

$$-\frac{d}{dx}\left(a \frac{du}{dx}\right) + cu - f = 0 \quad \text{for } a < x < b$$

Subject to von Neumann B.C.'s

$$\left(a \frac{\partial u}{\partial x}\right)_{x=a} = Q_a \quad + \quad \left(a \frac{\partial u}{\partial x}\right)_{x=b} = Q_b$$

Weak form

$$\int_a^b \left[a \frac{d\delta u}{dx} \frac{du}{dx} + c \delta u u - \delta u f \right] dx - \delta u(a) Q_a - \delta u(b) Q_b$$

$$B(\delta u, u) = \int_a^b \left[a \frac{d\delta u}{dx} \frac{du}{dx} + c \delta u u \right] dx$$

$$l(\delta u) = \int_a^b \delta u f dx + \delta u(a) Q_a + \delta u(b) Q_b$$

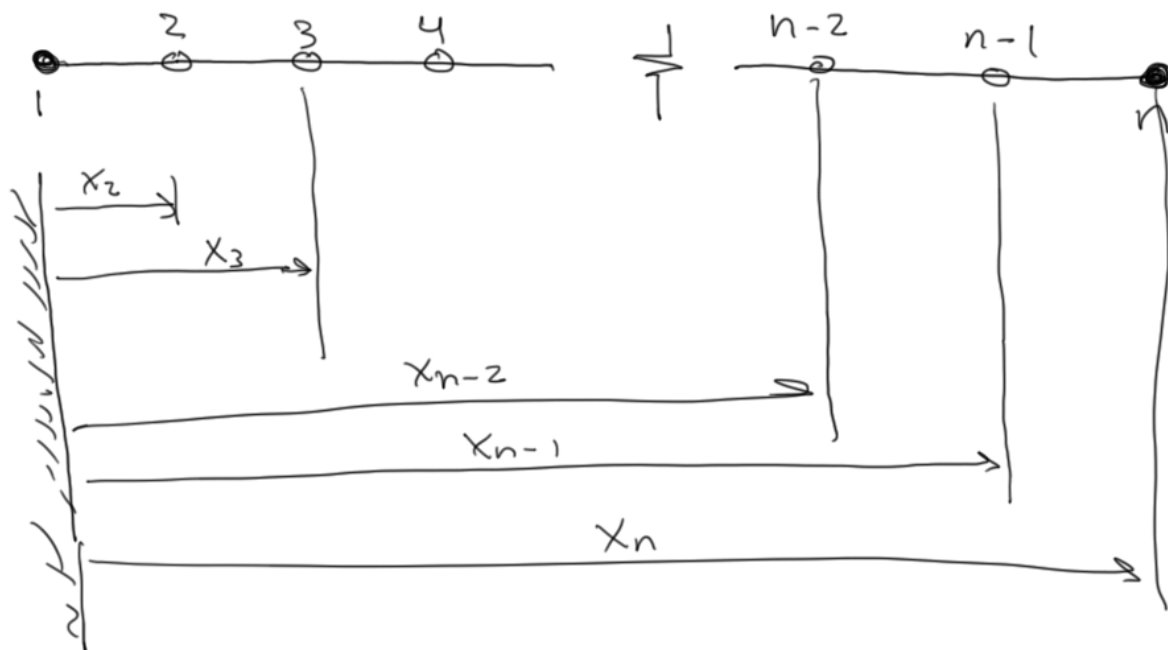
$$B(\delta u, u) = l(\delta u)$$

$$u \approx u^h = \sum_{j=1}^n N_j u_j \quad N_j \text{ of degree } n-1 \quad + \quad u_j \text{ are unknowns}$$

$$-\frac{d}{dx}\left(a \frac{du}{dx}\right) + cu - f = 0 \quad 0 < x < L$$

$$u(0) = u_0 \quad + \quad \left(a \frac{du}{dx}\right)_{x=L} = Q_0$$

	u	a	c	f	Q
Heat Transfer	Temp, T	Thermal conductivity kA	conv.	heat gen.	Heat, Q
Flow	p	resistance	0	0	point source
Elasticity	p or p	stiffness AE	0	Axial dist. force	Point load



$$(x_1, x_2), (x_2, x_3), \dots, (x_{n-1}, x_n)$$

$$0 = \sum_{i=1}^{n-1} \left\{ \int_{x_i}^{x_{i+1}} \left[a \frac{d\delta u}{dx} \frac{du}{dx} + c \delta u u - \delta u f \right] dx - \left[\delta u(x) a \frac{du}{dx} \right]_{x_i}^{x_{i+1}} \right\}$$

$$= \int_{x_1}^{x_n} \left[a \frac{d\delta u}{dx} \frac{du}{dx} + c \delta u u - \delta u f \right] dx - \delta u(x_1) \left[-a \frac{du}{dx} \right]_{x_1} - \delta u(x_2) \left[a \frac{du}{dx} \right]_{x_2} \\ - \delta u(x_2) \left[-a \frac{du}{dx} \right]_{x_2} - \delta u(x_3) \left[a \frac{du}{dx} \right]_{x_3} - \dots - \delta u(x_{n-1}) \left[a \frac{du}{dx} \right]_{x_{n-1}} \\ - \delta u(x_n) \left[a \frac{du}{dx} \right]_{x_n}$$

$$0 = \int_{x_1}^{x_n} \left[a \frac{d\delta u}{dx} \frac{du}{dx} + c \delta u u - \delta u f \right] dx - \delta u(x_1) Q_1 - \delta u(x_2) Q_2 \\ - \dots - \delta u(x_{n-1}) Q_{n-1} - \delta u(x_n) Q_n$$

where

$$Q_1 = \left[-a \frac{du}{dx} \right]_{x_1}$$

$$Q_2 = \left[\left(a \frac{du}{dx} \right)_{x_2^-} - \left(a \frac{du}{dx} \right)_{x_2^+} \right]$$

...

$$Q_{n-1} = \left[\left(a \frac{du}{dx} \right)_{x_{n-1}^-} - \left(a \frac{du}{dx} \right)_{x_{n-1}^+} \right]$$

$$Q_n = \left(a \frac{du}{dx} \right)_n$$

$$0 = \underbrace{\int_{x_a}^{x_b} \left(a \frac{d\delta u}{dx} \frac{du}{dx} + c \delta u u \right) dx}_{B(\delta u, u)} - \underbrace{\int_{x_a}^{x_b} \delta u f dx - \sum_{j=1}^n \delta u(x_j) Q_j}_{Q(\delta u)}$$

Let $u = N_j u_j$ + $\delta u_i = N_i$

For $i=1$

$$0 = \int_{x_a}^{x_b} \left[a \frac{dN_1}{dx} \left(\frac{d}{dx} (N_j u_j) \right) + c N_1 (N_j u_j) \right] dx - \int_{x_a}^{x_b} N_1 f dx - \sum_{j=1}^n N_1(x_j) Q_j$$

⋮

For $i=n$

$$0 = \int_{x_a}^{x_b} \left[a \frac{dN_n}{dx} \frac{dN_j}{dx} u_j + c N_n N_j u_j \right] dx - \int_{x_a}^{x_b} N_n f dx - \sum_{j=1}^n N_n(x_j) Q_j$$

∴ i th equation we have

$$0 = \underbrace{\left[\int_{x_a}^{x_b} a \frac{dN_i}{dx} \frac{dN_j}{dx} + c N_i N_j dx \right]}_{B(N_i, N_j)} u_j - \underbrace{\int_{x_a}^{x_b} N_i f dx}_{f_i} - Q_i$$

$$\underbrace{B(N_i, N_j)}_{K_{ij}} u_j - \underbrace{f_i - Q_i}_{\bar{F}_i} = 0$$

$$K_{ij} u_j = \bar{F}_i$$

$$K \vec{u} = \vec{F}$$

$$N_i(x_j) = \begin{cases} 1 & i=j \\ 0 & \text{otherwise} \end{cases}$$

$$K \vec{u} = \vec{F}$$

coefficient or "stiffness matrix" or "transmissibility"

$$\vec{u} = K^{-1} \vec{F}$$

Example

$$\text{Let } (x_a, x_b) = (0, L)$$

$$c = 0$$

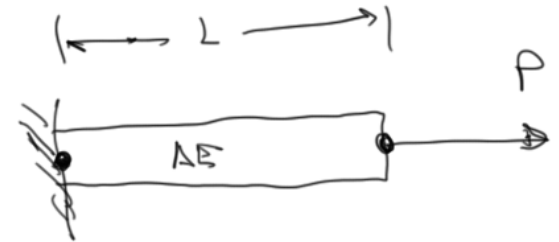
$$a = EA \quad \text{find } K_{ij}$$

$$K_{ij} = \int_0^L \left(EA \frac{dN_i}{dx} \frac{dN_j}{dx} \right) dx$$

$$= \begin{bmatrix} \cancel{\frac{EA}{L}} & \cancel{-\frac{EA}{L}} \\ \cancel{\frac{EA}{L}} & \frac{EA}{L} \end{bmatrix} \begin{Bmatrix} u_1 \\ u_2 \end{Bmatrix} = \begin{Bmatrix} 0 \\ P \end{Bmatrix}$$

$$u_1 = 0$$

$$\frac{EA}{L} u_2 = P \Rightarrow u_2 = \frac{PL}{EA}$$

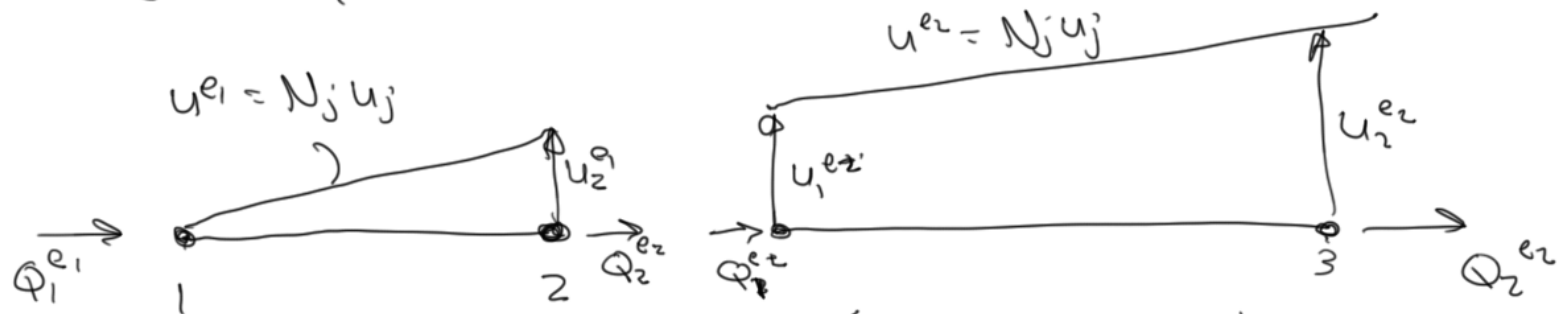


$$u(0) = 0$$

2n unknowns

$$(u_1, u_2, u_3, \dots, u_n) + (Q_1, Q_2, \dots, Q_n)$$

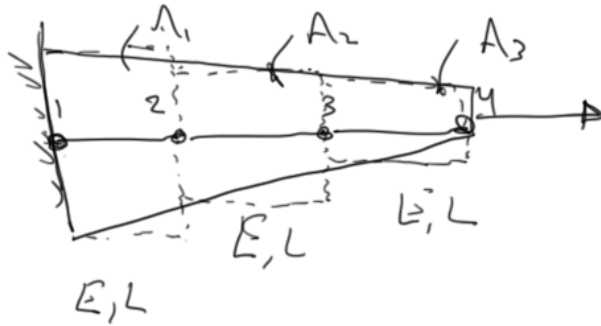
Continuity in u_i 's + "balance" Q_i 's



$$Q_2^{e1} + Q_1^{e2} = \begin{cases} 0 & \text{if no external source} \\ Q_d & \text{if external source of neg. } Q_d \end{cases}$$

$$K^{e1} = \begin{bmatrix} K_{11}^1 & K_{12}^1 \\ K_{21}^1 & K_{22}^1 \end{bmatrix} + K^{e2} = \begin{bmatrix} K_{11}^2 & K_{12}^2 \\ K_{12}^2 & K_{22}^2 \end{bmatrix}$$

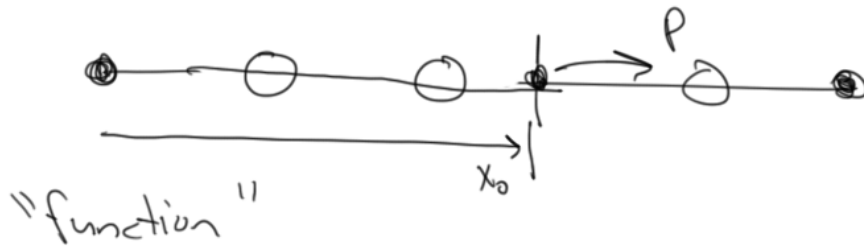
$$\begin{bmatrix} K_{11}^1 & K_{12}^1 & 0 \\ K_{21}^1 & K_{22}^1 + K_{11}^2 & K_{12}^2 \\ 0 & K_{21}^2 & K_{22}^2 \end{bmatrix} \begin{Bmatrix} u_1 \\ u_2 \\ u_3 \end{Bmatrix} = \begin{Bmatrix} f_1^1 \\ f_2^1 + f_1^2 \\ f_2^2 \end{Bmatrix} + \begin{Bmatrix} Q_1^1 \\ Q_2^1 + Q_1^2 \\ Q_2^2 \end{Bmatrix}$$



$$\begin{bmatrix}
 \cancel{\frac{A_1 E}{L}} & \cancel{\frac{-A_1 E}{L}} & 0 \\
 \cancel{\frac{-A_1 E}{L}} & \frac{(A_1 + A_2)E}{L} & \frac{-A_2 E}{L} \\
 0 & -\frac{A_2 E}{L} & \frac{(A_2 + A_3)E}{L} \\
 0 & 0 & -\frac{A_3 E}{L}
 \end{bmatrix}$$

$$\begin{bmatrix}
 0 \\
 0 \\
 -\frac{A_1 E}{L} \\
 \frac{A_3 E}{L}
 \end{bmatrix}
 \begin{Bmatrix}
 u_1 \\
 u_2 \\
 u_3 \\
 u_4
 \end{Bmatrix}
 =
 \begin{Bmatrix}
 0 \\
 0 \\
 0 \\
 P
 \end{Bmatrix}$$

What happens if Q_i is not at a node



$$f(x) = P \Delta(x - x_0)$$

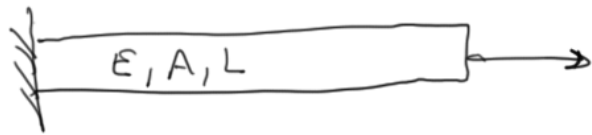
$$\int_{-\infty}^{\infty} f(x) \Delta(x - x_0) dx = f(x_0)$$

$$f_i^e = \int_{x_1}^{x_n} f(x) N_i(x) dx = \int_{x_1}^{x_n} P \Delta(x - x_0) N_i(x) dx = P N_i(x_0)$$



$$f_1 = P(1 - \frac{x_0}{L}), \quad f_2 = P(\frac{x_0}{L}) \Rightarrow f_1 + f_2 = P$$

$$f_1 = f_2 = \frac{P}{2}$$



$$P_1 = A\sigma_1 = AE\varepsilon_1 = AE \left[\frac{u_1 - u_2}{L} \right] = \frac{AE}{L} u_1 - \frac{AE}{L} u_2$$

$$P_2 = A\sigma_2 = AE\varepsilon_2 = AE \left[\frac{u_2 - u_1}{L} \right] = -\frac{AE}{L} u_1 + \frac{AE}{L} u_2$$

$$\begin{bmatrix} \frac{AE}{L} & -\frac{AE}{L} \\ -\frac{AE}{L} & \frac{AE}{L} \end{bmatrix} \begin{Bmatrix} u_1 \\ u_2 \end{Bmatrix} = \begin{Bmatrix} P_1 \\ P_2 \end{Bmatrix}$$