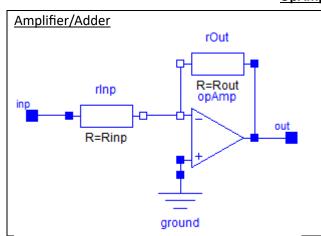
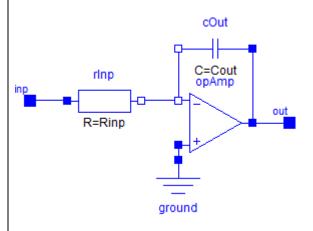
OpAmp-Circuits



$$\begin{split} &\frac{inp.\,v}{R_{inp}} + \frac{out.\,v}{R_{out}} = 0\\ &-out.\,v = k \cdot inp.\,v\\ &k = \frac{R_{out}}{R_{inp}} \end{split}$$

It is possible to add several inputs.

Integrator



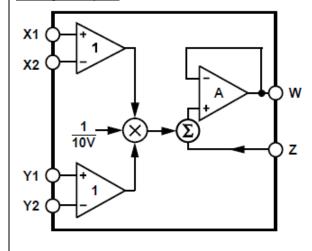
$$\frac{inp.v}{R_{inp}} + C_{out} \cdot \frac{d \ out.v}{dt} = 0$$

$$-out.v = v_0 + \frac{1}{\tau} \cdot \int_0^t inp.v \cdot dt$$

$$\tau = R_{inp} \cdot C_{out}$$

 $\tau = R_{inp} \cdot \mathcal{C}_{out}$ It is possible to integrate the sum of several inputs.

Analog Multiplier



Functional Block Diagram of AD633 Division by 10 V (scaling) inhibits overflow. Additional summing input Z is omitted. Negative inputs of X- and Y-amplifiers are connected to ground.

Possible implementations:

- Gilbert cell
- $y = e^{\ln(x_1) + \ln(x_2)}$ $y = \frac{(x_1 + x_2)^2 (x_1 x_2)^2}{4}$

1_Lotka-Volterra

https://en.wikipedia.org/wiki/Lotka%E2%80%93Volterra_equations https://en.wikipedia.org/wiki/Competitive_Lotka%E2%80%93Volterra_equations https://sprott.physics.wisc.edu/pubs/paper288.pdf

As a 2-dimensional predator-prey-model no chaos is reported:

$$\frac{dx}{dt} = r_x \cdot x - d_x \cdot x \cdot y$$
$$\frac{dy}{dt} = r_x \cdot x \cdot e_y \cdot y - d_y \cdot y$$

We might interpret x as number of hares (prey) and y as foxed (predator).

 r_{x} is the reproduction rate of hares, d_{x} the deathrate of hares due to foxes.

 $\emph{e}_\emph{y}$ is the efficiency in growing foxes from hares, $\emph{d}_\emph{y}$ the (natural) deathrate of foxes.

A n-dimensional Lotka-Volterra model is defined for $1 \le i \le n$ (n designates the number of species):

$$\frac{dx_i}{dt} = r_i \cdot x_i \cdot \left(1 - \sum_{j=1}^n a_{ij} \cdot x_j\right)$$

The vector [r] describes the reproduction rates of the species whereas the quadratic matrix [a] describes the competition between species.

2_Lorenz System

http://en.wikipedia.org/wiki/Lorenz attractor

Developed 1963 by Edward Lorenz to model atmospheric convection.

x is proportional to the rate of convection, y to the horizontal temperature variation and z to the vertical temperature variation. σ depicts the Prandtl number, ρ the Rayleigh number and β the physical dimensions.

The original parameters were:
$$\sigma=10, \rho=28, \beta=\frac{8}{3}$$

$$\frac{dx}{dt}=\sigma\cdot(y-x)$$

$$\frac{dy}{dt}=x\cdot(\rho-z)-y$$

$$\frac{dz}{dt}=x\cdot y-\beta\cdot z$$

 $\beta = \frac{1}{3}$ leads to a periodic solution.

For an implementation as an electronic circuit, the equations have to be scaled to keep the variables within the desired range. This can be compared with calculating per-unit values by dividing by reference values:

$$x' = \frac{x}{k_x}$$
$$y' = \frac{y}{k_y}$$
$$z' = \frac{z}{k_z}$$
$$t' = \frac{t}{\tau}$$

We also have to take into account that the analog multiplier divides by E_R to avoid overflow of the output. After that, none of the computing block should encounter an overflow.

This leads to the following set of equations:

$$\begin{split} &\frac{1}{\tau} \cdot \frac{dx'}{dt'} = -\sigma \cdot x' + \sigma \cdot \frac{k_y}{k_x} \cdot y' \\ &\frac{1}{\tau} \cdot \frac{dy'}{dt'} = \rho \cdot \frac{k_x}{k_y} \cdot x' - y' - \frac{k_x \cdot k_z \cdot V_S}{k_y} \cdot \frac{x' \cdot z'}{V_S} \\ &\frac{1}{\tau} \cdot \frac{dz'}{dt'} = \frac{k_x \cdot k_y \cdot V_S}{k_z} \cdot \frac{x' \cdot y'}{V_S} - \beta \cdot z' \end{split}$$

These equations can easily get implemented as blocks or as an electronic circuit.

3_Roessler System

https://en.wikipedia.org/wiki/R%C3%B6ssler attractor

A simple system of 3 ordinary nonlinear differential equations to study chaos without physical background.

$$\frac{dx}{dt} = -y - z$$

$$\frac{dy}{dt} = x + a \cdot y$$

$$\frac{dz}{dt} = b + (x - c) \cdot z$$

a=0.2, b=0.2 and c=1 give periodic results. Changing c=5.7 reveals chaotic results.

For an implementation as an electronic circuit, the equations have to be scaled to keep the variables within the desired range. This can be compared with calculating per-unit values by dividing by reference values:

$$x' = \frac{x}{k_x}$$

$$y' = \frac{y}{k_y}$$

$$z' = \frac{z}{k_z}$$

$$t' = \frac{t}{\tau}$$

We also have to take into account that the analog multiplier divides by E_R to avoid overflow of the output. After that, none of the computing block should encounter an overflow.

This leads to the following set of equations:

$$\frac{1}{\tau} \cdot \frac{dx'}{dt} = -\frac{k_y}{k_x} \cdot y' - \frac{k_z}{k_x} \cdot z'$$

$$\frac{1}{\tau} \cdot \frac{dy'}{dt} = \frac{k_x}{k_y} \cdot x' + a \cdot y'$$

$$\frac{1}{\tau} \cdot \frac{dz'}{dt} = \frac{b}{k_z} + k_x \cdot V_S \cdot \frac{x' \cdot z'}{V_S} - c \cdot z'$$

These equations can easily get implemented as blocks or as an electronic circuit.

4_Chua's Circuit

https://link.springer.com/book/10.1007/978-3-319-05900-6 (1.1)

https://nonlinear.eecs.berkeley.edu/chaos/chaos.html# Working With Chaos Simulation

$$L \cdot \frac{di_L}{dt} = v_2 - R_L \cdot i_L$$

$$C_2 \cdot \frac{dv_2}{dt} = -i_L - \frac{v_2 - v_1}{R}$$

$$C_1 \cdot \frac{dv_1}{dt} = -i_{NL} + \frac{v_2 - v_1}{R}$$

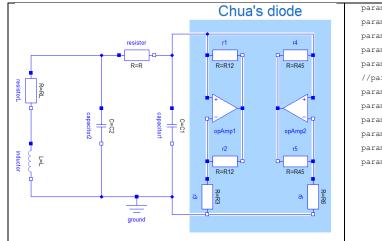
$$-i_{NL}(v_1) = \begin{cases} -\infty < v_1 < -V_e \to G_b \cdot (v_1 + V_e) - G_a \cdot V_e \\ -V_e < v_1 < +V_e \to G_a \cdot v_1 \\ +V_e < v_1 < +\infty \to G_b \cdot (v_1 - V_e) + G_a \cdot V_e \end{cases}$$

$$-\frac{i_{NL}}{v_1} = \begin{cases} -\infty < v_1 < -V_e \to G_b - (G_a - G_b) \cdot \frac{V_e}{v_1} \\ -V_e < v_1 < +V_e \to G_a \\ +V_e < v_1 < +\infty \to G_b + (G_a - G_b) \cdot \frac{V_e}{v_1} \end{cases}$$

$$-\frac{di_{NL}}{dv_1} = \begin{cases} -\infty < v_1 < -V_e \to G_b \\ -V_e < v_1 < +V_e \to G_a \\ +V_e < v_1 < +V_e \to G_a \end{cases}$$

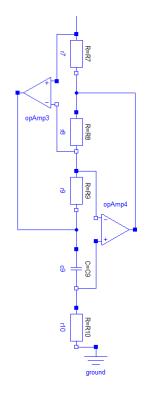
$$+V_e < v_1 < +V_e \to G_b$$

$$\begin{split} \tau_L \cdot \dot{v}_{RL} &= v_2 - v_{RL} \\ \tau_2 \cdot \dot{v}_2 &= +v_1 - v_2 - \frac{R}{R_L} \cdot v_{RL} \\ \tau_1 \cdot \dot{v}_1 &= -v_1 + v_2 + R \cdot g \cdot v_1 \\ g(v_1) &= \begin{cases} |v_1| > V_e \to G_b + (G_a - G_b) \cdot \frac{V_e}{|v_1|} \\ |v_1| < V_e \to G_a \end{cases} \end{split}$$



parameter SI.Resistance R=1.9e3 "Resistor";
parameter SI.Inductance L=18e-3 "Inductor";
parameter SI.Resistance RL=14 "Resistance of Inductor";
parameter SI.Capacitance C1=10.e-9 "Capacitor 1";
parameter SI.Capacitance C2=100e-9 "Capacitor 2";
//parameter of Chua's diode
parameter Real k0=15000.0 "No-load amplification ";
parameter SI.Voltage Vs=9 "Supply voltage of opAmps";
parameter SI.Resistance R12=220 "R1 and R2";
parameter SI.Resistance R3=2200 "R3";
parameter SI.Resistance R45=22e3 "R4 and R5";
parameter SI.Resistance R6=3300 "R6";

Chua's Circuit: Inductor Replacement



$$R_7 = 100 \Omega$$

$$R_8 = 1 k\Omega$$

$$R_9 = 1 k\Omega$$

$$R_{10} = 1.8 k\Omega$$

$$C_9 = 100 nF$$

$$R_7 \cdot i + R_8 \cdot (i + i_{OA4}) = 0$$

$$R_9 \cdot (i + i_{OA4}) + v_{C9} = 0$$

$$i + i_{OA4} + i_{OA3} = i_{C9}$$

$$i_{C9} = C_9 \cdot \frac{dv_{C9}}{dt}$$

$$v = R_{10} \cdot i_{C9}$$

$$(i + i_{OA4}) = -\frac{R_7}{R_8} \cdot i$$

$$v_{c9} = \frac{R_7 \cdot R_9}{R_8} \cdot i$$

$$i_{C9} = C_9 \cdot \frac{R_7 \cdot R_9}{R_8} \cdot \frac{di}{dt}$$

$$v = C_9 \cdot \frac{R_7 \cdot R_9 \cdot R_{10}}{R_8} \cdot \frac{di}{dt}$$

$$L = C_9 \cdot \frac{R_7 \cdot R_9 \cdot R_{10}}{R_8} = 18 \text{ mH}$$

$$L = C_9 \cdot \frac{R_7 \cdot R_9 \cdot R_{10}}{R_8} = 18 \, mF$$

5_Chaotic Diode Circuit

https://www.researchgate.net/publication/309351711 A simple chaotic circuit with a light-emitting diode

$$C \cdot \frac{dv_1}{dt} = -\frac{v_2}{R}$$

$$C \cdot \frac{dv_2}{dt} = -\frac{v_3}{R}$$

$$C \cdot \frac{dv_3}{dt} = -\frac{v_1}{R} - \frac{v_3}{R_b} - \frac{v_4}{R}$$

$$\frac{v_4}{R_a} = -I_{ds} \cdot \left(e^{\frac{v_2}{nV_t}} - 1\right)$$

$$\tau = R \cdot C$$

$$\tau \cdot \frac{dv_1}{dt} = -v_2$$

$$\tau \cdot \frac{dv_2}{dt} = -v_3$$

$$\tau \cdot \frac{dv_3}{dt} = -v_1 - \frac{R}{R_h} \cdot v_3 + R_a \cdot I_{ds} \cdot \left(e^{\frac{v_2}{nV_t}} - 1\right)$$

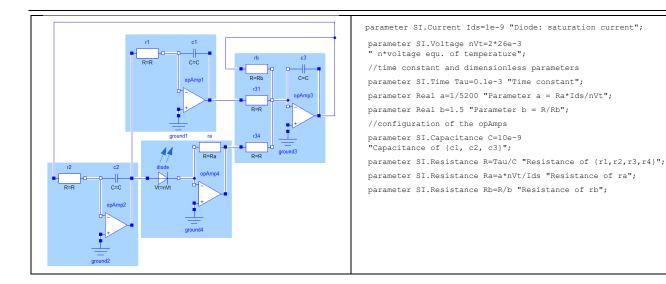
$$a = \frac{R_a \cdot I_{ds}}{nV_t}$$

$$b = \frac{R}{R_b}$$

$$\tau \cdot \dot{x}_1 = -x_2$$

$$\tau \cdot \dot{x}_2 = -x_3$$

$$\tau \cdot \dot{x}_3 = -x_1 + a \cdot (e^{x_2} - 1) - b \cdot x_3$$



6_Chaotic Oscillator

https://www.researchgate.net/publication/230925506_A_simple_chaotic_oscillator_for_educational_purposes
https://www.researchgate.net/publication/259216097_NUMERICAL_TREATMENT_OF_EDUCATIONAL_CHAOS_OSCILLATOR

$$\begin{split} i_L &= C \cdot \frac{dv_C}{dt} \\ L \cdot \frac{di_L}{dt} &= \left(k - 1 - \frac{R_L}{R}\right) \cdot R \cdot i_L - v_C - v_{C^*} \\ k &= 1 + \frac{R_2}{R_1} \\ C^* \cdot \frac{dv_{C^*}}{dt} &= I_0 + i_L - I_{DS} \cdot \left(e^{\frac{v_{C^*}}{nV_t}} - 1\right) \\ I_0 &\approx \frac{V_b}{R_0} \end{split}$$

$$\tau = \sqrt{L \cdot C}$$

$$Z = \sqrt{\frac{L}{C}}$$

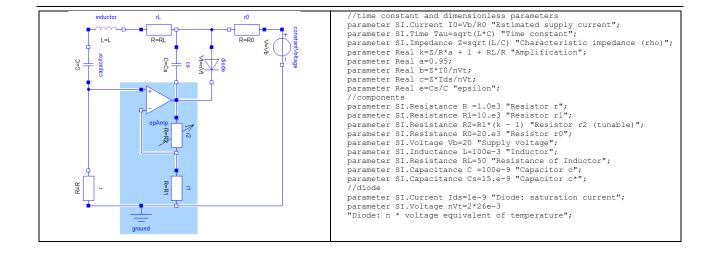
$$a = \left(k - 1 - \frac{R_L}{R}\right) \cdot \frac{R}{Z}$$

$$b = \frac{Z \cdot I_0}{nV_t}$$

$$c = \frac{Z \cdot I_{DS}}{nV_t}$$

$$e = \frac{C^*}{C}$$

$$\begin{split} \tau \cdot \frac{\dot{v}_C}{nV_t} &= \frac{Z \cdot i_L}{nV_t} \\ \tau \cdot \frac{Z \cdot i_L}{nV_t} &= \left(k - 1 - \frac{R_L}{R}\right) \cdot \frac{R}{Z} \cdot \frac{Z \cdot i_L}{nV_t} - \frac{v_C}{nV_t} - \frac{v_{C^*}}{nV_t} \\ \tau \cdot e \cdot \frac{\dot{v}_{C^*}}{nV_t} &= \frac{Z \cdot I_0}{nV_t} + \frac{Z \cdot i_L}{nV_t} - \frac{Z \cdot I_{DS}}{nV_t} \cdot \left(e^{\frac{v_{C^*}}{nV_t}} - 1\right) \end{split}$$



7_Colpitts Oscillator

https://link.springer.com/book/10.1007/978-3-319-05900-6 (1.3)

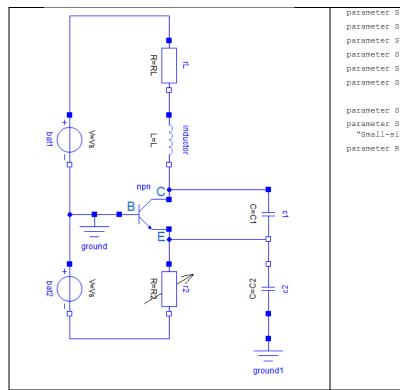
https://ieeexplore.ieee.org/document/331536

$$C_1 \cdot \frac{dv_1}{dt} = i_L - \beta \cdot i_B$$

$$C_2 \cdot \frac{dv_2}{dt} = -\frac{V_{s-} + v_2}{R_2} - i_L - i_B$$

$$L \cdot \frac{di_L}{dt} = V_{s+} - v_1 + v_2 - R_L \cdot i_L$$

$$i_B = \begin{cases} v_2 = v_{BE} \le V_{th} \to & 0 \\ v_2 = v_{BE} > V_{th} \to & \frac{v_2 - V_{th}}{R_{on}} \end{cases}$$



parameter SI.Resistance RL=35. "Resistance of L";

parameter SI.Inductance L=98.5e-6 "Inductor";

parameter SI.Resistance R2=1000 "Resistor 2";

parameter SI.Capacitance C1=54.e-9 "Capacitor 1";

parameter SI.Capacitance C2=54.e-9 "Capacitor 2";

parameter SI.Voltage Vs=5 "Source Voltage";

parameter SI.Voltage Vth=0.75 "Transistor threshold voltage";

parameter SI.Resistance Ron=100

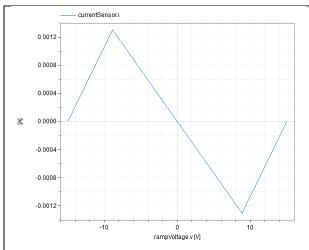
"Small-signal on-resistance of base-emitter junction";

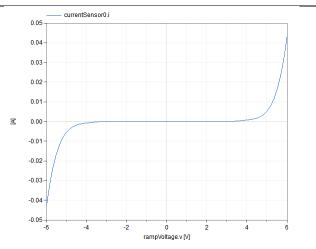
parameter Real beta=200 "Transistor forward current gain";

8_Shinriki Oscillator

https://pawn.physik.uni-wuerzburg.de/~slueck/PhyAmSa09/Home_files/Examensarbeit_Lueck.pdf https://ieeexplore.ieee.org/abstract/document/1456241

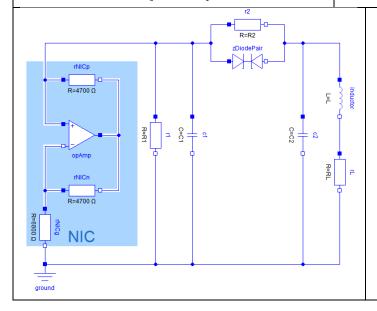
$$\begin{split} i_{z} &= \begin{cases} |v_{z}| < V_{bt} & 0 \\ |v_{z}| \geq V_{bt} & sign(v_{z}) \cdot [a \cdot (|v_{z}| - V_{bt}) + b \cdot (|v_{z}| - V_{bt})^{3} + c \cdot (|v_{z}| - V_{bt})^{5}] \end{cases} \\ & C_{1} \cdot \frac{dv_{1}}{dt} = -i_{NIC} - \frac{v_{1}}{R_{1}} - i_{z} \\ & C_{2} \cdot \frac{dv_{2}}{dt} = i_{z} - i_{L} \\ & v_{2} = L \cdot \frac{di_{L}}{dt} + R_{L} \cdot i_{L} \\ & g_{NIC} = \frac{di_{NIC}}{dv_{NIC}} = \begin{cases} |v_{NIC}| > V_{Lim} & G_{+} \\ |v_{NIC}| \leq V_{Lim} & G_{-} \end{cases} \end{split}$$





Characteristic of negative impedance converter

Characteristic of Zener diode pair



parameter SI.Inductance L=320e-3 "Inductor";
parameter SI.Resistance RL=100. "Resistor of L";
parameter SI.Resistance R1=60e3 "Resistor 1";
parameter SI.Resistance R2=20e3 "Resistor 2";
parameter SI.Capacitance C1=10.e-9 "Capacitor 1";
parameter SI.Capacitance C2=100e-9 "Capacitor 2";

$$a = 1,0862 \frac{mA}{V}$$

$$b = -0,1615 \frac{mA}{V^3}$$

$$c = 0,3021 \frac{mA}{V^5}$$

$$V_{Lim} = 8,870565 V$$

$$G_+ = 0,212766 mS$$

$$G_- = -0,147018 mS$$