$$p_{net} = (p_f - \sigma_3) = \frac{K_{Je}}{\sqrt{RL}}$$
 \Rightarrow center-cracked infinite plate

$$V = \frac{16(1-3^2)R^2(pnot)}{3E}$$

Sack (1946)

$$Pnet = \sqrt{\frac{\pi G_k E}{4(1-\partial^2)R}} = \sqrt{\frac{\pi}{4R}} \text{ Kiz.}$$

$$Sneddon (1946)$$

$$V = \frac{16(1-\partial^2)R^2(pnet)}{3E}$$
(onbine - elimite R

Lamb 1932

Plane strain in direction of he
where
$$E' = \frac{E}{(1-V^2)}$$

CL > leakoff coef. texp> exposure time

Mass balance

Perhins - Kem 1961

- Igrores Fracture Mechanics
- Plan Strain vertical direction
- Leakoft neglected
- Fixed height

was assumed constant

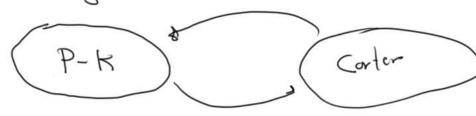
$$g_i = 2 \int_0^t u_L(t-\lambda) \frac{\partial A_1}{\partial \lambda} d\lambda + \overline{\omega} \frac{\partial A_1}{\partial t}$$

Harrington & Henryh (1975)

$$A_{f} = \frac{g_{i} \overline{\omega}}{4 \pi c_{i}^{2}} \left(e^{S^{2}} \operatorname{erfc}(S) + \frac{2}{\sqrt{\pi}} S - 1 \right) + A_{f} = \frac{g_{i} t}{\overline{\omega} + 2C_{i} \sqrt{2t}}$$

with
$$5 = \frac{2 C_L \sqrt{\pi t}}{\overline{\omega}} \quad \text{erfc(x)} = \frac{2}{\sqrt{\pi}} \int_{x}^{x} e^{-t^2} dt$$

Fractum length 1 can be obtained by dividing A(t) by 2 t by ht



$$\frac{E'}{128 \,\mu h^{f}} \frac{\partial^{2} \omega^{4}}{\partial x^{2}} = \frac{8CL}{\pi \sqrt{t-t_{exp}}} + \frac{\partial \omega}{\partial t} \qquad (PKN)$$