

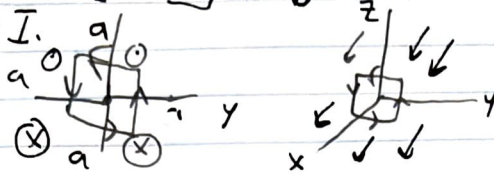
5.4 5.7 5.11 5.12 5.16 5.19 5.21 5.23 5.27

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5.12 repeat.

EMQHW 5.

CC current I . 5.4) At $\vec{B} = k z \hat{x}$ Force on square loop in yz plane.



$F = \int (I \times B) d\vec{l}$ left and right sides cancel by right hand rule.

$$\begin{aligned} \vec{F}_{top} &= \int (I \times B) d\vec{l} \Rightarrow \vec{F}_{top} = I \int d\vec{l} \times \vec{B} \quad I \text{ is constant} = I \int (-\hat{y} dy \times \frac{ka}{2} \hat{x}) \\ &= I \int \frac{ka}{2} dy \hat{z} \quad \vec{F}_{top} = \frac{Ika^2}{2} \hat{z} \quad \vec{F}_{bottom} = I \int d\vec{l} \times \vec{B} = I \int (\hat{y} dy \times \frac{-ka}{2} \hat{x}) = 0 \\ &= \frac{Ika^2}{2} \hat{z} \quad \text{So } \boxed{\vec{F}_{total} = Ika^2 \hat{z}} \end{aligned}$$

5.7) Show $\int_V \vec{j} dV = \frac{d\vec{p}}{dt}$. \vec{p} is total dipole moment.

$$\frac{d\vec{p}}{dt} = \frac{d}{dt} \int_V \rho \vec{r} dV = \int_V \frac{\partial \rho}{\partial t} \vec{r} dV = - \int_V (\nabla \cdot \vec{j}) \vec{r} dV \quad \text{Product rule 5.}$$

$$\nabla \cdot (x \vec{j}) = x (\nabla \cdot \vec{j}) + \vec{j} \cdot (\nabla x) \quad \nabla x = \hat{x} \text{ so } \nabla \cdot (x \vec{j}) = x (\nabla \cdot \vec{j}) + j_x$$

$$\text{So } \int_V (\nabla \cdot \vec{j}) x dV = \int_V \nabla \cdot (x \vec{j}) dV - \int_V j_x dV \quad \int_V \nabla \cdot (x \vec{j}) dV = 0 \text{ so}$$

$$\int_V (\nabla \cdot \vec{j}) x dV = - \int_V j_x dV \Rightarrow \int_V (\nabla \cdot \vec{j}) \vec{r} dV = - \int_V \vec{j} dV \text{ so } \frac{d\vec{p}}{dt} = \int_V \vec{j} dV$$

5.11) $B = \frac{\mu_0 n I}{2} \int \frac{a^2}{(a^2 + z^2)^{3/2}} dz$ from equation 5.41. $z = a \cot \theta$. Trig sub.

$$dz = -\frac{a}{\sin^2 \theta} d\theta \text{ so } \frac{1}{(a^2 + z^2)^{3/2}} = \frac{\sin^3 \theta}{a^3} \text{ so } B = \frac{\mu_0 n I}{2} \int \frac{a^2 \sin^3 \theta}{a^3 \sin^2 \theta} (-a d\theta)$$

$$\Rightarrow B = \frac{\mu_0 n I}{2} \int \frac{a \sin \theta}{a} d\theta \Rightarrow B = \frac{\mu_0 n I}{2} \int \sin \theta d\theta \Rightarrow \boxed{B = \frac{\mu_0 n I}{2} (\cos \theta_2 - \cos \theta_1)}$$

Now infinite solenoid. $\theta_2 = 0$ and $\theta_1 = \pi$. $\boxed{B = \mu_0 n I}$

5.12) $dB = \frac{\mu_0 dI}{2} \frac{(R \sin \theta)^2}{[(R \sin \theta)^2 + (R \cos \theta)^2]^{3/2}} = \frac{\mu_0 \sin^3 \theta dI}{2R}$ $dI = KR d\theta$ $K = \frac{Q\omega}{4\pi R}$ $\omega = \frac{Q}{4\pi R^2}$ $v = \omega R \sin \theta$

$$dI = \frac{Q}{4\pi R^2} \omega R \sin \theta R d\theta = \frac{Q\omega}{4\pi} \sin \theta d\theta \quad B = \frac{\mu_0}{2R} \frac{Q\omega}{4\pi} \int \sin^3 \theta d\theta = \frac{\mu_0 Q\omega}{8\pi R} \left(\frac{4}{3} \right) \quad \boxed{\vec{B} = \frac{\mu_0 Q\omega}{6\pi R} \hat{z}}$$

5.16) i) $\vec{B} = \mu_0 I (n_2 - n_1) \hat{z}$. ii) $\vec{B} = \mu_0 I n_2 \hat{z}$ iii) $\vec{B} = 0$.

5.19) This does not matter because $\int \vec{J} \cdot d\vec{a}$ works with any arbitrary surface because \vec{J} has no divergence.

5.21) Ampere's Law consistency with electrodynamics.

It's not consistent because it says $\nabla \times \vec{B} = \mu_0 \vec{J}$ But if you use 5.29 you get $\nabla \cdot (\nabla \times \vec{B}) = \mu_0 \nabla \cdot \vec{J}$ which is not consistent $\nabla \cdot \nabla \times \vec{f} = 0$.

The other Maxwell Equations do not have this issue. So Ampere's Law needs some work done to it!

5.23) Get magnetic vector potential of a finite section of a thin straight wire with current I . Check answer with 5.37.

$$A = \frac{\mu_0}{4\pi} \int \frac{I \hat{z}}{R} dz = \frac{\mu_0 I}{4\pi} \hat{z} \int_{z_1}^{z_2} \frac{dz}{\sqrt{z^2 + s^2}} = \frac{\mu_0 I}{4\pi} \hat{z} \left[\ln(z + \sqrt{z^2 + s^2}) \right]_{z_1}^{z_2}$$

So $\vec{A} = \frac{\mu_0 I}{4\pi} \ln \left[\frac{z_2 + \sqrt{z_2^2 + s^2}}{z_1 + \sqrt{z_1^2 + s^2}} \right] \hat{z}$. Now for the B-field.

$\vec{B} = \nabla \times \vec{A} \Rightarrow \vec{B} = -\frac{\partial A}{\partial s} \hat{\phi}$. Done in sage math. Lots of stuff going on in that derivative

Let $\frac{z_2}{\sqrt{z_2^2 + s^2}} = \sin \theta_2$ and $\frac{z_1}{\sqrt{z_1^2 + s^2}} = \sin \theta_1$

$$\vec{B} = \frac{\mu_0 I}{4\pi s} \left[\frac{z_2}{\sqrt{z_2^2 + s^2}} - \frac{z_1}{\sqrt{z_1^2 + s^2}} \right] \hat{\phi}$$

$$\vec{B} = \frac{\mu_0 I}{4\pi s} (\sin \theta_2 - \sin \theta_1) \hat{\phi}$$

This holds with 5.37

5.27) Get vector potential below and above plane surface current in 5.8.

$\vec{K} = K \hat{x}$. $\vec{B} = \pm \frac{\mu_0 K}{2} \hat{y}$. + for $z < 0$ and - for $z > 0$!

$\vec{B} = \nabla \times \vec{A} = \begin{vmatrix} \hat{x} & \hat{y} & \hat{z} \\ \frac{\partial}{\partial x} & \frac{\partial}{\partial y} & \frac{\partial}{\partial z} \\ A(x) & 0 & 0 \end{vmatrix} = \frac{\partial A}{\partial z} \hat{y} = \pm \frac{\mu_0 K}{2} \hat{y}$ A is only going to be in \hat{x} since A is parallel to \vec{K} .

$\frac{\partial A}{\partial z} = \pm \frac{\mu_0 K}{2}$

$\frac{\partial A}{\partial z} = \pm \frac{\mu_0 K}{2} \Rightarrow \int \partial A = \pm \frac{\mu_0 K}{2} \partial z$

$\vec{A} = \pm \frac{\mu_0 K}{2} z \hat{x}$ \hat{x} because $\vec{K} \propto \hat{x}$!