

1. Using equations of stresses around a cylindrical cavity, calculate near-wellbore effective radial  $\sigma_{rr}$  and hoop  $\sigma_{\theta\theta}$  stresses for a vertical well 8in diameter in the directions of  $S_{hmin}$  (4500 psi – acting E-W) and  $S_{Hmax}$  (6000 psi) up to 3ft of distance considering that  $P_p=3200$ psi and
  - a.  $P_w=3200$  psi.
  - b.  $P_w=4000$  psi.

The result should be presented as plots of stresses ( $\sigma_{rr}$ ,  $\sigma_{\theta\theta}$ ) as a function of distance from the center of the wellbore.

2. **Effect of overpressure:**

Consider the problem solved in class (Wellbore: vertical; Site: onshore, 7000 ft of depth,  $S_{hmin} = 4,300$  psi,  $S_{Hmax} = 6,300$  psi; Rock properties: UCS = 3,500 psi,  $\mu=0.6$ ,  $T_s = 800$  psi).

- a. Calculate wellbore pressure and corresponding mud weight for (i)  $w_{BO}=70^\circ$ , (ii)  $w_{BO}\sim 0^\circ$  ( $P_{Wshear}$ ), and (iii) for inducing tensile fractures ( $P_b$ ) for  $\lambda_p= 0.52$  and  $\lambda_p= 0.60$ . Compare with  $\lambda_p= 0.44$  solved in class. How does the drilling mud window change with overpressure?
- b. Assume horizontal stress directions near Dallas-Forth Worth region. What would the azimuth of breakouts and drilling induced fractures be? [http://dc-app3-14.gfz-potsdam.de/pub/stress\\_data/stress\\_data\\_frame.html](http://dc-app3-14.gfz-potsdam.de/pub/stress_data/stress_data_frame.html)

3. **Effect of stress anisotropy (differential stress):**

Consider the following problem, Wellbore: vertical; Site: onshore, 2 km of depth,  $\lambda_p= 0.44$ ,  $\sigma_{hmin} = 0.4 \sigma_v$ ; Rock properties: UCS = 7 MPa,  $q=3.9$ ,  $T_s = 2$  MPa. Calculate wellbore pressure and corresponding mud weight for (i)  $w_{BO}=45^\circ$ , (ii)  $w_{BO}\sim 0^\circ$ , and (iii) for inducing tensile fractures for

- a.  $\sigma_{Hmax} = 0.6 \sigma_v$ .
- b.  $\sigma_{Hmax} = 0.8 \sigma_v$ .
- c.  $\sigma_{Hmax} = 1.0 \sigma_v$ .
- d. How does the drilling mud window change with  $\sigma_{Hmax}/\sigma_{Hmin}$ ?

4. **Offshore:**

Consider the same formation as above but in offshore conditions, Wellbore: vertical; Site: offshore, 2 km of total depth, 500 m of water, hydrostatic pore pressure,  $\sigma_{hmin} = 0.4 \sigma_v$ ,  $\sigma_{Hmax} = 0.8 \sigma_v$ ; Rock properties: UCS = 7 MPa,  $q=3.9$ ,  $T_s = 2$  MPa. Calculate wellbore pressure and corresponding mud weight for (i)  $w_{BO}=45^\circ$ , (ii)  $w_{BO}\sim 0^\circ$ , and (iii) for inducing tensile fractures.

## 5. Horizontal wells:

Evaluate wellbore stability for horizontal wells that you will need to exploit in a gas reservoir subjected to a strike-slip stress environment.

- a. Draw cross-sections of wellbores drilled parallel to  $S_{hmin}$  and  $S_{Hmax}$ , identify involved stresses, and clearly mark expected positions of tensile fractures and wellbore breakouts.
- b. The horizontal wells lie at about 8000ft depth where it is estimated that  $S_{hmin}=50\text{MPa}$ ,  $S_{Hmax}=70\text{MPa}$  and  $\lambda_p=0.6$ . The unconfined compressive strength of the rock is 8500psi,  $\mu=1.0$ , and  $T_s=0$  psi is a good estimate for tensile strength, given the large density of natural fractures. Determine the mechanical stability limits on wellbore pressure for both horizontal well directions considered.
- c. Determine mud density window appropriate for these wells (keep in mind potential lost circulation).
- d. Which one appears to have a wider mud window? Justify