

Part I

TODO

unmentioned tables add lists to table of contents with addcontentsline http://www.emerson.emory.edu/services/latex/latex_162.html

unspecific hyperlinks Set hyperlinks to non-section parts with Hyperlink <https://tex.stackexchange.com/questions/44088/when-do-i-need-to-invoke-phantomsection> Better use \fullrefsec:Sectionlabel

Glossary Make glossaries Package work

Ellens Comments Implement Ellens Comments given in PDF

Formulas in Appendix Put formulas in Appendix

Methodology Have Paragraph on Methodology and remove search approach from literature study

MatlabToolbox Show differences between mathworks toolbox and corke to show decision

Typos Show typos and errors in sources

References Markup and references

literature review make sure all important sources are mentioned, and WHY they're IMPORTANT

Hyperlinks Find a way to toggle link colouring for publication

signature Remember to sign statement of own work

citation scheme see statement of own work - italics???

literature research new source check written content for newly added sources, especially invkin dyn model and Controller and add these to Literature review

title

Part II

Thesiswriting

HAN Master Major Project

Major Project Report

Using FANUC R-2000iC/210F (6-axis robot) for improved efficiency in FRC parts formation

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STATEMENT OF OWN WORK

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Figure 1: FANUC R-2000iC/210F 6-axis industrial robot arm

1. Summary

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2. List of Symbols

a acceleration 3

F force 3

t time 3

v velocity 3

x position 3

3. Acronyms

CAD Computer Aided Design 9

DCS Dual Check Safety 2

DDS Data Distribution System vi, 2, 4, 10

DH Denavit-Hartenberg iv, vi, 11–13, 17–19, 29

DOF degrees of freedom v, 1, 5, 6, 19, 24, 25, 29

DT Digital Twin 6, 7

EOAT End Of Arm Tooling 9, 11, 12, 14, 16, 24

ETCS European Train Control System 7

fig figure 2

FRC Fibre Reinforced Composites 2, 6–9

HMI Human Machine Interface 10

MIC Mobility Innovation Center 10

OS Operating System 4

PC Personal Computer 2

PL Production Line 7

PLC Programmable Logic Controller 9, 10

ROS Robot Operating System 2, 4

SPC Smart Production Cell 6, 7, 10

USB Universal Serial Bus 10

VC Visual Components 9

VFC Variable Frequency controller 10

4. Glossary

Closed-form solutions Closed form solutions in the context of this thesis describe a solution in a closed form expression and are used complementary to numerical Solutions [6](#)

iPendant Wired I/O device for FANUC robots that connects to the robot controller (here R30iA). Provides a touchscreen, buttons, deadman switch and E-stop for manual control, programming, monitoring and configuration of the robot. [10](#)

joint A joint is a connection between two links that allows for movement within certain constraints. [3–5](#)

link A link is a rigid body, defining the spatial relationship between two following axes. Links can be rotated or translated by joints, but don't deform themselves. [4](#)

Numerical Solutions Originally the term numerical solution describes a solution given in terms of numbers instead of an explicit closed form expression. In this work, the term "numerical solution" refers to numerical, iterative methods for solving the inverse kinematics problem by using a sequence of steps leading to incrementally better solutions for the joint angles. Examples for these methods are the jacobian inversion method, the optimization based method cyclic coordinate descent as shown by Lukas Barinka [\[6\]](#). [6](#)

5. Introduction

5.1 Abstract

This work aims to integrate a FANUC 210F 6 axis industrial robot arm into an experimental production line. As this production line is set in a research environment, gaining a deeper understanding of all involved systems is desired.

The dynamic behaviour of a physical system is best expressed with an analytical model. In order to control a robot arm, a kinematic model needs to be created. By attaching inertias and external forces, a dynamic model is obtained. With this model, a control algorithm can be derived.

The objective of this thesis is to derive the complete inverse kinematic model of a 6 DOF robotic arm analytically. For an exact numerical simulation of the device most steps are laid out theoretically and difficulties in the practical implementation are described. Additionally for follow up projects this work also contains a quick start guide and a safety manual for the robot in this setting . Finally to contribute to current research, twinning specifications will be defined.

5.2 Preface

Definition of a Robot Robots [35] can be defined as programmable movement automatas [4] that can perform tasks without human supervision and can be taught at least repetitive tasks. Increasingly, also ways to sense their surroundings are added and improve their movements according to the situation [52]. These sensors are placed additionally to the standard feedback-control sensors like pulse encoders.

Origin of Robots The origin of Robots is well documented in "Robotics, Vision and Control: Fundamental Algorithms in MATLAB" by Peter Corke [9]: "The term robot first appeared in a 1920 Czech science fiction play Rossum's Universal Robots" by Karel Čapek (pronounced Chapek). The term was coined by his brother Josef, and in the Czech language means serf labor but colloquially means hardwork or drudgery. The robots in the play were artificial people or androids and as in so many robot stories that follow this one, the robots rebel and it ends badly for humanity. Isaac Asimov's robot series, comprising many books and short stories written between 1950 and 1985, explored issues of human and robot interaction and morality. The robots in these stories are equipped with "positronic brains" in which the "Three laws of robotics" are encoded. These stories have influenced subsequent books and movies which in turn have shaped the public perception of what robots are. The mid twentieth century also saw the advent of the field of cybernetics – an uncommon term today but then an exciting science at the frontiers of understanding life and creating intelligent machines. The first patent for what we would now consider a robot was filed in 1954 by George C. Devol and issued in 1961. The device comprised a mechanical arm with a gripper that was mounted on a track and the sequence of motions was encoded as magnetic patterns stored on a rotating drum. The first robotics company, Unimation, was founded by Devol and Joseph Engelberger in 1956 and their first industrial robot shown in Fig. ?? was installed in 1961. [9]

Simple robots I have started working with robots and robotic systems in my bachelor studies. As a starting engineer, I was exploring the possibilities of automated manufacturing with CNC mills and 3D printers. These were very simplistic robotic systems based on a feedforward control with stepper motors for position control. For starting a production process, these devices had to be half automatically calibrated and the position and orientation needed to be taught by pointing the drill/printing head to the markerpoints. As no feedback control is usually available on these devices, loss of step control and other errors are possible and can go unnoticed until the end of production, when the part is inspected.

Current Robots Highly developed automated platforms like the Fanuc 210F have feedback-sensors and - control for point to point as well as tracking motion, computer vision as seen on the deltarobot, digital and analog I/O, builtin- safety like the [DCS](#) motion safety system and high speed fieldbus connectivity like Profient. With a teach pendant, these Robots can be configured and programmed. Alternatively [PC](#)-based proprietary manufacturer-specific software with a model based test cell can be used to program the robot.

Future robots To compete in the future developements of "Smart Manufacturing", "the Smart Cell project investigates on an automated production cell for the realization of structural composite components which must be produced in large scale or mass produced" (see [44], Smart-Cell project description). Besides research in materials and production, the automation environment system is of interest for this research. To manage the interaction between material but also the machines among each other, a [DDS](#) couples the subsystems as a middlware as seen in [fig. 5.1](#). A middleware is "glue code" that helps to interface systems with each other to exchange commands and data to use it as a single robotic system. [ROS](#) is a proposed middleware to model, simulate, and control the production line as a homogenous distributed system. Besides the classical publish subscribe pattern to simplify network programming, [ROS](#) provides an ecosystem of interchangeable nodes and drivers to provide a wide codebase for complex tasks.

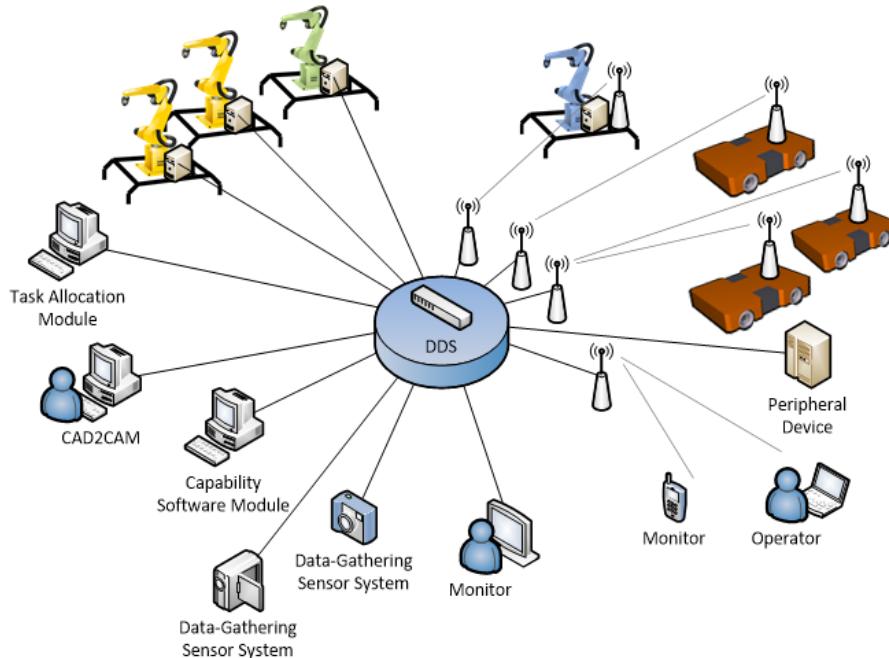


Figure 5.1: [DDS](#) as central information exchange platform

5.3 Problem Definition

For [FRC](#) part production, a robot arm can be used to load the press with raw material, as it allows for more flexibility in the production line than specialized low DOF pick and place systems. As the robot arm has many degrees of freedom, there are different strategies for a control cycle. There are two contrataction main constraints that need to balanced: On one hand, the movement of materials has to be achieved as fast as possible to minimize the cool-down of the molten [FRC](#). On the other hand, the accelerations and forces on it should be minimized while transferring, to make sure no material is lost in the transfer process which would lead to deformations on the final product. This makes it hard to find an ideal, fast control strategy to place the raw material into the press.

6. Sample

TEST TEST TEST

Reference symbols: x , v , a , t , F .

7. Literature survey

In the project plan, it was stated, that "the master level will be demonstrated by understanding and simulating the dynamics of a 6 axis Robot arm." (see [50], sect. Master Level) This should be done by creating a model of the robot arm. This model can then be used to create a controller. To create the model of the robot arm, a literature review is necessary to lay out the best approach.

Additionally to the modelling and control of the robot arm, digital twinning became a research topic within the project. In cooperation with Qing, an overall control strategy based was designed in visual Components. Visual components can provide twinning services like animation and control of existent machines with a virtual model. A review of existing literature on digital twinning will be done as well.

7.1 Methodology

To start the literature review, a set of first keywords was needed. Through an expert interview with the technical supervisor Trung Nguyen [28], who had already supervised other thesis projects in the domain of robotics, a list of keywords to start with was found in a quick discussion. Not all of these keywords were immediately clear, so it was necessary to find definitions for these. With the help of scientific databases and search engines, sources for these definitions could be found.

Keyword Description (Source with Search Engine)

6 axis robot serial 6 degree of freedom robots ([49] with HANQuest)

industrial robot arm some form of jointed structure achieved by the linking of a number of rotary and/or linear motions or **joint** ([54] with Science Direct)

inverse kinematics Determination of joint variables in terms of the end-effector position ([21] with Springer Link search)

Peter Corke robotics toolbox Matlab toolbox for the study and simulation of classical arm-type robotics, for example such things as kinematics, dynamics, and trajectory generation ([39] with Google, yahoo, duckduckGo)

motion planning find a sequence of valid configuration of the **joint** that guides a robot towards a goal ([9] on website of Peter Corke)

robot dynamics relationship between the forces acting on a robot mechanism and the accelerations they produce ([17], with Scholarpedia)

ROS Robot Operating System - framework for writing robot software. It is a collection of tools, libraries, and conventions that aim to simplify the task of creating complex and robust robot behaviour across a wide variety of robotic platforms. (in [37], About ROS, with Google ,yahoo, duckduckGo)

Spreading from these keywords, the literature can be extended with the help of HANQuest and Google scholar by the use of specific keyword combinations like "6DOF AND Industrial Robot AND Matlab model". Platforms like academia and researchgate help to find the right vocabulary for the field whilst also providing the papers and contact options with the authors. Certain authors like Peter Corke have their own website where they provide an extensive overview on their research, teachings and publications for free. Wikipedia and other specialized wikis like scholarpedia break down the concepts and provide a summarizing view for different topics in the field of robotics. Individual phrases and keywords are best triangulated with different search engines like Google, DuckduckGo or yahoo to name a few. Databases like libgen and scihub are essential for scientific work, as not all universities can purchase access packages for all publishers. For applied knowledge online manuals like the mathworks website or forums like stackexchange and roboDK provided most information. Information about the robot model was extracted from the manuals and other documents given by Fanuc.

7.2 Field of study

As seen in "Implementation of Robot Systems" [54], the FANUC 210F is an articulated robot arm, also called a jointed arm. It is a 6 axis robot that has six rotational [joint](#), each mounted on the previous [link](#). This type of robot has the ability to reach a point within the working envelope in more than one configuration or position with its final joint,. As there are multiple configurations possible to reach the same position, path planning would become an important topic. This means through inverse kinematics the motion of the [joint](#) needs to be determined without considering the local forces that cause them to move. As stated in the project plan, MATLAB was intended to be used. The robotics toolbox by Peter Corke was seen as a good tool for simulating these kinematics in MATLAB. When attaching the dynamics to this model, further simulations could be made to simulate the dynamic behaviour of the robot arm and create a controller.

7.3 ROS

"[ROS](#) is a flexible framework for writing robot software." as seen on the "about ROS" page of the ROS-project. As pointed out by other engineers on the "ROS Answers" page, a project related forum [45], the role of ROS is not clearly defined. ROS shares characteristics with middleware, frameworks, but also has [OS](#)-like features. [ROS](#) can take the Role of a [DDS](#), taking a central role in coordinating tasks and information on a distributed system of nodes. ROS can be used as a platform to create a digital twin.

7.4 Forward and inverse Kinematics

As stated in the online manual of MathWorks, "Kinematics is the study of motion without considering the cause of the motion, such as forces and torques." [31] Inverse Kinematics, also called backward kinematics is the logical opposite to forward kinematics also called direct kinematics (See figure 7.1).

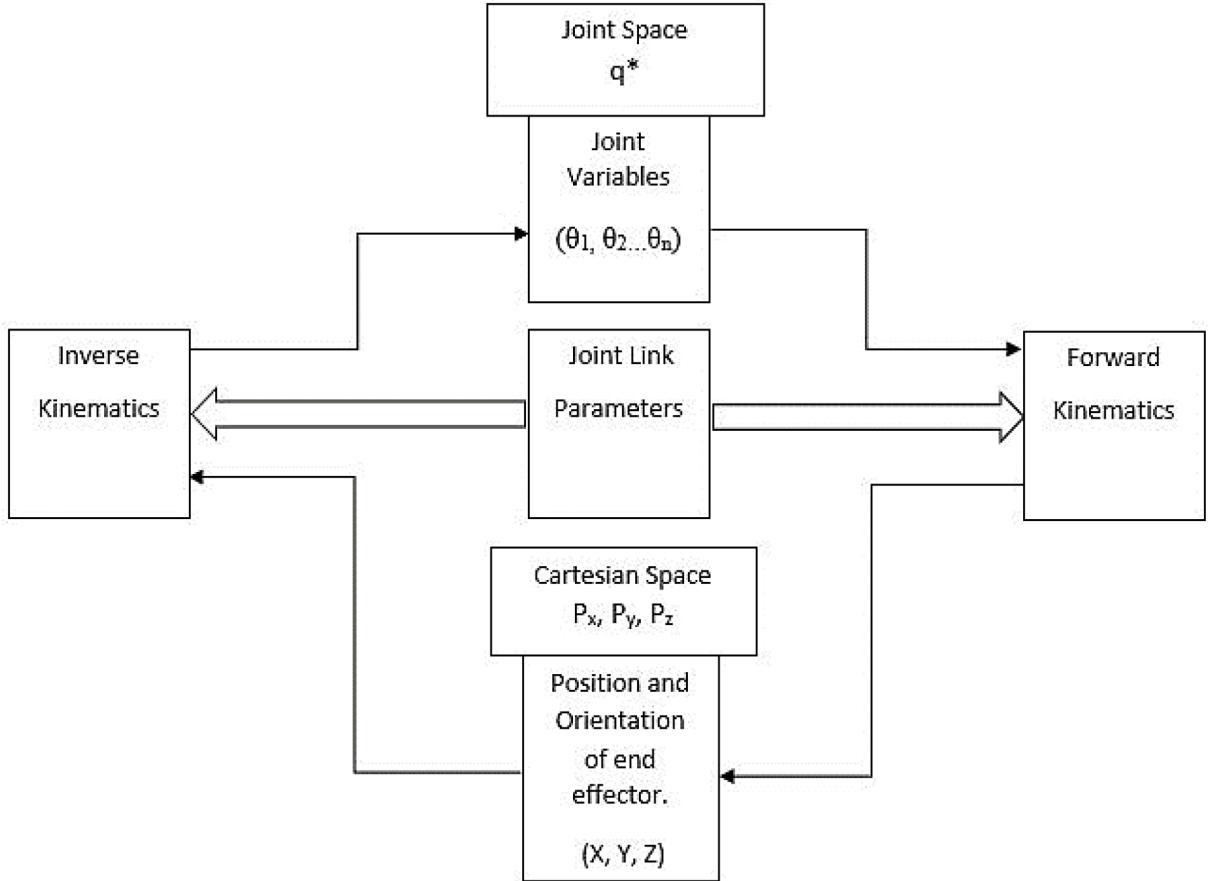


Figure 7.1: Relation between inverse and forward kinematics [20]

Mathworks [36] explains the relationship between forward and inverse kinematics. "Verallgemeinerte inverse Kinematik für Anwendungen in der Robotersimulation und der virtuellen Realität" [41] gives a good overview on the topic of forward and inverse kinematics and gives an idea about the Denavit-Hartenberg notation, a convention to map the local coordinate systems within a kinematic chain as found in robot arms.

As seen in "A Mathematical Introduction to Robotic Manipulation" [33], chapter 2.2 (obtained through Semantic Scholar, search phrase: robotic convention), there are several other conventions besides the "Denavit-Hartenberg notation" used in the robotics research field like the the "product of exponentials formulation". As most textbooks prefer a Denavit-Hartenberg fomulation of the kinematics (see [33], ch. 3.1 Manipulation using single robots), this convention will be chosen in this work as well. The forward kinematic analysis can be obtained as seen in "Forward Kinematic Analysis of an Industrial Robot " [8].

Solutions for forward kinematics are simple to obtain but solving inverse kinematics has been one of the main concerns in robot kinematics research. With more DOF, solutions get more complex as non-linear equations with transcendental functions need to be solved. For this set of equations, no general algorithms are available. Often algebraic, geometric and iterative methods for complex manipulators are used to find a solution to the inverse kinematic problem as stated by Tarun Pratap Singh et al. in the abstract of "Forward and Inverse Kinematic Analysis of Robotic Manipulators" [43].

To find a suitable method for solving the inverse kinematic problem, a definition for the solution is needed:

"A manipulator will be considered solvable if the joint variables can be determined by an algorithm that allows one to determine all sets of joint variables associated with a given position and orientation. [...] The algorithm should find all possible solutions" -Dr.-Ing. John Nassour [27]

With this definition of solvability, all systems with revolute and prismatic joint with 6 DOF in a single series chain are solvable with the current available research. [27]

As the goal is to find a suitable solution strategy for the inverse kinematic problem, it helps to map out the different types of methods. Solution strategies can be split into two classes as stated by Dr.-Ing. John Nassour in his presentation [27]:

Closed-form solutions

faster because analytical method
will find all solutions
Two approaches:

algebraic approach geometric approach

Numerical Solutions

slower because of iterative nature
not always find all solutions

As Numerical Solutions cannot always deliver all solutions and solve within an unknown number of operations as well as depend on the users decision for accuracy, [27] a closed-form solution will be preferred.

"6DOF inverse kinematics" the article "Inverse Kinematics Solution and Optimization of 6DOF Handling Robot" [55] offers an algebraic method to solve the inverse kinematic problem for 6 axis robots. A similar approach is shown in "Forward and Inverse Kinematic Analysis of Robotic Manipulators" [43]. Another approach can be found in "Forward and Inverse Kinematics Model for Robotic Welding Process Using KR-16KS KUKA Robot" [11]

As an alternative, a geometric modelling can be done as seen in "Workspace analysis and geometric modeling of 6 DOF Fanuc 200IC " [7]. A completely different approach is given in "A inverse kinematic solution of a 6-DOF industrial robot using ANN" by using artificial neural networks [2].

With one of these methods, a solution can be found for the inverse kinematic problem. This solution can then be verified with the robotics toolbox created by Corke [39].

7.5 Dynamic model

With this solution, a dynamic model of the robot can be created by attaching dynamics to the model as seen in "Control and Safety Mechanisms for a 3 DOF Manipulator with Human Interaction" [51] and "A mathematical introduction to Robotic Manipulation" [33]. A complete example of a dynamic simulation of a 6 DOF robot arm can be found in "Dynamic Multibody Simulation of a 6-DOF Robotic Arm" [25]

7.6 Controller

A controller for trajectory tracking can then be created with the model as seen in "Experimental Evaluation of Nonlinear Feedback and Feedforward Control Schemes for Manipulators" [22]

This controller could then be plugged into the real robot as stated in the "Control of a FANUC Robotic arm using MATLAB manual" [47] An example of this can be found in "Modelling and analysis of a 6 DOF robotic arm manipulator" [19]

7.7 Digital twinning

In the setup of the experimental production line for FRC at the SPC DT has been chosen as one of the key technologies for "Smart manufacturing". In the cooperation with Qing, there have been a few discrepancies on the understanding of a DT.

To approach this topic, the term digital twin has to be defined. This Concept was introduced for the first time by Grieves at one of his presentations about Product Lifecycle Management in 2003 at University of Michigan as a virtual representation of what has been produced [18]. As stated by Qinglin Qi [32], a DT is a high fidelity virtual model for physical objects in a digital way to simulate their behaviour. When looking on the Wikipedia page on digital twinning [12], a wide variety of definitions can be found. This shows, that the concept of the DT is not yet clearly defined. All of these definitions have in common though, that DTs are "digital replications of living as well as nonliving entities that enable data to be seamlessly transmitted between the physical and virtual worlds" [13].

To approach the problem form the other side, it might help to look at, what is not a digital twin. A virtual representation of a physical object without any exchange of data is a digital model [53]. If data is fed from the physical system into the model, a digital shadow is created [23]. Only a "bi-directional relation between a physical artefact and the set of its virtual models" [40] fulfils Schleich's vision of a DT.

As an example, a computer aided design (CAD) model is a representation of a physical entity and it is typically used to describe the shape, dimensions and materials of a construction. This model can be a 2D or a 3D model. Only if the latest sensor data associated with a matching physical device is fed into this CAD model, it can be considered a DS. [53] By simulating different scenarios in a model and representing the current state of the system the DS turns into a digital twin, if decisions are made automatically fed back through an actuator into the physical entity [40]. An implementation of this data transmission can be found in "Sensor Data Transmission from a Physical Twin to a Digital Twin" [1].

As the **DT** is mostly used in the context of production lines, it makes sense to look for similar examples in other industries, that have undergone comparable transformations with the beginning of the digital age. Such a comparable system can be found in the transport industry. **PLs** have several points in common with train networks. One of the latest internationally standardized systems in rail infrastructure is **ETCS** which will probably become the standard signalling and control component in all European countries. A great overview on the **ETCS**-standard is given by Thales on their website [14]

8. Setup of the physical Environment

The production line at **SPC** is planned to produce steering knuckles with **FRC**.

8.1 Steps in the production line

The planned production line consists of several steps that can be seen in figures 8.1 and 8.2.

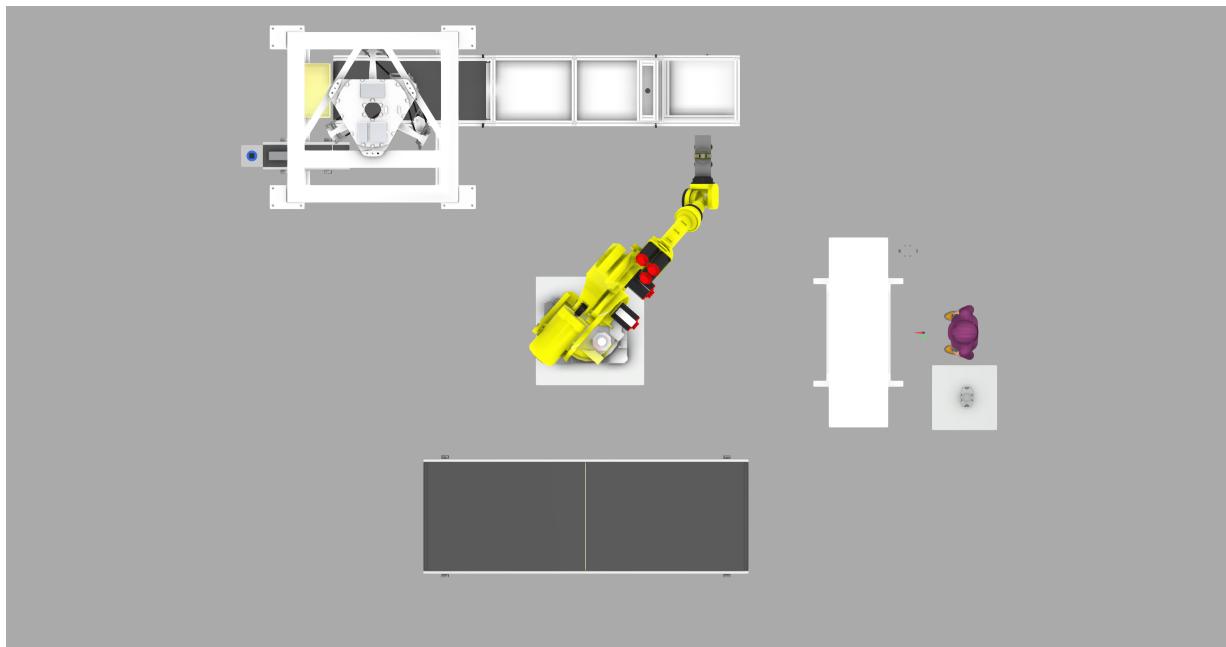


Figure 8.1: Top view of Production line layout, rendered with Visual Components [29]

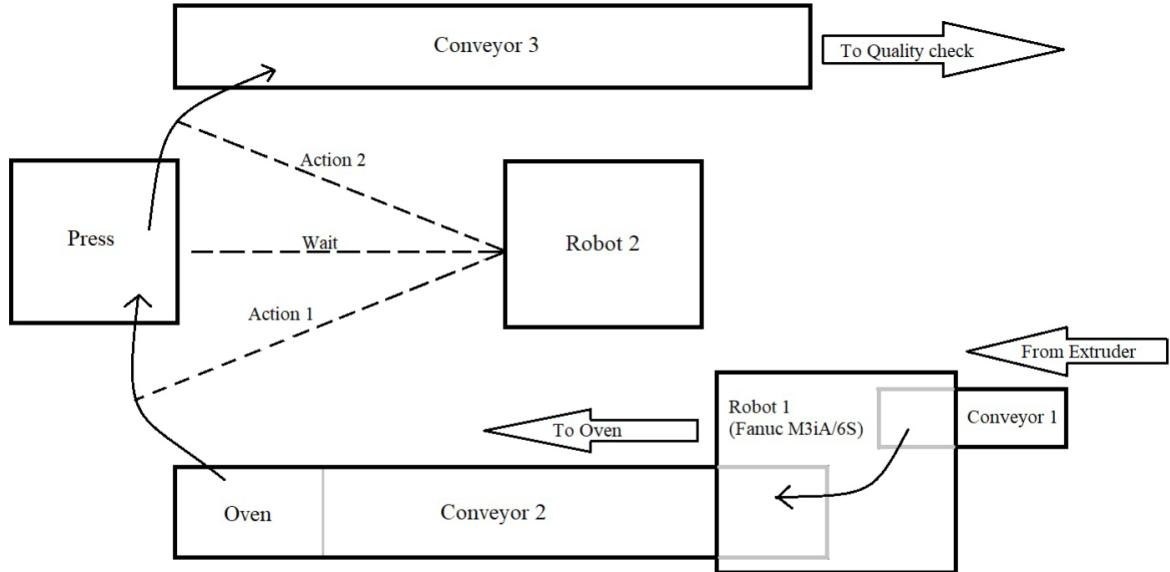


Figure 8.2: Schematic of the floorplan [29]

Extruder FRC raw material pellets are fed into an extruder. Alternatively, reprocessed material from steps down the production line is fed into the extruder. The extruder melts the raw material and releases it at its hot end. At the hot end of the extruder, the material is portioned into blops of 300g each by a guillotine.

Conveyor 1 The first conveyor belt transports the FRC material blops from the output of the [Extruder](#) to the [Deltarobot](#). At the end of the coveyor belt is a proximity sensor to detect incoming material.

Deltarobot After a signal is given from the proximity sensor of [Conveyor 1](#), a Fanuc M-3iA/6S 4-axis Delta-robot picks up the material and weighs it with a load cell built into the gripper of the robot. If the weight of the material is out of the desired range, it is discharged into a waste bin and recycled with the [Extruder](#). If the weight of the material is within an acceptable range, it is placed on [Conveyor 2](#). When placing the material on conveyor 2, the placement position and other data are communicated to processes further down the line. If needed, multiple blops of material can be stacked to the desired height while [Conveyor 2](#) keeps moving.

Conveyor 2 The second conveyor belt transports the sorted and arranged FRC material from the [Deltarobot](#) through the [Oven](#).

Oven The oven can be separated into several zones:

Oven entrance With the position data provided by the [Deltarobot](#) and the [Conveyor 2](#) speed, the oven door at the entrance can open at the right time to take in the material.

Heating Chamber In the heating chamber, the material is brought to the desired temperature with several induction heaters.

Internal door With the position data provided by the [Deltarobot](#) and the [Conveyor 2](#) speed, a door inside the oven can open at the right time to take in the material.

Buffer zone A buffer zone, separated from the [Heating Chamber](#) provides an area to keep the material at the desired temperature until it can be processed further.

Oven output When the [Hydraulic press](#) is ready, a door in the [Buffer zone](#) opens for the ?? to pick up the material.

Robot arm task 1 After a signal is given from the [Hydraulic press](#), a Fanuc 210F 6axis robot arm picks up the hot FRC material stack from the [Buffer zone](#) and places it in a [Hydraulic press](#) with a specialized gripper. After placing the part, the robot changes its gripper tool, and waits for its second task, see [Root arm task 2](#).

Hydraulic press After all material is placed and the [Robot arm task 1](#) has completely withdrawn from the press in a safe distance, the press will close the heated mould to give the [FRC](#)material its desired shape with heat and pressure.

Root arm task 2 When the forming process in the [Hydraulic press](#) is finished, the mould opens, and the same robot arm as in [Robot arm task 1](#) can use another gripper to pick up the [FRC](#)-part and place it on [Conveyor 3](#). After placing the part, the robot changes its gripper tool, and waits for its first task, see [Robot arm task 1](#).

Conveyor 3 The third conveyor belt transports the formed part from the press to the [Cobot](#).

Cobot When the material arrives at the cobot, it is picked up, and presented to a camera system for analysis. If the part fulfils the desired properties, it is given to further processing steps and packing. In case, it does not fulfil the desired properties, it can be recycled with the [Extruder](#).

8.2 Notes on choice of robot

The robot was chosen for this production line, as it provides a long reach. The arm without any [EOAT](#) can reach a full circle with a radius of 2655[mm] with its mounting plate. Also the overall weight of 1240[mm] allows for reasonably fast movements between 90 – 190[°/sec] depending on the axis while still giving a payload capacity of 210[Kg] at the mounting plate.[\[16\]](#) This high payload capacity is not needed directly, but it provides enough room for complex gripper designs, and provides room for future uses of the device.

8.3 Status of the production line at beginning of project

At the start of this thesis work, the [Hydraulic press](#) was already fixed to the ground. [Deltarobot](#),[Conveyor 2](#), and the robot arm were roughly placed at their final positions. No gripper tools were available for either robots. The [Extruder](#), [Oven](#), [Conveyor 1](#), [Cobot](#) and [Conveyor 3](#) were not available. Electricity for the machines was not made available. A safety-fence was not set up.

8.4 Status of the production line at the end of thesiswork

At the end of the project, the robots are positioned at a preferable position for their intended use. Interaction between press and robot arm were tested. Grippers were being developed in [CAD](#), and some standardized pneumatic grippers were tested on the robot arm for pick and place operations. [Conveyor 2](#) was positioned, and fixed to the ground. Also, it was also tested with a Profinet-controlled variable frequency drive via [PLC](#). A heat resistant belt still needs to be mounted. An [Extruder](#) was delivered, but still needs to be commissioned, tested and modified. An [Oven](#), [Conveyor 1](#), [Conveyor 3](#) and a Section-station are still missing. A preliminary safety fence with no electronic safeguard has been set up.

8.5 Set up process of Robot arm

8.5.1 Positioning

In order to integrate the robot arm into the production line, it needed to be mounted at its final position. This position was determined with a floorplan. To create the floorplan, the three members of SPC responsible for the [Deltarobot](#), the [Conveyor 2/Oven](#) and the robot arm worked out the positions of their machines with the help of Qing Groep. At Qing, the production line was modelled in [VC](#). With [VC](#) different positions for these machines could be tested. Simple pick and place programs could be simulated in that environment. These movements could be inspected and varied to allow a smooth and fast transfer of material. As the [Hydraulic press](#) was already fixed to the ground, all other positions were determined relative to the press. After estimating good positions via [VC](#) with respect to the movement range of the robot arm, the outlines of the machine feets were measured with a laser distance measurement system and marked on the floor. After placing the robots with a forklift on the desired positions, the actual positions were measured again with the laser distance measurement system, documented in an excel sheet and tested again in [VC](#). As the differences between actual and desired position were minimal, the simulations in [VC](#) did not show any problems. The robot arm and the other machines was then bolted down in the ground.

8.5.2 Comissioning

After the robot arm was positioned at its desired position, it could be plugged into the accompanying Fanuc R-30iA controller and was provided with electricity. This step was delayed a lot, as a safe and powerful enough electrical installation could not be provided by the [MIC](#) from the beginning of the project. After the robot and controller were running, the basic functions as found in the manuals could be tested. Manuals and configuration files were delivered by the previous owner, IRS Robotics, on a set of [USB](#)-sticks. These [USB](#) sticks had all kinds of manuals and configuration files for both robots without any context and order on them. An extensive search and ordering was needed to get the right manuals. Additionally, the previous owner had left a non-functional configuration on the robot, that was overcome by a complete factory reset with the help of Fanuc customer service. When these issues were overcome, the robots could be calibrated. As described in the manual, the robots have calibration markings. With these markings aligned, a calibration could be made with the [iPendant](#).

8.5.3 Fieldbus and Network setup

For the state of this thesis-work, the field bus and network- installation consists of following parts:

- [PLC](#)
- [HMI](#)-Display
- [VFC](#) for conveyor belt
- R-2000 iA Mate Controller for Delta robot
- R-2000 iA Controller for Robot arm
- Several student notebooks for configuration, monitoring and control of the machines

Additionally following devices are Planned:

- [DDS](#) (eventually consisting of several distributed nodes)
- cameras for process monitoring
- Controller for [Cobot](#)
- Controller for Extruder and Feeding system
- Part inspection system
- various sensors
-

The physical layer of the network and fieldbus is based on ethernet. A basic connection to the PLC via Profinet as well as to the network via IP/Ethernet at [SPC](#) was achieved.

9. Building of a Model

9.1 Forward Kinematics

To model the movements of the end effector of a kinematic chain, a forward kinematic analysis is needed.

9.1.1 Five step approach

A serial-link manipulator consists of links in a chain connected by joints. For describing the serial-link mechanism geometry the Denavit Hartenberg notation is one possible approach. It gives a description of a manipulator for kinematic solutions, Jacobians, dynamics, motion planning and simulation. This description can be obtained through a five step algorithm:[8]

1. Numbering of joints and links
2. Set up local coordinate reference frames
3. Establishing DH parameters for each link
4. Calculate homogeneous transformation matrices
5. Compute Forward Kinematic Equations

9.1.1.1 Numbering of joints and links

A serial link robot with n joints has $n + 1$ links.

numbering of links The numbering scheme for links starts at (0) with the fixed grounded base and then increases sequentially up to (n) for the end effector.

numbering of joints The numbering scheme for joints starts at (1) with the joint connecting the first movable link to the base and then increases sequentially up to n .

relation between links and joints Link (i) is connected to its

- lower link ($i - 1$) at its proximal [26] end by joint (i)
- upper link ($i + 1$) at its distal [26] end by joint ($i + 1$)

9.1.1.2 Set up local coordinate reference frames

With the Denavit-Hartenberg convention, local coordinate frames can be attached to the far end of the links (i) and their accompanying joints ($i + 1$). Each link (i) is described relative to the pose of the preceding link.

Assignment of z_i axes With the DH-notation, the z_i axes are assigned to link (i). By using the DH convention, both prismatic and revolute joints can be treated similarly:

revolute: z_i is the axis of revolution of joint ($i + 1$)

prismatic: z_i is the axis of translation of joint ($i + 1$)

This means, that joint z_i turns around axis z_i .

Direction of rotation With the direction of the z_i -axis, the direction of positive rotation around joint ($i + 1$) is also given by the right hand rule (see [34] and [38] at 10:35 for a visual representation). This means, the direction of positive rotation is counter-clockwise around the z_i -axis. With predictive choice of the direction of positive rotation, the direction of the z-axis can be chosen in order to minimize the DH-parameters (insert source here)

Base frame The base frame (0) can be chosen nearly arbitrarily. The origin of the base frame can be any point on z_0 . For simplicity, the origin of frame(0) can be put into joint(1). Usually, the x-axis of the base frame is chosen, so that it points in the direction of the EOAT in default position according to its base, [56] but can be chosen in any convenient manner [42].

Assignation of frames (i) Starting from frame (1) in an iterative process, frame (i) can be set up using frame ($i - 1$).

Three cases regarding the relationship of axes z_{i-1} and z_i need to be considered when setting up frames:

Non coplanar: Axes don't intersect and are not parallel. Line containing the common normal z_{i-1} to z_i defines x_i -axis and the point of intersection with z_i is the origin of frame (i)

- a) find common normal of the joint axes
- b) put origin in intersection of normal with joint axis
- c) put z_i axis in the joint axis
- d) x_i points in direction of the common normal, facing away from frame (0)
- e) add y_i according to right hand rule

Parallel: Axes are parallel. Line containing the normal through origin of frame ($i + 1$) and the z_i -axis defines the x_i -axis which is directed from origin of frame (i) toward the distal joint. The point of intersection of common normal with z_i -axis gives the origin of frame (i).

- a) look for normal originating from distal joint
- b) put origin in the intersection of the normal with the joint axis
- c) put the z_i axis in the joint axis of the link ($i + 1$)
- d) x_i points follows the common normal with the distal joint, pointing towards the distal joint
- e) add y_i according to right hand rule

Intersecting: Axes are intersecting. Line containing the normal to the plane formed by axes z_{i-1} and z_i gives the x_i -axis with positive direction chosen arbitrarily. Point of intersection of axes z_{i-1} and z_i is the origin of frame (i).

- a) put origin in intersection point of the axes
- b) put the z_i axis in the joint axis of the link ($i + 1$)
- c) x_i is perpendicular to both joint axes
- d) add y_i according to right hand rule

Assignation of EOAT frame As there is no distal joint for the **EOAT** frame, the steps for this frame are different:

- a) put origin on axis of proximal joint
- b) axis z_i follows direction of z_{i-1}
- c) x_i can be chosen arbitrarily, but is usually determined by screw holes
- d) add y_i according to right hand rule

9.1.1.3 Establishing DH parameters for each link

After assigning the local coordinate frames, the **DH**-Transformations have to be determined. This leads to a kinematic chain with each frame determined by the previous one [56].

Link0 - Link1 - Link2 - Link3 - Link4 - Link5 - Link6

Each **DH**-transformation consists of four elementary transformations[56]:

- 1) rotation around the x_i -axis with the amount of α_i
- 2) translation along x_i -axis with the amount of a_i
- 3) translation along z_i -axis with the amount of d_i
- 4) rotation around z_i -axis with the amount of θ_i

This shows that the **DH** robotic convention is a minimal line representation, as with four parameters, all possible lines in the Euclidean Space can be represented ([5], page 210).

Following from this, two pairs of parameters determine the joints and links [8]:

Links: represented by link length (a) and link twist (α)

Joints: represented by link offset (d) and joint angle (θ)

These are the DH-parameters which form the transformation matrices that connect serial link coordinate frames. They can be distinguished into parameters and variables. While constructive parameters are dependent on the construction of the robot and are constant, variables depend on the joint movement [43] [8] [56].

α_i angle between z_{i-1} and z_i , measured in plane normal to x_i (constructive parameter)

a_i distance between z_{i-1} and z_i , measured along x_i ; parallel to $z_{i-1} \times z_i$ for intersecting axes (constructive parameter)

d_i distance from the origin O_{i-1} of frame $i - 1$ to the intersection of the x_i axis with z_{i-1} , measured along z_{i-1} (constructive parameter in revolute joints, variable in prismatic joints)

θ_i angle between x_{i-1} and x_i , measured in plane normal to z_{i-1} (constructive parameter in prismatic joints, variable in revolute joints)

These parameters describe the relatively complex transformation of the coordinate system $i - 1$ into the coordinate system i by four subsequent elementary transformations [41]:

$$T_{i-1,i} = ROT(z_{i-1}, \theta_i) * TRANS(0, 0, d_i)^T * TRANS(a_i, 0, 0)^T * ROT(x_i, \alpha_i) \quad (9.1)$$

$ROT(v, \alpha)$ is a simple rotation around vector v with the angle α and $TRANS(x, y, z)^T$ is a translational movement along the vector $[x, y, z]^T$. For a visual representation of these parameters see figure 9.1

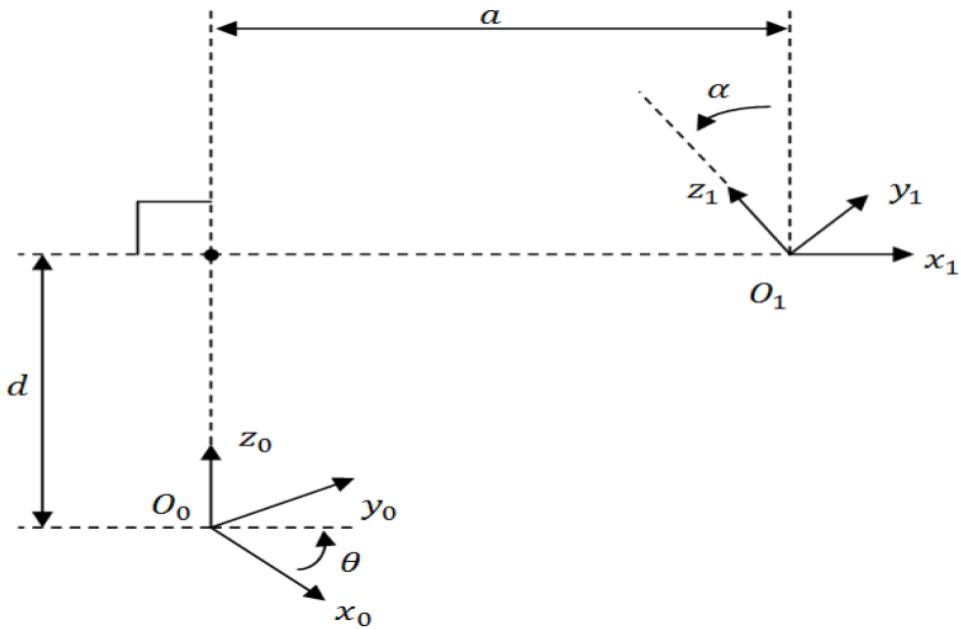


Figure 9.1: Visual representation of a DH-transformation

This visual representation gives a guide to attach the DH-parameters on serial-link mechanisms.

9.1.1.4 Calculate homogeneous transformation matrices

Locating reference frame $(i - 1)$ relative to (i) can be done by executing a series of transformations as given by equation 9.1. For simplification, they can be done with a 4×4 homogenous transformation matrix:

$${}^{i-1}T_i(\theta_i, d_i, a_i, \alpha_i) = R_z(\theta_i) * T_z(d_i) * T_x(a_i) * R_x(\alpha_i) \quad (9.2)$$

Equation 9.2 can be expanded into:

$${}^{i-1}T_i = \begin{bmatrix} \cos \theta_i & -\sin \theta_i * \cos \alpha_i & \sin \theta_i * \sin \alpha_i & a_i * \cos \theta_i \\ \sin \theta_i & \cos \theta_i * \cos \alpha_i & -\cos \theta_i * \sin \alpha_i & a_i * \sin \theta_i \\ 0 & \sin \alpha_i & \cos \alpha_i & d_i \\ 0 & 0 & 0 & 1 \end{bmatrix} \quad (9.3)$$

9.1.1.5 Compute Forward Kinematic Equations

In Forward kinematics, the kinematic equations of a robot are used to compute the position of the EOAT from the given joint parameters.

Sum of Transformations Matrix With the transformation matrices from frame (i) to $(i - 1)$, a 44 matrix for all joints on n links can be established as in equation 9.4

$${}^0T_n = \prod_n^{i=1} {}^{i-1}T_i \quad (9.4)$$

The resulting matrix has the form (see [55], eq 1):

$${}^0T_n = \begin{bmatrix} n & o & a & p \\ 0 & 0 & 0 & 1 \end{bmatrix} = \begin{bmatrix} n_x & o_x & a_x & p_x \\ n_y & o_y & a_y & p_y \\ n_z & o_z & a_z & p_z \\ 0 & 0 & 0 & 1 \end{bmatrix} \quad (9.5)$$

short notation The short notations for orientation, rotation and position are defined as:

n normal vector

o orientation vector

a approach vector

p position

Transformation to cartesian coordinates with euler angles These vectors can be transformed into the $[x, y, z, \alpha, \beta, \gamma]$ notation. Vector $p = [p_x, p_y, p_z]$ gives [x, y,z]. The rotational approach $[\alpha, \beta, \gamma]$ can be calculated with the rotation matrix R as seen in eq 9.6.

$$T = \begin{bmatrix} R & p \\ 0 & 1 \end{bmatrix} \quad (9.6)$$

The rotation matrix describes the relative orientation of two frames towards each other. As the columns $[n, o, a]$ are the unit vectors along the axes of one frame relative to the other reference frame, the relative orientation of a frame b with respect to a frame a is given by the rotation matrix as seen in eq ?? [8]

$${}^b_aR = \begin{bmatrix} {}_ax^b) & {}_ay^b) & {}_az^b) \end{bmatrix} = \begin{bmatrix} x^b \cdot x^a & y^b \cdot x^a & z^b \cdot x^a \\ x^b \cdot y^a & y^b \cdot y^a & z^b \cdot y^a \\ x^b \cdot z^a & y^b \cdot z^a & z^b \cdot z^a \end{bmatrix} \quad (9.7)$$

As in equation 9.8 the coordinates relative to the reference frame a , of a point p , of which the coordinates are known with respect to a frame b with the same origin can then be calculated (see [3], "Description of Position and Orientation) .

$${}_ap = {}_a^bR {}_bp \quad (9.8)$$

9.1.2 Forward kinematic equations of Fanuc 210F

9.1.2.1 Joint and link numbering in Fanuc 210F

The numbering scheme presented in subsubsection 9.1.1.1 Numbering of joints and links can be applied to the Fanuc 210F (see 9.2)

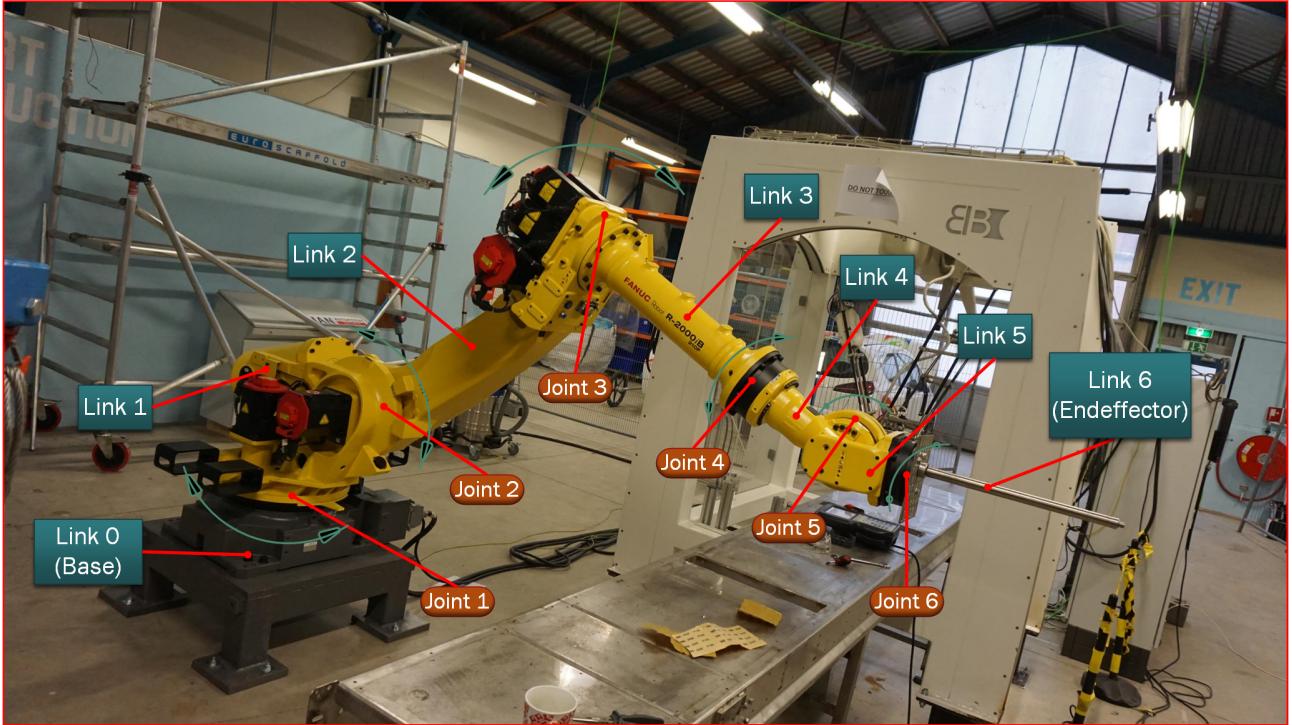


Figure 9.2: Links (turquoise) and joints (orange) in the FANUC 210F

z_i axes in Fanuc 210F As described in [section 9.1.1.2 Assigment of \$z_i\$ axes](#), the z_i axes can be attached to the Fanuc 210F (see figure 9.3).

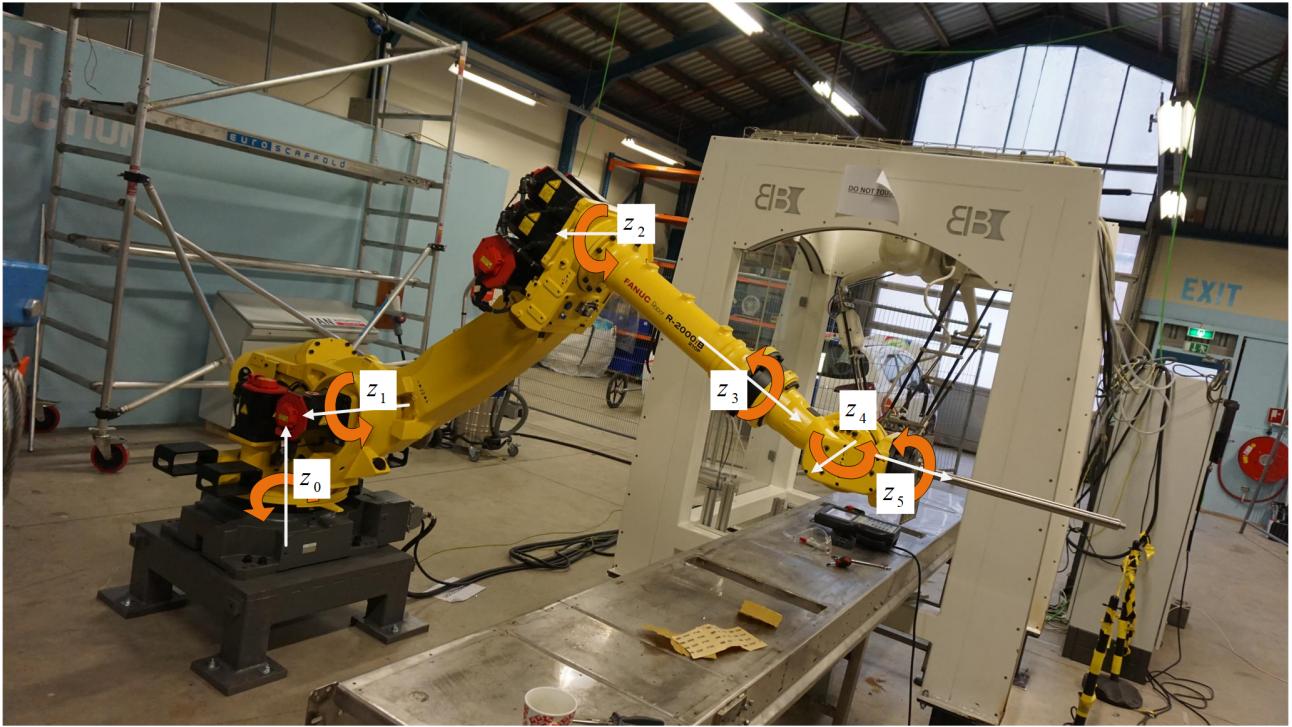


Figure 9.3: z_i axes on the Fanuc 210F with the direction of positive rotation (orange)

The positive direction of the triples z_1, z_2, z_4 and z_0, z_3, z_5 , was chosen to make sure, the x-axis would always have the same direction for parallel joints.

9.1.2.2 local coordinate reference frames on the Fanuc 210F

As described in [subsubsection 9.1.1.2 Set up local coordinate reference frames](#), the local coordinate reference frames can also be attached to the Fanuc 210F as seen in figure 9.4.

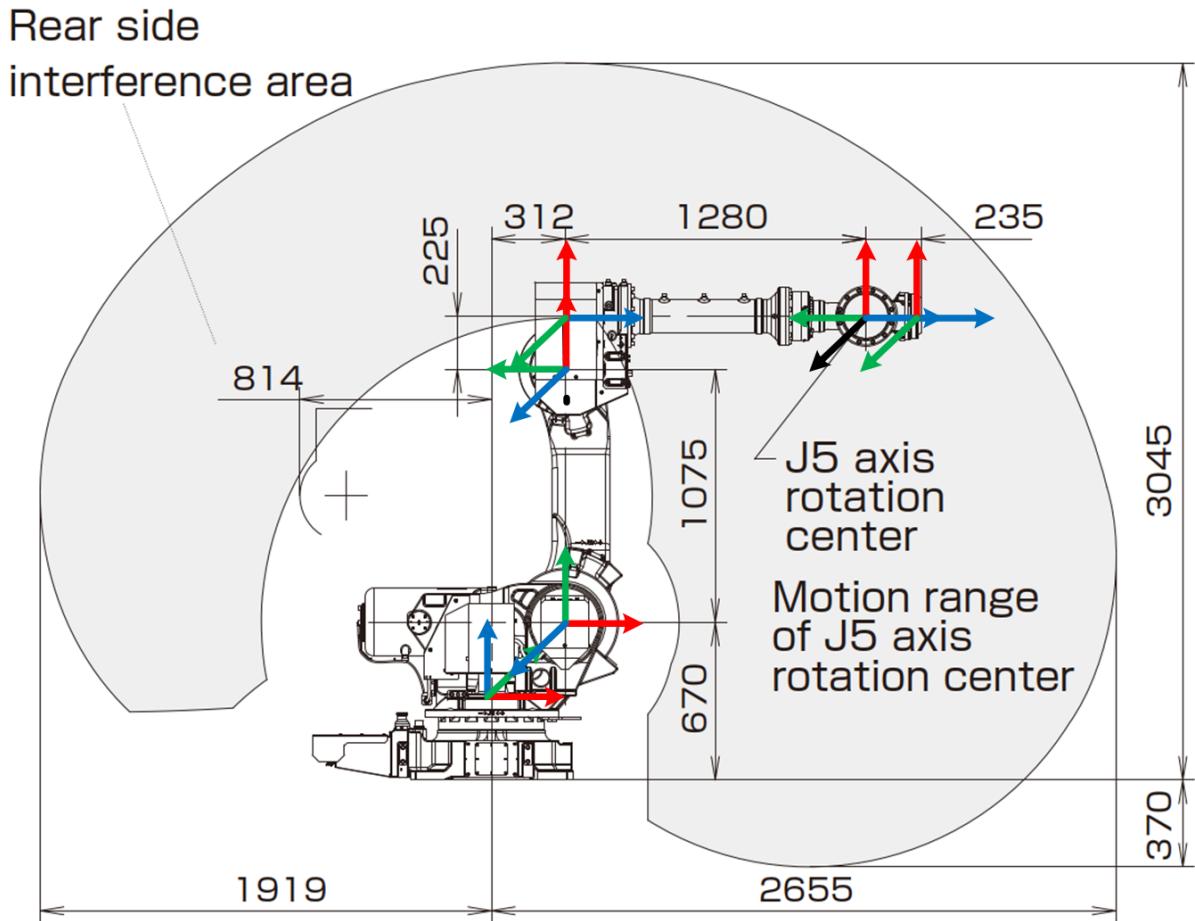


Figure 9.4: Coordinate reference frames for Fanuc 210F in standard (Normal) pose

Abstract view of coordinate frames For a better overview, the drawing of the robot can be removed, which reveals the pure coordinate frames. Here it can be described, in which relation the coordinate frames stand in relation to each other.

frame 0 (Base) The frame mapping starts with the base frame. For the base frame the z-axis is given through joint j_1 . Origin of frame 0 is put into joint 1. The x-axis is chosen to point in direction of the EOAT in standard pose see 9.4. This pose will also be chosen for alignment of all distal frames.

frame 1 For frame 1, the z-axes are not coplanar. Because of that, the z_0 -axis is extended until a common normal can be found that intersects with z_i to define the origin O_1 . x_1 departs from O_1 along the common normal. y_1 is added according to the right hand rule.

frame 2 As seen, in image 9.3, axes z_2 and z_1 are parallel. O_2 can be found at the intersection of the normal through O_1 with z_2 . x_2 follows the common normal with joint 4. y_2 is added according to the right hand rule.

frame 3 Joint 3 and joint 4 are not exactly aligned (see image 9.4), which prevents the z-axes to intersect. That's why axes z_3 and z_2 are not coplanar. z_3 runs parallel through the link 3, due to the orientation of the rotational axis. As the common normal between z_3 and z_2 defines x_3 , which in turn gives O_3 , the origin can be found far away from the physical position of the joint. y_3 is added according to the right hand rule.

frame 4 Joint 5 lies in line with joint 4. As z_3 follows this line, the axes z_4 and z_3 intersect in the center of joint 5, which gives O_4 . x_4 leaves the plane spanned by z_4 and z_3 perpendicular. The positive direction of x_4 is chosen to be similar as in frame 3 for simplicity. y_4 is added according to the right hand rule and points in direction of frame 3.

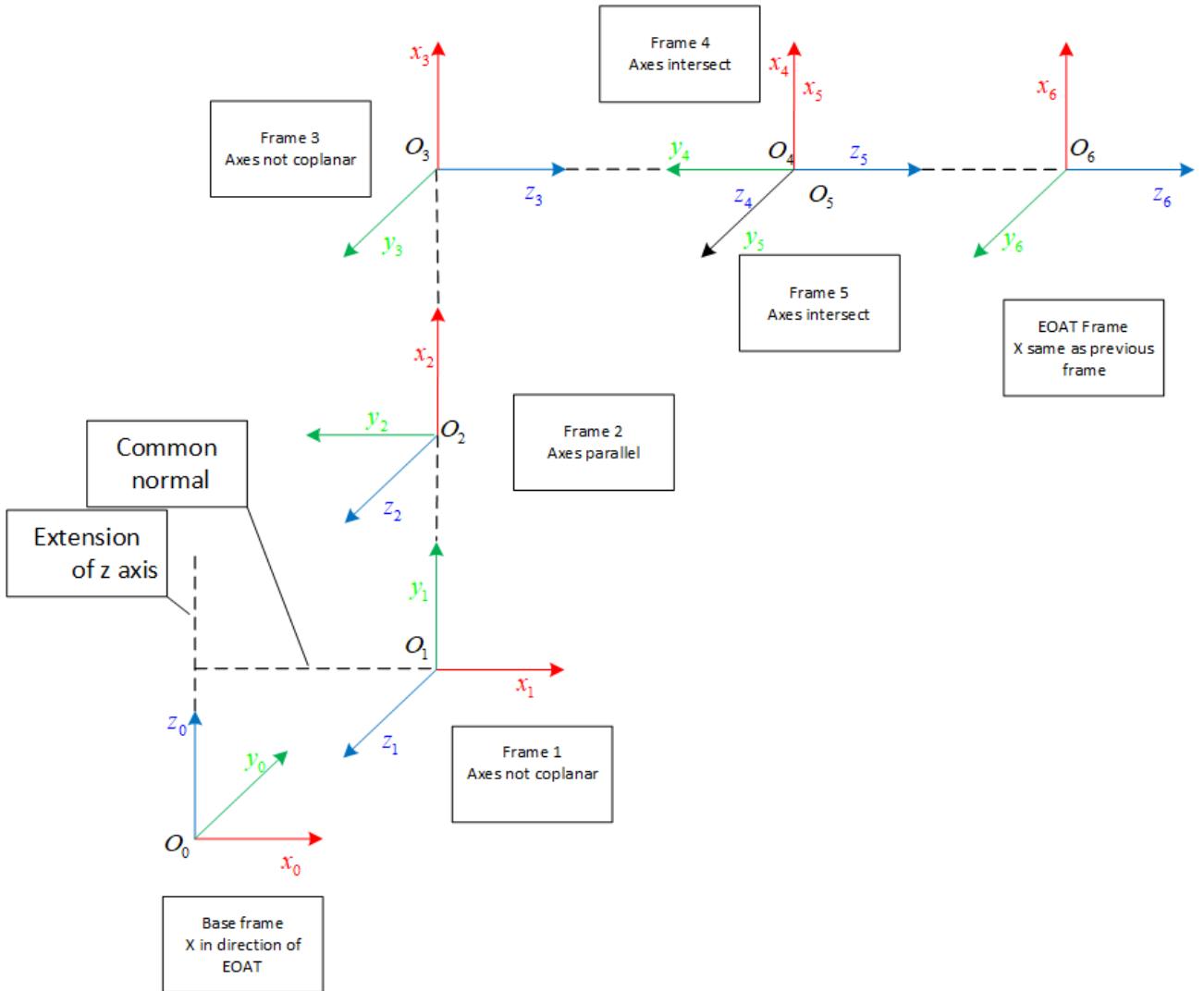


Figure 9.5: Coordinate reference frames for Fanuc 210F

frame 5 As z_5 lies in line with O_4 , the axes z_5 and z_4 intersect in O_4 which puts O_5 at the same position as O_4 . x_5 leaves the plane spanned by z_5 and z_4 perpendicular. The positive direction of x_5 is chosen to be similar as in frame 4 for simplicity, which puts x_5 and x_4 on top of each other. y_5 is added according to the right hand rule and as z_5 is turned 90 degrees relative to z_4 around $x_{4,5}$, y_5 is turned 90 degrees relative to z_4 around $x_{4,5}$ as well.

frame 6 (EOAT) z_6 lies in line with z_5 and is consequently parallel. as there are no distal joints, to reference x_6 , it can be chosen arbitrarily. For simplicity, it is chosen to be similar as in frame 5. y_6 is added according to the right hand rule.

9.1.2.3 Establishing DH parameters on the Fanuc 210F

As described in [subsubsection 9.1.1.3 Establishing DH parameters for each link](#), the DH-Parameters can also be determined for the Fanuc 210F. These parameters can be found with the help of the assigned coordinate frames as seen in figure [9.6](#). For simplicity, only non-zero DH-parameters are shown in this figure.

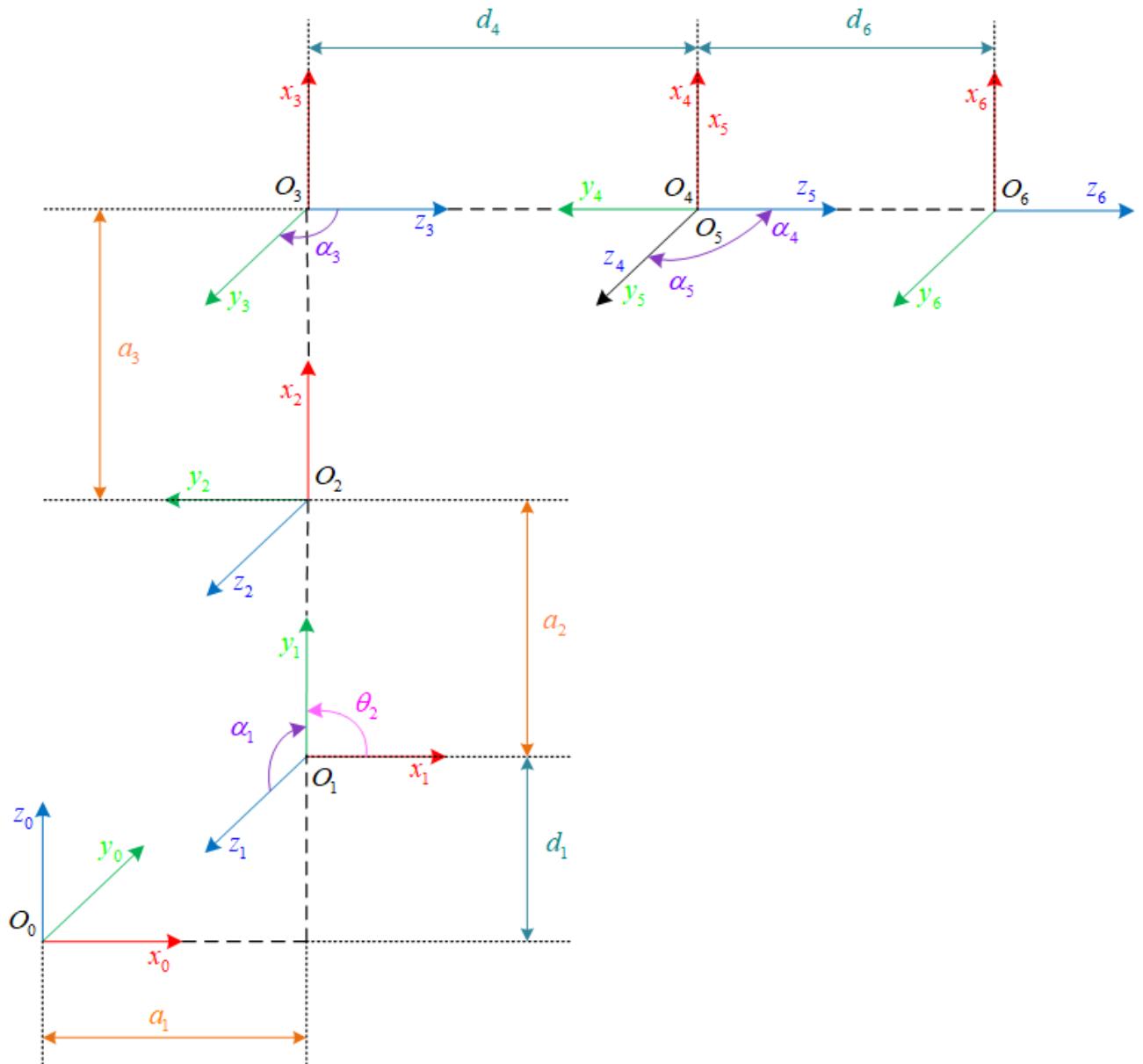


Figure 9.6: Assignment of DH-Parameters on the Fanuc 210F

To wrap this up, a summary of the D-H parameters for each link as follows from figure 9.6 can be found in table 9.1

Link	θ_i	d_i	a_i	α_i
1	θ_1	d_1	a_1	α_1
2	θ_2	0	a_2	0
3	θ_3	0	a_3	α_3
4	θ_4	d_4	0	α_4
5	θ_5	0	0	α_5
6	θ_6	d_6	0	0

Table 9.1: Denavit Hartenberg Parameters for Fanuc 210F

numeric values of DH-Parameters As can be seen from table 9.1, many DH-parameters are zero due to a good choice of pose and coordinate frames. All angles are plus or minus 90°.

Most of the frames have translational transformations in either a_i or d_i direction with link 1 and 5 being the exception. By lifting the base frame out of the joint, parameter d_1 could be set to zero as well. For better understanding, the origin of the frame was originally kept inside the joint. Frame 5 shares the origin with frame 4, not requiring any translational movement. Most of the frames are also rotated by 90 degree around

the x-axis with link 2 and 6 being the exception. Frame 6 was chosen with the same orientation as frame 5. Frame 2 has the same x-axis orientation as link 1 because joints two and three are parallel. There is just a rotational transformation around the z-axis of 90°. This is only due to the standard pose of the robot, as theta is a variable. For all coordinate frames theta is a variable, as all joints are revolute and none is translational. Besides the angle values for α_i which were easy to determine from the graphical interpretation in figure 9.6, following numeric values need to be determined through measurements or CAD-Drawings: d_1 , d_4 , d_6 and a_1 , a_2 , a_3 .

A great help to determine these values is fig 9.4. This technical drawing was obtained from the datasheet for all Fanuc R-2000iB series robots. With this drawing, following DH-parametes can be obtained:

$$a_1 = 312 \text{ [mm]}$$

$$a_2 = 1075 \text{ [mm]}$$

$$a_3 = 225 \text{ [mm]}$$

$$d_4 = 1280 \text{ [mm]}$$

$$d_6 = 235 \text{ [mm]}$$

The parameter d_1 cannot be determined from this drawing. It can either be measured on the actual robot, or defined as zero, as frame zero can be freely moved along the z-axis. A value of zero would put the origin of the base frame on the same height as frame 1, simplifying subsequent steps. It must be clear though, that all referencing in the forward and backward kinematics will be relative to this point. A change of this point of reference can be added later simply by adding another transformation matrix for translational movement along the z-axis as presented by Richard P. Paul [30].

This results in a table of numeric DH-parameters as seen in 9.2. The transformation ${}^{i-1}T_i$ depends only on a single variable θ_i as all of the other quantities stay constant, and all joints are revolute.

Link	θ_i	d_i	a_i	α_i
1	θ_1	0	312	$\pi/2$
2	θ_2	0	1075	0
3	θ_3	0	225	$\pi/2$
4	θ_4	1280	0	$-\pi/2$
5	θ_5	0	0	$\pi/2$
6	θ_6	235	0	0

Table 9.2: Numeric values of Denavit Hartenberg Parameters for Fanuc 210F

9.1.2.4 Calculate homogeneous transformation matrices

For further details on how to set up $R_z(\theta_i)$, $T_z(d_i)$, $T_x(a_i)$ and $R_x(\alpha_i)$ and form the transformation matrix in equation 9.3 see chapter one "HOMOGENEOUS TRANSFORMATIONS" in "Robot manipulators: mathematics, programming, and control: the computer control of robot manipulators" [30]. The basic techniques for setting up the translation and rotation matrices as well as how to combine them are described in that chapter .

9.1.2.5 Forward Kinematic Equations on the 210F

As shown in fig.9.3, the Fanuc 210F is a 6-DOF robotic arm with n=six revolute joints in series. Their orientation can be expressed in short form with

$$(R \perp R \parallel R \perp R \perp R \perp R) \quad (9.9)$$

With this, the complete transformation matrix can be derived in the form as described in 9.1.1.5:

$${}^0T_6 =$$

$$\begin{bmatrix}
\cos \theta_1 & -\sin \theta_1 * \cos \alpha_1 & \sin \theta_1 * \sin \alpha_1 & a_1 * \cos \theta_1 \\
\sin \theta_1 & \cos \theta_1 * \cos \alpha_1 & -\cos \theta_1 * \sin \alpha_1 & a_1 * \sin \theta_1 \\
0 & \sin \alpha_1 & \cos \alpha_1 & d_1 \\
0 & 0 & 0 & 1
\end{bmatrix} *$$

$$\begin{bmatrix}
\cos \theta_2 & -\sin \theta_2 * \cos \alpha_2 & \sin \theta_2 * \sin \alpha_2 & a_2 * \cos \theta_2 \\
\sin \theta_2 & \cos \theta_2 * \cos \alpha_2 & -\cos \theta_2 * \sin \alpha_2 & a_2 * \sin \theta_2 \\
0 & \sin \alpha_2 & \cos \alpha_2 & d_2 \\
0 & 0 & 0 & 1
\end{bmatrix} *$$

$$\begin{bmatrix}
\cos \theta_3 & -\sin \theta_3 * \cos \alpha_3 & \sin \theta_3 * \sin \alpha_3 & a_3 * \cos \theta_3 \\
\sin \theta_3 & \cos \theta_3 * \cos \alpha_3 & -\cos \theta_3 * \sin \alpha_3 & a_3 * \sin \theta_3 \\
0 & \sin \alpha_3 & \cos \alpha_3 & d_3 \\
0 & 0 & 0 & 1
\end{bmatrix} *$$

$$\begin{bmatrix}
\cos \theta_4 & -\sin \theta_4 * \cos \alpha_4 & \sin \theta_4 * \sin \alpha_4 & a_4 * \cos \theta_4 \\
\sin \theta_4 & \cos \theta_4 * \cos \alpha_4 & -\cos \theta_4 * \sin \alpha_4 & a_4 * \sin \theta_4 \\
0 & \sin \alpha_4 & \cos \alpha_4 & d_4 \\
0 & 0 & 0 & 1
\end{bmatrix} *$$

$$\begin{bmatrix}
\cos \theta_5 & -\sin \theta_5 * \cos \alpha_5 & \sin \theta_5 * \sin \alpha_5 & a_5 * \cos \theta_5 \\
\sin \theta_5 & \cos \theta_5 * \cos \alpha_5 & -\cos \theta_5 * \sin \alpha_5 & a_5 * \sin \theta_5 \\
0 & \sin \alpha_5 & \cos \alpha_5 & d_5 \\
0 & 0 & 0 & 1
\end{bmatrix} *$$

$$\begin{bmatrix}
\cos \theta_6 & -\sin \theta_6 * \cos \alpha_6 & \sin \theta_6 * \sin \alpha_6 & a_6 * \cos \theta_6 \\
\sin \theta_6 & \cos \theta_6 * \cos \alpha_6 & -\cos \theta_6 * \sin \alpha_6 & a_6 * \sin \theta_6 \\
0 & \sin \alpha_6 & \cos \alpha_6 & d_6 \\
0 & 0 & 0 & 1
\end{bmatrix}$$

(9.10)

This set of matrices can be filled with the numerical values from table 9.2:

$${}^0T_6 =$$

$$\begin{bmatrix}
\cos \theta_1 & -\sin \theta_1 * \cos(\pi/2) & \sin \theta_1 * \sin(\pi/2) & 312 * \cos \theta_1 \\
\sin \theta_1 & \cos \theta_1 * \cos(\pi/2) & -\cos \theta_1 * \sin(\pi/2) & 312 * \sin \theta_1 \\
0 & \sin(\pi/2) & \cos(\pi/2) & 0 \\
0 & 0 & 0 & 1
\end{bmatrix} *$$

$$\begin{bmatrix}
\cos \theta_2 & -\sin \theta_2 * \cos(0) & \sin \theta_2 * \sin(0) & 1075 * \cos \theta_2 \\
\sin \theta_2 & \cos \theta_2 * \cos(0) & -\cos \theta_2 * \sin(0) & 1075 * \sin \theta_2 \\
0 & \sin(0) & \cos(0) & 0 \\
0 & 0 & 0 & 1
\end{bmatrix} *$$

$$\begin{bmatrix}
\cos \theta_3 & -\sin \theta_3 * \cos(\pi/2) & \sin \theta_3 * \sin(\pi/2) & 225 * \cos \theta_3 \\
\sin \theta_3 & \cos \theta_3 * \cos(\pi/2) & -\cos \theta_3 * \sin(\pi/2) & 225 * \sin \theta_3 \\
0 & \sin(\pi/2) & \cos(\pi/2) & 0 \\
0 & 0 & 0 & 1
\end{bmatrix} *$$

$$\begin{bmatrix}
\cos \theta_4 & -\sin \theta_4 * \cos(-\pi/2) & \sin \theta_4 * \sin(-\pi/2) & 0 * \cos \theta_4 \\
\sin \theta_4 & \cos \theta_4 * \cos(-\pi/2) & -\cos \theta_4 * \sin(-\pi/2) & 0 * \sin \theta_4 \\
0 & \sin(-\pi/2) & \cos(-\pi/2) & 1280 \\
0 & 0 & 0 & 1
\end{bmatrix} *$$

$$\begin{bmatrix}
\cos \theta_5 & -\sin \theta_5 * \cos(\pi/2) & \sin \theta_5 * \sin(\pi/2) & 0 * \cos \theta_5 \\
\sin \theta_5 & \cos \theta_5 * \cos(\pi/2) & -\cos \theta_5 * \sin(\pi/2) & 0 * \sin \theta_5 \\
0 & \sin(\pi/2) & \cos(\pi/2) & 0 \\
0 & 0 & 0 & 1
\end{bmatrix} *$$

$$\begin{bmatrix}
\cos \theta_6 & -\sin \theta_6 * \cos(0) & \sin \theta_6 * \sin(0) & 0 * \cos \theta_6 \\
\sin \theta_6 & \cos \theta_6 * \cos(0) & -\cos \theta_6 * \sin(0) & 0 * \sin \theta_6 \\
0 & \sin(0) & \cos(0) & 235 \\
0 & 0 & 0 & 1
\end{bmatrix}$$

(9.11)

With some simplification this results in the following equation:

$${}^0T_6 =$$

$$\begin{bmatrix}
\cos \theta_1 & 0 & \sin \theta_1 & 312 * \cos \theta_1 \\
\sin \theta_1 & 0 & -\cos \theta_1 & 312 * \sin \theta_1 \\
0 & 1 & 0 & 0 \\
0 & 0 & 0 & 1
\end{bmatrix} *
\begin{bmatrix}
\cos \theta_2 & -\sin \theta_2 & 0 & 1075 * \cos \theta_2 \\
\sin \theta_2 & \cos \theta_2 & 0 & 1075 * \sin \theta_2 \\
0 & 0 & 1 & 0 \\
0 & 0 & 0 & 1
\end{bmatrix} *
\begin{bmatrix}
\cos \theta_3 & 0 & \sin \theta_3 & 225 * \cos \theta_3 \\
\sin \theta_3 & 0 & -\cos \theta_3 & 225 * \sin \theta_3 \\
0 & 1 & 0 & 0 \\
0 & 0 & 0 & 1
\end{bmatrix} *
\begin{bmatrix}
\cos \theta_4 & 0 & -\sin \theta_4 & 0 \\
\sin \theta_4 & 0 & \cos \theta_4 & 0 \\
0 & -1 & 0 & 1280 \\
0 & 0 & 0 & 1
\end{bmatrix} *
\begin{bmatrix}
\cos \theta_5 & 0 & \sin \theta_5 & 0 \\
\sin \theta_5 & 0 & -\cos \theta_5 & 0 \\
0 & 1 & 0 & 0 \\
0 & 0 & 0 & 1
\end{bmatrix} *
\begin{bmatrix}
\cos \theta_6 & -\sin \theta_6 & 0 & 0 \\
\sin \theta_6 & \cos \theta_6 & 0 & 0 \\
0 & 0 & 1 & 235 \\
0 & 0 & 0 & 1
\end{bmatrix}$$

(9.12)

With matrix 9.5, the forward kinematic equations can be formed:

$$\begin{aligned}
n_x &= \\
&\cos \theta_1 (\cos(\theta_2 + \theta_3)(\cos \theta_4 \cos \theta_5 \cos \theta_6 - \sin \theta_4 \sin \theta_6) - \sin(\theta_2 + \theta_3) \sin \theta_5 \cos \theta_6) \\
&+ \sin \theta_1 (\sin \theta_4 \cos \theta_5 \cos \theta_6 - \cos \theta_4 \sin \theta_6) \\
n_y &= \\
&\sin \theta_1 (\cos(\theta_2 + \theta_3)(\cos \theta_4 \cos \theta_5 \cos \theta_6 - \sin \theta_4 \sin \theta_6) - \sin(\theta_2 + \theta_3) \sin \theta_5 \cos \theta_6) \\
&- \cos \theta_1 (\sin \theta_4 \cos \theta_5 \cos \theta_6 - \cos \theta_4 \sin \theta_6) \\
n_z &= \\
&\sin(\theta_2 + \theta_3)(\cos \theta_4 \cos \theta_5 \cos \theta_6 - \sin \theta_4 \sin \theta_6) - \cos(\theta_2 + \theta_3) \sin \theta_5 \cos \theta_6 \\
o_x &= \\
&\cos \theta_1 (-\cos(\theta_2 + \theta_3)(\cos \theta_4 \cos \theta_5 \sin \theta_6 + \sin \theta_4 \cos \theta_6) - \sin(\theta_2 + \theta_3) \sin \theta_5 \sin \theta_6) \\
&- \sin \theta_1 (\sin \theta_4 \cos \theta_5 \sin \theta_6 - \cos \theta_4 \sin \theta_6) \\
o_y &= \\
&\sin \theta_1 (-\cos(\theta_2 + \theta_3)(\cos \theta_4 \cos \theta_5 \sin \theta_6 + \sin \theta_4 \cos \theta_6) - \sin(\theta_2 + \theta_3) \sin \theta_5 \sin \theta_6) \\
&+ \cos \theta_1 (\sin \theta_4 \cos \theta_5 \sin \theta_6 - \cos \theta_4 \sin \theta_6) \\
o_z &= \\
&-\sin(\theta_2 + \theta_3)(\cos \theta_4 \cos \theta_5 \sin \theta_6 + \sin \theta_4 \sin \theta_6) - \cos(\theta_2 + \theta_3) \sin \theta_5 \sin \theta_6 \\
a_x &= \\
&\cos \theta_1 (\cos(\theta_2 + \theta_3) \cos \theta_4 \sin \theta_5 + \sin(\theta_2 + \theta_3) \cos \theta_5) + \sin \theta_1 \sin \theta_4 \sin \theta_5 \\
a_y &= \\
&\sin \theta_1 (\cos(\theta_2 + \theta_3) \cos \theta_4 \sin \theta_5 + \sin(\theta_2 + \theta_3) \cos \theta_5) + \cos \theta_1 \sin \theta_4 \sin \theta_5 \\
a_z &= \\
&\sin(\theta_2 + \theta_3) \cos \theta_4 \sin \theta_5 - \cos(\theta_2 + \theta_3) \cos \theta_5 \\
p_x &= \\
&\cos \theta_1 (a_1 + a_2 \cos \theta_2 + a_3 \cos(\theta_2 + \theta_3) + d_4 \sin(\theta_2 + \theta_3) + d_6 (\cos(\theta_2 + \theta_3) \cos \theta_4 \sin \theta_5 + \sin(\theta_2 + \theta_3) \cos \theta_5)) \\
&+ d_6 \sin \theta_1 \sin \theta_4 \sin \theta_5 \\
p_y &= \\
&\sin \theta_1 (a_1 + a_2 \cos \theta_2 + a_3 \cos(\theta_2 + \theta_3) + d_4 \sin(\theta_2 + \theta_3) + d_6 (\cos(\theta_2 + \theta_3) \cos \theta_4 \sin \theta_5 + \sin(\theta_2 + \theta_3) \cos \theta_5)) \\
&+ d_6 \sin \theta_1 \sin \theta_4 \sin \theta_5 \\
p_z &= \\
&a_2 \sin \theta_2 + a_3 \sin(\theta_2 + \theta_3) - d_4 \cos(\theta_2 + \theta_3) + d_6 (\sin(\theta_2 + \theta_3) \cos \theta_4 \sin \theta_5 - \cos(\theta_2 + \theta_3) \cos \theta_5)
\end{aligned}$$

(9.13)

In these equations, the numerical values were replaced with their parameter name. These numeric values can be found in section 9.1.2.3.

These kinematic equations can be used to simulate the movements of a robot with given angle-values for the joints.

9.2 Inverse Kinematics

With the forward kinematic equations, the position of the end effector can be determined relative to the base frame for given values of the joint variables. In the context of robotics, it is also necessary to determine these joint variables for a given end effector position. This is referred to as the inverse kinematic problem. Solving the inverse kinematic problem for a given serial link actuator allows to transform a motion plan of the EOAT into joint actuator trajectories for the robot.

9.2.1 Existence of solutions

To determine the joint values for a EOAT-position it needs to be determined, if there exists a solution. Not all positions are equally reachable. There are two types of workspace:

Dextrous workspace volume of space that the robot end-effector can reach with all orientations

reachable workspace volume of space, that the robot can reach in at least one orientation

([10], ch4, p.102)

A manipulator with less than 6DOF cannot reach all positions and orientations in 3D-space. Further limitations can be imposed by the axis alignment. A planar manipulator for example cannot reach out of the plane. [10]

9.2.2 multiple solutions

A 6DOF robot has multiple sets of inverse solutions. To understand why there are multiple solutions, it helps to have a look at fig. ???. The same end effector position and orientation can be reached in two ways.

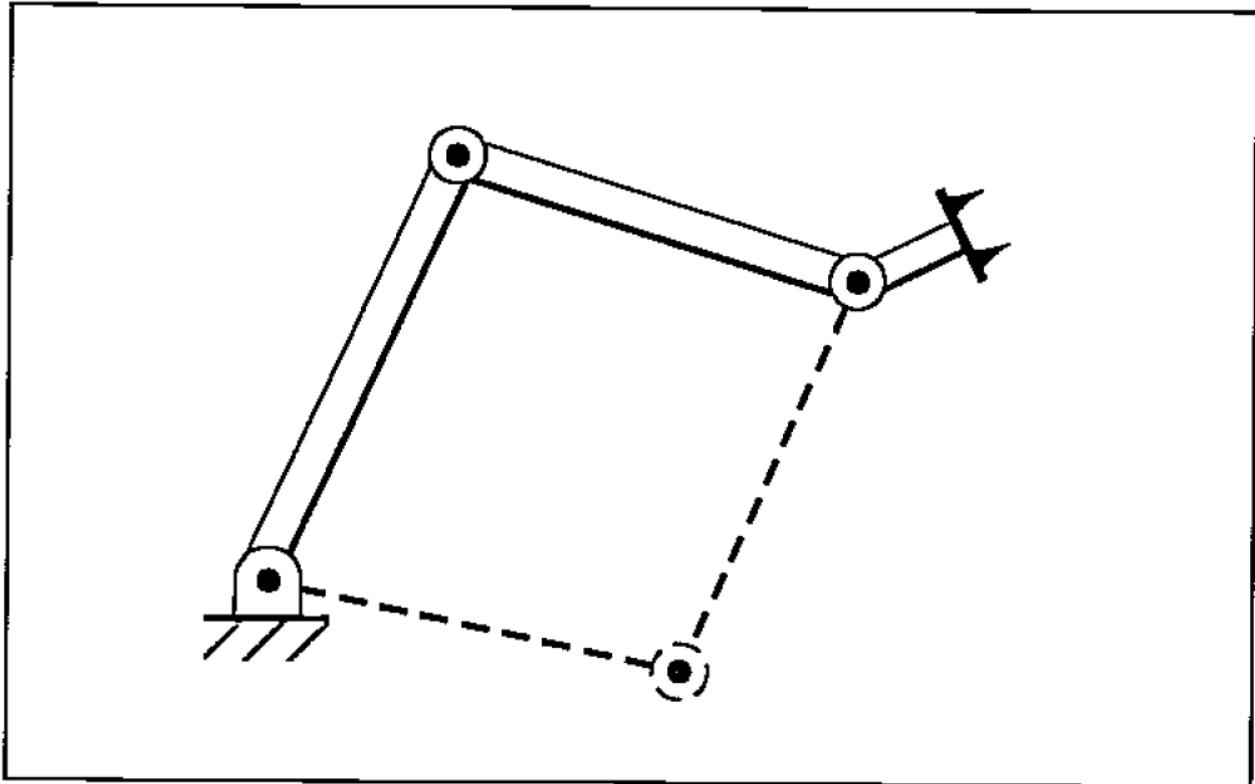


Figure 9.7: Three link manipulator with 2 solutions

This can be extended to the 6DOF serial link manipulators. As stated by YanWu et al. there are 8 groups of inverse solution for most EOAT-positions within the manipulator's workspace [55].

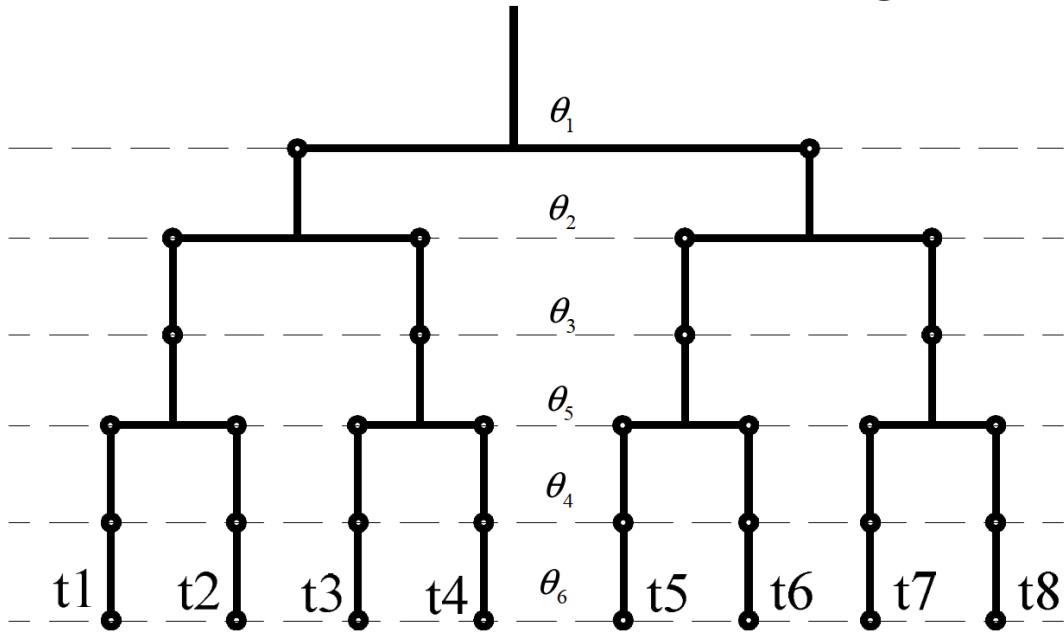


Figure 9.8: Tree of inverse solutions ([55], fig.2)

9.2.3 Inverse solution of 6 DOF Robot

As shown in chapter 9.1.1.5 the end effector position is defined by four 3×1 vectors (n, o, a, p). With these known, the joint variables ($\theta_1, \theta_2, \theta_3, \theta_4, \theta_5, \theta_6$) can be calculated. This problem is solved by the method of using the inverse transformation of unknown link pre-multiplication as presented by Yan Wu et al. [55].

Forward kinematic equation For a 6DOF Robot, the forward kinematic matrix equation from equation eqs. (9.4) and (9.5) can be reformulated into equation 9.14

$${}^6T = \begin{bmatrix} n_x & o_x & a_x & p_x \\ n_y & o_y & a_y & p_y \\ n_z & o_z & a_z & p_z \\ 0 & 0 & 0 & 1 \end{bmatrix} = {}^0T(\theta_1){}^1T(\theta_2){}^2T(\theta_3){}^3T(\theta_4){}^4T(\theta_5){}^5T(\theta_6) \quad (9.14)$$

9.2.4 The inverse Solution

With (n, o, a, p) known, the angle values of the joint variables can be determined by separation of the joint variables. In a first step eq. 9.14 is reformed into eq. 9.15.

$${}^2T_3 {}^3T_4 {}^4T_5 = {}^0T_6({}^0T_1)^{-1}({}^1T_2)^{-1}({}^5T_6)^{-1} \quad (9.15)$$

This gives 2 matrices, formed by the terms found in eq. 9.10. These matrices are the terms found in eq. 9.15. With the help of MATLAB and the symbolic toolbox, the inverses and the overall product of each side can be calculated.

$${}^2T_3 {}^3T_4 {}^4T_5 =$$

$$\begin{array}{cccc} 1 & 2 & 3 & 4 \\ \left(\begin{array}{c} c_3 c_4 c_5 - s_3 s_5 \\ s_3 c_4 c_5 + c_3 s_5 \\ -s_4 c_5 \\ 0 \end{array} \right) & \left(\begin{array}{c} -c_3 c_4 s_5 - s_3 c_5 \\ -s_3 c_4 s_5 + c_3 c_5 \\ s_4 s_5 \\ 0 \end{array} \right) & \left(\begin{array}{c} c_3 s_4 \\ s_3 s_4 \\ c_4 \\ 0 \end{array} \right) & \left(\begin{array}{c} c_3 a_3 - s_3 d_4 + a_2 \\ s_3 a_3 + c_3 d_4 \\ 0 \\ 1 \end{array} \right) \end{array} \quad (9.16)$$

In equations eqs. (9.16) and (9.17) $\sin(\theta_i)$ and $\cos(\theta_i)$ have been replaced by s_i and c_i to allow for appropriate presentation of the matrix. This abbreviation will be used for following steps as well.

As shown by eq. 9.15, the elements of matrices eqs. (9.16) and (9.17) are corresponding equal. This allows to find analytic expressions for all θ_i . As stated in section 9.2.2, there are two solutions for each θ_i .

θ_1 : By taking the elements (3,4) of equations eqs. (9.16) and (9.17) as corresponding equal, equation 9.18 is formed.

$$-(-s_1 a_x + c_1 a_y) d_6 - s_1 p_x + c_1 p_y = 0 \quad (9.18)$$

Reforming equation 9.18 gives a solution for θ_1 as seen in equation 9.19.

$$\theta_{1_1} = \text{atan2}(p_y - a_y d_6, p_x - a_x d_6) \quad \theta_{1_2} = \text{atan2}(-p_y + a_y d_6, -p_x + a_x d_6) \quad (9.19)$$

θ_2 : Taking elements (1,4) and (2,4) of equations eqs. (9.16) and (9.17) as corresponding equal, equations 9.20 and 9.21 are formed.

$$a_3c_3 - d_4s_3 + a_2 = -(c_2c_1a_x + c_2s_1a_y - s_2a_z)d_6 + c_2c_1p_x + c_2s_1p_y - s_2p_z - c_2a_1 \quad (9.20)$$

$$a_3s_3 + d_4c_3 = -(-s_2c_1a_x - s_2s_1a_y - c_2a_z)d_6s_2c_1p_xs_2s_1p_y - c_2p_z + s_2a_1 \quad (9.21)$$

For simplification of the terms in equations eqs. (9.20) and (9.21), middle variables are chosen:

$$u = c_1(p_x d_6 a_x) + s_1(p_y - a_y d_6) - a_1 \dots] v = p_z - a_z d_6 \quad (9.22)$$

With these middle variables equations eqs. (9.20) and (9.21) can be rewritten as seen in eqs. (9.23) and (9.24).

$$a_3c_3 - d_4s_3 = c_2u - s_2v - a_2 \quad (9.23)$$

$$a_3s_3 + d_4c_3 = -s_u - c_2v \quad (9.24)$$

To eliminate s_3 and c_3 equations eqs. (9.23) and (9.24) are squared and then added to form 9.25.

$$a_3^2 + d_4^2 = u^2 + v^2 - 2a_2c_2u + 2a_2s_2v + a_2^2 \quad (9.25)$$

$$\frac{a_3^2 + d_4^2 - u^2 - v^2 - a_2^2}{-2a_2} = c_2u - s_2v \quad (9.26)$$

This equation can be further simplified by taking another middle variable:

$$m = \frac{a_3^2 + d_4^2 - u^1 - v^2 - a_2^2}{-2a_2}$$

Reforming equation 9.26 and inserting the middle variable reveals a solution for θ_2 as seen in eq 9.27.

$$\theta_{2_{1/2}} = \text{atan2}(-v, u) \pm \text{atan2}(\sqrt{v^2 + u^2 - m^2}, m) \quad (9.27)$$

θ_3 : To receive θ_3 it helps to take equations eqs. (9.20) and (9.21). Equation 9.20 needs to be reformed into 9.28

$$a_c c_3 d_4 s_3 + a_2 = c_2 u - s_2 v \quad (9.28)$$

Squaring of equations eqs. (9.21) and (9.28) and adding them eliminates s_2 and c_2 as seen in eq 9.29

$$a_2^2 + a_3^2 + d_4^2 + 2a_2(a_3 c_3 - d_4 s_3) = u^2 + v^2 \quad (9.29)$$

$$a_3 c_3 - d_4 s_3 = \frac{a_3^2 + d_4^2 - u^2 - v^2 + a_2^2}{2a_2} \quad (9.30)$$

Again, this equation can be further simplified by taking another middle variable:

$$\frac{a_3^2 + d_4^2 - u^2 - v^2 + a_2^2}{2a_2}$$

Reforming equation 9.30 and inserting the middle variable reveals a solution for θ_3 as seen in eq 9.31.

$$\theta_{3_{1/2}} = \text{atan2}(-d_4, a_3) \pm A \tan(2(\sqrt{d_4^2 + a_3^2 - h^2}, h)) \quad (9.31)$$

θ_5 : Taking elements (2,2) and (1,2) of equations eqs. (9.16) and (9.17) as corresponding equal, equations 9.32 and 9.33 are formed.

$$-s_3 c_4 s_5 + c_3 c_5 = -c_1 s_2 a_x - s_1 s_2 a_y - c_2 a_z \quad (9.32)$$

$$-c_3 c_4 s_5 - s_3 c_4 = c_1 c_2 a_x + s_1 c_2 a_y - s_2 a_z \quad (9.33)$$

To combine equations eqs. (9.32) and (9.33), eq 9.32 is multiplied with c_3 and eq 9.33 is multiplied by s_2 . The resulting equations are then subtracted from each other giving eq 9.34.

$$c_5 = (-c_1 s_2 a_x - s_1 s_2 a_y - c_2 a_z)c_3 - (c_1 c_2 a_x + s_1 c_2 a_y - s_2 a_z)s_3 \quad (9.34)$$

Reforming equation 9.34 gives a solution for θ_5 as seen in equation 9.35.

$$\theta_{5_{1/2}} = \pm \text{acos}[(-c_1 s_2 a_x - s_1 s_2 a_y - c_2 a_z)c_3 - (c_1 c_2 a_x + s_1 c_2 a_y - s_2 a_z)s_3] \quad (9.35)$$

θ_4 : With θ_5 and θ_{1-3} known, equation 9.33 can be reformed into a solution for θ_4 as seen in equation 9.36

$$\theta_{4_{1/2}} = \pm \text{arccos}\left[\frac{c_1 c_2 a_x + s_1 c_2 a_y - s_2 a_z + s_3 c_5}{-c_3 s_5}\right] \quad (9.36)$$

θ_6 : By taking the elements (3,3) of equations eqs. (9.16) and (9.17) as corresponding equal, equation 9.37 is formed.

$$s_6(s_1 n_x - c_1 n_y) + c_6(s_1 o_x - c_1 o_y) = c_4 \quad (9.37)$$

With θ_4 and θ_1 known, equation 9.37 can be reformed into a solution for θ_6 as seen in equation 9.38.

$$\theta_{6_{1/2}} = \text{atan2}(s_1 n_x - c_1 n_y, s_1 o_x - c_1 o_y) \pm \text{atan2}(\sqrt{(s_1 n_x - c_1 n_y)^2 + (s_1 o_x - c_1 o_y)^2 - c_4^2}, c_4) \quad (9.38)$$

With equations eqs. (9.19), (9.27), (9.31), (9.35), (9.36) and (9.38) the values for $(\theta_1, \theta_2, \theta_3, \theta_4, \theta_5, \theta_6)$ can be calculated for all reachable end effector positions.

The $\text{atan2}(x, y)$ -function used in this solution which returns an angle between the positive x axis and a line pointing to $(x, y) \neq (0, 0)$. The function takes two arguments and returns a single value θ between $-\pi$ and π equivalent to the phase angle of complex numbers. While arctan can only solve in quadrant 1 and 4, arctan2 allows for calculation in all four quadrants because it differentiates between pos/neg x and y direction independently. It is mostly a question of implementation and solving method, so this new notation arose with programming languages.

9.2.5 Optimization of inverse kinematics solution

As stated in section 9.2.2, there exist eight sets of inverse solutions in the dexterous workspace (see 9.2.1). The optimal set of solutions can be found through an optimization function. This optimization function needs to find the set of solution that can reach the desired position fastest from the current position.

cost function Equation 9.39 is the cost function to be minimized.

$\theta_i(k+1)$: target angle

$\theta_i(k)$: departing angle

k_i power value

$$err = \min \sum_{i=1}^6 k_i [\theta_i(k+1) - \theta_i(k)] \quad (9.39)$$

As can be seen, this cost function minimizes the sum of angles over all axes for the movement of the end effector from position $[n_i, o_i, a_i, p_i]$ to $[n_{i+1}, o_{i+1}, a_{i+1}, p_{i+1}]$ by using the inverse solution presented in chapter 9.2.4.

limitations of cost function This cost function not necessarily gives the fastest path, as it does not account for the actual movement speed of the different axes. A possible solution for this would require multiplying with a cost factor between 0 and 1 for each joint (1 for the slowest joint) with the respective angle error to account for the difference in angular velocity.

description of implementation An implementation of this function receives the current position either in joint angles or Cartesian coordinates of the end-effector which could be given in form of a rotation matrix as seen in eq9.5 or in form of euclidean space and euler angle coordinates. $[x, y, z, \alpha, \beta, \gamma]$ which could be transformed by the inverse of equation 9.6 into a rotation matrix.

This algorithm would then start the calculation to get all possible paths in the tree of inverse solutions (see figure 9.8) for position $i + 1$.

algorithm for minimal computational effort To minimize the computational effort, following algorithm is proposed by Yan Wu et al. [55]:

1. The calculation starts with θ_1 by finding the two solutions for equation 9.19.
2. When calculating θ_2 :
 - (a) The term $v^2 + u^2 - m^2$ should be > 0 , otherwise the program can terminate the calculation of the subsequent steps of this group, return $err = inf$ or Nan , and provide a variable like $P = 1$ to determine the cause for the abortion of subsequent steps.
 - (b) If there is a solution for θ_2 it needs to be tested for extraneous roots. An extraneous root is introduced into an equation in the process of solving another equation, but is not a solution of the equation to be solved [46]. This test is done simply by substituting the solution for θ_2 into the original equation 9.25. If an extraneous root is found, the program can terminate and return $err = inf$ or Nan and $P = 2$ for cause of abortion.
3. If the calculation has been continued, θ_3 can be determined. Again a test for extraneous roots is necessary.
4. When calculating θ_5 , test for extraneous roots.
5. When calculating θ_4 , test for extraneous roots.
6. calculate θ_6
7. determine error as seen in eq 9.39 for all possible paths
8. find $\min(err(t_1^8))$

The resulting set of angle values is the result of the algorithm. It is the unique inverse solution, determined easiest to reach with the given cost function in eq 9.39.

10. Dynamic Modelling

10.1 Denavit-Hartenberg-Convention

The DH-Convention is a commonly used and simplifies the forward and backward transformation. It was named after Jaques Denavit and Richard Hartenberg who developed a general theory to describe a serial link mechanism. [24]

It consists of following parts:

- DH-Convention for establishing the coordinate systems
- DH-Transformation for generation of the coordinate systems
- DH-Parameters as a result form the transformations

Determining the coordinate systems is done according to set rules. Nevertheless, the choices of coordinate frames are also not unique, so different people will derive different, but correct frame assignments. This freedom of choice should be used to bring as many DH-Parameters as possible to zero. This simplifies subsequent equations and calculations. [56]

Each joint of the robot is described by four parameters.

10.2 Robot configurations

As mentioned before, a 6 DOF manipulator can reach the same position in multiple configurations. The different configurations in the solutions can be seen in the example of the FANUC robot arms (see figure 10.1)

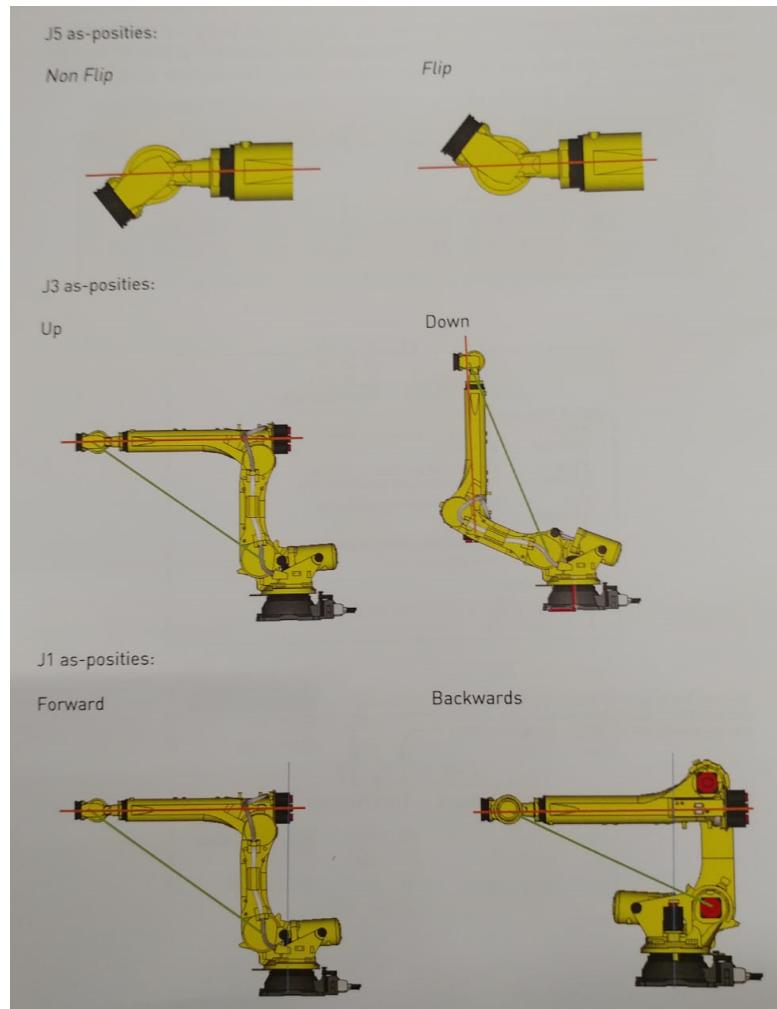


Figure 10.1: 6 axis robot configurations on the example of a FANUC Robot [15]

11. Development of a control strategy

12. Conclusions and further work

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Appendices

A. Appendix 1

B. Appendix 2

C. Robot Quick start guide

A big part of this was derived from [48].

C.1 Parts of the robot

A quick overview over the visible parts.

C.1.0.1 FANUC R-2000iC/210F 6 axis robotic arm

The robot has 6 movable joints with a possible payload attached to the end. Its features include a wide reach (2655 mm), sturdy but flexible arm design, a spring loaded counterbalance, relatively high payload capacity (210Kg) and fast moving axes. The joints also have hashes to indicate the zero positions which help with the calibration of the robot.

C.1.1 R30iA Robot Controller

The Robot is controlled using an original equipment manufacturer controller called the FANUC R30iA controller. Its features include faster sustained speed and superior position accuracies. It also has the I/O ports that are used to connect grippers and other payloads. (It also houses the camera circuits which are required to access the data from the SONY camera provided with the robot. - Delta only) The controller is also provided with a data card slot in which the special SD cards manufactured can be inserted and used as external memory. On the outside of the controller (side of iPendant at Delta) a USB port can be found. With these, programs, firmware files and other files can easily be transferred. Additionally, there is extended connectivity via its Ethernet port e.g. for FTP available.

C.1.2 iPendant

The teaching pendant is the primary user interface to the robot. It is used to move the joints of the robot manually, to program specific trajectories, to control the gripper, and various other actions. It also is an interface that can be used for input and output of the robot controller parameters. The user can access the system variables and position variables. (It is provided with a USB port that can be used to connect to a USB

drive for external storage. - Delta only) It can also be used to setup an FTP server and client in order to communicate with the PC.

C.1.2.1 Gripper

The robot as handed over does not have an active gripper system. It has been tested though with a pneumatic gripper controlled via the DO ports and pneumatic valves. A 2-way pneumatic valve, some piping and a pressure regulator are still available. (Delta Equipment varies here a lot).

C.2 iPendant Navigation Manual:

The teaching pendant is the primary user interface to the robot. This section deals with the important buttons on the TP.

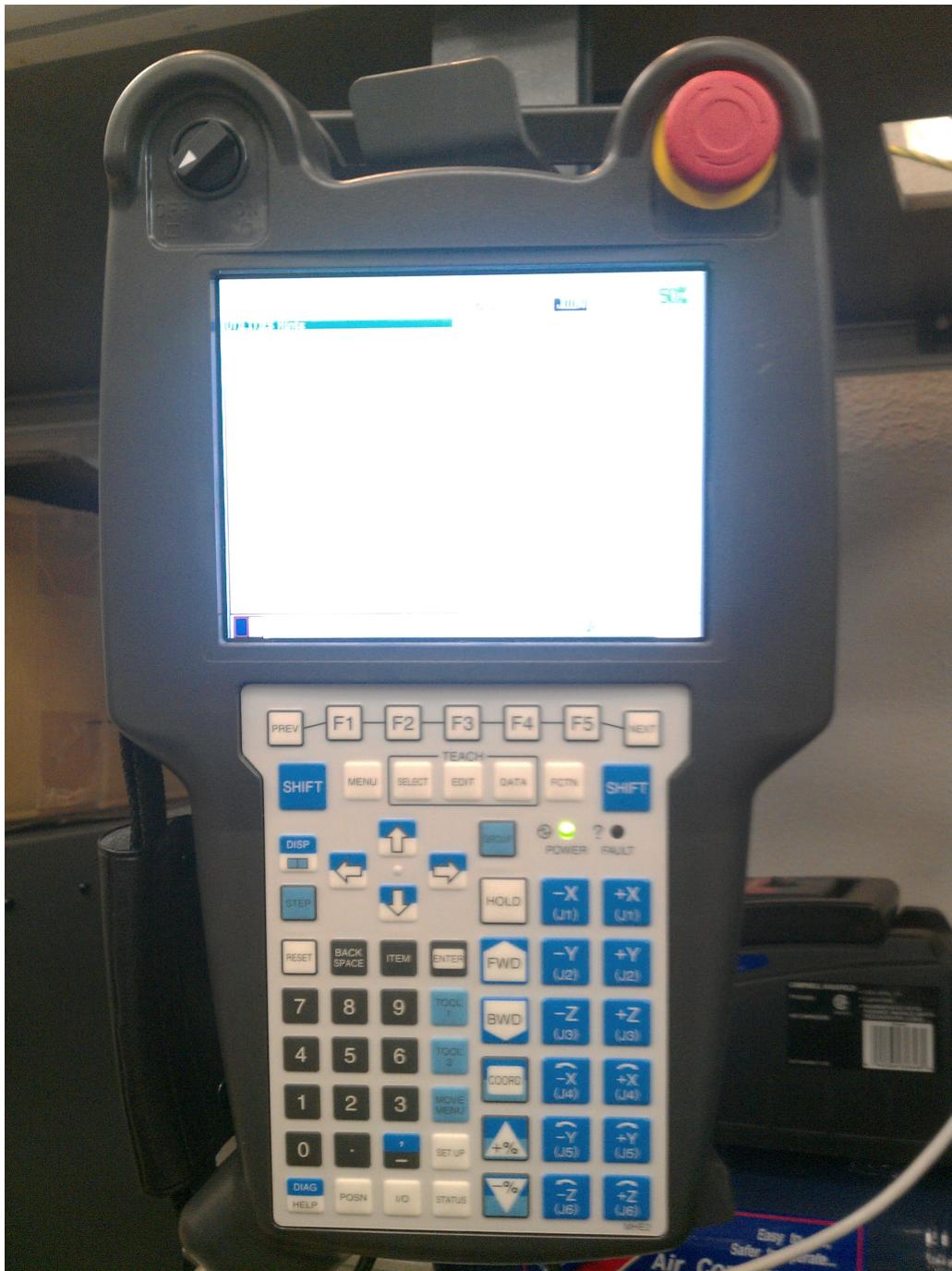


Figure C.1: Most important iPendant buttons numbered: This image from another iPendant than the ones available was chosen because of its labelling of buttons. Some buttons of the available iPendants are not labelled, so this picture can be used as a reference. Source: [48]

C.2.1 Emergency stop:

Makes the robot stop immediately by applying brakes. Use it only when necessary as the brakes wear down. There is also an E-stop on the controller. Press down on the button to activate it. Twist it to the right to release. If a slow and gradual halt is required, press HOLD on the iPendant. TP on/off Below the E-stop button. It should be ON to access any function in the Teach Pendant (Set-ups, calibration, programs etc) and OFF when running in AUTO mode. Deadman switch The 2 yellow bars behind the iPendant. 3 modes are available: Fully released, halfway pressed, fully pressed. Only the middle mode activates control.