



BNEN NTH pressure drop exam challenge

- Academic year 2025-2026
- v1.0
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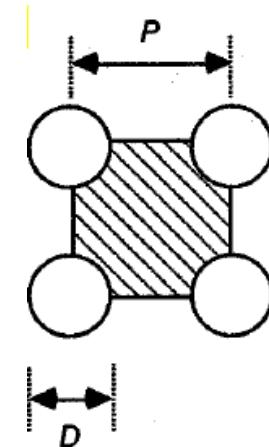
BNEN NTH pressure drop exam challenge

- A typical subchannel in a BWR reactor operates under the following conditions:

- Up-flow of water
- Inlet temperature = $T_{sat}(p_{in}) - 40^\circ\text{C}$
- Inlet pressure = 5500 kPa
- Heated length

- $L = 3.1 \text{ m}$ thus from $\frac{L}{2} = -1.55 \text{ m}$ to $\frac{L}{2} = 1.55 \text{ m}$

- Rod diameter = 10.3 mm and Pitch = 21.2 mm
- Relative wall roughness (λ/D_e) = 0.001
- Average heat flux for one pin = 2.4 MW/m²
- Axial heat flux distribution = cosine



- Plot the total pressure drop and its individual components in function of the mass flow rate through the subchannel



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SINGLE HEATED CHANNEL: STEADY-STATE ANALYSIS 607

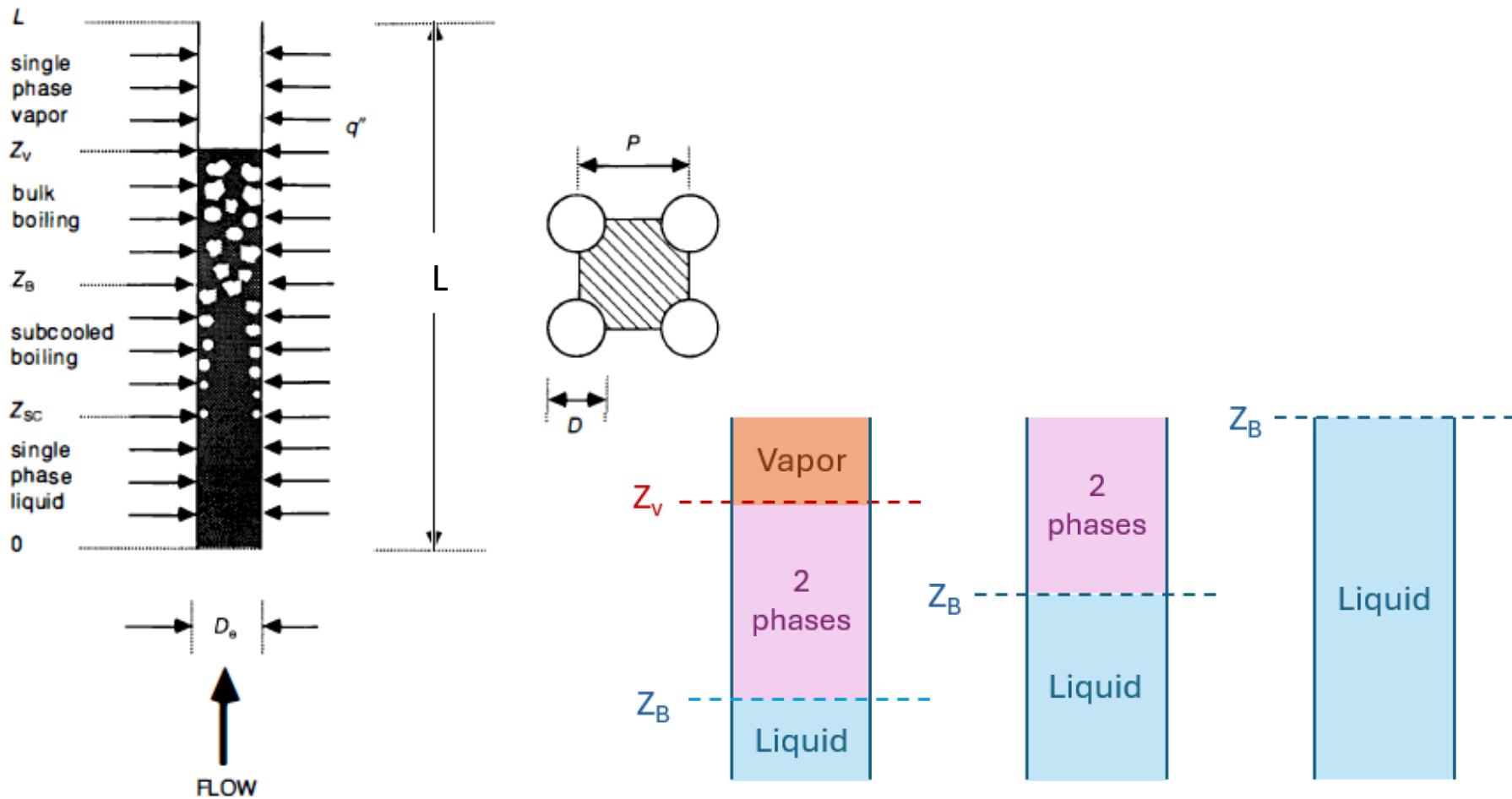


Figure 13-13 Subchannel flow region (left) and cross section (right).

Figure adopted from Brieux and Wlodarski 2024



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■ Day 3-5: Exam challenge

- Plot the total pressure drop through the subchannel and its individual components in function of the mass flow rate
 - For the range [0-2.5 kg/s]
 - Use McAdams correlation for the two phase pressure drop and Coolebrook for the monophase pressure drop
 - Assume constant material properties and use the inlet pressure to calculate those for the subcooled region
 - E.g. Four graphs (liquid, two phase, vapour, total) with each three components (acceleration, gravity and friction) - see example 13-4 of Todreas and Kazimi volume 1 old edition
- Extra
 - Plot z_B and z_V in terms of mass flow
 - Plot equilibrium and flow quality in terms of height for a mass flow of 0,1 kg/s
 - Which parameter can you change in order to (not) have an 'S' curve as shape? Explain why.
 - Use Jones' correlation as alternative for the two phase friction pressure drop (see p. 503 & 611 Todreas and Kazimi vol. 1 old ed.)
- Report requirements
 - Only report total pressure drop and its individual components in function of the mass flow rate through the subchannel
 - Reporting on extra's = bonus points
 - No reporting of exercises done on day 1-2
 - Focus
 - Assumptions that have been made and where e.g. formulas have been found
 - Explanation on the graph and formulas
 - Correctness of output
 - Lay-out is of minor importance
 - Maximum two students for one report



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- Day 1-2: guided exercises as support for the exam challenge
- Day 1: for a mass flow range [0 -> 2.5] kg/s
 - Calculate friction monophase pressure drop through the channel without heating
 - A First do this for a pipe diameter $D = 0.02 \text{ m}$ and with McAdams
 - B Then do it for the actual BWR subchannel and with McAdams
 - C Finally, do the same for the actual BWR subchannel and with Coolebrooke
 - Calculate two phase pressure drop through the channel
 - D First assume the inlet equilibrium quality is 0.15 and the channel is adiabatic (no heating)
 - E Then assume the inlet and outlet equilibrium quality are 0 and 0.15 respectively. Thus instead of using a heat flux as input it is assumed that the quality evolves linearly from inlet to outlet.
- Day 2: for a mass flow of 0.1 kg/s
 - A Find axial position where the equilibrium quality is zero:
 - This bulk boiling point (z_B)
 - Assume cosine axial heat distribution neglecting pressure drop for material properties
 - B Find axial position where the flow (dynamic quality) is one
 - This is where we have saturated vapour (z_V)
 - C Extra
 - Find axial position where the flow (dynamic quality) is zero: bubble detachment (z_D)
 - Plot the thermodynamic and flow quality at different heights (-L/2 to L/2) and use Levy's correlation
 - Find the position of maximum wall temperature



Day 1 – guidance for solution

■ Numerical modeling

- Discretization over height versus functions ?
- Will you use AI ?

■ Material properties

- See next slides



Day 1 – guidance for solution

■ Matlab Xsteam (also see example script)

```
%inlet properties

rho_in_L=XSteam('rho_pT',p_in_bar,T_in); %kg/m^3
mu_in_L=XSteam('my_pT',p_in_bar,T_in); %absolute/dynamic Pa s of kg/m/s
Cp_in_L=XSteam('Cp_pT',p_in_bar,T_in)*10^3; %J.kg°C

h_in=XSteam('h_pT',p_in_bar,T_in)*10^3; !! 

% properties at saturation at inlet

rho_satG_in=XSteam('rhoV_p',p_in_bar); %( kg/ m3)
rho_satL_in=XSteam('rhoL_p',p_in_bar); %( kg/ m3)
```

■ What is inlet temperature?



Day 1 – guidance for solution

■ Python IAPWS97

```
from iapws import IAPWS97 # requires pip install iapws numpy matplotlib
Tsat_in = IAPWS97(P=Pin_MPa, x=0).T # saturation temperature at inlet pressure
# fluid properties at inlet
fluid = IAPWS97(P=P, T=Tin+273.15) # [ K ]
rho = fluid.rho
h = fluid.h # [ kJ/kg ] !!
```

■ Python XSteam

```
from pyXSteam.XSteam import XSteam
steamTable = XSteam(XSteam.UNIT_SYSTEM_MKS) # m/kg/sec/°C/bar/W
```

Xsteam Install run the following in the console of for instance spyder
'python3 setup.py install'
OR
'pip install XSteamPython'



Day 1 – guidance for solution

■ Python XSteam

```
rho=steamTable.rho_pt(p_bar,T_C)      #( kg/ m3)
mu=steamTable.my_pt(p_bar,T_C)        # absolute/dynamic Pa.s
Cp=steamTable.Cp_pt(p_bar,T_C)*1000   # J/(kg*K)
k=steamTable.tc_pt(p_bar,T_C)         # W/mK
```

!!

```
h     =steamTable.h_pt(p_bar,T_C)*1000 # J/kg
```

```
roperties at saturation
Tsat_C  =steamTable.tsat_p(p_bar)    # °C
st_w    =steamTable.st_p(p_bar)       # N/m
rho_G   =steamTable.rhoV_p(p_bar)    # ( kg/ m3)
rho_L   =steamTable.rhoL_p(p_bar)    # ( kg/ m3)
h_sat_L =steamTable.hL_p(p_bar)*1000 # J/kg
h_sat_G =steamTable.hV_p(p_bar)*1000 # J/kg
```

Approach to get
viscosity of
saturated liquid

```
mu_satL  =steamTable.my_pt(p_bar,self.Tsat_C*.99)  # absolute/dynamic Pa.s of kg/m/s
muV=XSteam('my_pT',pLibbar,TsatLib*.101); %absolute/dynamic
k_satL   =steamTable.tcL_p(p_bar)                  # W/(m °C)
Cp_satL  =steamTable.CpL_t(p_bar)*1000            # J/(kg*K)
```