

1. Let's compare reservoirs with normal and reverse faulting regimes (onshore). For both regimes, plot the limits of  $S_1$  and  $S_3$  versus depth from 0 to 5 km assuming hydrostatic pore pressure and a state of stress limited by frictional strength of faults. Assume sliding friction coefficient is  $\mu=0.6$ . For both regimes, how does changing  $\mu$  from 0.6 to 1.0 change the maximum possible differential stress  $S_1-S_3$  at a fixed depth of  $z=5\text{km}$ ? Explain what that friction coefficient change physically means.
2. A given site offshore (sea floor at 500 ft) is subjected to a Normal Faulting stress regime. Over-pressure is first detected at 1500 ft (TVD) and at 2000 ft overpressure is  $\lambda_p=0.78$ . Calculate the total minimum horizontal stress  $S_{hmin}$  at this depth assuming frictional equilibrium of faults and friction angle  $30^\circ$ . Draw the corresponding Mohr circle with a solid line and draw an additional Mohr circle with a dashed line assuming hydrostatic pressure. (Assume typical water and lithostatic gradients)
3. Find out the orientations of (a) a hydraulic fracture and (b) a shear fracture both created in a site subjected to stresses  $S_v < S_{hmin} < S_{Hmax}$  where  $S_{Hmax}$  strikes E-W and  $\mu=0.8$ .
4. Find out the orientations of (a) a hydraulic fracture and (b) a shear fracture both created in a site subjected to stresses  $S_{hmin} < S_v < S_{Hmax}$  where  $S_{Hmax}$  strikes  $W20^\circ N$  and  $\mu=0.5$ .
5. For the following faults: (i) draw the corresponding points in a stereonet (lower hemisphere projection) map, (ii) convert to strike to azimuth convention, and (iii) draw equivalent geological map symbols.
  - (a)  $N55^\circ E, 45^\circ SE$
  - (b)  $E20^\circ S, 60^\circ NE$
  - (c)  $N20^\circ W, 25^\circ SW$
  - (d)  $S10^\circ W, 60^\circ NW$
6. In a given reservoir under study stresses are  $S_{hmin}=40\text{ MPa}$ ,  $S_{Hmax}=60\text{ MPa}$ ,  $S_v=45\text{ MPa}$ ,  $P_p=20\text{ MPa}$ , and  $S_{hmin}$  acts E-W. For each of the faults below, calculate (using the Mohr Circle method if possible) the normal and shear stress on the plane of the fault and then determine if the fault is prone to slip ( $\mu=0.6$ ).
  - a. Fault with strike north-south, dip  $65^\circ$  to the east
  - b. Fault with strike east-west, dip  $35^\circ$  to the north

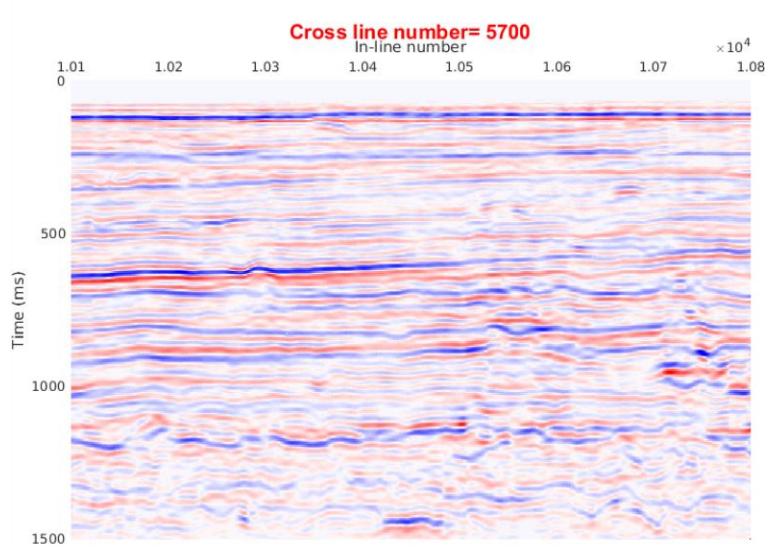
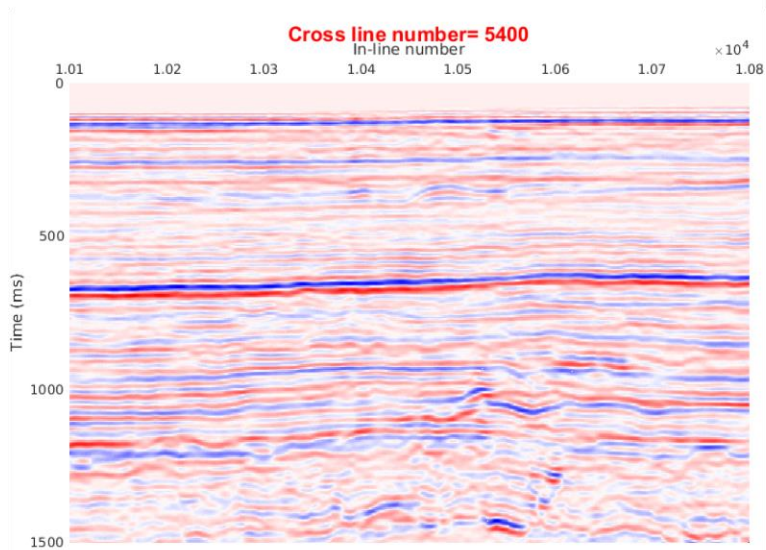
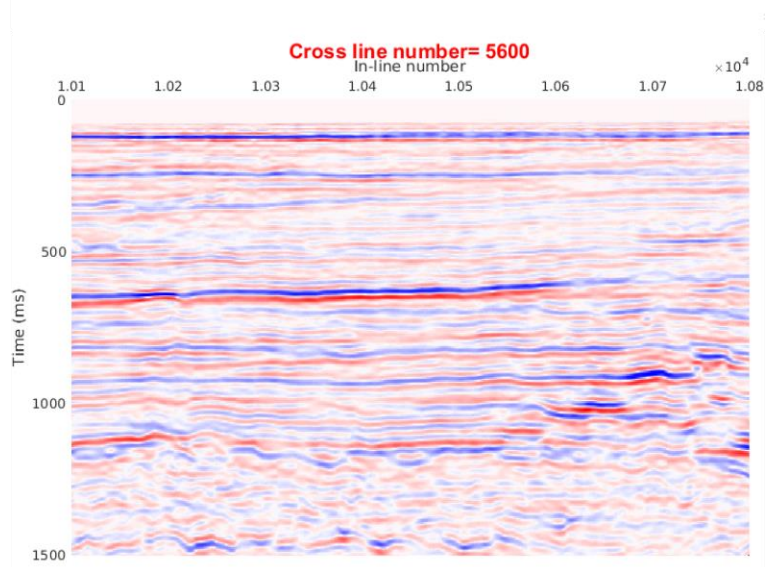
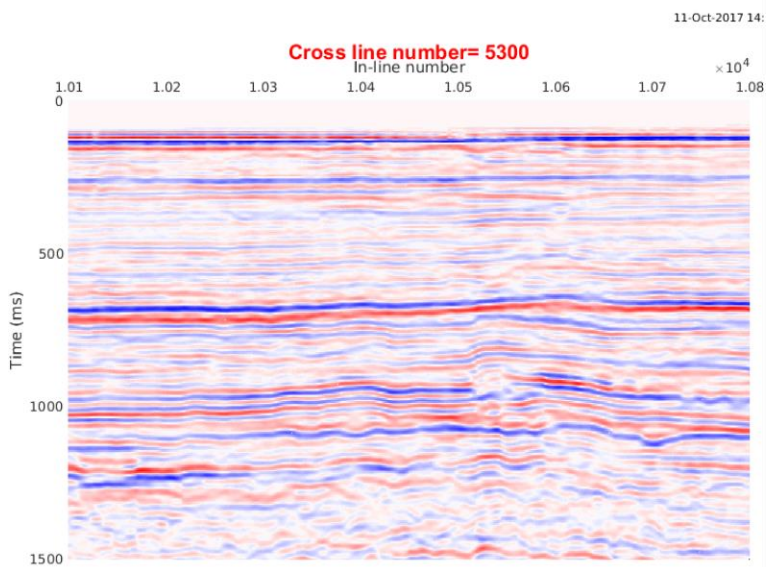
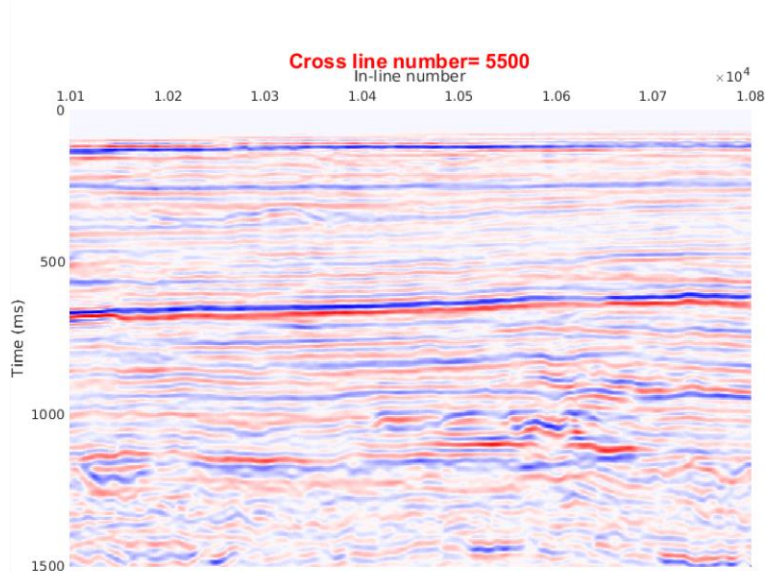
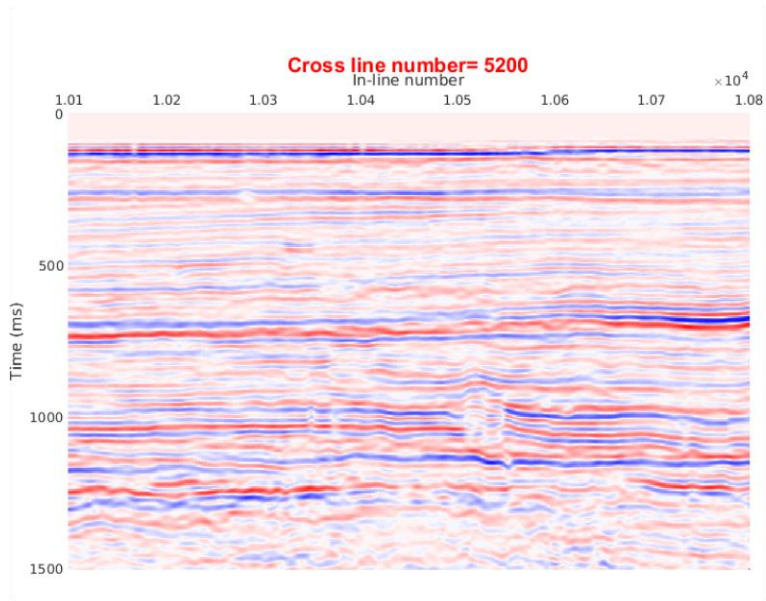
- c. Fault with strike  $060^\circ$ , dip  $90^\circ$
  - d. Fault with strike  $030^\circ$ , dip  $25^\circ$
7. (Optional - See class notes) Write a Matlab code that can obtain ( $S_n$ ,  $\tau_d$ ,  $\tau_s$ ,  $\sigma_n$ ) on an arbitrary fault with orientation (strike, dip) for a given state of stress ( $S_p$ ,  $\alpha$ ,  $\beta$ ,  $\gamma$ ).
- a. Verify with problems solved in lecture slides
  - b. Apply to solve all cases in problem 6
  - c. Apply code to solve stress on 100 fractures randomly oriented. Plot all results the respective 3D Mohr circle.
  - d. A nearby injection wellbore will perform water flooding. What is the additional pore pressure needed to start reactivating faults?

*Hint for problem 7:*

- Matlab function 'rand' can be used for creating an array of random values;

$r = a + (b-a)*\text{rand}(N,1)$  creates an array  $r$  ( $N \times 1$ ) of values in interval  $[a,b]$

8. (Real application problem) The following page contains seismic images (<http://www.glossary.oilfield.slb.com/Terms/c/crossline.aspx>) of a section the subsurface in the North Sea. We are interested in the Frigg sandstone formation. This is a hydrocarbon-bearing formation and it is located at about 1790 m of TVDSS.
- a. Calculate the water depth by measuring the two-way travel time and assuming  $V_P(\text{sea-water}) = 1450 \text{ m/s}$ .
  - b. Find the location of the Frigg Formation in the time axis assuming  $V_P(\text{sediments}) = 3000 \text{ m/s}$ .
  - c. Evaluate qualitatively the faulting at the reservoir depth. Describe how faulting could affect fluid flow.



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