



BNEN NTH pressure drop exam challenge

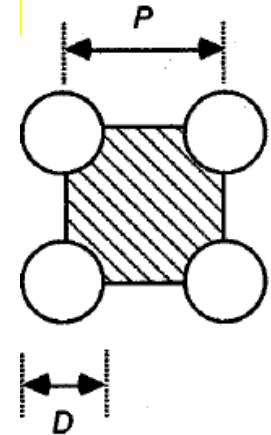
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- v1.0
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BNEN NTH pressure drop exam challenge

- A typical subchannel in a BWR reactor operates under the following conditions:

- Up-flow of water
- Inlet temperature = $T_{sat}(p_{in}) - 40^{\circ}\text{C}$
- Inlet pressure = 5500 kPa
- Heated length
 - $L = 3.1\text{ m}$ thus from $\frac{L}{2} = -1.55\text{ m}$ to $\frac{L}{2} = 1.55\text{ m}$
- Rod diameter = 10.3 mm and Pitch = 21.2 mm
- Relative wall roughness $(\lambda/D_e) = 0.001$
- Average heat flux for one pin = 2.4 MW/m^2
- Axial heat flux distribution = cosine



- Plot the total pressure drop and its individual components in function of the mass flow rate through the subchannel



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SINGLE HEATED CHANNEL: STEADY-STATE ANALYSIS 607

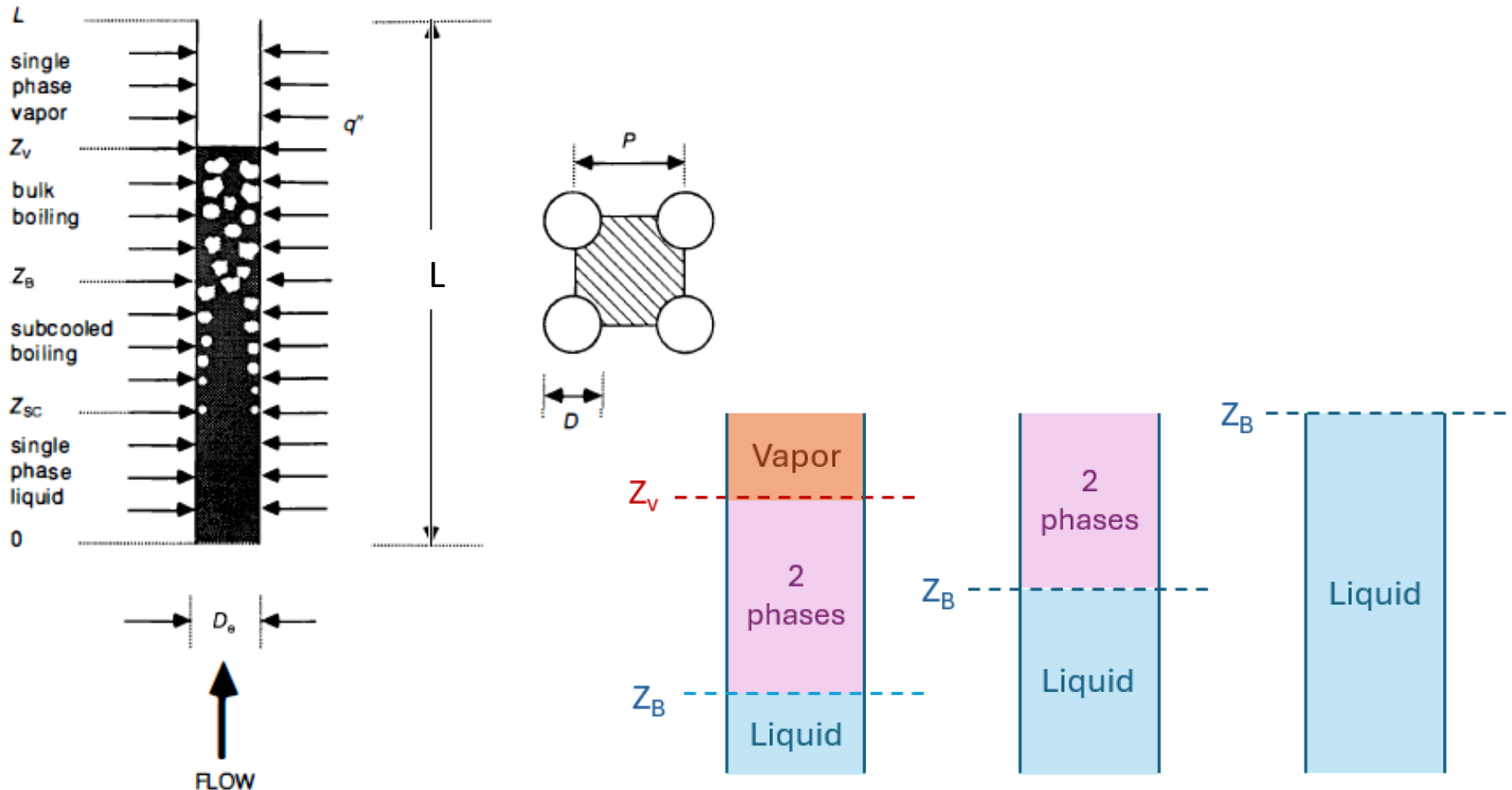


Figure 13-13 Subchannel flow region (left) and cross section (right).

Figure adopted from Brieux and Wlodarski 2024



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■ Day 3-5: Exam challenge

- Plot the total pressure drop through the subchannel and its individual components in function of the mass flow rate
 - For the range [0-2.5 kg/s]
 - Use McAdams correlation for the two phase pressure drop and Coolebrook for the monophasic pressure drop
 - Assume constant material properties and use the inlet pressure to calculate those for the subcooled region
 - E.g. Four graphs (liquid, two phase, vapour, total) with each three components (acceleration, gravity and friction) - see example 13-4 of Todreas and Kazimi volume 1 old edition
- Extra
 - Plot z_B and z_V in terms of mass flow
 - Plot equilibrium and flow quality in terms of height for a mass flow of 0,1 kg/s
 - Which parameter can you change in order to (not) have an 'S' curve as shape? Explain why.
 - Use Jones' correlation as alternative for the two phase friction pressure drop (see p. 503 & 611 Todreas and Kazimi vol. 1 old ed.)
- Report requirements
 - Only report total pressure drop and its individual components in function of the mass flow rate through the subchannel
 - Reporting on extra's = bonus points
 - No reporting of exercises done on day 1-2
 - Focus
 - Assumptions that have been made and where e.g. formulas have been found
 - Explanation on the graph and formulas
 - Correctness of output
 - Lay-out is of minor importance
 - Maximum two students for one report



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- Day 1-2: guided exercises as support for the exam challenge
- Day 1: for a mass flow range $[0 \rightarrow 2.5]$ kg/s
 - Calculate friction monophasic pressure drop through the channel without heating
 - A First do this for a pipe diameter $D = 0.02$ m and with McAdams
 - B Then do it for the actual BWR subchannel and with McAdams
 - C Finally, do the same for the actual BWR subchannel and with Coolebrooke
 - Calculate two phase pressure drop through the channel
 - D First assume the inlet equilibrium quality is 0.15 and the channel is adiabatic (no heating)
 - E Then assume the inlet and outlet equilibrium quality are 0 and 0.15 respectively. Thus instead of using a heat flux as input it is assumed that the quality evolves linearly from inlet to outlet.
- Day 2: for a mass flow of 0.1 kg/s
 - A Find axial position where the equilibrium quality is zero:
 - This bulk boiling point (z_B)
 - Assume cosine axial heat distribution neglecting pressure drop for material properties
 - B Find axial position where the flow (dynamic quality) is one
 - This is where we have saturated vapour (z_V)
 - C Extra
 - Find axial position where the flow (dynamic quality) is zero: bubble detachment (z_D)
 - Plot the thermodynamic and flow quality at different heights ($-L/2$ to $L/2$) and use Levy's correlation
 - Find the position of maximum wall temperature



Day 1 – guidance for solution

■ Numerical modeling

- Discretization over height versus functions ?
- Will you use AI ?

■ Material properties

- See next slides



Day 1 – guidance for solution

■ Matlab Xsteam (also see example script)

```
%inlet properties

rho_in_L=XSteam('rho_pT',p_in_bar,T_in); %kg/m^3
mu_in_L=XSteam('mu_pT',p_in_bar,T_in); %absolute/dynamic Pa s of kg/m/s
Cp_in_L=XSteam('Cp_pT',p_in_bar,T_in)*10^3; %J.kg°C

h_in=XSteam('h_pT',p_in_bar,T_in)*10^3;

% properties at saturation at inlet

rho_satG_in=XSteam('rhoV_p',p_in_bar); %( kg/ m3)
rho_satL_in=XSteam('rhoL_p',p_in_bar); %( kg/ m3)
```

!!

■ What is inlet temperature?



Day 1 – guidance for solution

■ Python IAPWS97 [MPa]

```
from iapws import IAPWS97 # requires pip install iapws numpy matplotlib
Tsat_in = IAPWS97(P=Pin_MPa, x=0).T # saturation temperature at inlet pressure

# fluid properties at inlet
fluid = IAPWS97(P=P, T=Tin+273.15)
rho = fluid.rho
h = fluid.h
```

[K]

[kJ/kg] !!

■ Python XSteam

```
from pyXSteam.XSteam import XSteam
steamTable = XSteam(XSteam.UNIT_SYSTEM_MKS) # m/kg/sec/°C/bar/W
```

```
Xsteam Install run the following in the console of for instance spyder
'python3 setup.py install'
OR
'pip install XSteamPython'
```




Day 1 – guidance for solution

Python XSteam

```
rho=steamTable.rho_pt(p_bar,T_C)      #( kg/ m3)
mu=steamTable.mu_pt(p_bar,T_C)        # absolute/dynamic Pa.s
Cp=steamTable.Cp_pt(p_bar,T_C)*1000  # % J/(kg*K)
k=steamTable.k_pt(p_bar,T_C)         # W/mK
```

```
h      =steamTable.h_pt(p_bar,T_C)*1000 # J/kg

perties at saturation
Tsats_C =steamTable.tsat_p(p_bar)      # °C
st_w     =steamTable.st_p(p_bar)        # N/m
rho_G     =steamTable.rhoV_p(p_bar)     # ( kg/ m3)
rho_L     =steamTable.rhoL_p(p_bar)     # ( kg/ m3)
h_sat_L   =steamTable.hL_p(p_bar)*1000 # J/kg
h_sat_G   =steamTable.hV_p(p_bar)*1000 # J/kg
```

```
mu_satL   =steamTable.mu_pt(p_bar,self.Tsat_C*.99) # absolute/dynamic Pa s of kg/m/s
muV=XSteam('my_pT',pLibbar,TsatLib*.101); %absolute/dynamic
k_satL    =steamTable.kL_p(p_bar)         # W/(m °C)
Cp_satL   =steamTable.CpL_t(p_bar)*1000   # J/(kg*K)
```

Approach to get
viscosity of
saturated liquid