2(b) Second Order MSD Equation

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Plant Description

The Mass-damper Spring Second order system is taken as Plant. It is used in as suspension.

```
% Equation: Mx''(t)+ Bx'(t) + Kx(t)= Kf(t).
% f = force; B= coefficient of friction; M = mass; v= velocity;
k=spring
%constant.
% Values: K1= 0.9 B1= 0.4 M1=1000 Wn=0.03; K2= 1 B2= 0.5 M2= 500
Wn=0.44;
%K3= 3 B3= 1.7 M3= 340 Wn=0.09;
```

Code:

```
clc;
B1 = 0.5
M1 = 5;
K1 = 1;
sys = tf([P*K1/M1],[1,B1/M1,K1/M1])
subplot(4,3,1);
impulse(sys);
title('Impulse Input for k');
subplot(4,3,2);
step(sys);
title('Step Input for k');
subplot(4,3,3);
[z,p,k] = tf2zp([P*K1/M1],[1,B1/M1,K1/M1])
pzmap(sys)
subplot(4,3,10);
bode(sys)
hold on;
S = stepinfo(sys)
sys = tf([P*K1/M1],[1,B1/M1,K1/M1,0])
subplot(4,3,4);
impulse(sys);
title('Impulse Input for 1/s');
subplot(4,3,5);
step(sys);
```

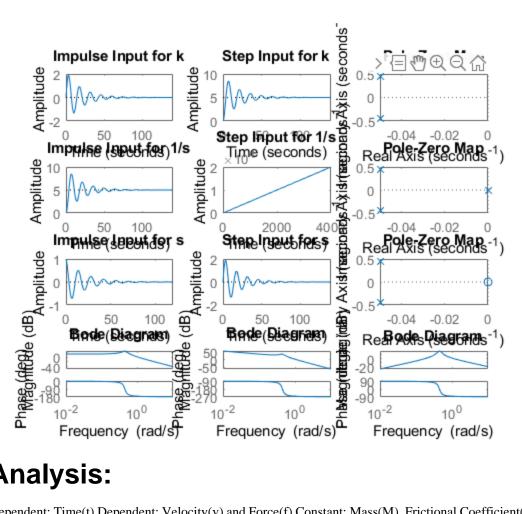
```
title('Step Input for 1/s');
subplot(4,3,6);
[z,p,k] = tf2zp([P*K1/M1],[1,B1/M1,K1/M1,0])
pzmap(sys)
subplot(4,3,11);
bode(sys)
hold on;
S = stepinfo(sys)
sys = tf([P*K1/M1,0],[1,B1/M1,K1/M1])
subplot(4,3,7);
impulse(sys);
title('Impulse Input for s');
subplot(4,3,8);
step(sys);
title('Step Input for s');
subplot(4,3,9);
[z,p,k] = tf2zp([P*K1/M1,0],[1,B1/M1,K1/M1])
pzmap(sys)
subplot(4,3,12);
bode(sys)
hold on;
S = stepinfo(sys)
B1 =
    0.5000
sys =
          1
  s^2 + 0.1 s + 0.2
Continuous-time transfer function.
z =
  0×1 empty double column vector
p =
  -0.0500 + 0.4444i
  -0.0500 - 0.4444i
k =
     1
```

```
S =
  struct with fields:
        RiseTime: 2.5448
    SettlingTime: 78.1524
     SettlingMin: 2.5361
     SettlingMax: 8.5106
       Overshoot: 70.2118
      Undershoot: 0
            Peak: 8.5106
        PeakTime: 7.0248
sys =
            1
  s^3 + 0.1 s^2 + 0.2 s
Continuous-time transfer function.
z =
  0 \times 1 empty double column vector
p =
  0.0000 + 0.0000i
  -0.0500 + 0.4444i
  -0.0500 - 0.4444i
k =
     1
S =
  struct with fields:
        RiseTime: NaN
    SettlingTime: NaN
     SettlingMin: NaN
     SettlingMax: NaN
       Overshoot: NaN
      Undershoot: NaN
            Peak: Inf
```

PeakTime: Inf

```
sys =
  s^2 + 0.1 s + 0.2
Continuous-time transfer function.
z =
     0
p =
  -0.0500 + 0.4444i
  -0.0500 - 0.4444i
k =
     1
S =
  struct with fields:
        RiseTime: 0
    SettlingTime: 81.5509
     SettlingMin: -1.3280
     SettlingMax: 1.8877
       Overshoot: Inf
      Undershoot: Inf
```

Peak: 1.8877
PeakTime: 3.5124



Math Analysis:

Independent: Time(t) Dependent: Velocity(v) and Force(f) Constant: Mass(M), Frictional Coefficient(B), Spring constant(K)

```
% Roots:((-B/M)+-sqrt(sq(B/M)-4K/M))/2
% IVT:
 1. For step input: 0
 2. For impulse input: 0
% FVT:
 1. For step input: 1
 2. For impulse input: K/M
 Time Response Results:
 K1= 0.9 B1= 0.4 M1=1000
응
         RiseTime: 2.5448
응
    SettlingTime: 78.1524
응
      SettlingMin: 2.5361
응
      SettlingMax: 8.5106
        Overshoot: 70.2118
응
       Undershoot: 0
응
응
             Peak: 8.5106
         PeakTime: 7.0248
```

```
%K2= 1 B2= 0.5 M2= 500
        RiseTime: NaN
   SettlingTime: NaN
응
    SettlingMin: NaN
    SettlingMax: NaN
      Overshoot: NaN
2
      Undershoot: NaN
            Peak: Inf
        PeakTime: Inf
%K3= 3 B3= 1.7 M3= 340
    RiseTime: 0
   SettlingTime: 81.5509
    SettlingMin: -1.3280
     SettlingMax: 1.8877
       Overshoot: Inf
      Undershoot: Inf
            Peak: 1.8877
        PeakTime: 3.5124
```

Comparison Analysis: (Speed, Accuracy and stability):

1) with proportionality controller, only the amplitude changes and all

```
%other stats are same as in 2nd order system without controller.
% 2) On adding an integrator controller, a pole is getting added at
the
%origin and makes the system marginally stable.
% 3) On adding a differentiator controller, a zero is added to the
origin
%making an unstable system stable.
% 4) On adding a differentiator controller, the overshoot increases
and
%also the response time increase.
```

Published with MATLAB® R2020b