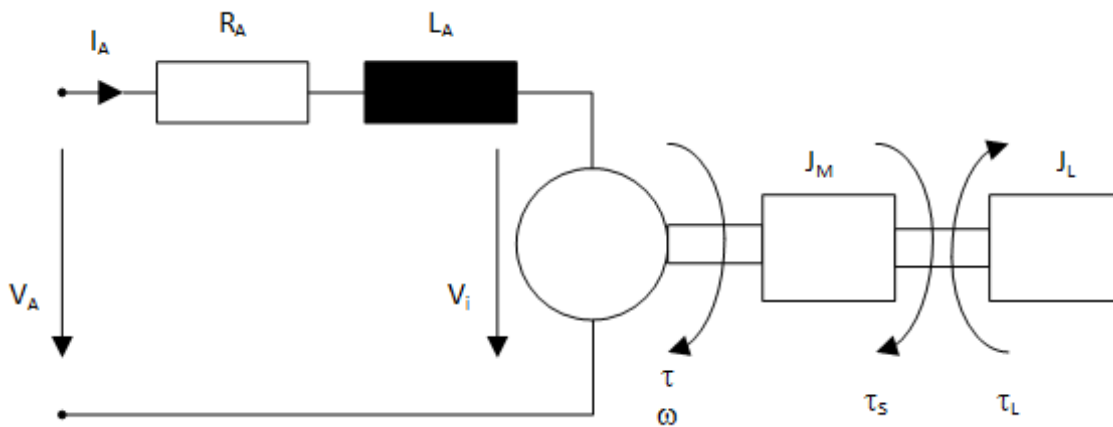


The kinetic energy of rotating masses is converted to electric energy using an electric machine and subsequently dissipated in the internal resistance and the external braking resistance to heat.

### DC-Machine with Permanentmagnet Excitation



Farady's Law:  $V_i = k\Phi \cdot \omega$

Lorentz' Law:  $\tau = k\Phi \cdot I_A$

These two basic equations get implemented in the „electro-mechanical converter“.

Kirchhoff's voltage law:  $V_A = R_A \cdot I_A + L_A \cdot \frac{dI_A}{dt} + V_i$

Equation of Motion:  $\tau - \tau_L = (J_r + J_L) \cdot \frac{d\omega}{dt}$

### Parameter sets:

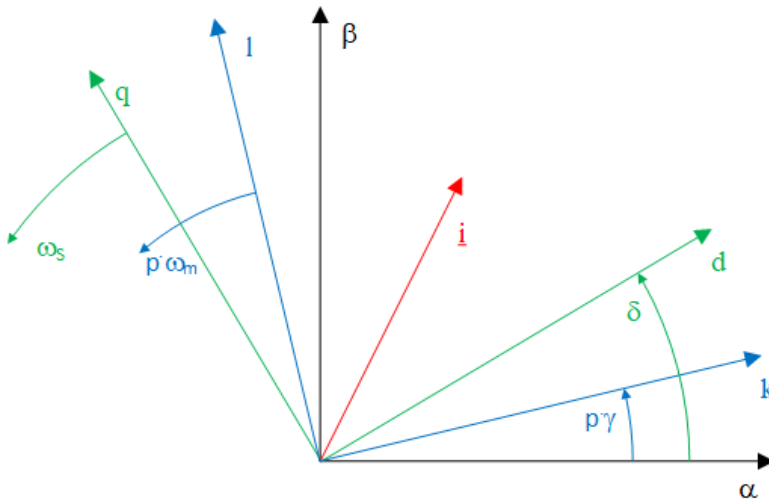
			Unite 48V	Unite XL
Nominal armature voltage	$V_{ANom}$	V	48	480
Nominal armature current	$I_{ANom}$	A	20	10
Armature resistance @ 20°C	$R_{ARef}$	Ω	0,23184	2,625
Nominal armature temperature	$T_{ANom}$	°C	95	95
Armature inductance	$L_A$	mH	0,6	6,5
Induced voltage at nom. speed	$V_{iNom}$	V	42	446
Nominal shaft speed	$\omega_{Nom}$	rpm	3150	1500
No-load speed	$\omega_0$	rpm	3600	1614
Machine constant	$k\phi$	Wb	0,127322243	2,839511426
Nominal torque	$\tau_{Nom}$	Nm	2,546444851	28,39511426
Rotor's moment of inertia	$J_r$	kg.m <sup>2</sup>	0,0012	0,012
Stator's moment of inertia	$J_s$		4 x $J_r$	4 x $J_r$

$$R_A(95^\circ) = R_A(20^\circ) \cdot \frac{235^\circ + 95^\circ}{235^\circ + 20^\circ}$$

$$V_{iNom} = V_{ANom} - R_{A95^\circ} \cdot I_{ANom} = k\phi \cdot \omega_{Nom}$$

$$V_{ANom} = k\phi \cdot \omega_0 \rightarrow \omega_0 = \omega_{Nom} \cdot \frac{V_{ANom}}{V_{iNom}}$$

### Synchronous Machine with Permanentmagnet Excitation



Stator fixed frame  $\alpha + j\beta$

Rotor fixed frame  $k + jl$

Field fixed frame  $d + jq$

For synchronous machines the field fixed frame and the rotor fixed frame are the same.

$\gamma$  is the mechanical angle of the rotor  $\varphi_m$  (with respect to the stator).

For this machine Clarke and Park transform for voltages and currents are implemented in the corresponding electro-mechanical converter:

$$\begin{bmatrix} \cos(p \cdot \varphi_m) & -\sin(p \cdot \varphi_m) \\ \sin(p \cdot \varphi_m) & \cos(p \cdot \varphi_m) \end{bmatrix} \cdot \begin{bmatrix} i_d \\ i_q \end{bmatrix} = \frac{2}{3} \cdot \begin{bmatrix} \cos\left(0 \cdot \frac{2\pi}{3}\right) & \cos\left(1 \cdot \frac{2\pi}{3}\right) & \cos\left(2 \cdot \frac{2\pi}{3}\right) \\ \sin\left(0 \cdot \frac{2\pi}{3}\right) & \sin\left(1 \cdot \frac{2\pi}{3}\right) & \sin\left(2 \cdot \frac{2\pi}{3}\right) \end{bmatrix} \cdot \begin{bmatrix} i_u \\ i_v \\ i_w \end{bmatrix}$$

The zero components fulfills the following equation:

$$i_0 = \frac{1}{3} \cdot (i_u + i_v + i_w)$$

$$v_0 = L_0 \cdot \frac{di_0}{dt}$$

#### Set of Equations:

Due to magnetic saliency and the permanent magnets acting in one fixed direction with respect to the rotor the equations have to be implemented in the rotor fixed frame:

$$v_d = R_s \cdot i_d + L_d \cdot \frac{di_d}{dt} - p \cdot \omega_m \cdot L_q \cdot i_q$$

$$v_q = R_s \cdot i_q + L_q \cdot \frac{di_q}{dt} + p \cdot \omega_m \cdot L_d \cdot i_d + p \cdot \omega_m \cdot \psi_{PM}$$

$$\tau = \frac{3}{2} \cdot p \cdot [\psi_{PM} + (L_d - L_q) \cdot i_d] \cdot i_q$$

$$\tau - \tau_L = (J_r + J_L) \cdot \frac{d\omega}{dt}$$

**Parameter sets:**

			S1FT7102	S1FT7105
Nominal RMS stator voltage per phase	$V_{sNom}$	V	$400/\sqrt{3}$	$400/\sqrt{3}$
Nominal RMS stator current per phase	$I_{ANom}$	A	8	15
Stator resistance @ 20°C	$R_{sRef}$	$\Omega$	0,6	0,15
Nominal stator winding temperature	$T_{sNom}$	°C	95	95
d-axis inductance	$L_d$	mH	12,5	4,2
q-axis inductance	$L_q$	mH	12,5	4,2
zero component inductance	$L_0$	mH	1,25	0,42
Open circuit RMS voltage at nom. speed	$V_{sOC}$	V	183,8571932	199,7631931
Nominal shaft speed	$\omega_{Nom}$	rpm	1500	2000
Number of pole pairs	$p$		5	5
Nominal stator frequency	$f_s$	Hz	125	166,6666667
Rotor's moment of inertia	$J_r$	kg.m <sup>2</sup>	0,009	0,018
Stator's moment of inertia	$J_s$		$4 \times J_r$	$4 \times J_r$

The machines have  $m = 3$  stator phases, the windings are star-connected.

Stator frequency is strictly related to mechanical shaft speed:

$$2\pi \cdot f_s = p \cdot \omega_m$$

Flux linkage space phasor of stator due to permanent magnets can be calculated from open circuit voltage at nominal speed:

$$\sqrt{2} \cdot V_{sOC} = \psi_{PM} \cdot 2\pi \cdot f_s$$