







Part 3

Advanced Compact MOSFET Model: Parameter extraction 🗆 প্রাপ্ত

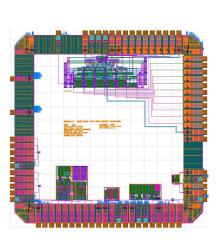


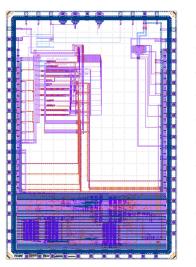
Deni Germano Alves Neto

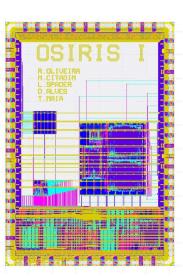
https://github.com/ACMmodel/MOSFET_model

About me

- Universidade Federal de Santa Catarina UFSC Brazil
- Undergrad and Masters in IC design 2022
 - Subject : Ultra-Low-Voltage IC circuits $V_{DD} < 100 \ mV$
 - Dissertation: Ultra-Low-Voltage Standard Cell Library
 - ACM for low voltage circuits
- Contact with open-source IC design :
 - Chipathon SSCS 2021 : Analog-front-end for Biosignals AFEbio
 - Chipathon-SSCS & UNIC-CASS 2023/2024 Analog/Digital IC design
- Start PhD in 2023 : MOSFET Modeling ACM2
- Joint PhD between UFSC and
- UGA Grenoble INP
 - TIMA (Currently based)
 - RFIC design











Outline

- ACM2 : Parameter Extraction
 - 3-DC-parameter model
 - VT0, IS and n
 - Transconductances in Saturation
 - Sigma & Zeta
 - DC and small-signals characteristics
 - Example: Inverter CMOS
- Overview of Open-source environment
 - Automatic parameter extraction

ACM2: A simple 5-DC-parameter MOSFET model

$$V_P = \frac{V_{GB} - V_{T0} + \sigma(V_{DB} + V_{SB})}{n}$$
$$\frac{V_P - V_{SB}}{\phi_t} = q_s - 1 + \ln(q_s)$$

Used to calculate q_s

$$q_{dsat} = q_s + 1 + \frac{1}{\zeta} - \sqrt{\left(1 + \frac{1}{\zeta}\right)^2 + \frac{2q_s}{\zeta}}$$

$$\frac{V_{DS}}{\phi_t} = q_s - q_d + \ln\left(\frac{q_s - q_{dsat}}{q_d - q_{dsat}}\right)$$

Used to calculate q_d

$$I_D = I_S \frac{(q_s + q_d + 2)}{1 + \zeta(q_s - q_d)} (q_s - q_d)$$

Specific current I_S (W,L)

Threshold voltage V_{T0} (W,L)

Slope factor n (W,L)

DIBL factor σ (W,L)

V_{sat} effect ζ (W,L)

I_{so} , $V_{\tau o}$ and n extraction \rightarrow let's simplify and use only the 3-parameter model (no sat no DIBL)

DC equations

$$I_D = I_S \frac{(q_S + q_d + 2)}{1 + \zeta(q_S - q_d)} (q_S - q_d) \qquad \text{where} \qquad I_S = \mu C_{ox} n \frac{\phi_t^2 W}{2} = I_{SH} \frac{W}{L}$$

$$I_{S} = \mu C_{ox} n \frac{\phi_t^2 W}{2} = I_{SH} \frac{W}{L}$$

$$\frac{V_{DS}}{\phi_t} = q_S - q_D + \ln\left(\frac{q_S - q_{Dsat}}{q_D - q_{Dsat}}\right)$$
 No saturation effect \rightarrow no ζ , no q_{Dsat}

$$\frac{V_P - V_{SB}}{\phi_t} = q_s - 1 + \ln(q_s)$$

$$V_P = \frac{V_{GB} - V_{T0} + \sigma(V_{DB} + V_{SB})}{n}$$
 No DIBL effect \rightarrow no σ

Remember that:

$$I_D = I_S [i_f - i_r]$$

with
$$\begin{cases} q_s = \sqrt{1+i_f} - 1 & \text{for forward current} \\ q_D = \sqrt{1+i_r} - 1 & \text{for reverse current} \end{cases}$$

Then we re-write:

$$\frac{V_{DS}}{\phi_t} = \sqrt{1 + i_f} - \sqrt{1 + i_r} + \ln\left(\frac{\sqrt{1 + i_f} - 1}{\sqrt{1 + i_r} - 1}\right) \qquad \frac{V_P - V_{SB}}{\phi_t} = \sqrt{1 + i_f} - 2 + \ln\left(\sqrt{1 + i_f} - 1\right)$$

$$\frac{V_P - V_{SB}}{\phi_t} = \sqrt{1 + i_f} - 2 + \ln\left(\sqrt{1 + i_f} - 1\right)$$

I_{so} , $V_{\tau o}$ and n extraction \rightarrow let's simplify and use only the 3-parameter model (no sat no DIBL)

From DC equations

If we choose $i_f = 3 \iff q_S = 1 \iff V_P = 0 \iff V_{GB} = V_{T0}$

$$\frac{V_P - \frac{V_{\overline{SB}}}{\phi_t}}{\phi_t} = \sqrt{1 + i_f} - 2 + \ln\left(\sqrt{1 + i_f} - 1\right)$$

If we add that we want to work at $V_{DS} = {\phi_t}/{2}$

$$V_{DS} = \frac{\phi_t}{2}$$

Since
$$\frac{V_{DS}}{\phi_t} = \sqrt{1 + i_f} - \sqrt{1 + i_r} + \ln\left(\frac{\sqrt{1 + i_f} - 1}{\sqrt{1 + i_r} - 1}\right) \quad V_{GB}$$

Then
$$i_r = 2.12$$
 and $I_D = I_{S0}[i_f - i_r] = 0.88$ I_{S0}

Consequence on small signal equations for $i_f = 3$ and $V_{DS} = {\phi_t}/{2}$

$$\frac{g_m}{I_D} = \frac{1}{n\phi_t} \cdot \frac{2}{\left(\sqrt{1+i_f} + \sqrt{1+i_r}\right)} = \frac{0.531}{n\phi_t}$$

Meanwhile
$$\frac{g_m}{I_D}\bigg|_{max} = \frac{1}{n\phi_t}$$
 $i_f(i_r) \approx 0$

3PM-ACM model in a nutshell

$$I_D = I_S [i_f - i_r]$$
 where $I_S = \mu C_{ox} n \frac{\phi_t^2 W}{2L} = I_{SH} \frac{W}{L}$

$$\frac{V_P - V_{S(D)B}}{\phi_t} = \sqrt{1 + i_{f(r)}} - 2 + \ln\left(\sqrt{1 + i_{f(r)}} - 1\right) \qquad V_P \cong \frac{V_{GB} - V_{T0}}{n}$$

DC eqs

If we choose $i_f = 3$





RHS = 0 $V_{GB} = V_{T0}$

$$\frac{V_{DS}}{\phi_t} = \sqrt{1 + i_f} - \sqrt{1 + i_r} + \ln\left(\frac{\sqrt{1 + i_f} - 1}{\sqrt{1 + i_r} - 1}\right)$$

$$g_{ms(d)} = \frac{2I_S}{\phi_t} \left(\sqrt{1 + i_{f(r)}} - 1 \right) \longrightarrow \frac{W}{L} = \frac{g_{ms(d)} \phi_t}{2I_{SH} \left(\sqrt{1 + i_{f(r)}} - 1 \right)}$$

$$g_m = \frac{g_{ms} - g_{md}}{n}$$

$$\frac{g_m}{I_D} = \frac{d(\ln I_D)}{dV_G} = \frac{2}{n\phi_t(\sqrt{1+i_f} + \sqrt{1+i_r})}$$

Small -signal eqs

I_{S} , V_{TO} and n extraction

The g_m/I_D method

Let us choose: $V_{DS} = \frac{\phi_t}{2}$ and $i_f = 3$

$$\frac{V_{DS}}{\phi_t} = \sqrt{1 + i_f} - \sqrt{1 + i_r} + \ln\left(\frac{\sqrt{1 + i_f} - 1}{\sqrt{1 + i_r} - 1}\right)$$

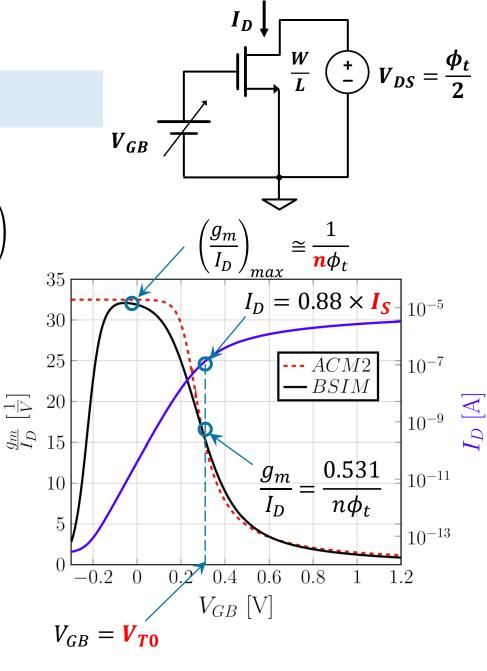
Thus: $i_r = 2.12$

$$\frac{g_m}{I_D} = \frac{d(\ln I_D)}{dV_G} = \frac{2}{n\phi_t(\sqrt{1+i_f} + \sqrt{1+i_r})}$$

$$\frac{g_m}{I_D} = \frac{0.531}{n\phi_t} = 0.531 \left(\frac{g_m}{I_D}\right)_{max}$$

$$I_D = I_S(i_f - i_r)$$

$$I_D = (3 - 2.12) I_S = 0.88 I_S$$



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ACM2: Transconductances in saturation

$$I_{Dsat} = \frac{2I_{S}}{\zeta}q_{dsat} \quad \text{where} \quad \begin{cases} I_{S} = \mu C_{ox}n\frac{\varphi_{t}^{2}W}{2}\frac{W}{L} = I_{SH}\frac{W}{L} \\ q_{dsat} = q_{s} + 1 + \frac{1}{\zeta} - \sqrt{\left(1 + \frac{1}{\zeta}\right)^{2} + \frac{2q_{s}}{\zeta}} \end{cases}$$

Definitions
$$\begin{cases} g_m \triangleq \frac{\partial I_{Dsat}}{\partial V_G} & g_d \triangleq \frac{\partial I_{Dsat}}{\partial V_D} & g_{msat3} \triangleq \frac{\partial^3 I_{Dsat}}{\partial V_G^3} \end{cases}$$

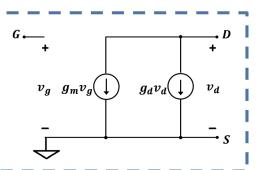
Transconductances in terms of q_s :

$$g_{msat} = \frac{2I_S}{n\phi_t} \frac{q_s}{1 + \zeta(q_s + 1)} \qquad g_{dsat} = \sigma \frac{2I_S}{n\phi_t} \frac{q_s}{1 + \zeta(q_s + 1)} \qquad g_{dsat} = \sigma g_{msat}$$

$$g_{msat3} = \frac{16I_S}{(n\phi_t)^3} \frac{q_S}{(q_S+1)^3} \frac{2 - 2\zeta q_S - 3\zeta q_S^2}{(\zeta q_S+2)^4}$$

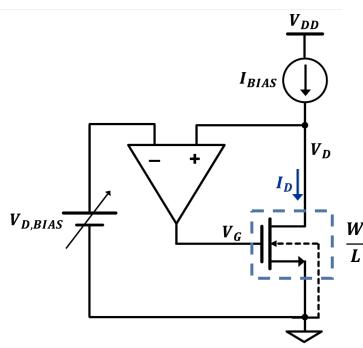
Extraction of σ

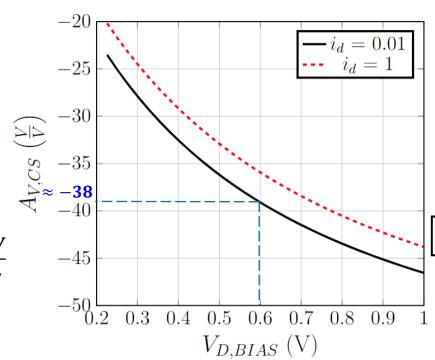
Common-Source Intrinsic-Gain method



In saturation : $g_{dsat} = \sigma g_{msat}$

$$A_{V,CS} = \frac{\Delta v_D}{\Delta v_G} = -\frac{g_{msat}}{g_{dsat}} = \frac{\frac{\partial I_{Dsat}}{\partial V_G}}{\frac{\partial I_{Dsat}}{\partial V_D}} = -\frac{\frac{2I_S}{n\phi_t} \frac{q_S}{1 + \zeta(q_S + 1)}}{\sigma \frac{2I_S}{n\phi_t} \frac{q_S}{1 + \zeta(q_S + 1)}} = -\frac{1}{\sigma}$$





Example:

$$A_{V,CS} = -\frac{1}{\sigma}$$

$$\sigma = -\frac{1}{(-38)}$$

$$\sigma = 0.026$$

ζ extraction

$$i_{dsat} = \frac{2}{\zeta} q_{dsat}$$

$$q_S = \sqrt{1 + \frac{2}{\zeta}q_{dsat}} - 1 + q_{dsat}$$

•
$$q_s$$
 calculated using parameters (V_{T0} , n , σ) and UCCM.

$$\zeta = \frac{2(q_s + 1 - \sqrt{1 + i_{dsat}})}{i_{dsat}}$$

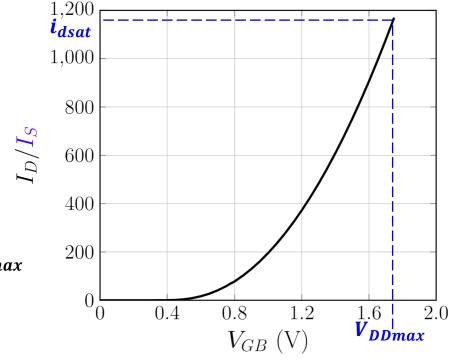


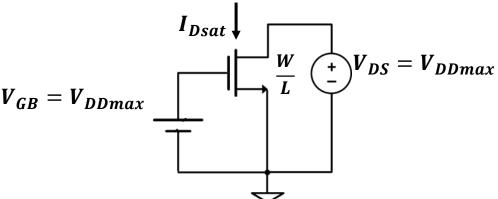
$$V_P = \frac{V_{GB} - V_{T0} + \sigma(V_{DB} + V_{SB})}{n}$$

$$\frac{V_P - V_{S(D)B}}{\phi_t} = q_S - 1 + \ln(q_S)$$

$$I_{Dsat} = I_D(V_G = V_D = V_{DDmax} \text{ and } V_S = V_B)$$

 $i_{dsat} = I_{Dsat}/I_S.$

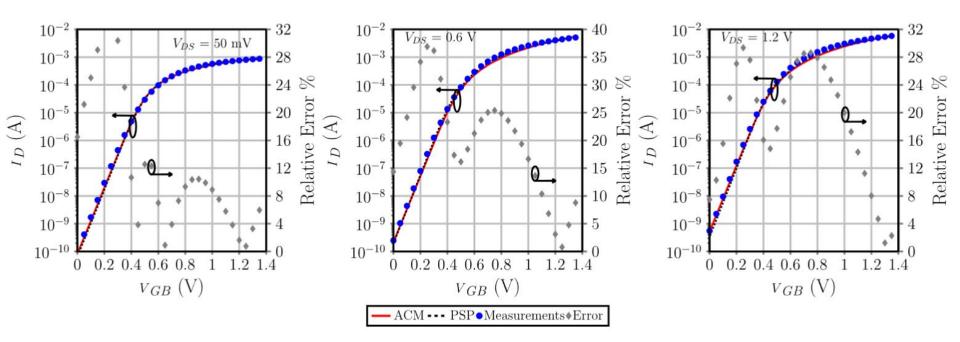




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ACM2¹ vs PSP – 130 nm SiGe IHP² $I_D vs V_{GB}$

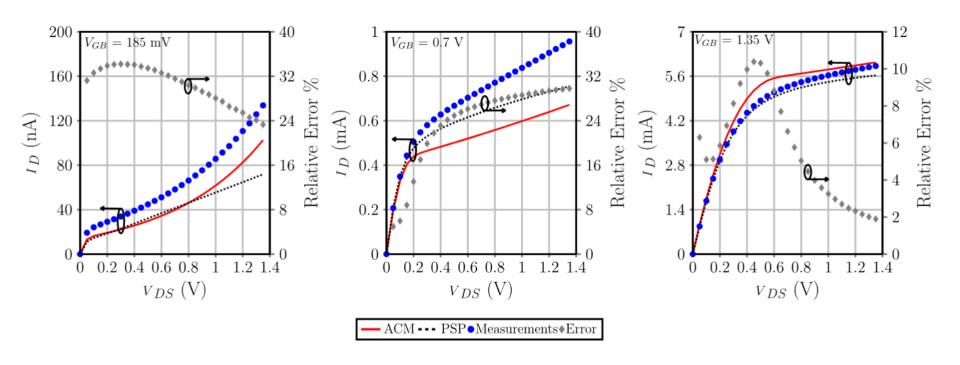


Characteristics of a LVT NMOS bulk transistor with W /L = 10μ m/ 120 nm.

ACM2: implemented in verilog-A, compiled by OPENVAF, simulated in Ngspice

² Institut for High-Performance Microelectronics (IHP) open-source PDK

ACM2¹ vs PSP – 130 nm SiGe IHP² $I_D vs V_{DS}$

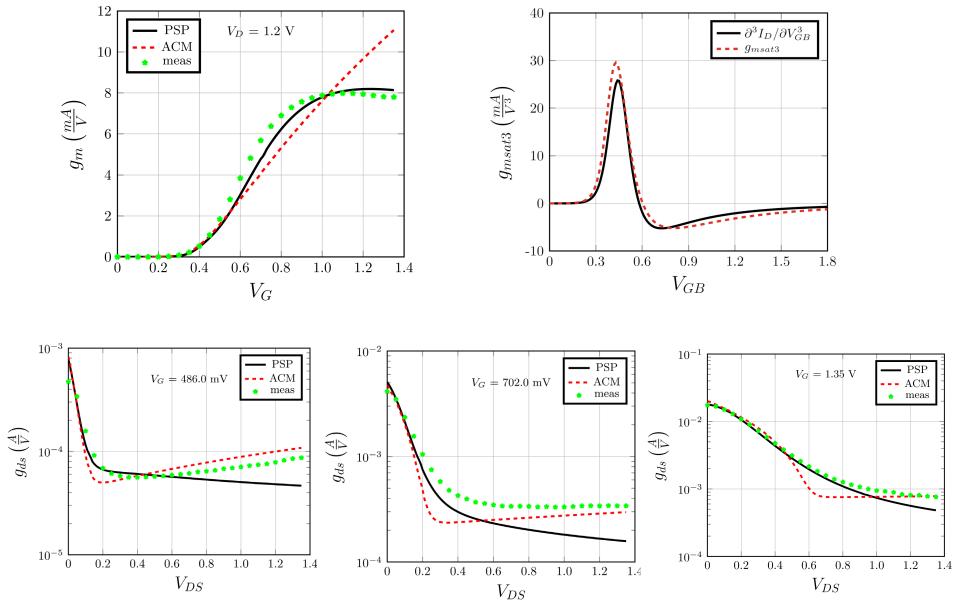


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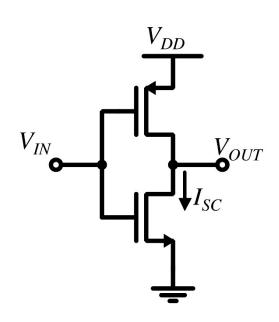
¹ACM2: implemented in verilog-A, compiled by OPENVAF, simulated in Ngspice

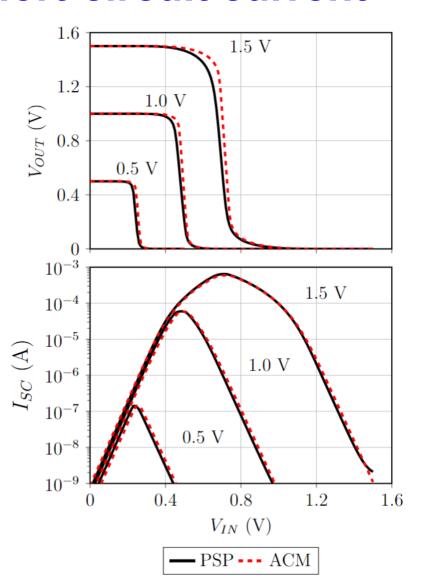
² Institut for High-Performance Microelectronics (IHP) open-source PDK

5PM-ACM2: Transconductance gm, gm3 and gds

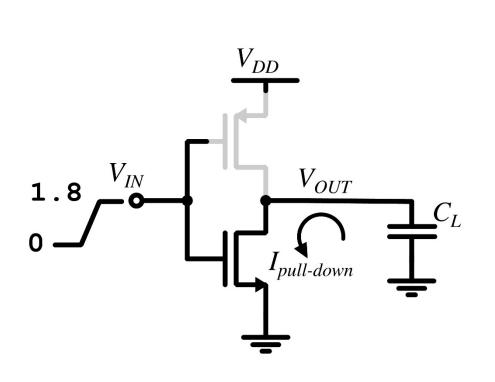


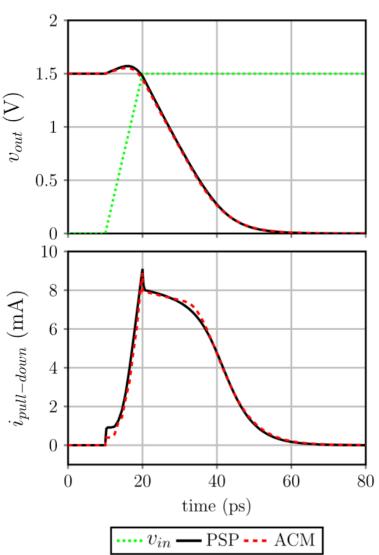
CMOS Inverter in 130 nm bulk VTC and short-circuit current





CMOS Inverter in 130 nm bulk Output Voltage and pull-down current



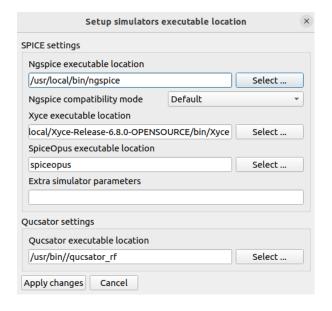


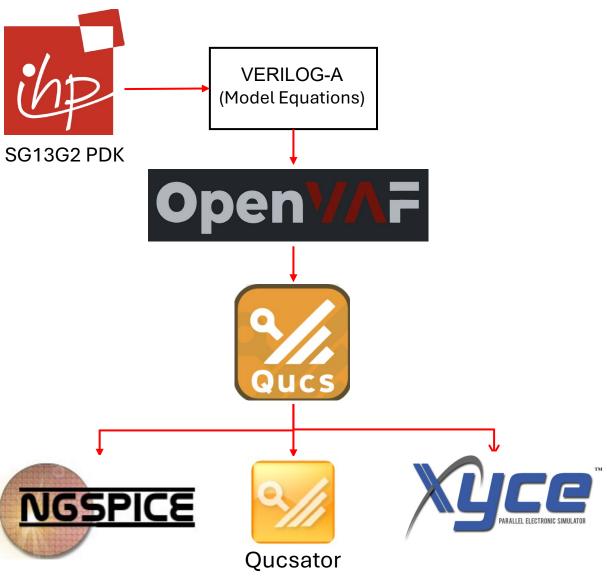
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Qucs-S: Quite universal circuit simulator with SPICE

Simulation setup:



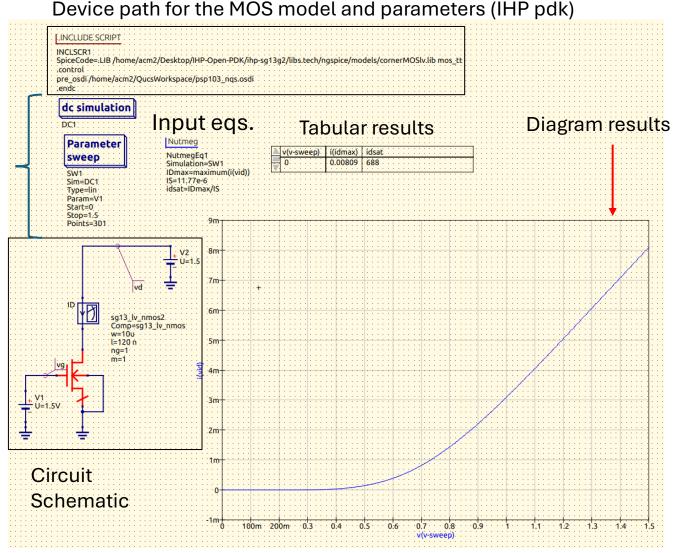


Qucs-S: Quite universal circuit simulator with SPICE

Simulations

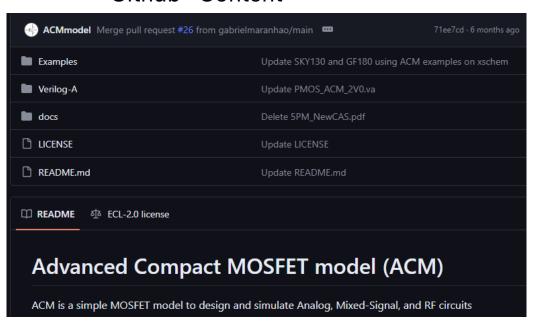
Control

- Ngspice simulations:
 - DC
 - AC
 - TRAN
 - S-parameters
 - Noise
 - Fourier

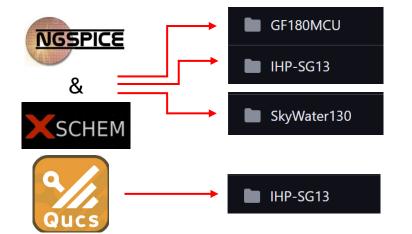


Github - ACM2

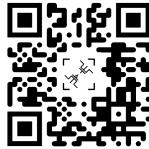
Github - Content



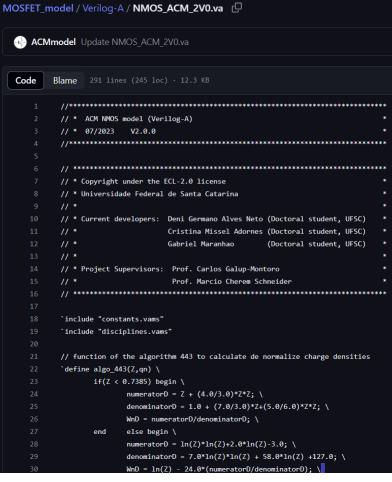
Examples of PDKs and circuit simulators using the ACM model







Verilog-A code Available!



I_{SO} , V_{TO} and n extraction

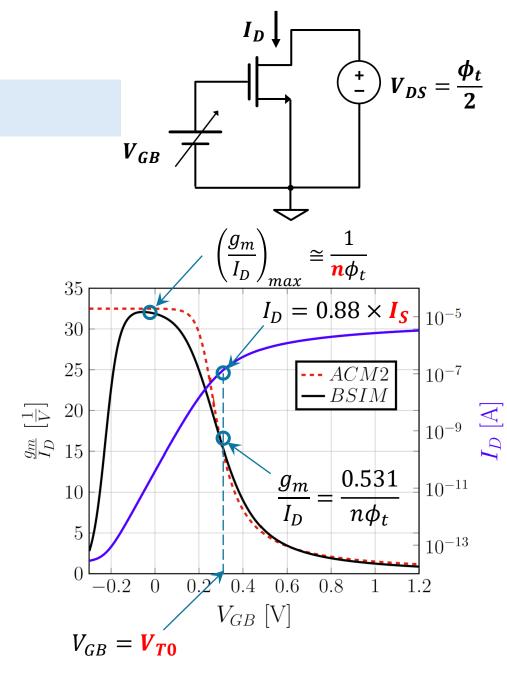
The g_m/I_D method

We identify the
$$\frac{g_m}{I_D}\Big|_{max} \rightarrow n$$

We calculate
$$0.531 \frac{g_m}{I_D}\Big|_{max} \rightarrow V_{TO}$$

We read the value of $I_D \rightarrow I_S$

Practical part → Go to QuCS!



Let's go to Qucs-S!

Useful links:

- Qucs-S oficial page: https://ra3xdh.github.io/
- Qucs-S iterative doc: https://qucs-s-help.readthedocs.io/
- Ngspice oficial page: https://ngspice.sourceforge.io/index.html
- Google Colab: ACM2 & LNA design:

https://colab.research.google.com/drive/1s3PKF6pf3zIhlTj6jcqhCLlcGfJ_UEE?usp=sharing

Summary – The ACM2 model

- A truly compact MOSFET model with single-piece functions
- Implemented in Verilog-A for simulation
- Interchangeable between simulators (SPICE or SPECTRE)
- Verify in all three open-source PDKs (Sky130, GF180, IHP-SG13G2)
- Helpful to designers (only 5-DC-parameters)
- Simplified parameter extraction procedure
 - Accepts parameters extracted from simulations or chip measurements

Acknowledgments









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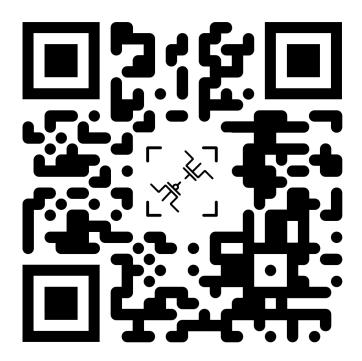
References

- D. Germano Alves Neto et al., "Design-Oriented Single-Piece 5-DC-Parameter MOSFET Model," in IEEE Access, vol. 12, pp. 87420-87437, 2024.
- ACM2 Github: https://github.com/ACMmodel/MOSFET_model
- IHP Github : https://github.com/IHP-GmbH/IHP-Open-PDK

"Scan me"

- Available in Github:
 - DC model
 - Small-signal model
 - Dynamic model
 - Thermal &

Flicker noise models (1/f)



Step-by-Step extraction

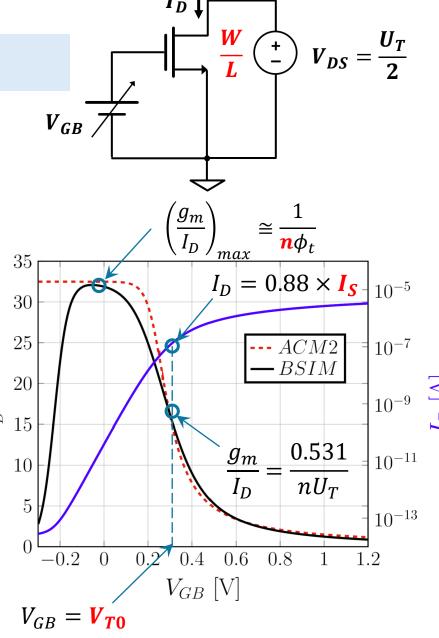
I_{SO} , V_{TO} and n extraction

g_m/I_D method - Steps!

- 1. Assemble the circuit for extraction
- Define the VDS value
- 3. Do a voltage sweep in VGB and measure the drain current ID
- 4. Put on the right side of the plot the ID in semilog y axis
- 5. Plot the gm/ID characteristics using equation in Qucs-s.

$$\frac{g_m}{I_D} = \frac{d(\ln I_D)}{dV_G}$$

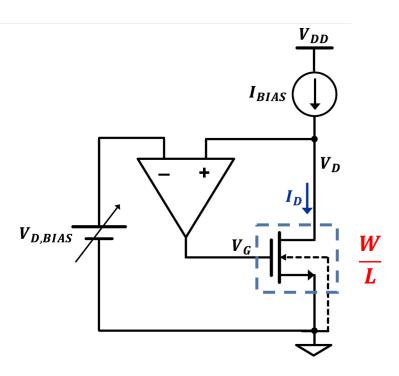
- 6. With a cursor measure the maximum of gm/ID
- 7. With gm/ID(max) multiply it by 0.531 to find the S_{1} point in which VGB = VT0
- 8. IS is the same VGB value but in the ID curve divided by 0.88
- 9. n is extracted from the gm/ID(max) value and ϕ_t = 25.8 mV (room temperature)



σ extraction

Common-Source Intrinsic-Gain method - Steps!

$$A_{V,CS} = \frac{\Delta v_D}{\Delta v_G} = -\frac{g_{msat}}{g_{dsat}} = -\frac{1}{\sigma}$$



- 1. Assemble the circuit for extraction
- 2. Define the IBIAS = 100 nA (weak inversion)
- Use Qucs-S equations to calculate the derivate of vd and vg
- 4. Using equations set the equation for sigma
- 5. Do a voltage sweep in VD,BIAS from 0.2 V to 1 V
- 6. With a cursor measure the value for sigma at VD = VDDmax/3

ζ extraction

Saturation method - Steps!

- 1. Assemble the circuit for extraction
- 2. Define $V_G = V_D = V_{DDmax}$ and $V_S = V_B$ = 0 V
- 3. Using equations set the equation for i_{dsat} = I_{Dsat}/I_{S0}
- 4. Insert a table in Qucs-s to evaluate i_{dsat}

Google Colab: ACM2 & LNA design:

https://colab.research.google.com/drive/1s3PK F6pf3zIhlTj6jc-qhCLlcGfJ_UEE?usp=sharing

5. Using the Colab, in the section Zeta extraction, we will insert the value of the appropriate idsat for the python code which calculate qs transcendant equation and then zeta!

