9 turbine farm can extract from the previously described windconditions, this case neglects the loads.

Case 2 and 3: Power production at 80 and 60%: These cases are run at 80 and 60 percent of the maximum power output determined in the first case. The goal of these cases is to find the optimal running procedure given a required constant poweroutput. the required

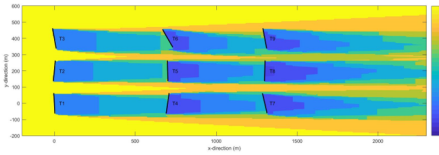


Figure 6: *page filler, not the accurate figure.*

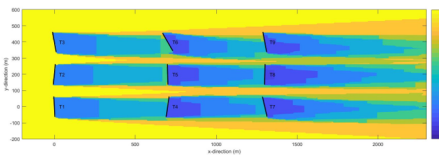


Figure 7: *page filler, not the accurate figure.*

power output chosen for this paper is link to the maximum possible, since ...why?

i. Comparing

Power converges reading out the maximum power, stating that power production does indeed approach the ref power

DELs decrease comparing loads, also among eachoter, wat is the effect of lower ref power on the loads/

More?

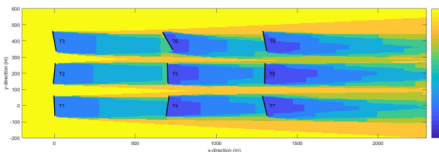


Figure 8: *page filler, not the accurate figure.*

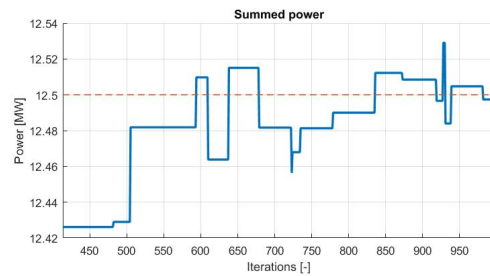


Figure 9: *page filler, not the accurate figure.*

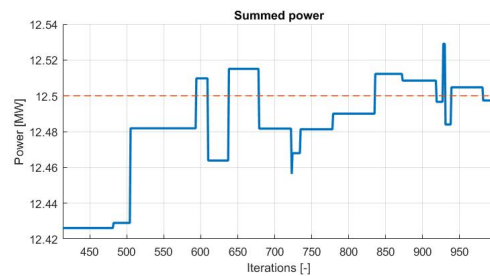


Figure 10: *page filler, not the accurate figure.*

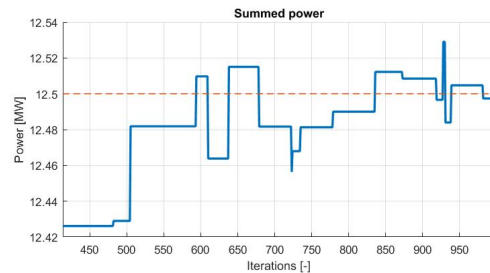


Figure 11: *page filler, not the accurate figure.*

IV. CONCLUSION, DISCUSSION AND RECOMMENDATIONS

What have we done and how to interpret the results

i. Conclusion

Conclusion about the results, Power reduction by axial induction and yaw control will lead to a reduction in the loads on the wind farm.

ii. Discussion+Recommendations

This article which presents the results of an multi-objective wind farm optimization through yaw control and axial induction is bound to a number of limitations.

- FLORIS, a low fidelity steady state model is used to calculate the flow in the wind farm. Turbulence and dynamic propagation of the wake as a consequence of turbine settings and the effect of wakes influencing each other are not implemented. Moreover, the turbine determines its loads only for the most overlapping wake on the turbine, for the other wakes is a mean value taken. The effects in the wakes and the effect of multiple wakes on one turbine can have a significant influence on the loads of the turbine. Our results for reference power tracking and load minimizations are only obtained from a three by three setup of wind turbines. Another setup or number of wind turbines may lead to other results.
- FAST calculates the loads on the turbine based on a modeled inflow field which also does not take turbulence effects in the wake into account. The effect of dynamic propagation of the wake will lead to other load values. The shear effect on the wind speed of the inflow field is calculated for a reference height and speed. Also the shear

constant was set for a flat ocean ground surface. The continuous wake profile uses only the velocity in the inner wake zone and the diameter of the outer wake zone from Gebraad. [11] The partition of the wake in several wake zones with its own diameter and velocity is not longer implemented. For a sufficient model of the wake, a continuous function with more adjustable variables compared to one Gaussian should be considered.

- The look-up-table with the DEL values is made for parameters with a step size.
-

REFERENCES

- [1] Energieonderzoek Centrum Nederland. "Nationale Energieverkenning 2016"
- [2] J. O. G. Tande. "Grid integration of wind farms," in Wind Energy, 2003
- [3] «««« HEAD D. S. Zalkind and L. Y. Pao. "The fatigue loading effects of yaw control for wind plants," in American Control Conference (ACC), 2016 ===== D. S. Zalkind and L. Y. Pao. "The fatigue loading effects of yaw control for wind plants," in American Control Conference (ACC), 2016
- [4] P. A. Fleming, P. M. Gebraad, S. Lee, J. W. van Wingerden, K. Johnson, M. Churchfield, P. Moriarty. "Evaluating techniques for redirecting turbine wakes using SOWFA." in Renewable Energy, 2014
- [5] A. D. Hansen, P. S. Jørgensen, F. Iov, F. Blaabjerg. "Centralised power control of wind farm with doubly fed induction generators." in Renewable Energy, 2005
- [6] S. Boersma, B. M. Doekemeijer, P. M. O. Gebraad, P. A. Fleming, J. Annoni, A. K. Scholbrock, J. A. Frederik, and

- J-W. van Wingerden. "A Tutorial on Control-Oriented Modeling and Control of Wind Farms," presented at the American Control Conference, 2017 »»»»>2be9d50664f6e6083b7ca432cdf660485459e205
- [7] S. K. Kanev and F. J. Savenije. "Active wake control: loads trends," in *Wind Energy*, 2017
- [8] B. Wilson. "Wind Farm Control: Robust Multi-Objective Optimization of a Wind Farm for Different Control Strategies," Unpublished Master's Thesis, 2017
- [9] M. T. van Dijk, J. W. van Wingerden, T. Ashuri, Y. Li, and M. A. Rotea. "Yaw-Misalignment and its Impact on Wind Turbine Loads and Wind Farm Power Output," in *Journal of Physics: Conference Series*, 2016
- [10] M. Bastankhah and F. Porte-Agel. "Experimental and theoretical study of wind turbine wakes in yawed conditions," in *Journal of Fluid Mechanics*, 2016
- [11] P. M. O. Gebraad, F. W. Teeuwisse, J. W. Wingerden, P. A. Fleming, S. D. Ruben, J. R. Marden and L. Y. Pao. "Wind plant power optimization through yaw control using a parametric model for wake effects—a CFD simulation study," in *Wind Energy*, 2016
- [12] J. M. Jonkman and M. L. Buhl Jr. "FAST User's Guide," National Renewable Energy Laboratory, Golden, CO, Technical Report No. NREL/EL-500-38230, 2005
- [13] E. Firtin, O. Guler, and S. A. Akdag. "Investigation of wind shear coefficients and their effect on electrical energy generation," in *Applied Energy*, 2011
- [14] A. Chougule, S. T. Kandukuri, and H.-G. Beyer. "Assessment of synthetic winds through spectral modeling and validation using FAST." *Journal of Physics: Conference Series*. Vol. 753. No. 4. IOP Publishing, 2016.
- [15] J. R. Marden, D. R. Shalom, and L. Y. Pao. "A model-free approach to wind farm control using game theoretic methods." *IEEE Transactions on Control Systems Technology* 21.4 (2013): 1207-1214.
- [16] M. van Dijk. "A Study on Yaw-Misalignment: Combined Optimization of Wind Farm Power Production and Structural Loading," Unpublished Master's Thesis, 2016