UNIT-1

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1 Ray Theory Transmission

1.1 Total internal reflection

$$\frac{\sin \phi_1}{\sin \phi_2} = \frac{n_2}{n_1} \tag{1}$$

1.2 Acceptance angle

$$NA = n_0 \sin \theta_a = (n_1^2 - n_2^2)^{\frac{1}{2}}$$
 (2)

1.3 Numerical aperture

$$n_0 \sin \theta_1 = n_1 \sin \theta_2$$

$$= n_1 \cos \phi \quad \because \phi = \frac{\pi}{2} - \theta_2$$

$$= n_1 (1 - \sin^2 \phi)^{\frac{1}{2}}$$
(3)

refractive index difference:

$$\Delta = \frac{n_1^2 - n_2^2}{2n_1^2} = \frac{n_1 - n_2}{n_1} \quad for \Delta \ll 1$$
(4)

$$\therefore NA = n_1(2\Delta)^{\frac{1}{2}} \tag{5}$$

2 EM mode Theory

$$\nabla^{2}\Psi = \frac{\partial^{2}\Psi}{\partial x^{2}} + \frac{\partial^{2}\Psi}{\partial y^{2}} \frac{\partial^{2}\Psi}{\partial z^{2}}
= \frac{\partial^{2}\Psi}{\partial r^{2}} + \frac{1}{r} \frac{\partial\Psi}{\partial r} + \frac{1}{r^{2}} \frac{\partial^{2}\Psi}{\partial \phi^{2}} + \frac{\partial^{2}\Psi}{\partial z^{2}}$$
(6)

solution to equation 6 is given by:

$$\Psi = \Psi_0 e^{j(\omega t - \mathbf{k} \cdot \mathbf{r})} \tag{7}$$

where $k = |\mathbf{k}| = \frac{2\pi}{\lambda}$

2.1 Phase and group velocity

$$v_p = \frac{\omega}{\beta} \tag{8}$$

$$v_g = \frac{\partial \omega}{\partial \beta} \tag{9}$$

$$\beta = n_1 \frac{2\pi}{\lambda} = \frac{n_1 \omega}{c} \tag{10}$$

thus eq 8 and eq 9 become:

$$v_{p} = \frac{c}{n_{1}}$$

$$v_{g} = \frac{d\lambda}{d\beta} \cdot \frac{d\omega}{d\lambda}$$

$$= \frac{c}{n_{1} - \lambda \frac{dn_{1}}{d\lambda}}$$

$$= \frac{c}{N_{g}}$$
(11)

3 Cylinderical Fiber

3.1 Modes

$$\frac{\partial^2 \Psi}{\partial r^2} + \frac{1}{r} \frac{\partial \Psi}{\partial r} + \frac{1}{r^2} \frac{\partial^2 \Psi}{\partial \phi^2} + (n_1^2 k^2 - \beta^2) \Psi = 0$$
 (12)

where

$$n_1 k < \beta < n_2 k$$

solution of wave equation has the form

$$\Psi = E(r) \left[\frac{\cos(l\phi)}{\sin(l\phi)} e^{wt - \beta z} \right]$$
(13)

substitute above eq in eq 12 gives:

$$\frac{\partial^2 \mathbf{E}}{\partial r^2} + \frac{1}{r} \frac{\partial \mathbf{E}}{\partial r} + \left[(n_1^2 k^2 - \beta^2) - \frac{l^2}{r^2} \right] \mathbf{E} = \mathbf{0}$$
 (14)

solution to the above eq is given by:

$$E(r) = \begin{cases} GJ_l(UR), & \text{for } R < 1\\ GJ_l(U)\frac{K_i(WR)}{K_i(W)} & \text{for } R > 1 \end{cases}$$
 (15)

where G is amplitude coefficient, R = r/a $J_l \& K_l$ is Bessel's function and modified Bessel's function U and W are eigen values in core and cladding:

$$U = a(n_1^2 k^2 - \beta^2)$$

$$W = a(\beta^2 - n_2^2 k^2)$$
(16)

normalized frequency:

$$V = (U^{2} + W^{2})^{1/2}$$

$$= ka (n_{1}^{2} + n_{2}^{2})^{1/2}$$

$$= \frac{2\pi}{\lambda} a(NA)$$
(17)

normalized propagation constant:

$$b = 1 - \frac{U^2}{V^2}$$

$$= \frac{(\beta/k)^2 - n_2^2}{n_1^2 - n_2^2}$$

$$= \frac{(\beta/k)^2 - n_2^2}{2n_1^2 \Delta}$$
(18)

3.2 Fiber Index

3.2.1 Step Index

$$n(r) = \begin{cases} n_1 & r < a \text{ core} \\ n_2 & r \ge a \text{ cladding} \end{cases}$$
 (19)

No. of guided modes or mode volume

$$M_s = \frac{V^2}{2} \tag{20}$$

3.2.2 Graded Index

$$n(r) = \begin{cases} n_1 (1 - 2\Delta(r/a)^{\alpha})^{1/2} & r < a \text{ core} \\ n_1 (1 - 2\Delta)^{1/2} = n_2 & r \ge a \text{ cladding} \end{cases}$$
 (21)

No. of guided modes or mode volume

$$M_g = \left(\frac{\alpha}{\alpha + 2}\right) \left(\frac{V^2}{2}\right) \tag{22}$$

4 Single Mode fiber

4.1 Cutoff wavelength

$$V_c = 2.405(1 - 2/\alpha)^{1/2} \tag{23}$$

$$\lambda_c = \frac{2\pi}{V_c} a n_1 (2\Delta)^{1/2} \tag{24}$$