

Control Systems - Report



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1(a) First Order Equation with open loop and without controller

Plant Description

The Mass-damper first order system is taken as Plant. Equation: $f = Bv + M v'$ f = force; B = coefficient of friction; M = mass ; v = velocity. Values: $B_1 = 0.4$, $M_1 = 1000$; $B_2 = 0.5$, $M_2 = 500$; $B_3 = 1.7$, $M_3 = 340$;

Code

```
clc;
B1= ([0.1 0.5 1.7]);
M1=( [1000 5 340]);
for i=1:3
    sys = tf([1/M1(i)],[1,B1(i)/M1(i)])
    figure(i);
    subplot(2,1,1);
    impulse(sys);
    title('Impulse Input');
    subplot(2,1,2);
    step(sys);
    title('Step Input');
    [z,p,k]= tf2zp([1/M1(i)],[1,B1(i)/M1(i)])
    figure(4);
    zplane(z,p);
    xlim([-4*1e5 2*1e5]);
    ylim([-4*1e5 2*1e5]);
    hold on;
    S = stepinfo(sys)
end
```

sys =

```

    0.001
-----
s + 0.0001
```

Continuous-time transfer function.

z =

```
0x1 empty double column vector
```

p =

```
-1.0000e-04
```

k =

```
1.0000e-03
```

```
S =
```

```
struct with fields:
```

```
    RiseTime: 2.1970e+04
SettlingTime: 3.9121e+04
SettlingMin: 9.0450
SettlingMax: 9.9997
    Overshoot: 0
    Undershoot: 0
        Peak: 9.9997
    PeakTime: 1.0546e+05
```

```
sys =
```

```
    0.2
-----
s + 0.1
```

```
Continuous-time transfer function.
```

```
z =
```

```
0x1 empty double column vector
```

```
p =
```

```
-0.1000
```

```
k =
```

```
0.2000
```

```
S =
```

```
struct with fields:
```

```
    RiseTime: 21.9701
SettlingTime: 39.1207
SettlingMin: 1.8090
SettlingMax: 1.9999
    Overshoot: 0
```

```
Undershoot: 0
Peak: 1.9999
PeakTime: 105.4584
```

```
sys =
```

```
0.002941
-----
s + 0.005
```

```
Continuous-time transfer function.
```

```
z =
```

```
0x1 empty double column vector
```

```
p =
```

```
-0.0050
```

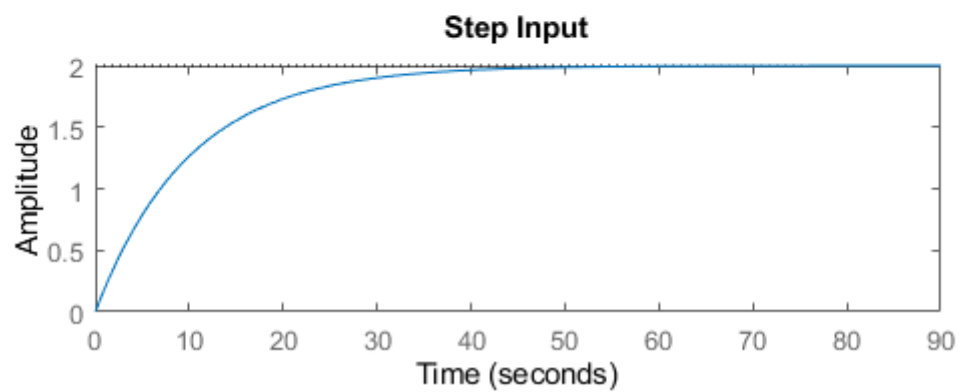
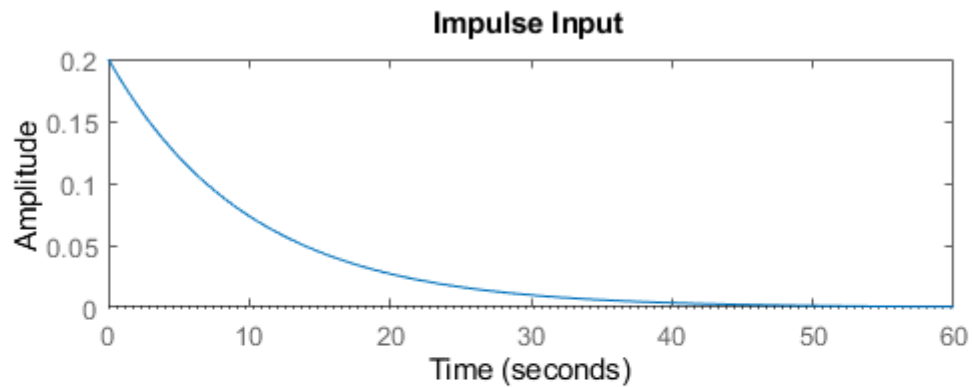
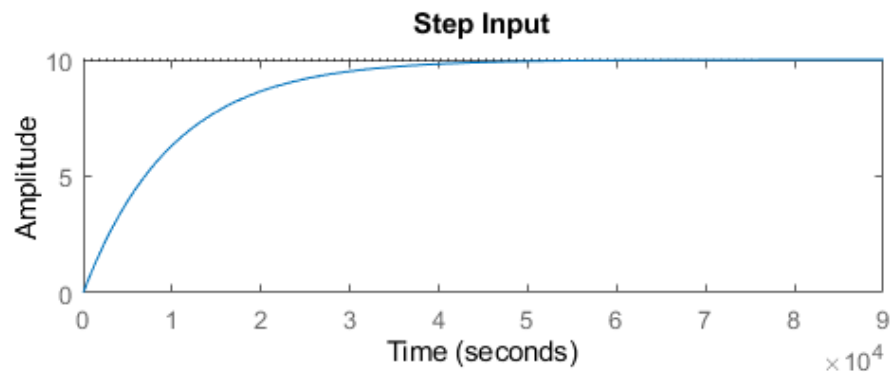
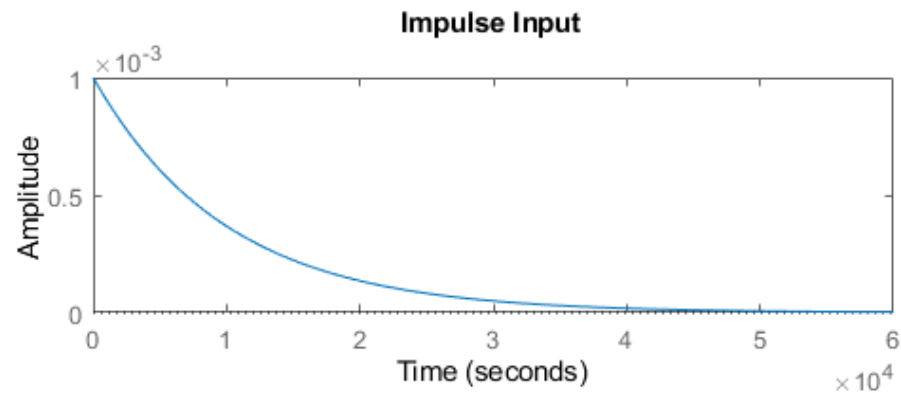
```
k =
```

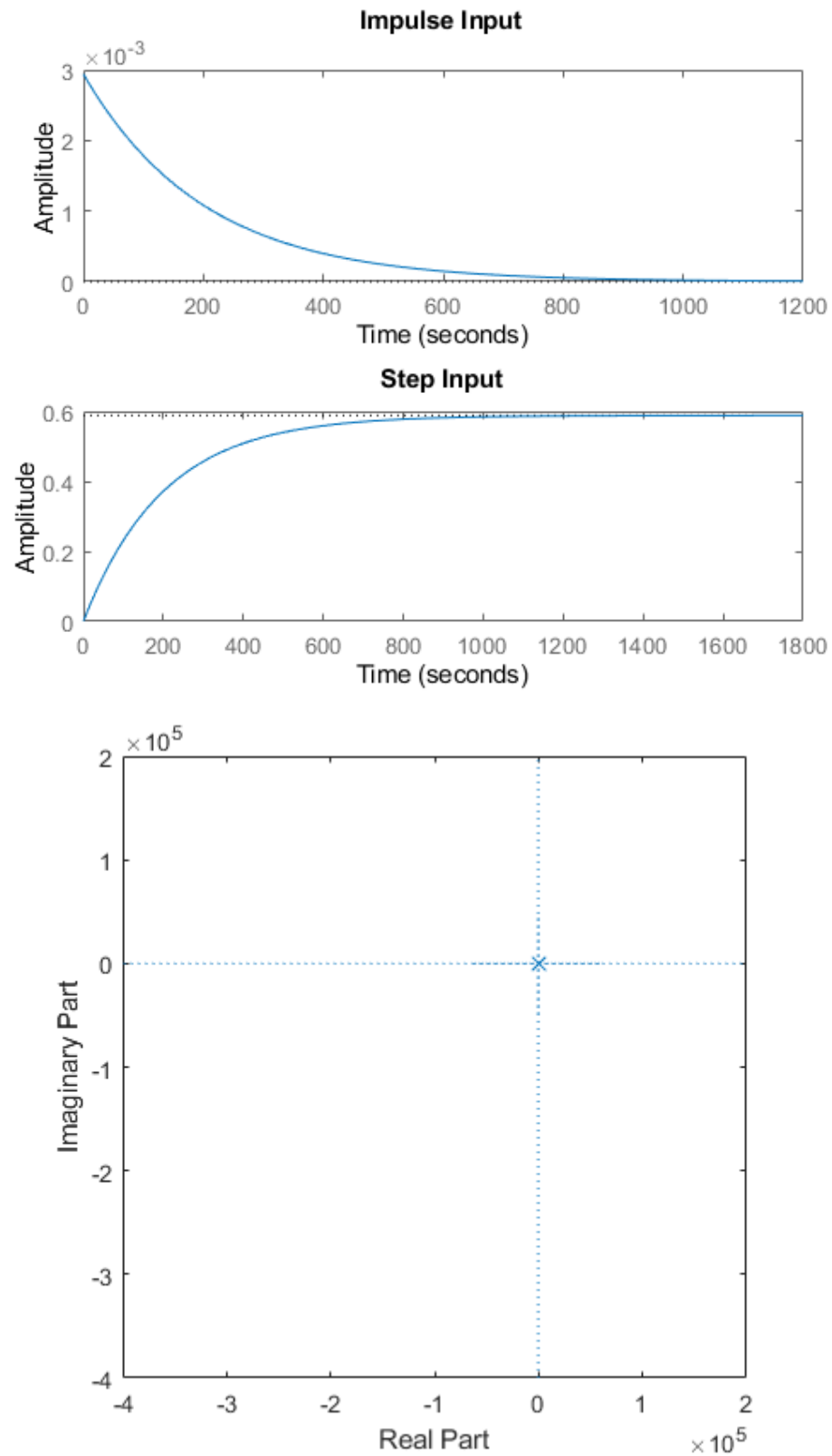
```
0.0029
```

```
s =
```

```
struct with fields:
```

```
    RiseTime: 439.4013
SettlingTime: 782.4149
SettlingMin: 0.5321
SettlingMax: 0.5882
    Overshoot: 0
    Undershoot: 0
        Peak: 0.5882
    PeakTime: 2.1092e+03
```





Math Analysis

Independent: Time(t) Dependent: Velocity(v) and Force(f) Constant: Mass(M) and Frictional Coefficient(B)

```
% Roots: (-B)/M

% IVT:
% 1. For step input: 0
% 2. For impulse input: 1/M

% FVT:
% 1. For step input: 1/B
% 2. For impulse input: 0

% Time Response Results:
% Rise Time :4tau = (4M)/B; where tau = M/B
```

Comparison Analysis:(Speed, Accuracy and stability):

1) $s=0.001/(0.0001s+1)$ - a stable system as the poles are in the 2nd

```
%and 3rd quadrant.
% 2) There is no overshoot since it's a first order system.
% 3) The rise time of 2nd system is least and hence it is the fastest
%system.
% 4) The settling time of 2nd system is least and hence making it more
%accurate than the rest of them.
% 5) The poles are moving farther away, the more the system becomes stable,
%as we can see in 2nd system.
```

1(b) First Order Equation with open loop and controller

Plant Description

The Mass-damper first order system is taken as Plant. Equation: $f = Bv + M v'$ f = force; B = coefficient of friction; M = mass ; v = velocity. Values: $B_1= 0.4$, $M_1=1000$; $B_2= 0.5$, $M_2= 500$; $B_3= 1.7$, $M_3= 340$;

Code

```
clc;
B1= 0.5;
M1= 5;
P = 2;

sys = tf([P/M1],[1,B1/M1])
subplot(3,4,1);
impz(sys);
title('Impulse Input for k');
subplot(3,4,2);
```

```

step(sys);
title('Step Input for k');
subplot(3,4,3);
[z,p,k]= tf2zp([P/M1],[1,B1/M1])
pzmap(sys)
subplot(3,4,4);
bode(sys)
hold on;
S = stepinfo(sys)

sys = tf([P/M1],[1,B1/M1,0])
subplot(3,4,5);
impulse(sys);
title('Impulse Input for 1/s');
subplot(3,4,6);
step(sys);
title('Step Input for 1/s');
subplot(3,4,7);
[z,p,k]= tf2zp([P/M1],[1,B1/M1,0])
pzmap(sys)
subplot(3,4,8);
bode(sys)
hold on;
S = stepinfo(sys)

sys = tf([P/M1,0],[1,B1/M1])
subplot(3,4,9);
impulse(sys);
title('Impulse Input for s');
subplot(3,4,10);
step(sys);
title('Step Input for s');
subplot(3,4,11);
[z,p,k]= tf2zp([P/M1,0],[1,B1/M1])
pzmap(sys)
subplot(3,4,12);
bode(sys)
hold on;
S = stepinfo(sys)

```

```
sys =
```

```

    0.4
-----
s + 0.1

```

Continuous-time transfer function.

```
z =
```

0x1 empty double column vector

p =

-0.1000

k =

0.4000

s =

struct with fields:

RiseTime: 21.9701
SettlingTime: 39.1207
SettlingMin: 3.6180
SettlingMax: 3.9999
Overshoot: 0
Undershoot: 0
Peak: 3.9999
PeakTime: 105.4584

sys =

0.4

s^2 + 0.1 s

Continuous-time transfer function.

z =

0x1 empty double column vector

p =

0
-0.1000

k =

0.4000

S =

struct with fields:

```
RiseTime: NaN
SettlingTime: NaN
SettlingMin: NaN
SettlingMax: NaN
Overshoot: NaN
Undershoot: NaN
Peak: Inf
PeakTime: Inf
```

sys =

```
0.4 s
-----
s + 0.1
```

Continuous-time transfer function.

z =

0

p =

-0.1000

k =

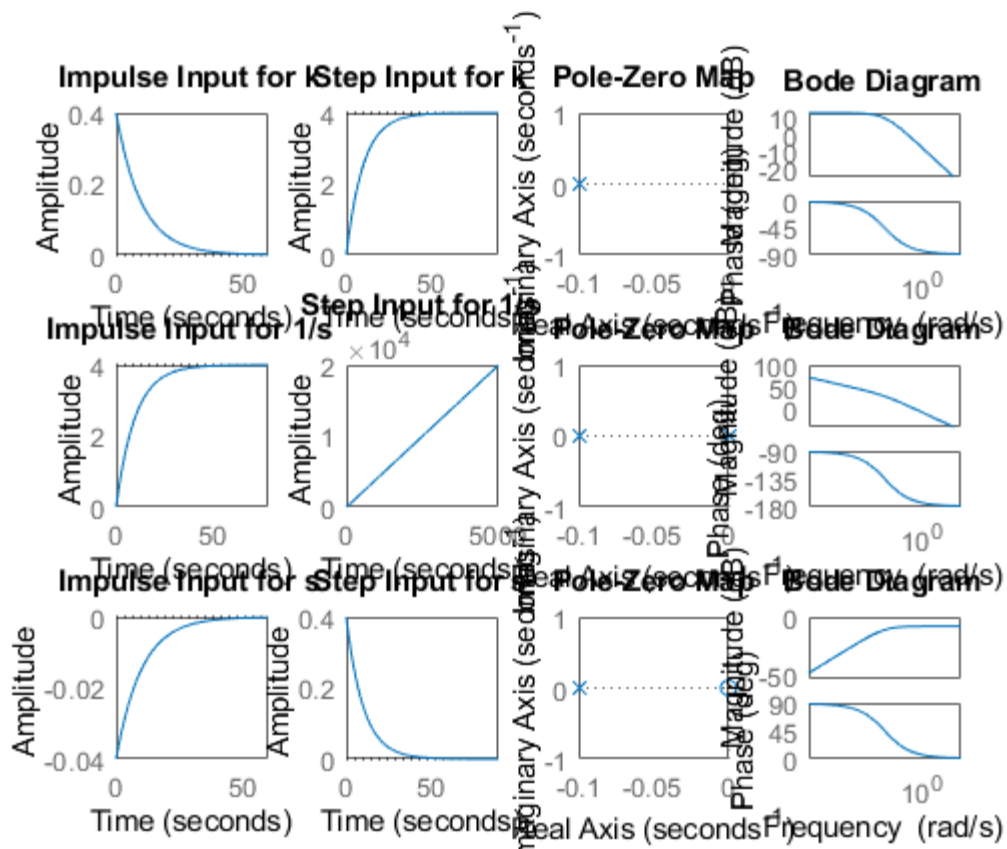
0.4000

S =

struct with fields:

```
RiseTime: 21.9701
SettlingTime: 39.1207
SettlingMin: 1.0521e-05
SettlingMax: 0.0382
Overshoot: 0
Undershoot: 7.2058e+17
Peak: 0.4000
```

PeakTime: 0



Math Analysis

Independent: Time(t) Dependent: Velocity(v) and Force(f) Constant: Mass(M) and Frictional Coefficient(B)

```
% Roots: (-B)/M

% IVT:
% 1. For step input: 0
% 2. For impulse input: 1/M

% FVT:
% 1. For step input: 1/B
% 2. For impulse input: 0

% Time Response Results:
% Rise Time :4tau = (4M)/B; where tau = M/B
```

Comparison Analysis:(Speed, Accuracy and stability):

1) when a Proportionality controller is introduced, only the amplitude

```
%is getting incremented and all other parameters like rise time, settling
%time remain same as first order without controller.
% 2) when an integrator controller is introduced, a pole gets added at the
%origin and makes the system marginally stable.
% 3) when a differentiator controller is introduced, a zero gets added to
%the origin making any unstable system also stable.
% 4) PID controllers control the whole system making them unstable to
%stable, more stable, add poles, add zeros.
```

1(c) First Order Equation

Plant Description

The Mass-damper first order system is taken as Plant. Equation: $f = Bv + M v'$ f = force; B = coefficient of friction; M = mass ; v = velocity. Values: $B1= 0.4$, $M1=1000$; $B2= 0.5$, $M2= 500$; $B3= 1.7$, $M3= 340$;

Code

```
%Negative Feedback using gain input
clc;
B1= 0.5;
M1= 5;
P = 2;
sys = tf([P],[M1,B1+1])
figure(1);
subplot(2,2,1);
impz(sys);
title('Impulse Input for k');
subplot(2,2,2);
step(sys);
title('Step Input for k');
subplot(2,2,3);
[z,p,k]= tf2zp([P],[M1,B1+1])
pzmap(sys)
subplot(2,2,4)
bode(sys)
margin(sys)
[Gm,Pm,wcg,wcp] = margin(sys)
hold on;
S = stepinfo(sys)

B2= 0.5;
M2= 5;
P2 = 2;
sys = tf([P2],[M2,B2+1,0])
figure(2)
subplot(2,2,1);
impz(sys);
```

```
title('Impulse Input for Integrator controller');
subplot(2,2,2);
step(sys);
title('Step Input for Integrator controller ');
subplot(2,2,3);
[z,p,k]= tf2zp([P2],[M2,B2+1,0])
pzmap(sys)
subplot(2,2,4)
bode(sys)
margin(sys)
[Gm,Pm,wcg,wcp] = margin(sys)
hold on;
S = stepinfo(sys)
```

```
%Positive Feedback using integral input
```

```
B3= 0.8;
M3= 5;
sys = tf([1],[M3,B3-1,0])
figure(3);
subplot(2,2,1);
impz(sys);
title('Step Input for Positive feedback');
subplot(2,2,2);
step(sys);
title('Step Input for Positive feedback');
subplot(2,2,3);
[z,p,k]= tf2zp([1],[M3,B3-1,0])
pzmap(sys)
subplot(2,2,4)
bode(sys)
margin(sys)
[Gm,Pm,wcg,wcp] = margin(sys)
hold on;
S = stepinfo(sys)
```

```
%Positive Feedback using differentiator input
```

```
B4= 0.8;
M4= 5;
sys = tf([1,0],[M4,B4-1])
figure(4)
subplot(2,2,1);
impz(sys);
title('Step Input for Positive feedback');
subplot(2,2,2);
step(sys);
title('Step Input for Positive feedback');
subplot(2,2,3);
[z,p,k]= tf2zp([1,0],[M4,B4-1])
pzmap(sys)
subplot(2,2,4)
bode(sys)
```



```
margin(sys)
[Gm,Pm,wcg,wcp] = margin(sys)
hold on;
s = stepinfo(sys)
```

```
sys =
```

```
      2
-----
5 s + 1.5
```

```
Continuous-time transfer function.
```

```
z =
```

```
0x1 empty double column vector
```

```
p =
```

```
-0.3000
```

```
k =
```

```
0.4000
```

```
Gm =
```

```
Inf
```

```
Pm =
```

```
138.5925
```

```
wcg =
```

```
NaN
```

```
wcp =
```

```
0.2646
```

```
s =
```

struct with fields:

```
RiseTime: 7.3234
SettlingTime: 13.0402
SettlingMin: 1.2060
SettlingMax: 1.3333
Overshoot: 0
Undershoot: 0
Peak: 1.3333
PeakTime: 35.1528
```

sys =

```
      2
-----
5 s^2 + 1.5 s
```

Continuous-time transfer function.

z =

0x1 empty double column vector

p =

```
      0
-0.3000
```

k =

```
0.4000
```

Gm =

```
Inf
```

Pm =

```
26.6470
```

wcg =

```
Inf
```

wcp =

0.5979

S =

struct with fields:

RiseTime: NaN
SettlingTime: NaN
SettlingMin: NaN
SettlingMax: NaN
Overshoot: NaN
Undershoot: NaN
Peak: Inf
PeakTime: Inf

sys =

1

5 s^2 - 0.2 s

Continuous-time transfer function.

z =

0x1 empty double column vector

p =

0
0.0400

k =

0.2000

warning: The closed-loop system is unstable.

Gm =

Inf

Pm =

-5.1214

wcg =

Inf

wcp =

0.4463

S =

struct with fields:

RiseTime: NaN
SettlingTime: NaN
SettlingMin: NaN
SettlingMax: NaN
Overshoot: NaN
Undershoot: NaN
Peak: Inf
PeakTime: Inf

sys =

s

5 s - 0.2

Continuous-time transfer function.

z =

0

p =

0.0400

k =

0.2000

warning: The closed-loop system is unstable.

Gm =

Inf

Pm =

Inf

wcg =

NaN

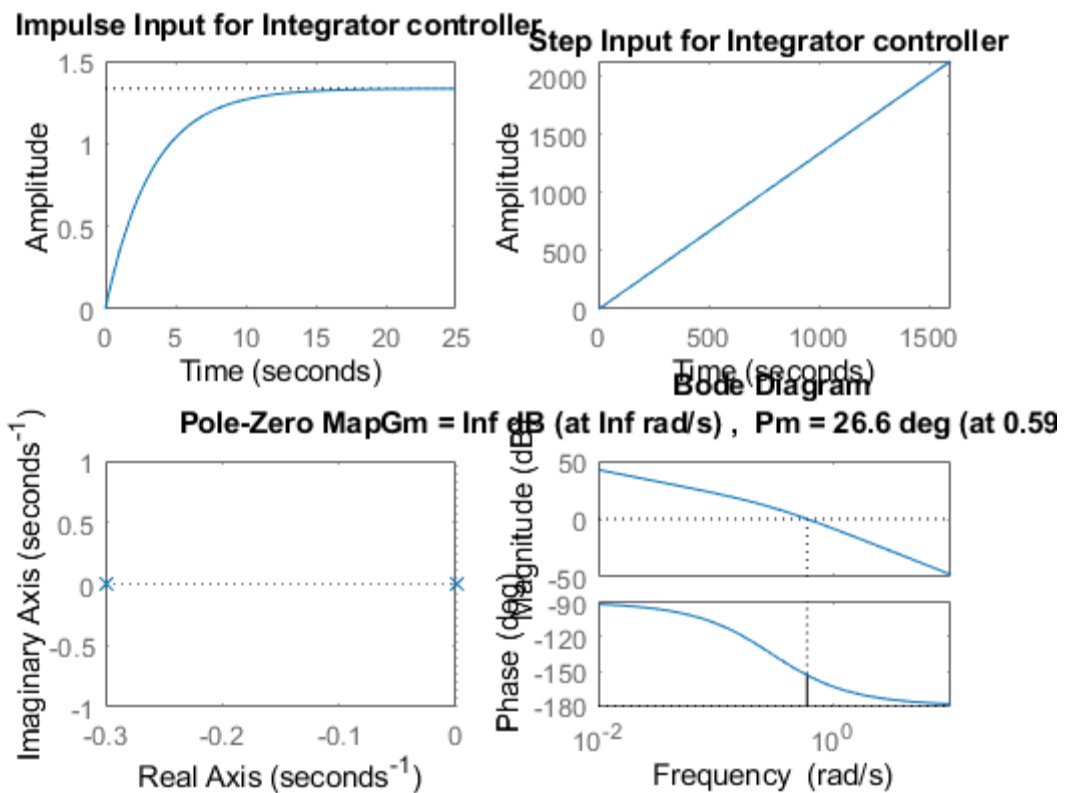
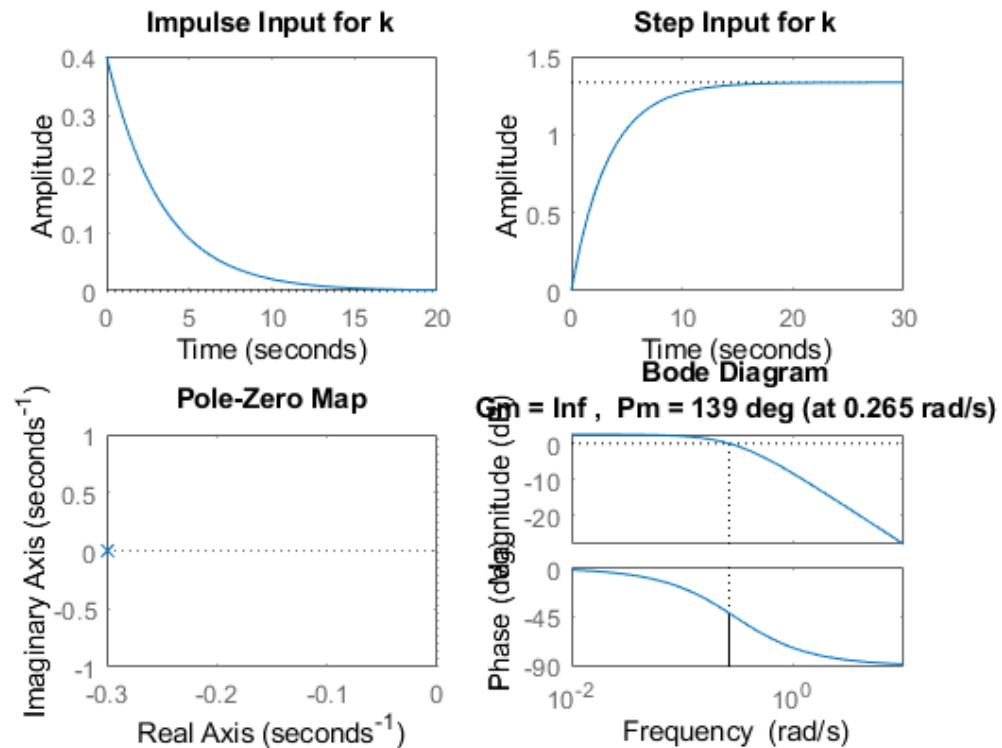
wcp =

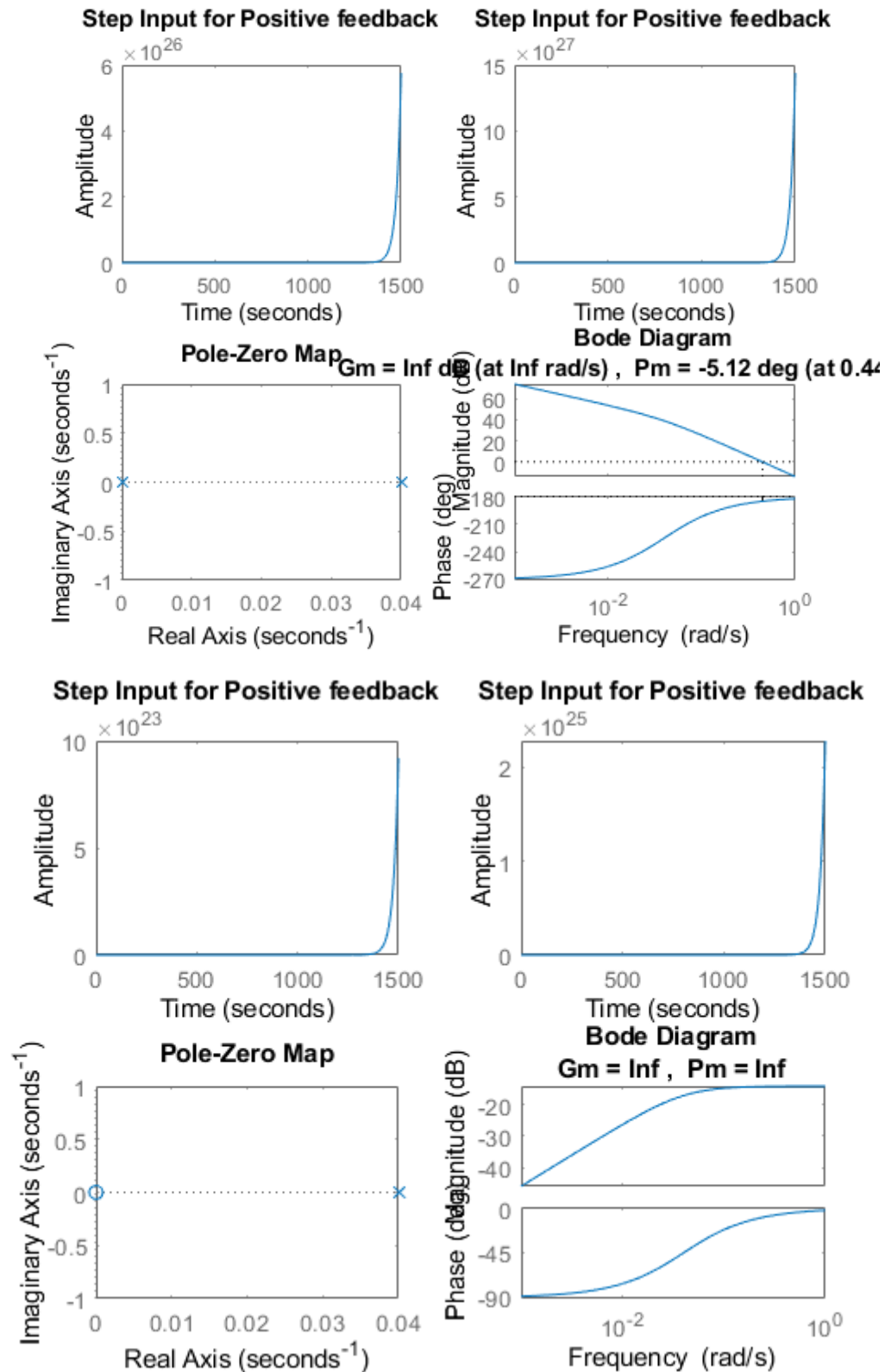
NaN

S =

struct with fields:

RiseTime: NaN
SettlingTime: NaN
SettlingMin: NaN
SettlingMax: NaN
Overshoot: NaN
Undershoot: NaN
Peak: Inf
PeakTime: Inf





Math Analysis

Independent: Time(t) Dependent: Velocity(v) and Force(f) Constant: Mass(M) and Frictional Coefficient(B)

```
% Roots: (-B)/M

% IVT:
% 1. For step input: 0
% 2. For impulse input: 1/M

% FVT:
% 1. For step input: 1/B
% 2. For impulse input: 0

% Time Response Results:
% Rise Time :4tau = (4M)/B; where tau = M/B
```

Comparison Analysis:(Speed, Accuracy and stability):

1) When a P controller is introduced in a negative feedback system, the

```
%rise time and settling time decrease making the system more stable and
%more faster.
% 2) The P controller increases the amplitude of the entire system as well.
% 3) The gain margin is infinity and phase margin is 139 deg indicating
%that the loop never goes below 180 degree. The loop gain tf is a stable
%low pass of first order.
% 4) For positive feedback with controllers, the system becomes unstable.
```

2(a) Second Order MSD Equation

Plant Description

The Mass-damper Spring Second order system is taken as Plant. It is used in as suspension. Equation: $Mx''(t) + Bx'(t) + Kx(t) = Kf(t)$. f = force; B= coefficient of friction; M = mass ; v= velocity; k=spring

```
%constant.
% Values: K1= 0.9 B1= 0.4 M1=1000 wn=0.03 ; K2= 1 B2= 0.5 M2= 500 wn=0.44;
%K3= 3 B3= 1.7 M3= 340 wn=0.09;
```

Code

```
clc;
B1= ([0.1 0.5 1.7]);
M1=([1000 5 340]);
K1 = ([0.9 1 3]);
for i=1:3
    sys = tf([K1(i)/M1(i)], [1, B1(i)/M1(i), K1(i)/M1(i)])
```



```

figure(i);
subplot(2,1,1);
impz(sys);
title('Impulse Input');
subplot(2,1,2);
step(sys);
title('Step Input');
[z,p,k]= tf2zp([K1(i)/M1(i)], [1,B1(i)/M1(i),K1(i)/M1(i)])
figure(4);
zplane(z,p);
xlim([-5*1e5 3*1e5]);
ylim([-5*1e5 3*1e5]);
hold on;
s = stepinfo(sys)
end

```

sys =

```

      0.0009
-----
s^2 + 0.0001 s + 0.0009

```

Continuous-time transfer function.

z =

0x1 empty double column vector

p =

```

-0.0001 + 0.0300i
-0.0001 - 0.0300i

```

k =

9.0000e-04

s =

struct with fields:

```

    RiseTime: 34.7791
  SettlingTime: 7.8226e+04
    SettlingMin: 0.0104
    SettlingMax: 1.9948
    Overshoot: 99.4778

```

```
Undershoot: 0
Peak: 1.9948
PeakTime: 104.7198
```

```
sys =
```

```
0.2
-----
s^2 + 0.1 s + 0.2
```

```
Continuous-time transfer function.
```

```
z =
```

```
0x1 empty double column vector
```

```
p =
```

```
-0.0500 + 0.4444i
-0.0500 - 0.4444i
```

```
k =
```

```
0.2000
```

```
s =
```

```
struct with fields:
```

```
RiseTime: 2.5448
SettlingTime: 78.1524
SettlingMin: 0.5072
SettlingMax: 1.7021
Overshoot: 70.2118
Undershoot: 0
Peak: 1.7021
PeakTime: 7.0248
```

```
sys =
```

```
0.008824
-----
s^2 + 0.005 s + 0.008824
```

```
Continuous-time transfer function.
```

z =

0x1 empty double column vector

p =

-0.0025 + 0.0939i

-0.0025 - 0.0939i

k =

0.0088

s =

struct with fields:

RiseTime: 11.3230

SettlingTime: 1.5426e+03

SettlingMin: 0.1540

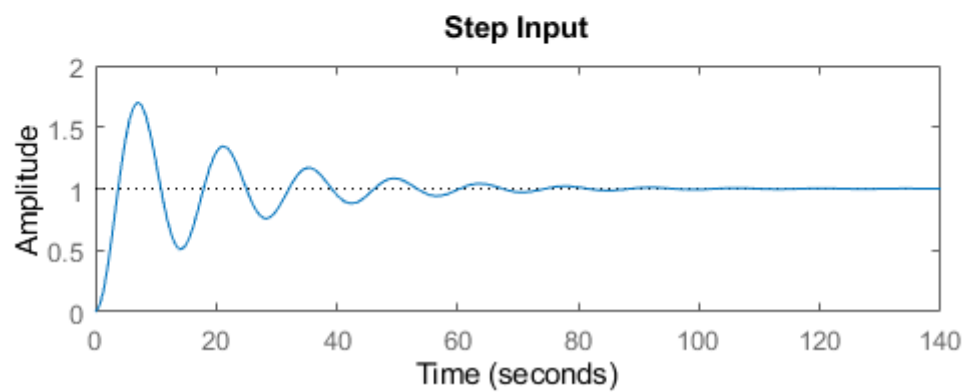
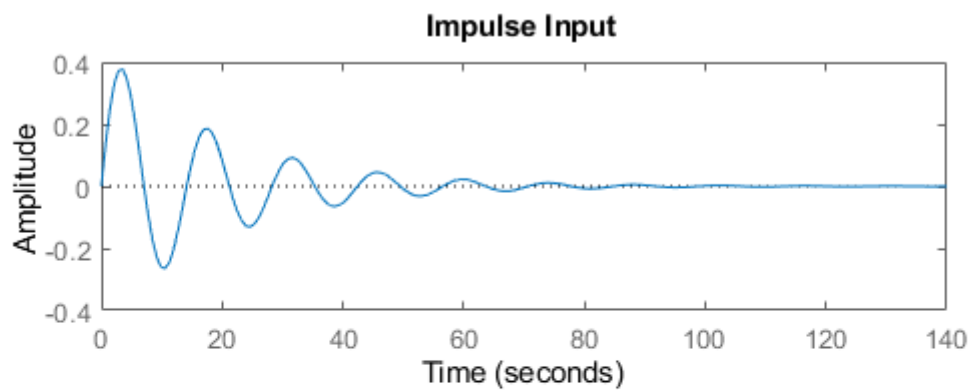
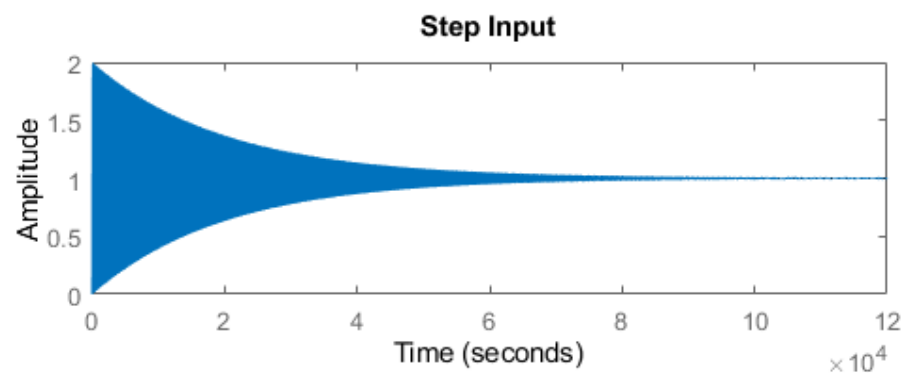
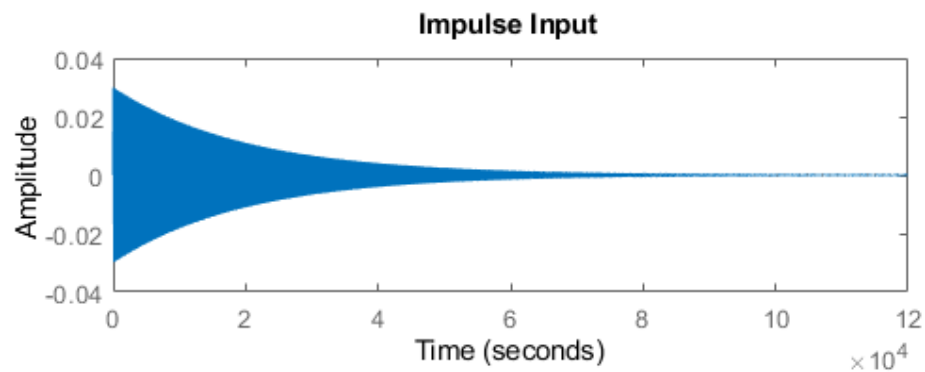
SettlingMax: 1.9198

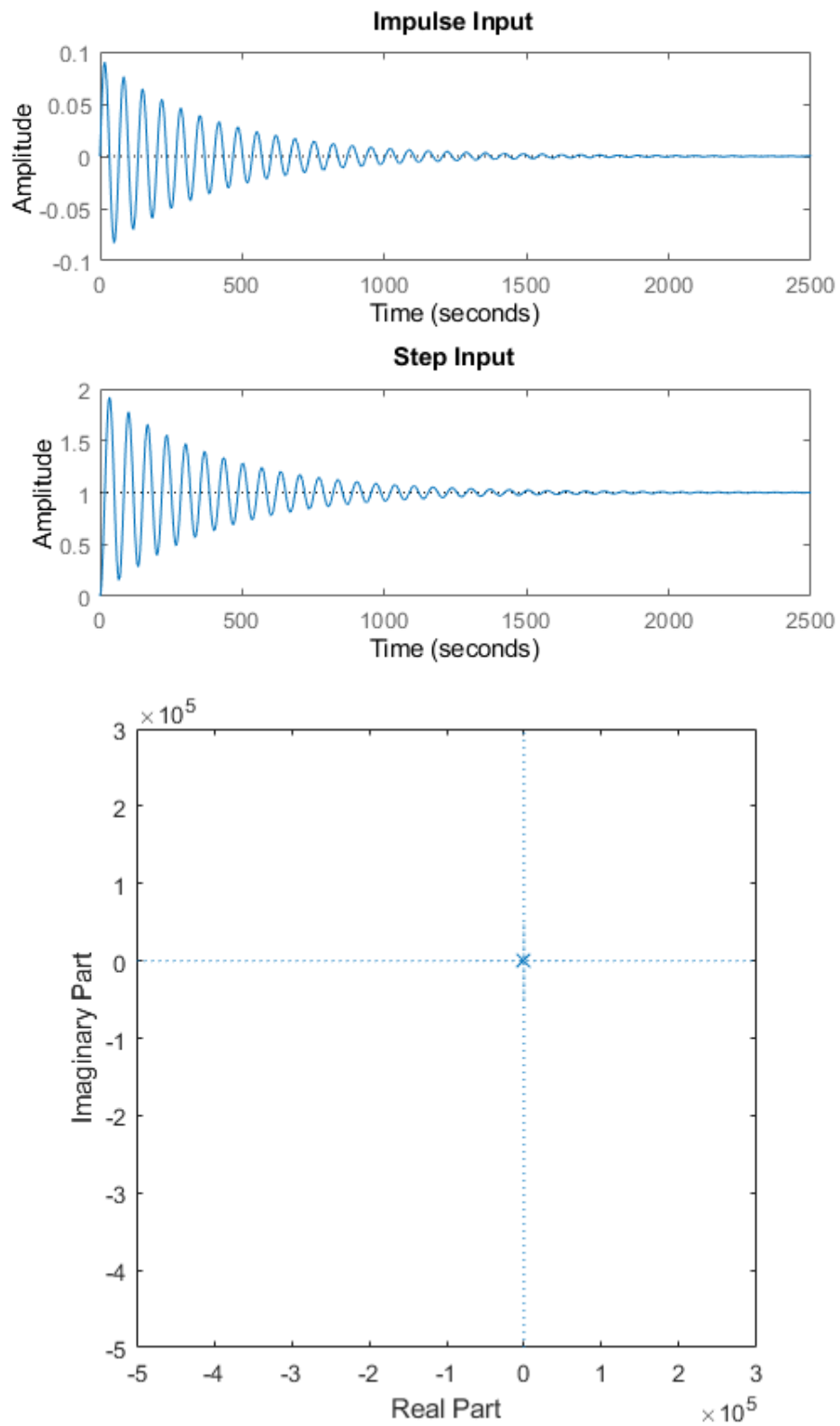
Overshoot: 91.9760

Undershoot: 0

Peak: 1.9198

PeakTime: 33.4448





Math Analysis:

Independent: Time(t) Dependent: Velocity(v) and Force(f) Constant: Mass(M), Frictional Coefficient(B), Spring constant(K) Roots: $\frac{(-B/M) \pm \sqrt{(B/M)^2 - 4K/M}}{2}$

```
% IVT:
% 1. For step input: 0
% 2. For impulse input: 0

% FVT:
% 1. For step input: 1
% 2. For impulse input: K/M

% Time Response Results:
%      RiseTime: 34.7791
%      SettlingTime: 7.8226e+04
%      SettlingMin: 0.0104
%      SettlingMax: 1.9948
%      Overshoot: 99.4778
%      Undershoot: 0
%      Peak: 1.9948
%      PeakTime: 104.7198

%K2= 1 B2= 0.5 M2= 500
%      RiseTime: 2.5448
%      SettlingTime: 78.1524
%      SettlingMin: 0.5072
%      SettlingMax: 1.7021
%      Overshoot: 70.2118
%      Undershoot: 0
%      Peak: 1.7021
%      PeakTime: 7.0248

%K3= 3 B3= 1.7 M3= 340
%      RiseTime: 11.3230
%      SettlingTime: 1.5426e+03
%      SettlingMin: 0.1540
%      SettlingMax: 1.9198
%      Overshoot: 91.9760
%      Undershoot: 0
%      Peak: 1.9198
%      PeakTime: 33.4448
```

Comparison Analysis:(Speed, Accuracy and stability):

1) For sys 1 poles are on the LHS and they are complex conjugates which

```
%makes the system stable.
% 2) For sys 2 poles are on LHS and they are complex conjugates which makes
%the system stable.
% 3) For sys 3 poles are on LHS and they are complex conjugates which makes
```

```
%the system stable.
% 4) sys 2 has the least rising time and settling time making the system
%fastest and most stable.
```

2(b) Second Order MSD Equation

Plant Description

The Mass-damper Spring Second order system is taken as Plant. It is used in as suspension.

```
% Equation:  $Mx''(t) + Bx'(t) + Kx(t) = Kf(t)$ .
% f = force; B= coefficient of friction; M = mass ; v= velocity; k=spring
%constant.
% Values: K1= 0.9 B1= 0.4 M1=1000 wn=0.03 ; K2= 1 B2= 0.5 M2= 500 wn=0.44;
%K3= 3 B3= 1.7 M3= 340 wn=0.09;
```

Code

```
clc;
B1= 0.5
M1= 5;
K1 =1;
P=5;
sys = tf([P*K1/M1],[1,B1/M1,K1/M1])
subplot(4,3,1);
impz(sys);
title('Impulse Input for k');
subplot(4,3,2);
step(sys);
title('Step Input for k');
subplot(4,3,3);
[z,p,k]= tf2zp([P*K1/M1],[1,B1/M1,K1/M1])
pzmap(sys)
subplot(4,3,10);
bode(sys)
hold on;
S = stepinfo(sys)

sys = tf([P*K1/M1],[1,B1/M1,K1/M1,0])
subplot(4,3,4);
impz(sys);
title('Impulse Input for 1/s');
subplot(4,3,5);
step(sys);
title('Step Input for 1/s');
subplot(4,3,6);
[z,p,k]= tf2zp([P*K1/M1],[1,B1/M1,K1/M1,0])
pzmap(sys)
```

```

subplot(4,3,11);
bode(sys)
hold on;
S = stepinfo(sys)

sys = tf([P*K1/M1,0],[1,B1/M1,K1/M1])
subplot(4,3,7);
impulse(sys);
title('Impulse Input for s');
subplot(4,3,8);
step(sys);
title('Step Input for s');
subplot(4,3,9);
[z,p,k]= tf2zp([P*K1/M1,0],[1,B1/M1,K1/M1])
pzmap(sys)
subplot(4,3,12);
bode(sys)
hold on;
S = stepinfo(sys)

```

B1 =

0.5000

sys =

$$\frac{1}{s^2 + 0.1s + 0.2}$$

Continuous-time transfer function.

z =

0x1 empty double column vector

p =

-0.0500 + 0.4444i
-0.0500 - 0.4444i

k =

1

S =

struct with fields:

```
RiseTime: 2.5448
SettlingTime: 78.1524
SettlingMin: 2.5361
SettlingMax: 8.5106
Overshoot: 70.2118
Undershoot: 0
Peak: 8.5106
PeakTime: 7.0248
```

sys =

```
      1
-----
s^3 + 0.1 s^2 + 0.2 s
```

Continuous-time transfer function.

z =

0x1 empty double column vector

p =

```
0.0000 + 0.0000i
-0.0500 + 0.4444i
-0.0500 - 0.4444i
```

k =

```
1
```

S =

struct with fields:

```
RiseTime: NaN
SettlingTime: NaN
SettlingMin: NaN
SettlingMax: NaN
Overshoot: NaN
Undershoot: NaN
Peak: Inf
```

```
PeakTime: Inf
```

```
sys =
```

```
      s
-----
s^2 + 0.1 s + 0.2
```

```
Continuous-time transfer function.
```

```
z =
```

```
0
```

```
p =
```

```
-0.0500 + 0.4444i
-0.0500 - 0.4444i
```

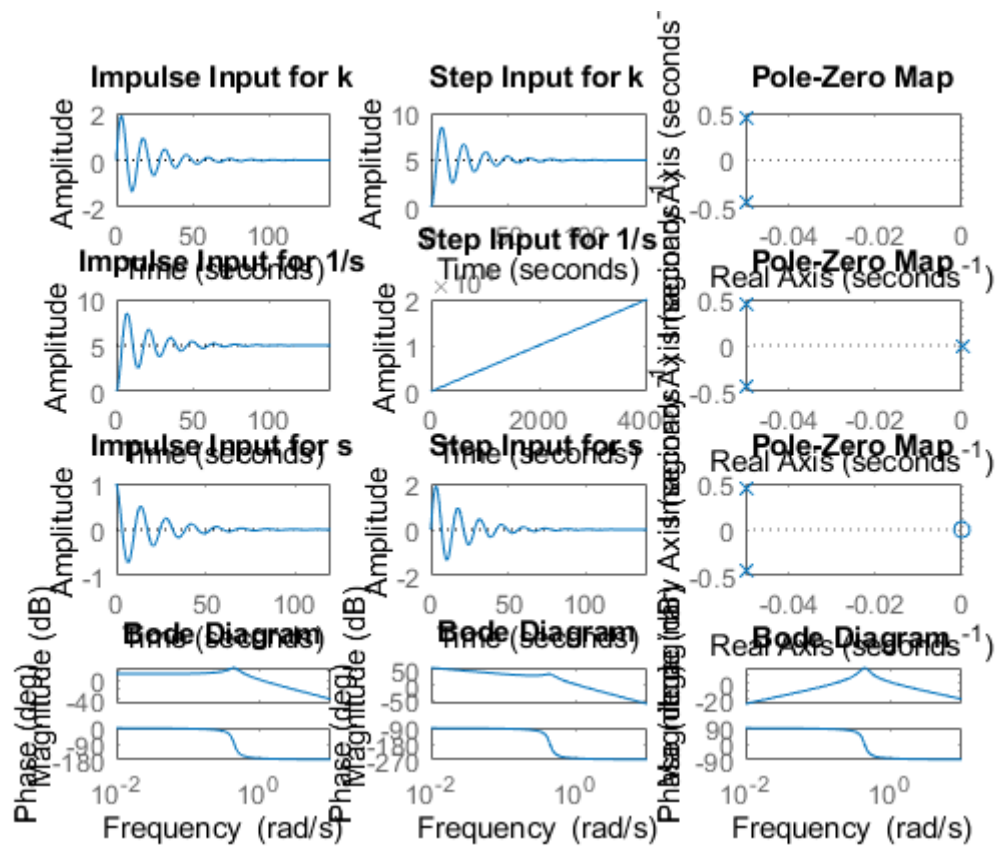
```
k =
```

```
1
```

```
s =
```

```
struct with fields:
```

```
    RiseTime: 0
SettlingTime: 81.5509
SettlingMin: -1.3280
SettlingMax: 1.8877
    Overshoot: Inf
    Undershoot: Inf
         Peak: 1.8877
    PeakTime: 3.5124
```



Math Analysis:

Independent: Time(t) Dependent: Velocity(v) and Force(f) Constant: Mass(M), Frictional Coefficient(B), Spring constant(K)

```
% Roots: ((-B/M)+-sqrt(sq(B/M)-4K/M))/2

% IVT:
% 1. For step input: 0
% 2. For impulse input: 0

% FVT:
% 1. For step input: 1
% 2. For impulse input: K/M

% Time Response Results:
% K1= 0.9 B1= 0.4 M1=1000
% RiseTime: 2.5448
% SettlingTime: 78.1524
% SettlingMin: 2.5361
% SettlingMax: 8.5106
% Overshoot: 70.2118
% Undershoot: 0
% Peak: 8.5106
```

```
%      PeakTime: 7.0248
```

```
%K2= 1 B2= 0.5 M2= 500
```

```
%      RiseTime: NaN
```

```
%      SettlingTime: NaN
```

```
%      SettlingMin: NaN
```

```
%      SettlingMax: NaN
```

```
%      Overshoot: NaN
```

```
%      Undershoot: NaN
```

```
%      Peak: Inf
```

```
%      PeakTime: Inf
```

```
%K3= 3 B3= 1.7 M3= 340
```

```
%      RiseTime: 0
```

```
%      SettlingTime: 81.5509
```

```
%      SettlingMin: -1.3280
```

```
%      SettlingMax: 1.8877
```

```
%      Overshoot: Inf
```

```
%      Undershoot: Inf
```

```
%      Peak: 1.8877
```

```
%      PeakTime: 3.5124
```

Comparison Analysis:(Speed, Accuracy and stability):

1) with proportionality controller, only the amplitude changes and all

```
%other stats are same as in 2nd order system without controller.
```

```
% 2) On adding an integrator controller, a pole is getting added at the  
%origin and makes the system marginally stable.
```

```
% 3) On adding a differentiator controller, a zero is added to the origin  
%making an unstable system stable.
```

```
% 4) On adding a differentiator controller, the overshoot increases and  
%also the response time increase.
```

2(c) Second Order MSD Equation

Plant Description

The Mass-damper Spring Second order system is taken as Plant. It is used in as suspension.

```
% Equation:  $Mx''(t) + Bx'(t) + Kx(t) = Kf(t)$ .
```

```
% f = force; B= coefficient of friction; M = mass ; v= velocity; k=spring  
%constant.
```

```
% Values: K1= 0.9 B1= 0.4 M1=1000 wn=0.03 ; K2= 1 B2= 0.5 M2= 500 wn=0.44;
```

```
%K3= 3 B3= 1.7 M3= 340 wn=0.09; B4= 9 M4= 5 K4=1;
```

Code

```
%For negative feedback
clc;
B1= 0.5
M1= 5;
K1 =1;
P=5;

sys = tf([P*K1],[M1,B1,2*K1])
subplot(4,4,1);
impulse(sys);
title('Impulse Input for k');
subplot(4,4,2);
step(sys);
title('Step Input for k');
subplot(4,4,3);
[z,p,k]= tf2zp([P*K1],[M1,B1,2*K1])
pzmap(sys)
subplot(4,4,4)
bode(sys)
margin(sys)
[Gm,Pm,wcg,wcp] = margin(sys)
hold on;
S = stepinfo(sys)

B2= -9
M2= 5;
K2=1;
P2=5;

sys = tf([P2*K2],[M2,B2,2*K2])
subplot(4,4,5);
impulse(sys);
title('Impulse Input for k- Unstable');
subplot(4,4,6);
step(sys);
title('Step Input for k- Unstable');
subplot(4,4,7);
[z,p,k]= tf2zp([P2*K2],[M2,B2,2*K2])
pzmap(sys)
subplot(4,4,8)
bode(sys)
margin(sys)
[Gm,Pm,wcg,wcp] = margin(sys)
hold on;
S = stepinfo(sys)

% For Positive feedback using I & D
```

```

B3= 9
M3= 5;
K3=1;
sys = tf([K3],[M3,B3,0,0])
subplot(4,4,9);
impz(sys);
title('Impulse Input for Positive feedback 1/s ');
subplot(4,4,10);
step(sys);
title('Step Input for Positive feedback 1/s');
subplot(4,4,11);
[z,p,k]= tf2zp([K3],[M3,B3,0,0])
pzmap(sys)
subplot(4,4,12)
bode(sys)
margin(sys)
[Gm,Pm,wcg,wcp] = margin(sys)
hold on;
s = stepinfo(sys)

```

```

B4= 9
M4= 5;
K4=1;
sys = tf([K4,0],[M4,B4,0])
subplot(4,4,13);
impz(sys);
title('Impulse Input for Positive feedback s ');
subplot(4,4,14);
step(sys);
title('Step Input for Positive feedback s');
subplot(4,4,15);
[z,p,k]= tf2zp([K4,0],[M4,B4,0])
pzmap(sys)
subplot(4,4,16)
bode(sys)
margin(sys)
[Gm,Pm,wcg,wcp] = margin(sys)
hold on;
s = stepinfo(sys)

```

B1 =

0.5000

sys =

5

```
5 s^2 + 0.5 s + 2
```

Continuous-time transfer function.

z =

```
0x1 empty double column vector
```

p =

```
-0.0500 + 0.6305i  
-0.0500 - 0.6305i
```

k =

```
1
```

Gm =

```
Inf
```

Pm =

```
6.7782
```

wcg =

```
Inf
```

wcp =

```
1.1803
```

s =

```
struct with fields:
```

```
    RiseTime: 1.7526  
SettlingTime: 75.6433  
SettlingMin: 0.9814  
SettlingMax: 4.4486  
    Overshoot: 77.9429  
Undershoot: 0
```

Peak: 4.4486
PeakTime: 4.9673

B2 =

-9

sys =

$$\frac{5}{5s^2 - 9s + 2}$$

Continuous-time transfer function.

z =

0x1 empty double column vector

p =

1.5403
0.2597

k =

1

warning: The closed-loop system is unstable.

Gm =

Inf

Pm =

-95.4008

wcg =

Inf

wcp =

0.5531

S =

struct with fields:

RiseTime: NaN
SettlingTime: NaN
SettlingMin: NaN
SettlingMax: NaN
Overshoot: NaN
Undershoot: NaN
Peak: Inf
PeakTime: Inf

B3 =

9

sys =

1

5 s^3 + 9 s^2

Continuous-time transfer function.

z =

0x1 empty double column vector

p =

0
0
-1.8000

k =

0.2000

warning: The closed-loop system is unstable.

Gm =

0

Pm =

-10.4065

wcg =

0

wcp =

0.3306

S =

struct with fields:

```
    RiseTime: NaN
  SettlingTime: NaN
  SettlingMin: NaN
  SettlingMax: NaN
    Overshoot: NaN
  Undershoot: NaN
        Peak: Inf
    PeakTime: Inf
```

B4 =

9

sys =

```
    s
-----
5 s^2 + 9 s
```

Continuous-time transfer function.

z =

0

p =

0
-1.8000

k =

0.2000

warning: The closed-loop system is unstable.

Gm =

Inf

Pm =

Inf

wcg =

NaN

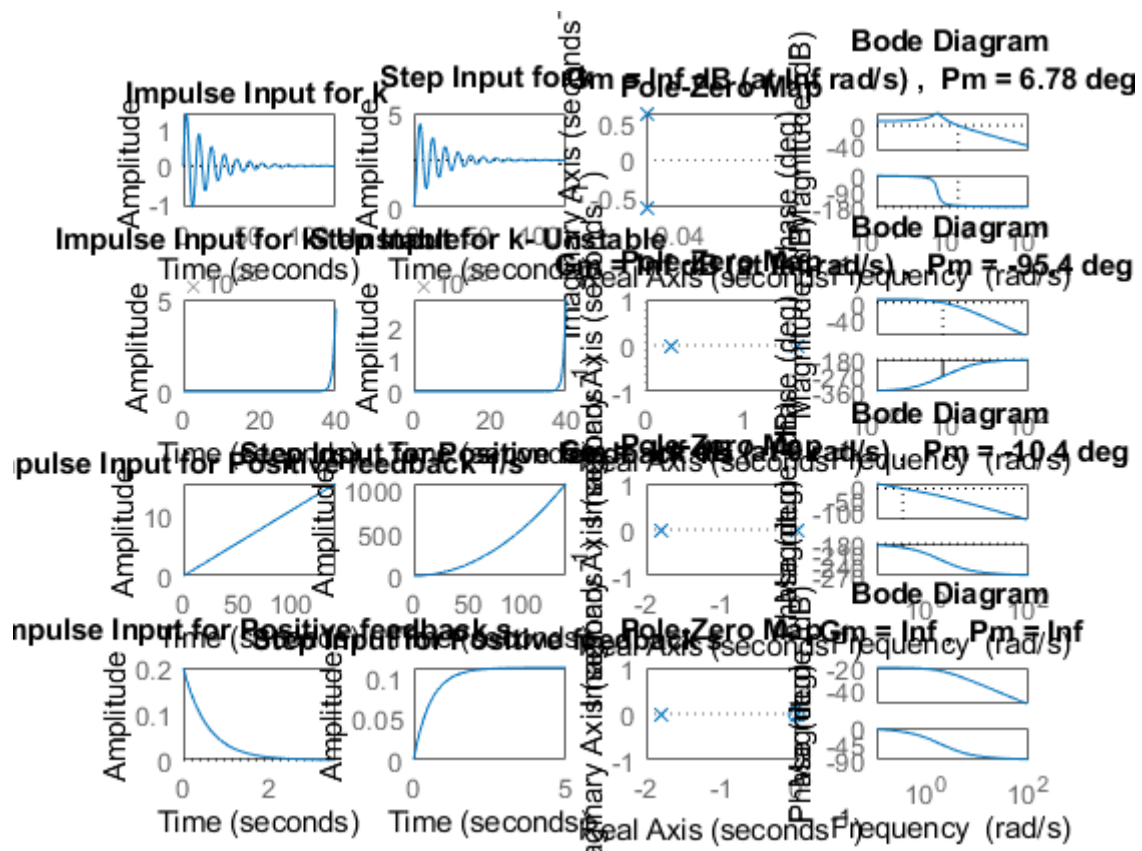
wcp =

NaN

S =

struct with fields:

RiseTime: 1.2206
SettlingTime: 2.1734
SettlingMin: 0.1005
SettlingMax: 0.1111
Overshoot: 0
Undershoot: 0
Peak: 0.1111
PeakTime: 5.8588



Math Analysis:

Independent: Time(t) Dependent: Velocity(v) and Force(f) Constant: Mass(M), Frictional Coefficient(B), Spring constant(K)

```
% Roots: ((-B/M)+-sqrt(sq(B/M)-4K/M))/2

% IVT:
% 1. For step input: 0
% 2. For impulse input: 0

% FVT:
% 1. For step input: 1
% 2. For impulse input: K/M

% Time Response Results:
% K1= 0.9 B1= 0.4 M1=1000
% RiseTime: 1.7526
% SettlingTime: 75.6433
% SettlingMin: 0.9814
% SettlingMax: 4.4486
% Overshoot: 77.9429
% Undershoot: 0
% Peak: 4.4486
```

```
%      PeakTime: 4.9673
```

```
%K2= 1 B2= 0.5 M2= 500
```

```
%      RiseTime: NaN
```

```
%      SettlingTime: NaN
```

```
%      SettlingMin: NaN
```

```
%      SettlingMax: NaN
```

```
%      Overshoot: NaN
```

```
%      Undershoot: NaN
```

```
%      Peak: Inf
```

```
%      PeakTime: Inf
```

```
%K3= 3 B3= 1.7 M3= 340
```

```
%      RiseTime: NaN
```

```
%      SettlingTime: NaN
```

```
%      SettlingMin: NaN
```

```
%      SettlingMax: NaN
```

```
%      Overshoot: NaN
```

```
%      Undershoot: NaN
```

```
%      Peak: Inf
```

```
%      PeakTime: Inf
```

```
%K4= 1 B4= 9 M4= 5;
```

```
%      RiseTime: 1.2206
```

```
%      SettlingTime: 2.1734
```

```
%      SettlingMin: 0.1005
```

```
%      SettlingMax: 0.1111
```

```
%      Overshoot: 0
```

```
%      Undershoot: 0
```

```
%      Peak: 0.1111
```

```
%      PeakTime: 5.8588
```

Comparison Analysis:(Speed, Accuracy and stability):

%-ve feedback

% 1) On adding a -ve feedback, the stability of the system reaches at a faster speed.

% 2) The gain margin is infinity and the phase margin is +ve value making the system stable.

% 3) When the gain margin is infinity and the phase margin is -ve value the system becomes unstable.

%+ve feedback

% 1) When the gain margin is 0 and the phase margin is -ve value the system becomes unstable.

% 2) When both gain margin and phase margin are infinity, the errors get accumulated and makes the system unstable.

2(d) Movement of Poles.

Description: Movement of poles is shown along the real and imaginary axis

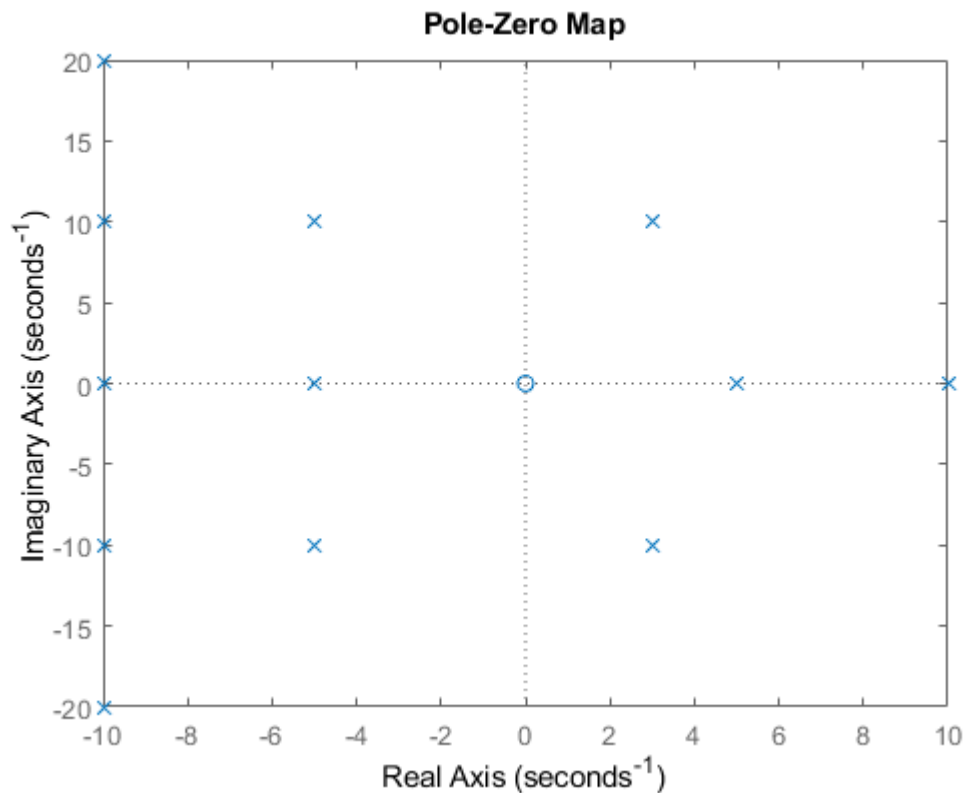
```
clc;
poles = [-10+20i -10-20i -5+10i -5-10i -10+10i -10-10i 3+10i 3-10i -5+0i +5+0i -10+0i +10-0i ];
zeros = [0 0];
gain = 0.9;
s=zpk(zeros,poles,gain);
pzplot(s)
[wn,zeta] = damp(s)
```

wn =

```
5.0000
5.0000
10.0000
10.0000
10.4403
10.4403
11.1803
11.1803
14.1421
14.1421
22.3607
22.3607
```

zeta =

```
1.0000
-1.0000
1.0000
-1.0000
-0.2873
-0.2873
0.4472
0.4472
0.7071
0.7071
0.4472
0.4472
```



Analysis

If we move along the roots along the ω_n , the frequency of the system increases. Overshoot remains same. If we move along the $j\omega$ axis, overshoot of system increases. frequency of system increases. If we move along $\zeta \omega_n$ axis or σ , Overshoot increases, frequency decreases on right side movement. Overshoot decreases, frequency increases on left side movement.

2(e) Roots of the Standard Equation

Code

```
clc;
zeta=1;
TF=tf([1],[1,(2*zeta),1])
sys = tf([1],[1,(2*zeta),1])
figure
subplot(2,3,1)
s = stepinfo(sys)
[z,p,k]= tf2zp([1],[1,(2*zeta),1])
zplane(z,p)

zeta=0.7 ;
```

```

TF=tf([1],[1,(2*zeta),1])
sys = tf([1],[1,(2*zeta),1])
subplot(2,3,2)
S = stepinfo(sys)
[z,p,k]= tf2zp([1],[1,(2*zeta),1])
zplane(z,p)

zeta=2;
TF=tf([1],[1,(2*zeta),1])
sys = tf([1],[1,(2*zeta),1])
subplot(2,3,3)
S = stepinfo(sys)
[z,p,k]= tf2zp([1],[1,(2*zeta),1])
zplane(z,p)

zeta=-1.85;
TF=tf([1],[1,(2*zeta),1])
sys = tf([1],[1,(2*zeta),1])
subplot(2,3,4)
S = stepinfo(sys)
[z,p,k]= tf2zp([1],[1,(2*zeta),1])
zplane(z,p)

zeta=-0.4;
TF=tf([1],[1,(2*zeta),1])
sys = tf([1],[1,(2*zeta),1])
subplot(2,3,5)
S = stepinfo(sys)
[z,p,k]= tf2zp([1],[1,(2*zeta),1])
zplane(z,p)

zeta=-2.45;
TF=tf([1],[1,(2*zeta),1])
sys = tf([1],[1,(2*zeta),1])
subplot(2,3,6)
S = stepinfo(sys)
[z,p,k]= tf2zp([1],[1,(2*zeta),1])
zplane(z,p)

```

TF =

$$\frac{1}{s^2 + 2s + 1}$$

Continuous-time transfer function.

sys =

$$\frac{1}{s^2 + 2s + 1}$$

Continuous-time transfer function.

S =

struct with fields:

```

    RiseTime: 3.3579
    SettlingTime: 5.8339
    SettlingMin: 0.9000
    SettlingMax: 0.9994
    Overshoot: 0
    Undershoot: 0
    Peak: 0.9994
    PeakTime: 9.7900

```

z =

0x1 empty double column vector

p =

```

-1
-1

```

k =

```

1

```

TF =

$$\frac{1}{s^2 + 1.4s + 1}$$

Continuous-time transfer function.

sys =

$$\frac{1}{s^2 + 1.4s + 1}$$

Continuous-time transfer function.

S =

struct with fields:

```

    RiseTime: 2.1268
    SettlingTime: 5.9789
    SettlingMin: 0.9001
    SettlingMax: 1.0460
    Overshoot: 4.5986
    Undershoot: 0
    Peak: 1.0460
    PeakTime: 4.4078

```

z =

0x1 empty double column vector

p =

```

-0.7000 + 0.7141i
-0.7000 - 0.7141i

```

k =

1

TF =

```

    1
-----
s^2 + 4 s + 1

```

Continuous-time transfer function.

sys =

```

    1
-----
s^2 + 4 s + 1

```

Continuous-time transfer function.

S =

struct with fields:

```
RiseTime: 8.2308
SettlingTime: 14.8789
SettlingMin: 0.9017
SettlingMax: 0.9993
Overshoot: 0
Undershoot: 0
Peak: 0.9993
PeakTime: 27.3269
```

z =

0x1 empty double column vector

p =

```
-3.7321
-0.2679
```

k =

1

TF =

```
      1
-----
s^2 - 3.7 s + 1
```

Continuous-time transfer function.

sys =

```
      1
-----
s^2 - 3.7 s + 1
```

Continuous-time transfer function.

S =

```
struct with fields:
```

```

    RiseTime: NaN
SettlingTime: NaN
SettlingMin: NaN
SettlingMax: NaN
    Overshoot: NaN
    Undershoot: NaN
        Peak: Inf
    PeakTime: Inf

```

```
z =
```

```
0x1 empty double column vector
```

```
p =
```

```

3.4064
0.2936

```

```
k =
```

```
1
```

```
TF =
```

```

      1
-----
s^2 - 0.8 s + 1

```

```
Continuous-time transfer function.
```

```
sys =
```

```

      1
-----
s^2 - 0.8 s + 1

```

```
Continuous-time transfer function.
```

```
s =
```

```
struct with fields:
```

```

    RiseTime: NaN

```

```
SettlingTime: NaN
SettlingMin: NaN
SettlingMax: NaN
Overshoot: NaN
Undershoot: NaN
Peak: Inf
PeakTime: Inf
```

```
z =
```

```
0x1 empty double column vector
```

```
p =
```

```
0.4000 + 0.9165i
0.4000 - 0.9165i
```

```
k =
```

```
1
```

```
TF =
```

```
1
-----
s^2 - 4.9 s + 1
```

Continuous-time transfer function.

```
sys =
```

```
1
-----
s^2 - 4.9 s + 1
```

Continuous-time transfer function.

```
s =
```

```
struct with fields:
```

```
RiseTime: NaN
SettlingTime: NaN
SettlingMin: NaN
SettlingMax: NaN
```

Overshoot: NaN
Undershoot: NaN
Peak: Inf
PeakTime: Inf

z =

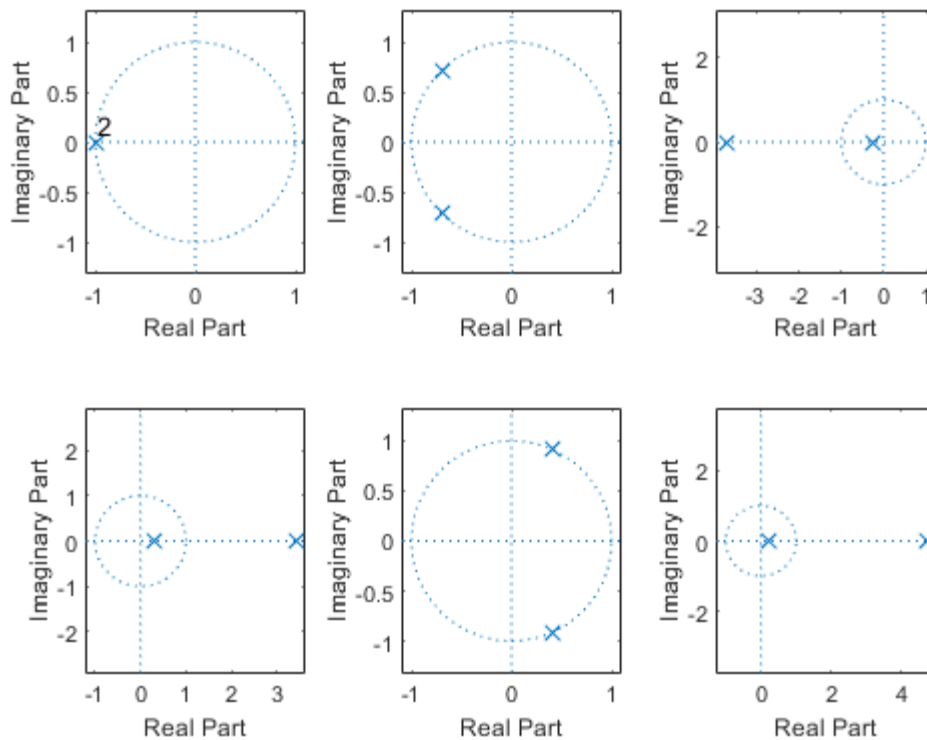
0x1 empty double column vector

p =

4.6866
0.2134

k =

1



Comparison Analysis:

1st value rise on negative x axis means: Critically-damped case & stable 2nd value rise in 2nd & 3rd quadrant means: Under-damp case & stable 3rd value rise on negative x axis means: Overdamped case & stable 4th value rise on positive x axis means: unstable 5th value rise on 1st & 4th quadrant means: unstable 6th value rise on positive x axis means: unstable

2(f) PID Analysis

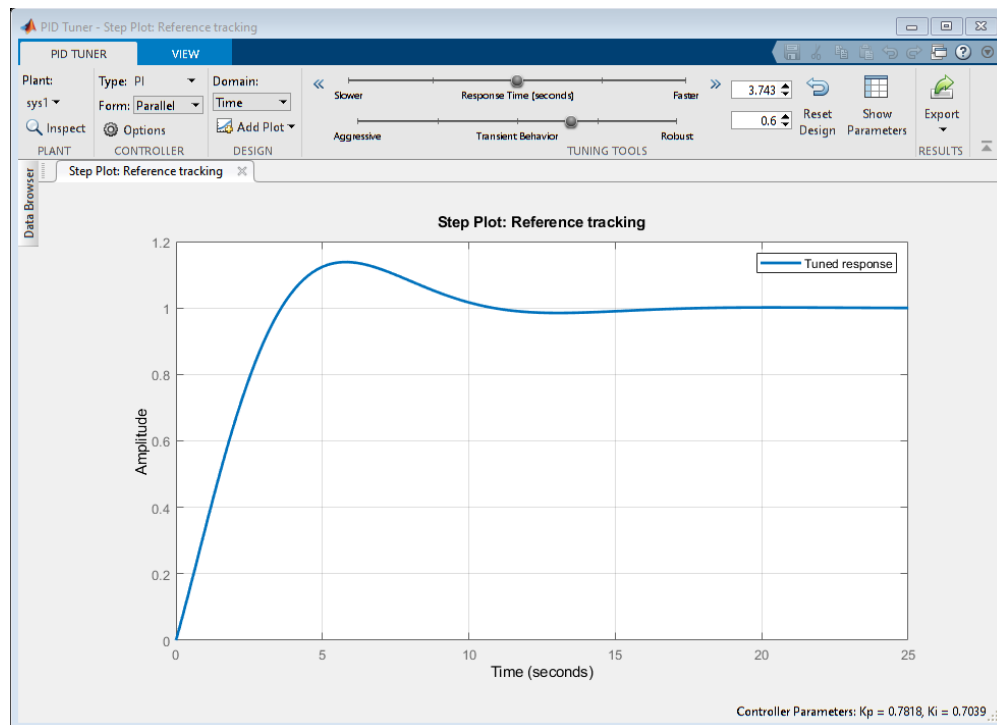
First Order System PID Analysis

```
clc;
B1= 0.5;
M1= 5;
P1 = 2;
sys1 = tf([P1],[M1,B1+1])
pidTuner(sys1)
```

```
sys1 =

      2
-----
 5 s + 1.5
```

Continuous-time transfer function.



Second Order System PID Analysis

```

B2= 0.5
M2= 5;
K2 =1;
P2=5;
sys2 = tf([P2*K2],[M2,B2,2*K2])
pidTuner(sys2)

```

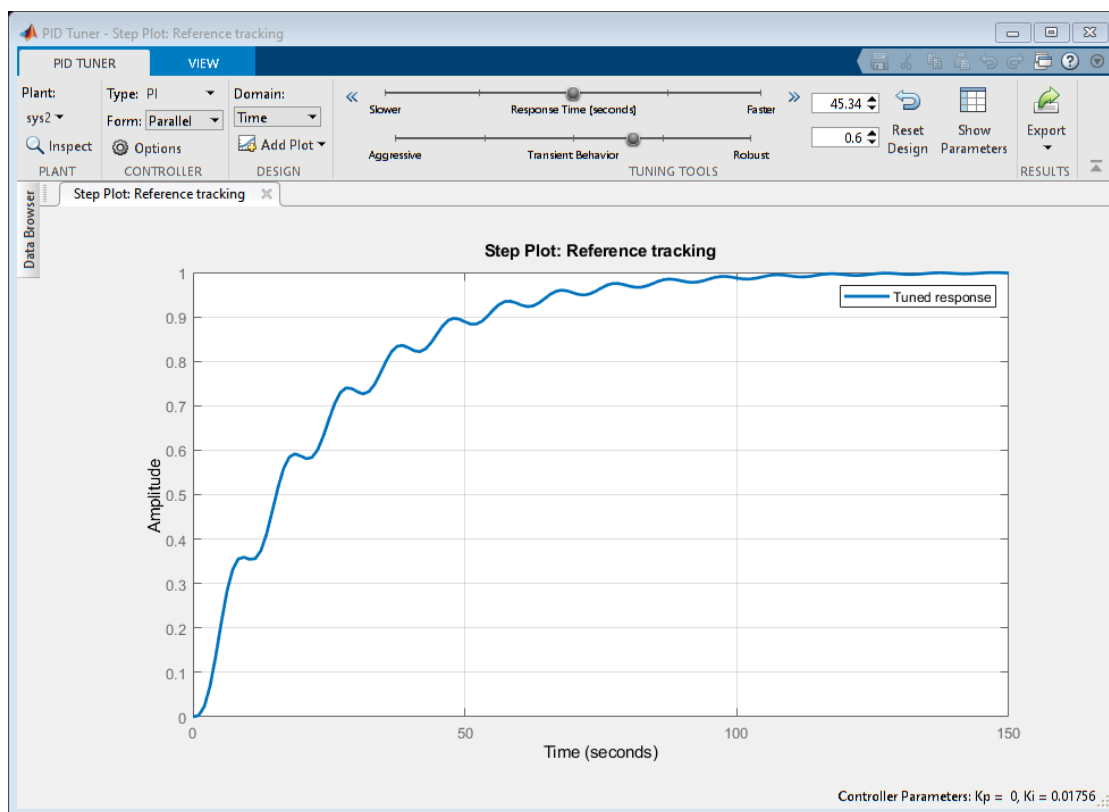
B2 =

0.5000

sys2 =

$$\frac{5}{5s^2 + 0.5s + 2}$$

Continuous-time transfer function.



Comparison Analysis:

First Order sys: PI: Ideal system: $K_p = 0.78$ (Un-Tuned) $K_i = 0.7$ $T_r = 2.7$ $T_s = 9.87$
 Overshoot= 13.8%
 Best system: $K_p = 1.25$
 (After Tuning) $K_i = 0.46$
 $T_r = 3.59$
 $T_s = 5.39$
 Overshoot= 1.33%
 PD: Ideal system: $K_p = 53.18$
 (Un-Tuned) $K_d = 0$
 $T_r = 0.102$
 $T_s = 0.181$
 Overshoot= 0
 Best system: $K_p = 53.18$
 (After Tuning) $K_d = 0$
 $T_r = 0.102$
 $T_s = 0.181$
 Overshoot= 0
 PID: Ideal system: $K_p = 1.07$
 (Un-Tuned) $K_i = 0.53$
 $K_d = 0$
 $T_r = 3.04$
 $T_s = 10.6$
 Overshoot= 6.08%
 Best system: $K_p = 1.07$
 (After Tuning) $K_i = 0.53$
 $K_d = 0$
 $T_r = 3.04$
 $T_s = 10.6$
 Overshoot= 6.08%

```
% Second Order sys:
%   PI: Ideal system: Tr= 51.1
%       (Un-Tuned)  Ts= 94.3
%                   Overshoot= 0%
%
%       Best system: Tr= 50.4
%       (After Tuning) Ts= 93.4
%                   Overshoot= 0.00235%
%
%   PD: Ideal system: Kp= 2697.9
%       (Un-Tuned)  Kd= 63.48
%                   Tr= 0.0179
%                   Ts= 0.13
%                   Overshoot= 24.3%
%
%       Best system: Kp= 27.35
%       (After Tuning) Kd= 6.251
%                   Tr= 0.175
%                   Ts= 1.35
%                   Overshoot= 24.71%
%
%   PID: Ideal system: Kp= 3.053
%       (Un-Tuned)  Ki= 0.68
%                   Kd= 2.66
```

```
%           Tr= 0.495
%           Ts= 9.3
%           Overshoot= 12.4%
%
%   Best system: Kp= 3.053
% (After Tuning) Ki= 0.68
%           Kd= 2.66
%           Tr= 0.495
%           Ts= 9.3
%           Overshoot= 12.4%
```

3(a) Second Order Exponential Decay system

Plant Description

It is a exponential decay system of a radioactive material Equation- $dM/dt = -kA(e^{-kt})$ M =mass, k =constant, A = non zero constant, t =time Values- $k=0.14$, $A=200$

Without Controller

```
clc;
k= 0.14;
A= 200;
sys = tf([-k*A],[1,k,0])
figure(1);
subplot(3,1,1);
impz(sys);
title('Impulse Input');
subplot(3,1,2);
step(sys);
title('Step Input');
[z,p,k] = tf2zp([-k*A],[1,k,0])
subplot(3,1,3);
zplane(z,p);
S = stepinfo(sys)
```

```
sys =
```

```
      -28
-----
s^2 + 0.14 s
```

Continuous-time transfer function.

```
z =
```

0x1 empty double column vector

p =

0
-0.1400

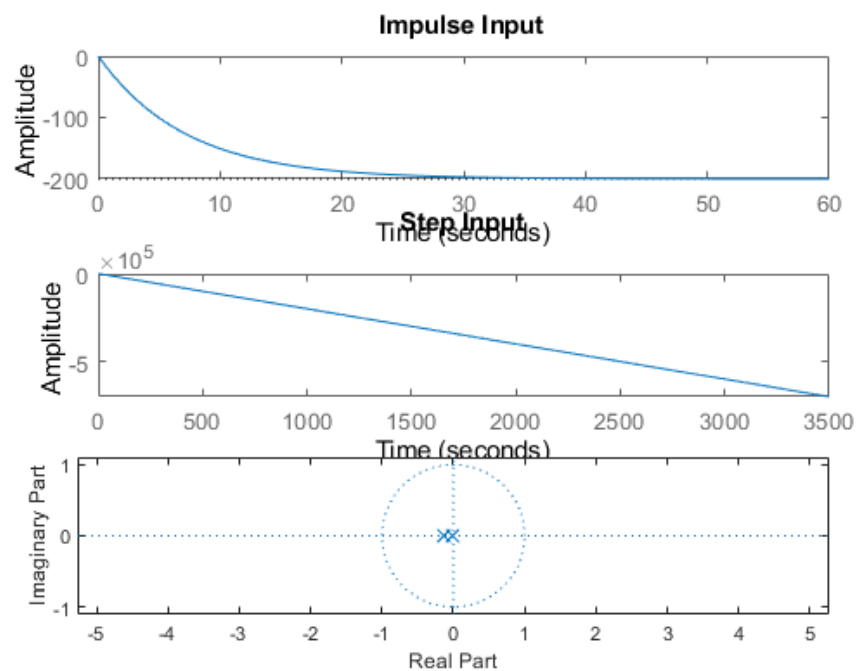
k =

-28.0000

s =

struct with fields:

RiseTime: NaN
SettlingTime: NaN
SettlingMin: NaN
SettlingMax: NaN
Overshoot: NaN
Undershoot: NaN
Peak: Inf
PeakTime: Inf



Open Loop with Controller (P)

```
P= 2;
sys = tf([P*(-k)*A],[1,k,0])
figure(2);
subplot(3,1,1);
impz(sys);
title('Impulse Input');
subplot(3,1,2);
step(sys);
title('Step Input');
[z,p,k] = tf2zp([P*(-k)*A],[1,k,0])
subplot(3,1,3);
zplane(z,p);
S = stepinfo(sys)
```

```
sys =
```

```
1.12e04
-----
s^2 - 28 s
```

Continuous-time transfer function.

```
z =
```

```
0x1 empty double column vector
```

```
p =
```

```
0
28.0000
```

```
k =
```

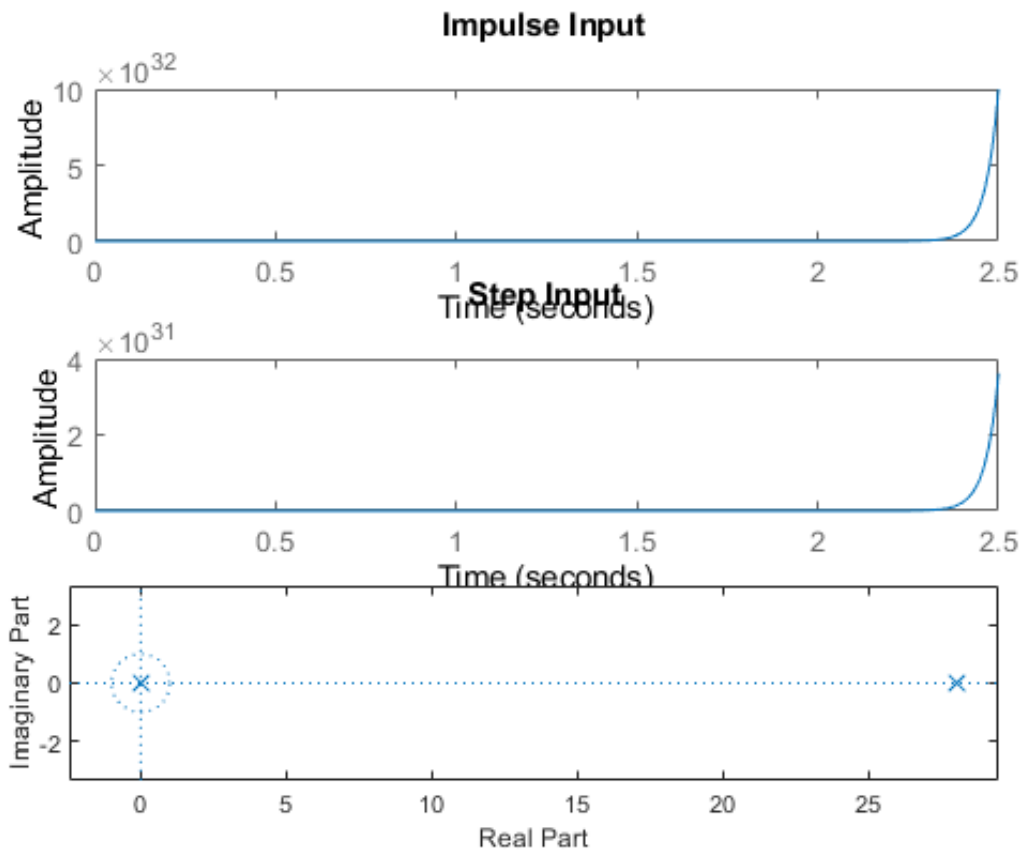
```
1.1200e+04
```

```
S =
```

```
struct with fields:
```

```
RiseTime: NaN
SettlingTime: NaN
SettlingMin: NaN
SettlingMax: NaN
```

Overshoot: NaN
 Undershoot: NaN
 Peak: Inf
 PeakTime: Inf



Open Loop with Controller (I)

```
sys = tf([(-k)*A],[1,k,0,0])
figure(3);
subplot(3,1,1);
impz(sys);
title('Impulse Input');
subplot(3,1,2);
step(sys);
title('Step Input');
[z,p,k] = tf2zp([(-k)*A],[1,k,0,0])
subplot(3,1,3);
zplane(z,p);
s = stepinfo(sys)
```

sys =

$$\frac{-2.24e06}{s^3 + 1.12e04 s^2}$$

Continuous-time transfer function.

z =

0x1 empty double column vector

p =

1.0e+04 *
0
0
-1.1200

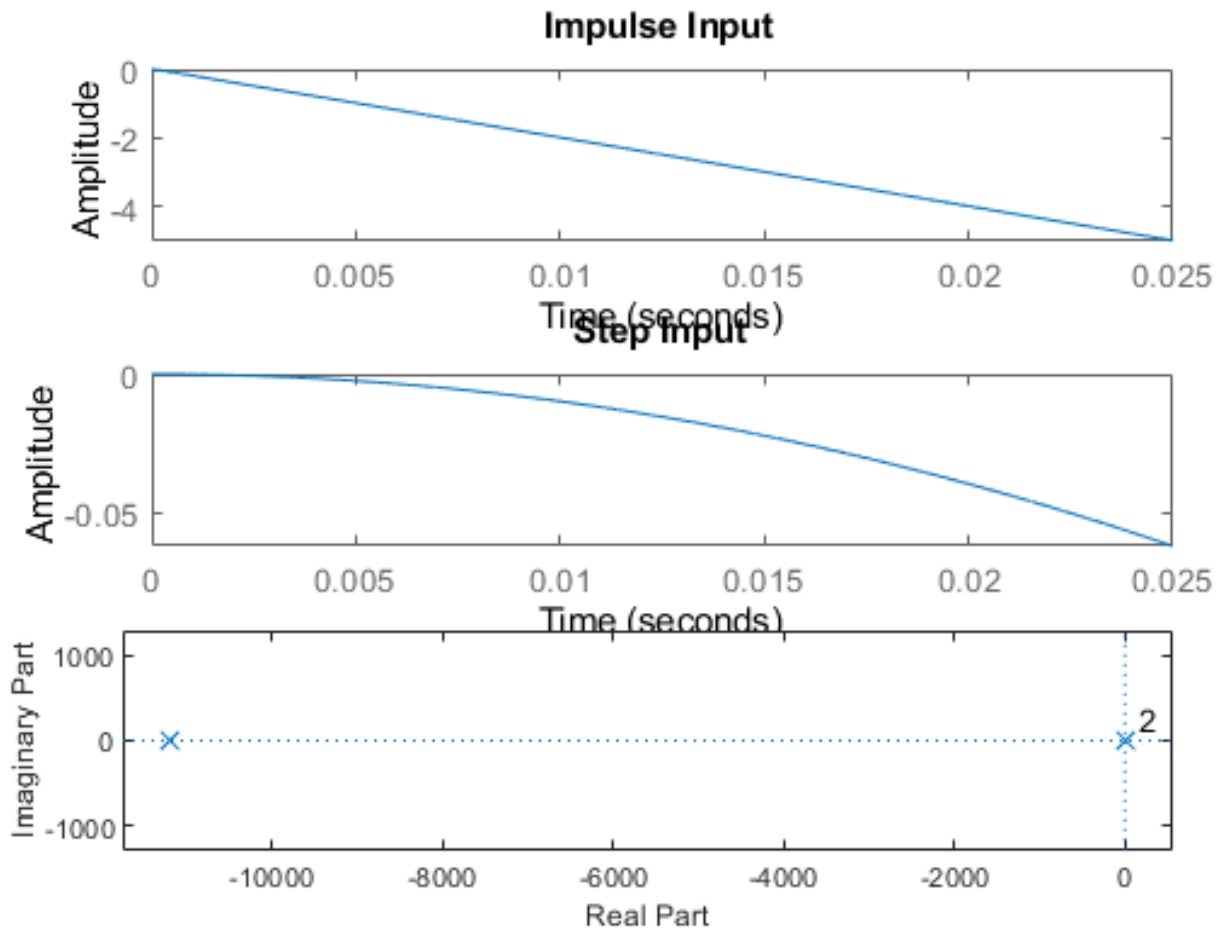
k =

-2.2400e+06

s =

struct with fields:

RiseTime: NaN
SettlingTime: NaN
SettlingMin: NaN
SettlingMax: NaN
Overshoot: NaN
Undershoot: NaN
Peak: Inf
PeakTime: Inf



Closed Loop- Negative feedback with Controller (D)

```
sys = tf([(-k)*A,0],[1,k,(-k)*A])
figure(4);
subplot(3,1,1);
impz(sys);
title('Impulse Input');
subplot(3,1,2);
step(sys);
title('Step Input');
[z,p,k] = tf2zp([(-k)*A,0],[1,k,(-k)*A])
subplot(3,1,3);
zplane(z,p);
s = stepinfo(sys)
```

sys =

4.48e08 s

$s^2 - 2.24e06 s + 4.48e08$

Continuous-time transfer function.

z =

0

p =

1.0e+06 *

2.2398

0.0002

k =

4.4800e+08

s =

struct with fields:

RiseTime: NaN

SettlingTime: NaN

SettlingMin: NaN

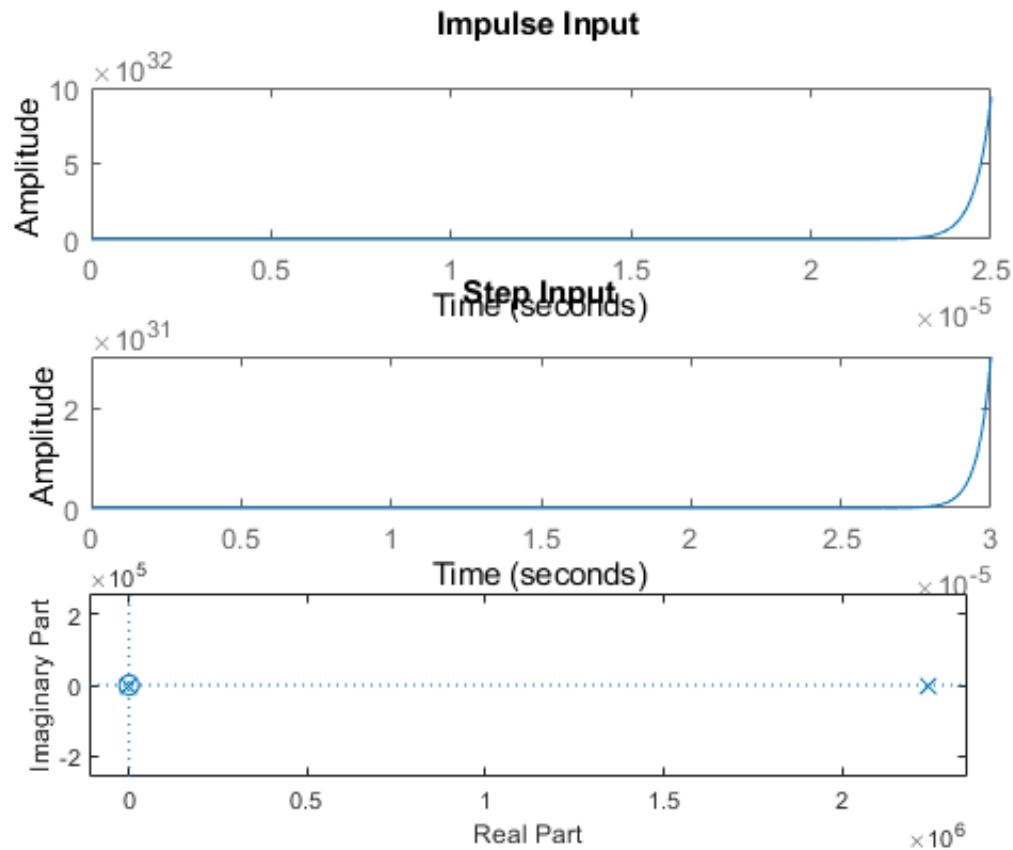
SettlingMax: NaN

Overshoot: NaN

Undershoot: NaN

Peak: Inf

PeakTime: Inf



Closed Loop- Positive feedback with Controller (D)

```
sys = tf([-k]*A, [1, k, k*A])
figure(5);
subplot(3,1,1);
impz(sys);
title('Impulse Input');
subplot(3,1,2);
step(sys);
title('Step Input');
[z,p,k] = tf2zp([-k*A, 0], [1, k, k*A])
subplot(3,1,3);
zplane(z,p);
S = stepinfo(sys)
```

```
sys =

      -8.96e10 s
-----
s^2 + 4.48e08 s + 8.96e10
```

Continuous-time transfer function.

z =

0

p =

1.0e+08 *

-4.4800

-0.0000

k =

-8.9600e+10

s =

struct with fields:

RiseTime: 0

SettlingTime: 0.0196

SettlingMin: -199.9633

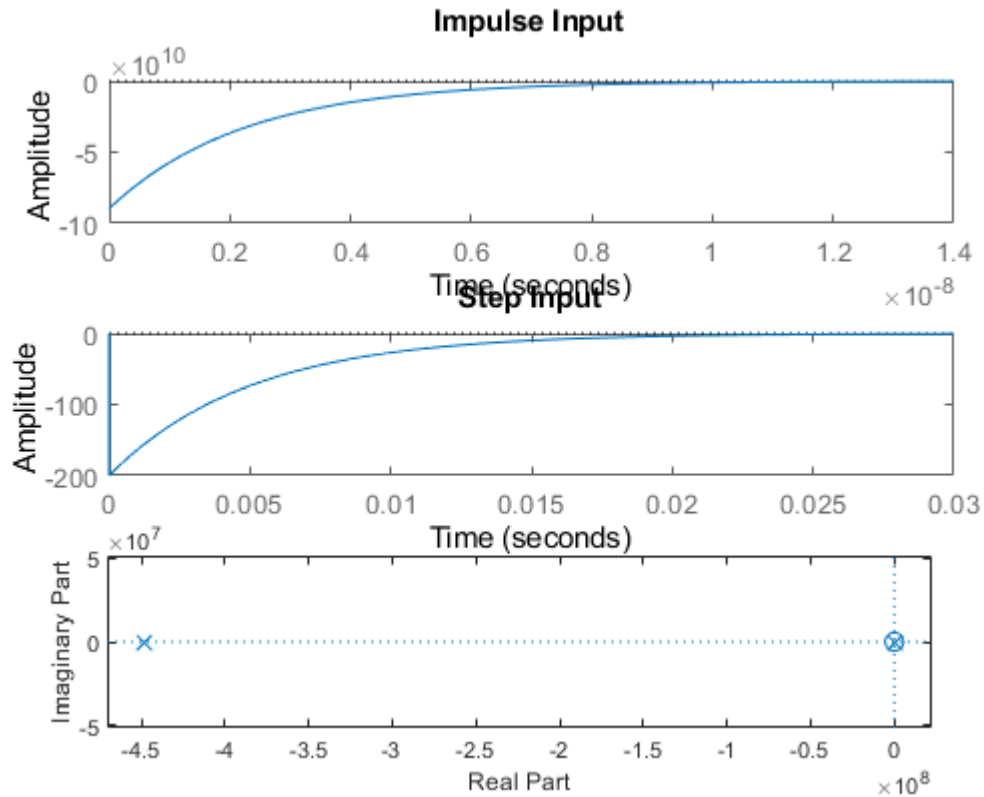
SettlingMax: -0.2598

Overshoot: Inf

Undershoot: Inf

Peak: 199.9633

PeakTime: 9.2103e-07



Math Analysis

Independent: Time(t) Dependent: Mass(M) Constant: Non-zero constant(A), Constant(A)

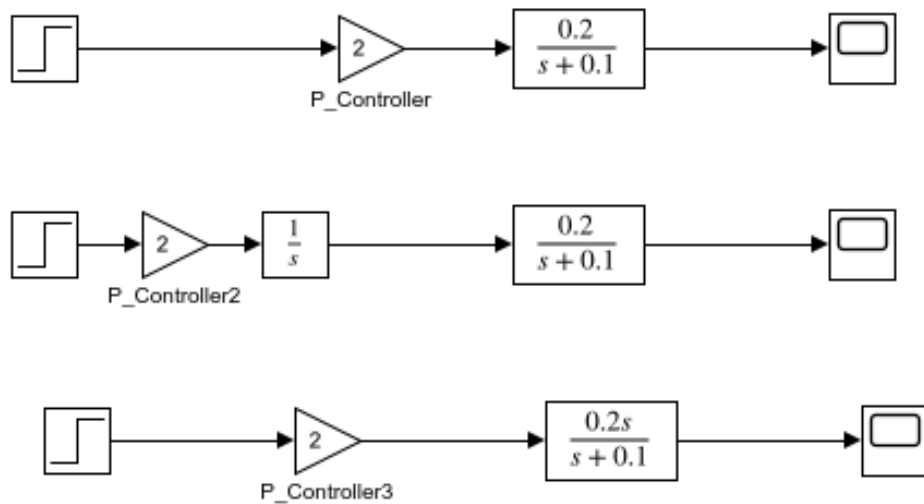
Comparison Analysis

- 1) System without controller behaves exactly like an exponential decay with the system decaying exponentially.
- 2) On adding a proportionality controller to system, the system becomes unstable.
- 3) On adding a Integrator controller to system, the response times have decreased hugely, making the system reach stability faster than a P controller.
- 4) Integrator controller adds a pole to zero also.
- 5) On addition of a differentiator controller in negative feedback the system becomes unstable.
- 6) A zero gets added at origin due to the differentiator.
- 7) On addition of a differentiator controller in positive feedback the system becomes stable.

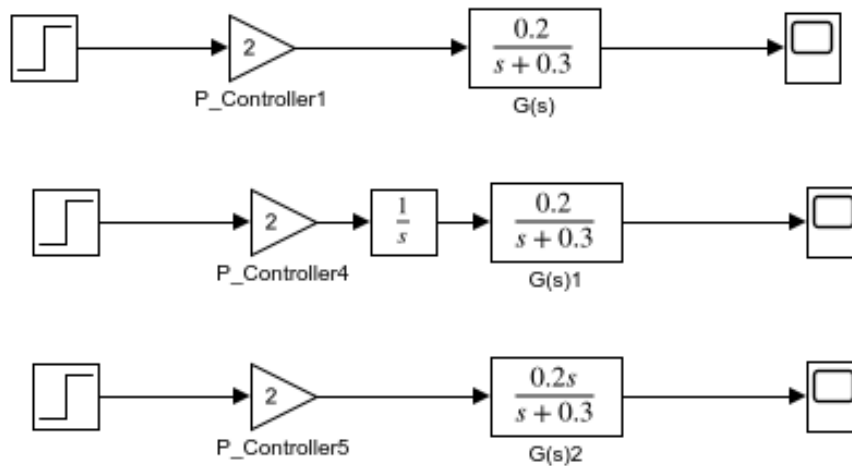
4(a) 1st Order Differential Equation Model

This was done in Simulink of MATLAB R2020b.

FIRST ORDER OPEN LOOP WITH CONTROLLERS

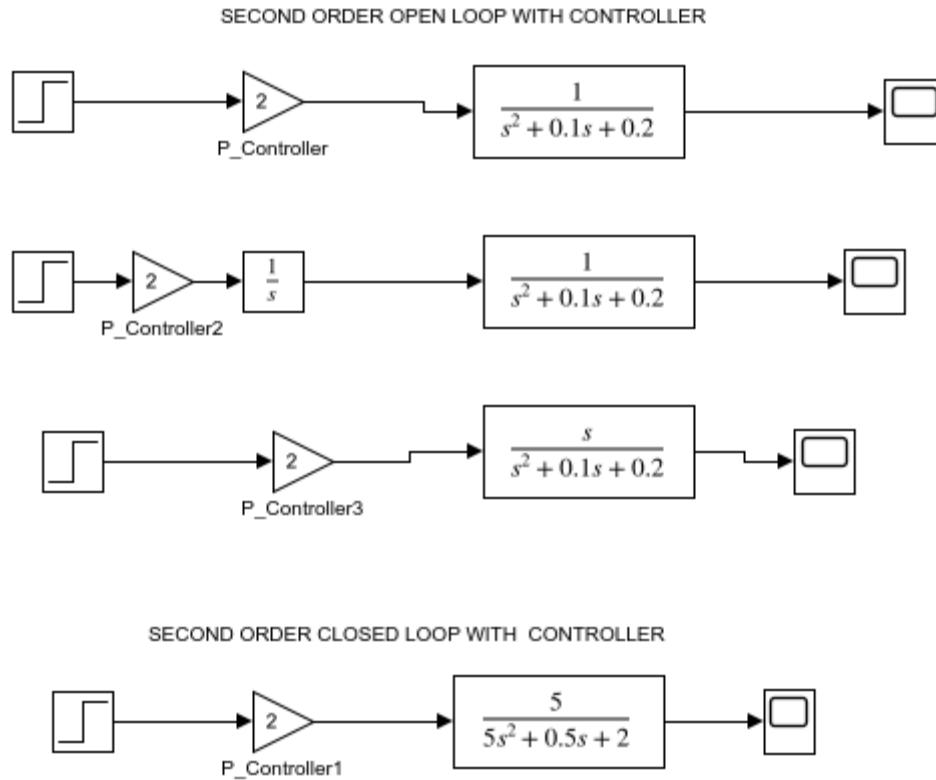


FIRST ORDER CLOSED LOOP WITH CONTROLLER



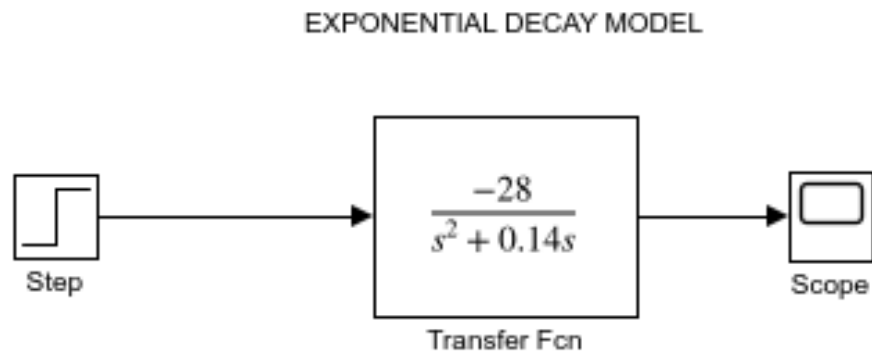
4(b) 2nd Order Differential Equation Model

This was done in Simulink of MATLAB R2020b.



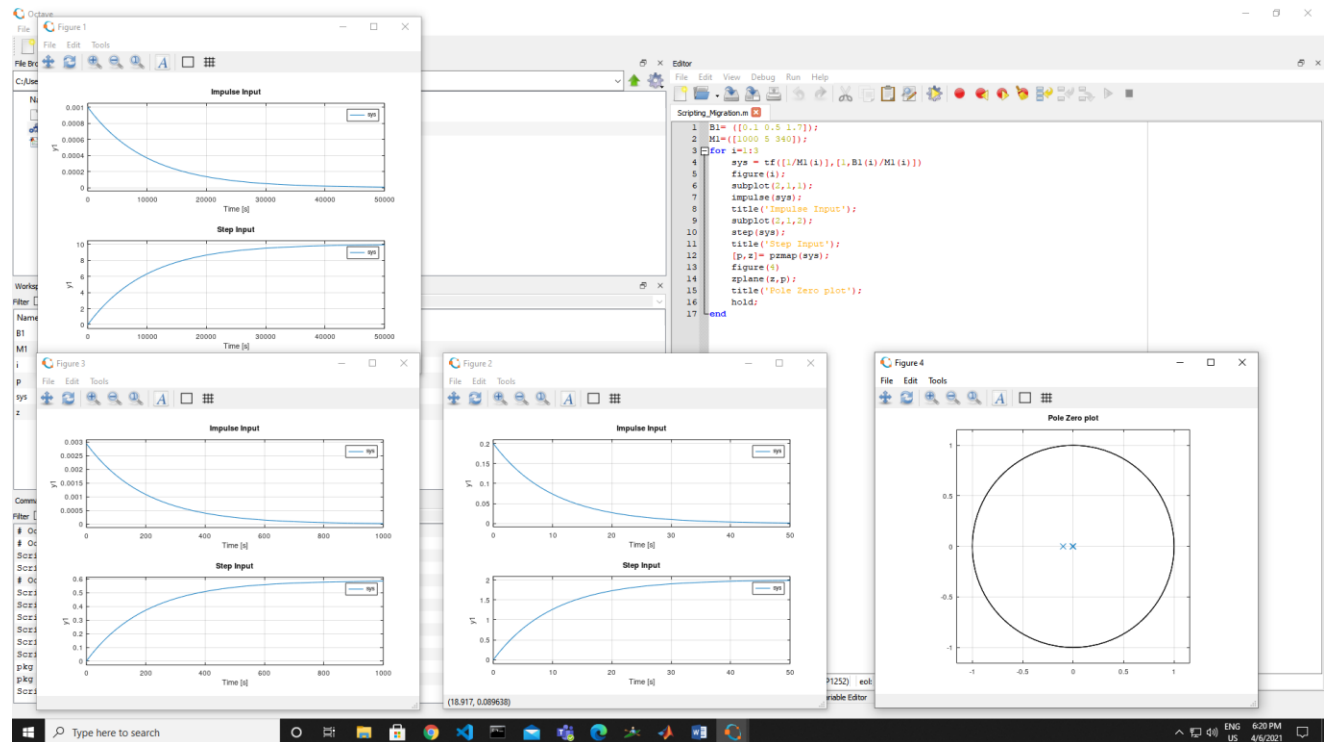
4(c) Exponential Decay- Radioactive Material Model

This was done in Simulink of MATLAB R2020b.



5(a) Migration of Scripts to GNU Octave

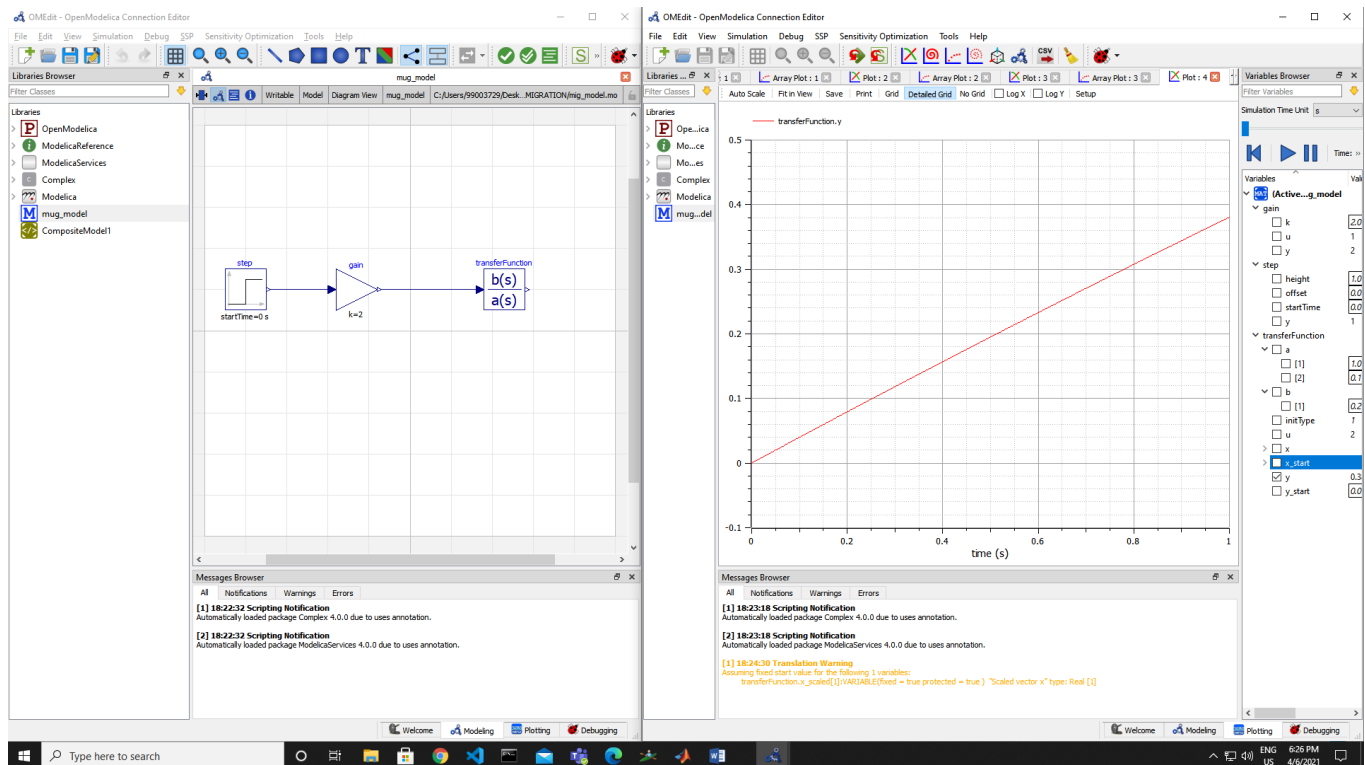
The results matched with the scripts executed in the MATLAB R2020b



GNU Octave is software featuring a high-level programming language, primarily intended for numerical computations. Octave helps in solving linear and nonlinear problems numerically, and for performing other numerical experiments using a language that is mostly compatible with MATLAB.

5(b) Migration of Model to OpenModelica

The results matched with the models executed in Simulink of MATLAB R2020b.



OpenModelica is a free and open source environment based on the Modelica modeling language for modeling, simulating, optimizing and analyzing complex dynamic systems. This software is actively developed by Open Source Modelica Consortium, a non-profit, non-governmental organization.