- 大学物理笔记
 - 。 多普勒效应
 - 驻波(stationary wave)
 - 。 第九章 Relativistic Mechanics 相对论力学
 - 9.1 伽利略变换
 - 9.2 洛伦兹变换 Lorentz Transformation
 - 9.3 时空图和孪生paradox
 - 9.4 相对论运动学
 - 9.5 相对论动力学(Relativistic Dynamics)
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 - 。 第十章 温度
 - 10.1 Equilibruim state
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 - 11.3 热容和比热容(Heat capacity and specific heat capacity)
 - 11.4 Free expansion and internal energy of gas
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 - 12.1 内容
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 - 12.4 热力学势
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 - 13.1 理想气体
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 - 14.1 范德瓦尔斯方程
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 - 14.3 克拉伯龙方程
- 习题课
 - 0 9.3
 - 0 9.16
 - o 11.9
 - 0 12.8
 - 0 12.12
 - o 12.13
 - 0 12.11

多普勒效应

source: v_s , observer: v_O ,distance L

issued at t=0, x=0, recieved at $t_1^\prime, L+v_Ot_1^\prime$

issued at $t=T, x=v_ST$, received at $t_2^\prime, L+v_Ot_2^\prime$

由运动学:

$$egin{aligned} v_P t_1' &= L + v_O t_1' \ v_P (t_2' - T) &= L + v_O t_2' - v_S T \end{aligned}$$

于是

$$t_1' = rac{L}{v_P - v_O} \ t_2' = rac{L}{v_P - v_O} + rac{v_P - v_S}{v_P - v_O} T \ T' = t_2' - t_1' = rac{v_P - v_S}{v_P - v_O} T \
onumber \
onu$$

Discussion:

 $v_O > v_S$ (including $v_S \leq 0$):separating, u' <
u, Doppler redshift

 $v_S>v_O$ (including $v_O\leq 0$):approaching, u'>
u , Doppler blueshift

靠近:频率变高;远离:频率变低

考虑波源的运动与波振面的运动(supersonic speed $v_S>v_p$)

马赫锥: $sin heta=rac{vP}{vS}$

驻波(stationary wave)

推导

由 $kx-\omega t-\phi=const$,求导得 $v=rac{\omega}{k}$

$$egin{aligned} u_1 &= Acos(kx - \omega t - \phi) \ u_2 &= Acos(kx + \omega t) \ &= Acos(k(x + rac{\omega}{k}t)) \ \end{pmatrix}$$
 $egin{aligned} egin{aligned} egin{aligned} eta &= 2Acos(kx - rac{\phi}{2})cos(wt + rac{\phi}{2}) \end{aligned}$

令
$$(u_1+u_2)_{x=0}=0$$
,得 $\phi=\pi$; 令 $(u_1+u_2)_{x=L}=0$,得 $L=rac{n\pi}{k}=rac{n\lambda}{2}$

注意
$$\lambda=T\cdot v_P=rac{2\pi}{\omega}\cdotrac{\omega}{k}=rac{2\pi}{k}$$
 , $k=rac{2\pi}{\lambda}$, $\omega=vk$,有
$$f=rac{\omega}{2\pi}=rac{kv}{2\pi}=nrac{v}{2L}$$
 $=f_n$ $=nf_1$

波节(node),波腹(antinode)的定义

• 半波损失

fixed hard boundary; from high spped to low speed

由(1)式,令 $(u_1+u_2)_{x=0}=0$,得 $\phi=\pi$,即为在固定端的相差

第九章 Relativistic Mechanics 相对论力学

9.1 伽利略变换

- 观测者:一套矫正好的时钟,可记录 x, y, z, t
- ・ 结果 $t_A'-t_B'=t_A-t_B$, $x_A'-x_B'=x_A-x_B-u(t_A-t_B)$ 同时测量: $x_A'-x_B'=x_A-x_B$

速度直接叠加加速度不变

- Galileo's relativity: 力学定律在不同惯性参考系中相同
- 电学:不满足麦克斯韦方程组

9.2 洛伦兹变换 Lorentz Transformation

- Two basic principles of Special Theory of Relativity
 - 。 所有惯性参考系中物理定律相同(力学,电学等)
 - 。 光速不变
- 推导

假定变换为线性变换(考虑匀速直线运动);

待定系数:

$$x' = a_{11}x + a_{12}y + a_{13}z + a_{14}t$$
 $y' = y$
 $z' = z$

For arbitrary y,z if x'=0,x=ut;则

$$x' = a_{11}(u)(x - ut), a_{11}(0) = 1 (1.1)$$

By the priciple of relativity, we have

$$x = a_{11}(-u)(x' + ut'), #\lambda(1.1), 有$$

$$t' = f(x, x'(u, t)) = a_{44}t + a_{41}x$$

从而

$$x' = a(x - ut)$$

$$t' = b(t - ex)$$
(1.2)

解得 $x=rac{1}{\Delta}(bx'+aut')$

与
$$x = a_{11}(-u)(x'+ut')$$
比较,得 $a = b$

考虑光速不变:假设 t=t'=0时在原点发出光信号,有

$$x^{2} + y^{2} + z^{2} = c^{2}t^{2}$$

 $x'^{2} + y'^{2} + z'^{2} = c^{2}t'^{2}$

代入 (1.2)式,有

$$e=rac{u}{c^2}$$

$$a=rac{1}{\sqrt{1-eta^2}}=\gamma=\sqrt{1-rac{v^2}{c^2}}$$
 其中 $eta=rac{u}{c}$

完整的变换关系为

$$x' = \gamma(x - ut)$$

 $y' = y$
 $z' = z$
 $t' = \gamma(t - \frac{u}{c^2}x)$

考虑事件对 $(x'_1, t'_1), (x'_2, t'_2)$,洛伦兹变换是

$$\Delta x' = \gamma(\Delta x - u\Delta t)$$

$$\Delta y' = \Delta y$$

$$\Delta z' = \Delta z$$

$$\Delta t' = \gamma(\Delta t - \frac{u}{c^2}\Delta x)$$
(1.3)

- 讨论
 - \circ 逆变换: $u \rightarrow -u$ 直接根据相对性原理
 - o Invariance of spacetime interval 时空间隔不变: $(\Delta s)^2=(c\Delta t)^2-(\Delta x)^2-(\Delta y)^2-(\Delta z)^2=(\Delta s')^2$
 - 。 伽利略变换:时间归时间 空间归空间 时间空间分别不变
- 事件对
 - 。 光信号联系: $(c\Delta t)^2 = (\Delta x)^2, \Delta s = 0$
 - 。 固有时间间隔与固有空间间隔

Simultaneous measurement $\Delta x' = \ell_0$ in $S'(\Delta t' = 0)$ 形成一个事件 the same pair of events in S:

$$\Delta x = \gamma(\Delta x' + u\Delta t') = \gamma \Delta x' = \gamma \ell_0$$
 同时的相对性 $\Delta t = \gamma(\Delta t + \frac{u}{c^2}\Delta x') = 0$

也即
$$\ell=\ell_0\sqrt{1-rac{v^2}{c^2}}=rac{\ell_0}{\gamma}$$

• 用光速不变推出钟慢:

$$\Delta t'=rac{2L_0}{c} \ (rac{u\Delta t}{2})^2+L_0^2=(rac{c\Delta t}{2})^2($$
用到光速不变 $)$ $\Delta t=rac{2L_0}{\sqrt{c^2-u^2}}=rac{2L_0/c}{\sqrt{1-eta^2}}=\gamma\Delta t'$

• 用光速不变推出尺缩:

$$c\Delta t_1 = L + u\Delta t_1, c\Delta t_2 = L - u\Delta t_2$$
 $\Delta t = \Delta t_1 + \Delta t_2 = \frac{L}{c+u} + \frac{L}{c-u} = \frac{2L}{c} \frac{1}{1-\beta^2}$
 $\Delta t' = \frac{2L_0}{c} = \gamma \Delta t$
 $\frac{2L_0}{c\gamma} = \frac{2L}{c} \frac{1}{1-\beta^2}$
于是 $L = \frac{L_0}{\gamma}$

- 因果律及信号传播(Causality and signal speed)
 - \circ An event $P(x_P,t_P)$ causes an event $Q(x_Q,t_Q)$. 信号传输速度

$$v_S = rac{x_Q - x_P}{t_Q - t_P} = rac{\Delta x}{\Delta t}$$

在 S'(u) 系中时间间隔为

$$\Delta t' = \gamma \Delta t (1 - \frac{uv_S}{c^2})$$

为保证先后次序,必须有

$$1-rac{uv_S}{c^2} < 0$$
则 $v_S < c$

• 光多普勒效应

$$\circ$$
 $ext{ } ext{ }$

$$\circ$$
 redshift: $u_0 = \sqrt{rac{1-eta}{1+eta}}
u_e$

• 波动方程: 用洛伦兹变换恰好符合(洛伦兹不变)

9.3 时空图和孪生paradox

- Minkowski Space
 - 。 洛伦兹变换在时空图中的体现
- Twin paradox: 在宇宙飞船加速,减速的过程中经历了非惯性系
- Pole-barn Paradox: 火车进隧道;火车系:隧道收缩;地面系:火车收缩
 - 涉及同时的相对性:看能否在地面系同时关上前门和后门(火车系觉得没有同时)
 - 地面系的观测者觉得能关进去,在火车系的观测者看来后门早就关起来了
- Visual Apperance
 - 。 球不变 立方体转过一个角度

9.4 相对论运动学

• 速度变换公式(求导可得)

$$v'_{x} = rac{v_{x} - u}{1 - v_{x} rac{u}{c^{2}}} \ v'_{y} = rac{v_{y}}{\gamma(1 - v_{x} rac{u}{c^{2}})} \ v'_{z} = rac{v_{z}}{\gamma(1 - v_{x} rac{u}{c^{2}})}$$

9.5 相对论动力学(Relativistic Dynamics)

- 广义相对论: 引力场,非惯性系
- 讨论 m, p, F, E_k, a
- Discuss a completely inelastic collision(保持动量守恒)

$$\circ$$
 In $S'(-u):u,-u\to 0,0$

$$\circ$$
 In $S:v_x,0 o u,u;$ $v_x=rac{u+u}{1+urac{u}{c^2}}(9.5.1)$

$$\circ$$
 而 $mrac{u+u}{1+rac{uu}{2}}+m imes 0=2mu$,动量守恒不成立.

$$\circ$$
 假定 $m \equiv m(v), m_0 \equiv m(0)$,有

$$egin{aligned} m(v_x)+m_0&=m_{total}(u)\ m(v_x)\cdot v_x+m_0\cdot 0&=m_t(u)u\ &=[m(v_x)+m_0]u\ rac{x}{arphi m}(v_x)&=rac{m_0}{rac{v_x}{u}-1} \end{aligned}$$

由
$$(9.5.1)$$
, $\dfrac{v_x}{u}-1=\sqrt{1-eta^2}$,则 $m(v)=\gamma m_0$. 于是

$$p=\gamma m_0 v$$
 $E_k=\int F\cdot dx=\int rac{d}{dt}(mv)\cdot dx=\int v\cdot d(mv)$
 $ec{\mathbb{M}}d(mv)=vdm+mdv$
 $ec{\mathbb{M}}E_k=\int (v^2dm+mvdv)$

考虑
$$m^2(1-rac{v^2}{c^2})=m_0^2, m^2(c^2-v^2)=m_0^2c^2$$
,两边微分得 $c^22mdm-v^22mdm-m^22vdv=0, \ c^2dm-v^2dm-mdv=0, c^2dm=v^2dm+mdv$

于是

$$egin{aligned} E_k &= \int c^2 dm = mc^2 - m_0 c^2 \ &= m_0 c^2 \Big[rac{1}{\sqrt{1 - rac{v^2}{c^2}}} - 1 \Big] \ &= (\gamma - 1) m_0 c^2 \end{aligned}$$

- 讨论
 - 。 牛顿力学中

$$E_k = \int v \cdot d(mv) = \int mv \cdot dv = rac{1}{2} mv^2$$

- 相对论中,mass-energy $E=mc^2=E_k+m_0c^2$ 已知动能求速度: $\gamma=rac{E_k}{m_0c^2}+1$
- 相对论能量-动量关系

$$\circ$$
 $E=\sqrt{c^2p^2+m_0^2c^4}$

• 若
$$m_0 = 0, E = cp, p = \frac{E}{c}$$

• 若 $cp << m_0 c^2$,泰勒展开后得到牛顿力学.

期末考试大致内容

- 相对论运动学: 速度的变换
- 理想气体(或给定气体的状态方程) 等温膨胀,绝热等过程, 功和热, 内能等
- 理想气体的性质: 速度,平均动能等
- 过程中温度的变化,熵的变化
- 过程中 **亥姆霍兹自由能变**, 求平衡态(可能有数学上求导等)
- 比热容, 温度.
- 相变 三相点.

Project Proposal

- structure
 - Template

- Guideline
- · how and where
- · basics of thesis writing
- deadline

第十章 温度

10.1 Equilibruim state

•	System	exchange
	isolated	×
	closed	energy
	open	energy&matter

- Thermodynamic Equilibruim state: 宏观状态不随时间改变,除非外界条件发生变化.
- description of equilibruim state: state variables
 - extensive quantity: $F(n \ systems) = nF(1 \ system)$
 - \circ intensive quantity: $F(n \ systems) = F(1 \ system)$
- relaxation time τ : 恢复平衡所用时间
- Quasi-static process 准静态过程: $t >> \tau$, 每一点都是平衡态, 可以在状态图上画出.
- No-dissipative, quasi-static process is reversible. (无耗散准静态过程是可逆的); All natural process(自发过程) is irreversible.
 - 。 系统和外界同时恢复初态

10.2 Thermal equilibruim and temperature

- The zeroth law of thermodynamics: 热平衡的传递性(热平衡的系统有共同性质)
- 温度: 衡量热平衡的一种物理性质
- 各种温标

10.4 物态方程

- 微分的常见写法 $\left(rac{\partial U}{\partial V}
 ight)_T$, $\left(rac{\partial U}{\partial V}
 ight)_P$. 保持右下标不变
- P,V,T不独立, $f(P,V,T)=0 \rightarrow U(T,P)=U(T,V(P,T))=U(T,V)=0$
- 等压线膨胀系数 $a_\ell = \frac{1}{L} \frac{\partial L}{\partial T_p}$; $\alpha_V = \frac{1}{V} (\frac{\partial V}{\partial T})_P = \frac{1}{L^3} (\frac{\partial L^3}{\partial T})_P = 3\alpha_\ell$
- 等温线膨胀系数 $\kappa_T = -rac{1}{V}rac{\partial V}{\partial p}_T$
- 体积变化方程

$$rac{dV}{V} = rac{1}{V} ig(rac{\partial V}{\partial T}ig)_p dT + rac{1}{V} ig(rac{\partial V}{\partial p}ig)_T dp = lpha_V(T) dT - \kappa_T(p) dp$$
(全微分)

$$egin{aligned} lnrac{V}{V_0} &= lpha_V \Delta T - \kappa_T \Delta p \ V &= V_0 (1 + lpha_V \Delta T - \kappa_T \Delta p) \end{aligned}$$

• Van der Waal's equation

$$\left[p+a(rac{n}{V})^2
ight](V-nb)=nRT$$

推导: 对1mol理想气体:

$$p = rac{RT}{V_m} \leftarrow rac{RT}{V_m - b} ($$
相互作用,体积减小)
$$\leftarrow rac{RT}{V_m - b} - rac{a}{V^2} ($$
相互作用,压强减小,体积越小作用力越大)

第十一章 热力学第一定律

11.1 功,内能和热力学第一定律

- 准静态过程压活塞 $\bar{d}W=-p\bar{d}V$, $W=-\int_{V_i}^{V_f}pdV$ (依赖于 P-V图上的路径,不是全微分)
- 绝热功: Internal energy function $\Delta U=U_B-U_A\equiv W_{BA}\equiv -W_{AB}$ (用与路径无关的绝热功定义内能变化)
- 非绝热功: $\Delta U=W+Q$ 外界做的功和外界传给内部的热量; 微分 $dU=\bar{d}Q+\bar{d}W$ (功和热不是全微分,与路径有关)

11.3 热容和比热容(Heat capacity and specific heat capacity)

•
$$C = \lim_{\Delta T o 0} \frac{\Delta Q}{\Delta T}$$
; specific: $C_m = \frac{C}{n}$

- 。 C=0: 绝热(adiabatic)过程, $\Delta Q=0$
- $C=\infty$: 等温(isothermal)过程, $\Delta T=0$

$$\bullet \ \ C_V = \lim_{\Delta T \to 0} (\frac{\Delta Q}{\Delta T})_V = \lim_{\Delta T \to 0} (\frac{\Delta U}{\Delta T})_V = \big(\frac{\partial U}{\partial T}\big)_V$$

•
$$C_P = \lim_{\Delta T \to 0} (\frac{\Delta Q}{\Delta T})_p = \lim_{\Delta T \to 0} (\frac{\Delta U + p\Delta V}{\Delta T})_p = (\frac{\partial (U + pV)}{\partial T})_p \equiv (\frac{\partial H}{\partial T})_{p'} H = U + pV$$
: enthalpy, 焓

- ullet ratio of specific heat: $\gamma = rac{C_p}{C_V}$
- · heat capacity of ideal gases

monatomic ideal gas
$$C_V=rac{3}{2}nR$$
 双原子 ideal gas $C_V=rac{5}{2}nR$ 三原子 ideal gas $C_V=rac{6}{2}nR$

11.4 Free expansion and internal energy of gas

• Case of free expansion

$$U = U(T, V)$$

$$dU = \left(\frac{\partial U}{\partial T}\right)_V dT + \left(\frac{\partial U}{\partial V}\right)_T dV$$

$$T = T(U, V)$$

$$dU = \left(\frac{\partial U}{\partial T}\right)_V \left[\left(\frac{\partial T}{\partial U}\right)_V dU + \left(\frac{\partial T}{\partial V}\right)_U dV\right] + \left(\frac{\partial U}{\partial V}\right)_T dV$$
对照左右,得
$$\left(\frac{\partial U}{\partial T}\right)_V \left(\frac{\partial T}{\partial U}\right)_V = 1$$

$$\left(\frac{\partial U}{\partial V}\right)_T = -\left(\frac{\partial U}{\partial T}\right)_V \left(\frac{\partial T}{\partial V}\right)_U = -C_V \left(\frac{\partial T}{\partial V}\right)_U \to \text{焦耳系数} = 0(理想气体)$$
故 $U = U(T)$

- 焦耳的实验非常不严谨
- 理想气体:

$$dU(T) = rac{dU}{dT}dT = C_V dT$$
 $U = U_0 + C_V T$
 $dQ = dU - dW = C_V dT + p dV$
理想气体: $d(pV) = d(nRT)$
 $p dV + V dp = nR dT, p dV = nR dT - V dp$
 $dQ = (C_V + nR) dT - V dp$
 $C_p = C_V + nR o C_V = rac{nR}{\gamma - 1}, C_p = rac{\gamma nR}{\gamma - 1}$

11.5 Adiabatic equation

$$egin{aligned} dQ &= dU - dW, \ &= C_V dT + p dV \ C_V dT + p dV &= 0 \ orall V dp + p dV &= nRdT = (\gamma - 1)C_V dT \end{aligned}$$

消去 dT,得

$$Vdp + \gamma pdV = 0$$
 $\frac{dp}{p} + \gamma \frac{dV}{V} = 0$ $lnp + \gamma lnV = C$ $pV^{\gamma} = C$

由 $\gamma > 1$, 绝热线比等温线陡峭

· adiabatic work

$$egin{align} W_S &= -\int_{V_1}^{V_2} p dV = -C \int_{V_1}^{V_2} rac{dV}{V^\gamma} = rac{C}{\gamma-1} (rac{V_2}{V_2^\gamma} - rac{V_1}{V_1^\gamma}) \ &= rac{1}{\gamma-1} (p_2 V_2 - p_1 V_1) \ &= rac{nR}{\gamma-1} (T_2 - T_1) \ &= C_V (T_2 - T_1) = \Delta U \ \end{cases}$$

• 声音的传播: 绝热

11.6 卡诺循环

- 高温热源 T_1 等温膨胀 \rightarrow 绝热膨胀 \rightarrow 低温热源 T_2 等温压缩 \rightarrow 绝热压缩
- $T_1, U = U(T_1) = const$ 热机吸热,做功
- T_2 热机放热
- 整个循环: $\Delta U=0, \Delta Q_{12}+\Delta Q_{34}-\Delta W=0$

效率
$$\eta = \frac{\Delta W}{\Delta Q_{12}} = \frac{\Delta Q_{12} + \Delta Q_{34}}{\Delta Q_{12}} = \frac{Q_1 - Q_2}{Q_1}$$
 (考察做功过程中的放热 Q_2 , 放热越多效率越低)
等温过程: $Q_1 = \Delta W_{12} = \int_{V_1}^{V_2} p dV = \int_{V_1}^{V_2} \frac{nRT_1}{V} dV = nRT_1 ln \frac{V_2}{V_1}$ $Q_2 = -\Delta Q_{34} = nRT_2 ln \frac{V_3}{V_1}$

$$egin{align} Q_2 & -\Delta Q_{34} - nn T_2 in rac{V_4}{V_4} \ & \eta = 1 - rac{T_2 ln rac{V_3}{V_4}}{T_1 ln rac{V_2}{V_1}} \ & 2
ightarrow 3: & T_1 V_2^{\gamma - 1} = T_2 V_3^{\gamma - 1} \ & 4
ightarrow 1: & T_1 V_1^{\gamma - 1} = T_2 V_4^{\gamma - 1} \ & \eta = 1 - rac{T_2}{T_1} \ \end{pmatrix}$$

要学会将此推导推广到其他热机上

- 可逆过程: 外界不可逆
- 逆卡诺循环: 从低温热源吸热 到高温热源被做功,放热

第十二章 热力学第二定律

12.1 内容

- No process is possible whose sole result is the absorption of heat from a reservoir and the conversion of this heat into work.
- No process is possible whose sole result is the transfer of heat from a cooler to a hotter body.
- 自发过程具有方向性

12.2 卡诺定理

• 任何热机效率不超过可逆热机

• 证明: 任意热机做功驱动可逆热机的逆过程, 反证法与热二矛盾

12.3 熵与熵原理

• 熵的引入

假设 $Q_2 < 0$ 为放热:

效率不大于卡诺热机:
$$\eta_A = 1 + \frac{Q_2}{Q_1} \le 1 - \frac{T_2}{T_1}$$

$$\sum_{i=1}^2 \frac{Q_i}{T_i} \le 0$$
一般过程: $\sum_{i=1}^n \frac{Q_i}{T_i} \le 0$ (系统与很多热源接触)
$$\oint \frac{dQ}{T} \le 0$$
(取等:可逆过程,考虑 $Q_i \to -Q_i$)
(环路积分)
写作全微分: $\frac{\bar{d}Q}{T} \equiv dS$

$$S_B - S_A = \int_A^B \left(\frac{dQ}{T}\right)_R$$

若环路中包含不可逆过程:

$$egin{aligned} \oint \left(rac{dQ}{T}
ight) < 0 \ \int_A^B \left(rac{dQ}{T}
ight)_{IR} + \int_A^B \left(rac{dQ}{T}
ight)_R < 0 \ \int_A^B \left(rac{dQ}{T}
ight)_{IR} - \int_B^A \left(rac{dQ}{T}
ight)_R < 0 \ S_B - S_A > \int_A^B \left(rac{dQ}{T}
ight)_{IR} \ \int_A^B dS > \int_A^B \left(rac{dQ}{T}
ight)_{IR} \ dS > \left(rac{dQ}{T}
ight)_{IR} \end{aligned}$$

- 熵原理: 任何过程: $dS \geq rac{dQ}{T}$
 - 绝热过程: dQ=0; 可逆: dS=0, isentropic 等熵过程
 - \circ 孤立系统: $dS \geq 0$; 非平衡趋于平衡: 熵增加; 平衡态: 宏观特征不变,熵最大
- 热二的另一种形式: The entropy of an isolated system never decreases.

$$\circ$$
 从单一热源吸热的熵变: $\Delta S = rac{\Delta Q}{T} = rac{-Q}{T} < 0$,矛盾!

。 两热源
$$T_1 > T_2$$
, T_1 吸热, T_2 放热: $\Delta S = rac{I_Q}{T_1} - rac{Q}{T_2} < 0$, 矛盾!

- 克劳修斯不等式的证明: 考虑多热源与单一热源 T₀由多个卡诺机联合:
 - 系统作循环过程,分别与热源 T_i 交换 Q_i 的热量
 - \circ $T_0 \to T_i$ 之间加上卡诺热机
 - $\circ T_0 \rightarrow Q_{0i}$
 - \circ Carnot engines: $rac{Q_{0i}}{T_0} = rac{Q_i}{T_i}$
 - o 对整个辅助系统: T_i ,系统,热机不变, 热源 T_0 放热,对外做功. 第一定律: $\sum\limits_{n=1}^n Q_{0i} = \sum\limits_{n=1}^n W_i$
 - 。 第二定律: 没有真正做功 $\sum\limits_{n=1}^nQ_{0i}=T_0\sum\limits_{n=1}^nrac{Q_i}{T_i}=\sum\limits_{n=1}^nW_i\leq 0$

• 求熵变

。 理想气体

$$dS = rac{1}{T}(dU + pdV)$$
(第一定律) $= C_V rac{dT}{T} + nR rac{dV}{V}$ (第二类曲线积分) $S_f - S_i = C_v ln rac{T_f}{T_i} + nR ln rac{V_f}{V_i}$ $S = C_v ln T + nR ln V + S_0$

状态函数: $S(T,V) = C_v lnT + nR lnV + S_0$

- • Free expansion from V o 2V(T=const):用熵作为状态函数来求: $\Delta S=nRln2>0$, irreversible
 - 。 热库reservior $\Delta S = \int rac{dQ}{T} = rac{\Delta Q}{T}$ 吸热熵增,放热熵减
 - 。 由准静态过程连接的状态: $\Delta S = \int_i^f rac{dQ}{T}, dQ = C_p dT \ / \ C_V dT$
 - 。 由不可逆过程联系的: 找到相应的可逆过程(如不可逆的自由膨胀转化为等温过程) $\Delta S = rac{1}{T} \int p dV = nR ln rac{V_f}{V_i}$
 - 。 混合: $\Delta S = \int_{T_1}^{T_f} rac{m_1 c_1 dT}{T} + \int_{T_2}^{T_f} rac{m_2 c_2 dT}{T}$
 - 吉布斯佯谬: 相同气体混合

• 再探功与热

- 做功: 有广义距离: 电热丝,搅拌,微波炉等;
- 。 但这些功只能转化为热,熵也就增加了⇒耗散功; 只要有耗散,就不可逆
- 熵的微观解释: $S = k_B lnW, W$: 微观状态数
 - 。 自由膨胀到两倍体积: N个粒子, $W=2^NW_0,\ \Delta S=k_BNln2$
 - 熵: 广延量: 微观状态用乘法原理计算, lnW可加
 - 习题 (12.9):棋盘密度最大:平衡状态

12.4 热力学势

• 内能的计算

$$dQ=TdS$$
 $dU=TdS-pdV+\mu dn$
 $(fundamental\ equation\ of\ thermodynamics)$
 $(\mu dn$ 代表与外界的物质交换, μ 指化学势)
 $\left(\frac{\partial U}{\partial S}\right)_{V,n}=T,\left(\frac{\partial U}{\partial V}\right)_{S,n}=-p,\left(\frac{\partial U}{\partial n}\right)_{S,V}=\mu$
 U 是广延量:
$$U(\lambda S,\lambda V,\lambda n)=\lambda U(S,V,n)$$
两边对 λ 求导数:

两边对 λ 求导数:

$$ig(rac{\partial U}{\partial(\lambda S)}ig)S + ig(rac{\partial U}{\partial(\lambda V)}ig) + ig(rac{\partial U}{\partial(\lambda n)}ig)_n = U$$
 $\diamondsuit \lambda = 1:$
 $U = TS - pV + \mu n$

欧拉齐次函数定理:设 $f(x_1, x_2, \cdots, x_n)$ 是k次函数

$$f(\lambda x_1, \lambda x_2, \cdots, \lambda x_n) = \lambda^k f(x_1, x_2, \cdots, x_n)$$
 $\sum_{n=1}^n rac{\partial f}{\partial (\lambda x_i)} rac{\partial (\lambda x_i)}{\partial \lambda} = k \lambda^{k-1} f(x_1, x_2, \cdots, x_n)$ 令 $\lambda = 1$,得 $\sum_{n=1}^n rac{\partial f}{\partial x_i} x_i = k f(x_1, x_2, \cdots, x_n)$

其他热力学势的引入

$$dU = TdS - pdV - Vdp + Vdp + \mu dn$$
 $d(U + pV) = TdS + Vdp + \mu dn \equiv dH$
 $(\sim reaction\ heat, enthopy)$
 $dU = TdS - pdV + \mu dn - TdS - SdT$
 $d(U - TS) = -SdT - pdV + \mu dn \equiv dF$
 $(\sim useful\ work,\ Helmholtz\ free\ energy)$
 $d(U - TS + pV) = -SdT + Vdp + \mu dn \equiv dG$
 $(Gibbs\ free\ energy)$
 $G = F + pV = H - TS(free\ enthopy)$
 $F = U - TS$

Legendre变换:

$$df = udx + vdy$$
,是 x 与 y 的函数 $g = f - ux$ $dg = df - udx - xdu$ $= udx + vdy - udx - xdu$ $= -xdu + vdy$,是 u 与 y 的函数

。 化学势的求法:
$$\mu=ig(rac{\partial G}{\partial n}ig)_{T,p'}$$
摩尔吉布斯自由能 $G=ig(rac{\partial G}{\partial n}ig)_{T,p}n=\mu n$ $dG=nd\mu+\mu dn$ $nd\mu=-SdT+Vdp$ $d\mu=-S_mdT+V_mdp$ $(S_m: 摩尔熵, V_m: 摩尔体积)$

• 麦克斯韦关系

$$U(S,V,n) = TS - pV + \mu n$$
 $\frac{\partial}{\partial p}(\frac{\partial G}{\partial T}) = \frac{\partial}{\partial T}(\frac{\partial G}{\partial p}) = \frac{\partial^2 G}{\partial T \partial p}$
 $-(\frac{\partial S}{\partial p})_{T,n} = (\frac{\partial V}{\partial T})_{p,n}$
 $($ 也可从全微分理解 $)$
 $dU = TdS - pdV$
 $= T\Big[(\frac{\partial S}{\partial T})_V dT + (\frac{\partial S}{\partial V})_T dV - pdV\Big]$
由 $dF = -SdT - pdV$,结合麦克斯韦关系:
 $= T\Big[(\frac{\partial S}{\partial T})_V dT + (\frac{\partial p}{\partial T})_V dV - pdV\Big]$
考虑 $C_V = T(\frac{\partial S}{\partial T})_V$:
 $= C_V dT + T(\frac{\partial p}{\partial T})_V dV - pdV$
 $(\frac{\partial U}{\partial V})_T = T(\frac{\partial p}{\partial T})_V - p$

Criteria of thermodynamics equilibrium

$$egin{aligned} \Delta S_t &= \Delta S + \Delta S_0 = \Delta S - rac{\Delta Q}{T_0} \ & where \ Q \ is \ released \ to \ the \ system \ &= \Delta S - rac{\Delta U - \Delta W - \mu \Delta n}{T_0} \geq 0 \ & \Delta U \leq T_0 \Delta S + \Delta W + \mu \Delta n \ & (\Delta U)_{S,V,n} \leq 0 \ & \Delta F = \Delta (U - TS) \leq -S\Delta T - p\Delta V + \mu \Delta n \ & (\Delta F)_{T,V,n} \leq 0 \ & \Delta G = \Delta (F = pV) \leq -S\Delta T + V\Delta p + \mu \Delta n \ & (\Delta G)_{T,p,n} \leq 0 \end{aligned}$$

- 热力学势的物理意义
 - 。 $(\Delta H)_p=\Delta U+p\Delta V=\Delta Q$,化学反应中等压过程的反应热. $\Delta H>0$: endothermic 吸热; $\Delta H<0$: exothermic 放热
 - \circ 等温最大功与亥姆霍兹自由能 设想系统与reservoir T_0 接触,这是等温过程

$$\Delta S_t = \Delta S + \Delta S_{reservoir}$$
 (热源损失 ΔQ 的热量)
$$= \Delta S - \frac{\Delta Q}{T_0} \geq 0$$
 对系统:
$$\Delta Q = \Delta U - \Delta W_{to\ system}$$
 $\Delta W_{to\ system} \geq \Delta U - T_0 \Delta S = \Delta F$ $\Delta W_{by\ system} = -\Delta W \leq -\Delta F$

• 。 额外功与吉布斯自由能

等温等压过程/isothermalisobaric:

$$egin{aligned} \Delta W &= -p\Delta V + \Delta W_{other}(non-expansion\ work) \ \Delta W &\geq \Delta U - T_0\Delta S \ -\Delta W_{other} &\leq \Delta (U-TS+pV) \equiv -\Delta G \end{aligned}$$

• 平衡条件: 温度,压强,化学势

第十三章 理想气体的微观模型

Microscopic Model for Ideal gas

13.1 理想气体

- Microscopic description
 - \circ It contains of N identical molecules
 - The molecules obey Newton's law
 - \circ The average spacing >> r(相互作用不产生内能的改变)
 - Collisions are elastic and are of negligible duration.
- Microscopic meaning of pressure

考虑粒子撞壁运动

$$egin{aligned} \Delta t &= rac{2\ell}{v_x}$$
撞击频率 $ar{F} = -rac{\Delta p_x}{\Delta t} (the\ force\ on\ wall) \ &= rac{2mv_x}{rac{2\ell}{v_x}} = rac{mv_x^2}{\ell} \ p &= rac{1}{\ell^2} \sum_{n=1}^N ar{F}_n = rac{m}{\ell^3} (v_{x1}^2 + v_{x2}^2 + \cdots) \ &= rac{Nm}{\ell^3} rac{(v_{x1}^2 + v_{x2}^2 + \cdots)}{N} \ &= rac{Nm}{\ell^3} ar{v_x^2} \ &= rac{Nm}{3V} ar{v}^2 (isotropic\ \hat{\Phi}\ ert \ ert \ ert \ ert \) \ &= rac{1}{3}
ho ar{v}^2 \end{aligned}$

 $\Delta p_x = p_f - p_i = -2mv_x$

定义方均根速率
$$v_{rms} = \sqrt{ar{v^2}} = \sqrt{rac{3p}{
ho}}$$

• Microscopic interpretation of T and U

$$egin{align} pV &= rac{2}{3}N(rac{1}{2}mar{v^2}) \ nRT &= rac{2}{3}N(rac{1}{2}mar{v^2}) \ rac{1}{2}mar{v^2} &= rac{3}{2}rac{R}{N}T = rac{3}{2}rac{R}{N_A}T = rac{3}{2}k_BT \ \end{array}$$

k_B:玻尔兹曼常数 联系宏观温度与微观速度

LHS:单个粒子内能

• 理想气体定体积热容 C_V

。 monatomic: 只有平动自由度 $U=(3 imesrac{1}{2}k_BT)N=rac{3}{2}k_BNT=rac{3}{2}nRT$, 对 T求导即得 C_V

。 diatomic: 多两个转动自由度

。 ployatomic: 多三个转动自由度

13.2 Equilibrium distributions

$$egin{aligned} ar{v^2} &= rac{n_1 v_1'^2 + n_2 v_2'^2 + \cdots}{N} \ &= \int v^2 rac{dn}{N} \end{aligned}$$

在引入的速度空间内 dn is the number of modules in $v_x \to v_x + dv_x, y, z$ 亦然, i.e. $\frac{dn}{N}$ is the probability that one molecule near v. It's proportional to dv_x . Let us suppose

$$rac{dn(v_x,v_y,v_z)}{N} = f(v_x) dv_x f(v_y) dv_y f(v_z) dv_z$$

速度各向同,与方向无关:

$$f(v_x)f(v_y)f(v_z) = \phi(v^2) = \phi(v_x^2 + v_y^2 + v_z^2)$$

 $Simplest\ solution:$

$$f(v_x) = Cexp(-rac{v_x^2}{lpha^2})$$

 $probability\ satisfies\ normalization:$

$$egin{aligned} 1 &= \int rac{dn}{N} \ &= \int (f(v_x) dv_x)^3 \ &= C \int exp(-rac{v_x^2}{lpha^2}) dv_x \ C &= rac{1}{\int_{-\infty}^{\infty} exp(-rac{v_x^2}{lpha^2}) dv_x} \ &= rac{1}{lpha \int_{-\infty}^{\infty} exp(-rac{v_x^2}{lpha^2}) drac{v_x}{lpha}} \ &= rac{1}{lpha \sqrt{\pi}} \end{aligned}$$

于是

$$\begin{split} \frac{dn(v_x,v_y,v_z)}{N} &= (\frac{1}{\alpha\sqrt{\pi}})^3 exp\Big[-\frac{v_x^2 + v_y^2 + v_z^2}{\alpha^2}\Big] \\ &= (\frac{1}{\alpha\sqrt{\pi}})e^{-\frac{v_x^2}{\alpha^2}} dv_x (\frac{1}{\alpha\sqrt{\pi}})e^{-\frac{v_y^2}{\alpha^2}} dv_y (\frac{1}{\alpha\sqrt{\pi}})e^{-\frac{v_z^2}{\alpha^2}} dv_z \\ \bar{v}^2 &= \int (v_x^2 + v_y^2 + v_z^2) \frac{dn(v_x,v_y,v_z)}{N} \\ &= 3\int_{-\infty}^{\infty} v_x^2 (\frac{1}{\alpha\sqrt{\pi}})e^{-\frac{v_x^2}{\alpha^2}} dv_x (v_x \text{対} dv_y \text{持分得1}) \\ &= 3 \times \frac{2\alpha^2}{\sqrt{\pi}} \int_0^{\infty} y^2 e^{-y^2} dy \\ &= 3 \times \frac{2\alpha^2}{\sqrt{\pi}} \frac{1}{2}\Gamma(\frac{3}{2}) = 3 \times \frac{2\alpha^2}{\sqrt{\pi}} \frac{1}{4}\Gamma(\frac{1}{2}) = 3 \times \frac{2\alpha^2}{\sqrt{\pi}} \frac{1}{4}\sqrt{\pi} \\ &= \frac{3}{2}\alpha^2 \\ \alpha^2 &= 2k_BT/m \end{split}$$

从而有Maxwell velocity distribution:

$$egin{aligned} rac{dn(v_x,v_y,v_z)}{N} &= (rac{m}{2\pi k_B T})^{rac{3}{2}} exp \Big[-rac{m(v_x^2+v_y^2+v_z^2)}{2k_B T} \Big] dv_x dv_y dv_z \ dn(v_x,v_y,v_z) &= n_0 (rac{m}{2\pi k_B T})^{rac{3}{2}} exp \Big[-rac{m(v_x^2+v_y^2+v_z^2)}{2k_B T} \Big] dv_x dv_y dv_z \end{aligned}$$

Maxwell speed distribution: 将速度空间的体积元换为速率空间的球壳

$$egin{align} dv_x dv_y dv_z &
ightarrow 4\pi v^2 dv \ dn(v) &= n_0 (rac{m}{2\pi k_B T})^{rac{3}{2}} exp \Big[-rac{rac{1}{2} m v^2}{k_B T} \Big] 4\pi v^2 dv \ &= f(v) dv \ rac{d}{dv} f(v) &= 0, 知 \ v_m &= \sqrt{rac{2k_B T}{m}} \ \end{cases}$$

 $Maxwellian\ can\ be\ written\ as$:

$$rac{dn(v)}{N} = 4\pi (rac{1}{\pi v_m^2})^{rac{3}{2}} exp(-rac{v^2}{v_m^2}) v^2 dv$$

The average speed

• Gaussian intergral using Gamma function:

$$I = \int_0^\infty e^{-x^2} dx$$
 $\Gamma(v) = \int_0^\infty e^{-t} t^{v-1} dt$
 $I = \int_0^\infty e^{-y} rac{1}{2\sqrt{y}} dy$
 $= rac{1}{2}\Gamma(rac{1}{2})$
 $= rac{\sqrt{\pi}}{2}$
 $I_n = \int_0^\infty x^n e^{-x^2} dx = rac{1}{2}\Gamma(rac{n+1}{2})$

13.3 Equipartition theorem

第十四章 相变 Phase Transition

14.1 范德瓦尔斯方程

- $p=\frac{nRT}{V-nb}-a(\frac{n}{V})^2$.第二项:吸引力;第一项:最小体积(斥力).高温低密度:趋于理想气体
- Critical point临界点.求临界状态:

$$egin{aligned} ig(rac{\partial p}{\partial V}ig)_T &= 0 \ ig(rac{\partial^2 p}{\partial V^2}ig)_T &= 0 \end{aligned}$$
求出 p_C, V_C, T_C

- p-V图的稳定性分析
- 一摩尔物质isotherms: $dG=Vdp,g=\int vdp$

确定临界点.C — G:气液共存

$$egin{aligned} 0 &= g_G - g_C \ &= \int_{pC}^{pG} v(p) dp \ &= (\int_C^D + \int_D^E + \int_E^F + \int_F^G) v(p) dp \ &= (\int_C^D - \int_E^D) - (\int_F^E - \int_F^G) v(p) dp \ &= A_{CDEC} - A_{EFGE} \end{aligned}$$

(Maxwell equal area construction)

• $v = xv_q + (1-x)v_\ell$,求摩尔分数

14.2 Phase and Phase Diagrams

- A:三相点 ; C:临界点: p-V图那条线的极大值点.临界温度以上,无法区分气体与液体,Supercritical fluid
- 线:相平衡曲线

14.3 克拉伯龙方程

• 相平衡:化学势相等.共存曲线

$$\mu^I(T,p)=\mu^{II}(T,p)$$

According to Gibbs-Duheim equation:

$$egin{aligned} d\mu^I &= d\mu^{II} \ -S_m^I dT + V_m^I dp &= -S_m^{II} dT + V_m^{II} dp \ & \left(rac{\partial p}{\partial T}
ight)_{CO} = rac{S_m^I - S_m^{II}}{V_m^I - V_m^{II}} \ &= rac{T\Delta S_m}{T\Delta V_m} \ \Delta G &= \Delta H - T\Delta S = 0: \ &= rac{\Delta H_m}{T\Delta V_m} = rac{\ell}{T\Delta V_m} (latent\ heat) \end{aligned}$$

汽化过程的斜率: $\frac{dp}{dT} = \frac{\ell_V p}{RT^2}$

• 沿冰线:

$$egin{aligned} \Delta T &= T - T_t r \ &= rac{T(V_{mw} - V_{mi})}{\ell_F} \Delta p \end{aligned}$$

习题课

9.3

• Known x=0, x'=-200m, to find t:

$$x' = \gamma(x - ut)$$

或用尺缩

• To find t':

$$x = \gamma(x' + ut')$$

9.16

• Conservation of mass-energy:

$$m_{n0}\,c^2=m_{p0}\,c^2+m_ec^2+E_
u$$

• Conservation of 动量:

$$egin{aligned} p_e + p_
u &= 0 \ E_
u &= c p_
u \ E_e^2 &= p_e^2 c^2 + E_0^2 \ rac{1}{c} \sqrt{E_e^2 - E_0^2} &= rac{E_
u}{c} \end{aligned}$$

11.9

$$\begin{split} \eta &= \frac{W}{\Delta Q_{BC}} \\ &= \frac{\Delta Q_{BC} - \Delta Q_{AD}}{\Delta Q_{BC}} \\ &= 1 - \frac{\Delta Q_{AD}}{\Delta Q_{BC}} \\ &= 1 - \frac{T_D - T_A}{T_C - T_B} \end{split}$$

12.8

$$\Delta S = (\int_{333K}^{T_f} + \int_{T_f}^{288}) rac{mcdT}{T} + rac{\Delta Q_s}{T_s}$$

12.12

show that

$$\big(\frac{\partial \mu}{\partial V_m}\big)_T = V_m \big(\frac{\partial p}{\partial V_m}\big)_T$$

$$egin{align} d\mu &= -sdT + vdp \ ig(rac{\partial \mu}{\partial v}ig)_T &= ig(rac{\partial \mu}{\partial p}ig)_T ig(rac{\partial p}{\partial v}ig)_T &= vig(rac{\partial p}{\partial v}ig)_T \ or: \ d\mu &= -sdT + vig[ig(rac{\partial p}{\partial T}ig)_v dT + ig(rac{\partial p}{\partial v}ig)_T dvig] \ &= &= -sdT + v[ig(rac{\partial p}{\partial T}ig)_v dT + ig(rac{\partial p}{\partial v}ig)_T dvig] \ \end{array}$$

12.13

show that

$$TdS = C_p dT - TVlpha dp \ TdS = C_V dT + Trac{lpha}{\kappa} dV$$

$$egin{aligned} dH &= TdS + Vdp \ &= Tig(rac{\partial S}{\partial T}ig)_p dT + [Tig(rac{\partial S}{\partial p}ig)_T + V]dp \ C_p &= ig(rac{\partial H}{\partial T}ig)_p = Tig(rac{\partial S}{\partial T}ig)_p \ ig(rac{\partial H}{\partial p}ig)_T = Tig(rac{\partial S}{\partial p}ig)_T + V = -Tig(rac{\partial V}{\partial T}ig)_p + V \end{aligned}$$

Thus

$$egin{aligned} TdS &= Tig(rac{\partial S}{\partial T}ig)_p dT + Tig(rac{\partial S}{\partial p}ig)_T dp \ &= C_p dT - Tig(rac{\partial V}{\partial T}ig)_p dp \ &= C_p dT - TVlpha dp \end{aligned}$$

and

-

$$egin{aligned} TdS &= Tig(rac{\partial S}{\partial T}ig)_V dT + Tig(rac{\partial S}{\partial V}ig)_T dV \ &= C_V dT + Tig(rac{\partial p}{\partial T}ig)_V dV \end{aligned}$$

 $Cyclic\ chain\ rule:$

$$egin{aligned} &= C_V dT - T rac{ig(rac{\partial V}{\partial T}ig)_p}{ig(rac{\partial V}{\partial p}ig)_T} dV \ &= C_V dT + T rac{lpha}{\kappa} dV \end{aligned}$$

12.11

show that

$$ig(rac{\partial C_V}{\partial V}ig)_T = Tig(rac{\partial^2 p}{\partial T^2}ig)_V \ ig(rac{\partial C_p}{\partial V}ig)_T = Tig(rac{\partial^2 V}{\partial T^2}ig)_p$$

$$(\frac{\partial C_V}{\partial V})_T = T(\frac{\partial (\frac{\partial S}{\partial T})_V}{\partial V})_T$$

$$= T(\frac{\partial (\frac{\partial S}{\partial V})_T}{\partial T})_V$$

$$= T(\frac{\partial (\frac{\partial p}{\partial T})_V}{\partial T})_V$$

$$= T(\frac{\partial^2 p}{\partial T^2})_V$$

show

$$rac{\kappa_T}{\kappa_S} = rac{C_p}{C_V}$$

$$TdS = ig(rac{\partial U}{\partial p}ig)_V dp + ig[ig(rac{\partial U}{\partial V}ig)_p + pig]dV$$

Let dS=0,we have

$$\begin{split} &(\frac{\partial V}{\partial p})_S = -\frac{\left(\frac{\partial U}{\partial p}\right)_V}{\left(\frac{\partial U}{\partial V}\right)_p + p} \\ &(\frac{\partial U}{\partial p})_V = \left(\frac{\partial U}{\partial T}\right)_V \left(\frac{\partial T}{\partial p}\right)_V \\ &= C_V \left(\frac{\partial T}{\partial p}\right)_V \\ &(\frac{\partial U}{\partial V}\right)_p = \left(\frac{\partial U}{\partial T}\right)_p \left(\frac{\partial T}{\partial V}\right)_p \\ &(\frac{\partial U}{\partial V}\right)_p + p = \left[\left(\frac{\partial U}{\partial T}\right)_p + p \left(\frac{\partial V}{\partial T}\right)_p\right] \left(\frac{\partial T}{\partial V}\right)_p \\ &= C_p \left(\frac{\partial T}{\partial V}\right)_p \end{split}$$

Therefore,

$$egin{aligned} ig(rac{\partial V}{\partial p}ig)_S &= -rac{ig(rac{\partial U}{\partial p}ig)_V}{ig(rac{\partial U}{\partial V}ig)_p + p} \ &= -rac{C_V}{C_p}rac{ig(rac{\partial T}{\partial p}ig)_V}{ig(rac{\partial T}{\partial V}ig)_p} \ &= rac{C_V}{C_p}ig(rac{\partial V}{\partial p}ig)_T \end{aligned}$$

移项得证.