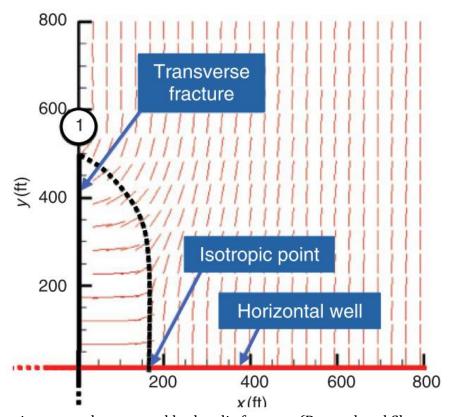
## **Project #8: Hydraulic Fracturing**

## 1) Stress shadows and interference

Read the paper "Roussel, N. P., & Sharma, M. M. (2011). Optimizing fracture spacing and sequencing in horizontal-well fracturing. *SPE Production & Operations*, 26(02), 173-184."

- (a) Calculate the point of principal stress reversal (isotropic point in Fig. 11) with a constant pressure and plane-strain solution utilizing your FreeFEM++ linear elasticity code. Use all parameters as in Table 1. Note:  $\Delta S_{yy} = v \left( \Delta S_{xx} + \Delta S_{zz} \right)$
- (b) Repeat (a) for fracture width 6mm, 8mm, and 10 mm. Plot stress reversal distance as a function of fracture width



S<sub>Hmax</sub> direction around a propped hydraulic fracture (Roussel and Sharma, 2011)

## 2) Coupled hydraulic fracturing modeling

A single hydraulic fracture treatment will be performed in a tight sandstone. The hydraulic fracture height is expected to be  $h_f$  = 170 ft. The tight sandstone has a plane-strain modulus E' = 8.9 MMpsi. The (two-wing) injection rate will be 50 bbl/min (constant) during 1 hour.

## Compute:

- a. The expected fracture half-length  $x_f$ , fracture width at the wellbore  $w_{w,0}$ , and net pressure  $p_n$  as a function of time with the PKN model (no leak-off) assuming the fracturing fluid has a (constant) viscosity 2 cP.
- b. The expected fracture half-length  $x_f$ , fracture width at the wellbore  $w_{w,0}$ , and net pressure  $p_n$  as a function of time with the PKN model (no leak-off). Now the fracturing fluid has a viscosity 2 cP with no proppant (initial 10 min), and increases in steps of 10 min with 2 cP in each step (due to increasing proppant concentration).
- c. What should you do to your solution in order to consider leak-off? Justify and explain briefly the algorithm to calculate  $x_f$ ,  $w_{w,0}$ , and  $p_n$ .

Hint: convert all quantities to the SI system first

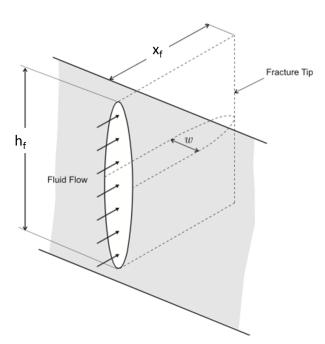


Fig. 1. Schematic showing PKN fracture geometry.

Figure: Adachi et al. 2007

- (1) Linear elasticity
- (2) Negligible Toughness
- (3) No leak-off
- (4) Laminar flow, constant injection rate
  - Fracture half-length

$$x_f = 0.524 \left( \frac{i^3 E'}{\mu h_f^4} \right)^{1/5} (t)^{4/5}$$

Maximum width at the wellbore

$$w_{w,0} = 3.04 \left(\frac{i^2 \mu}{E' h_f}\right)^{1/5} (t)^{1/5}$$

Net Pressure at the wellbore

$$p_{n,w} = 1.52 \left( \frac{E^{14} i^2 \mu}{h_f^6} \right)^{1/5} (t)^{1/5}$$