2. δ(t) is a unit impulse at t=0, the limit I'M
as Δ → 0 of the punction:

 $\delta(t-a)$ is a unit include occurring where t-a=0 i.e. at t=a.

For a continuous function f(t), $f(t) \delta(t-a)$ is approximately the product f(t) \times $\delta(f(a)) \int f(a) da$

As $\Delta \rightarrow 0$, the product is only non-zero very near t=aSo $\int \delta(t-a) f(t) dt$ $rac{range}{range} \int \delta(t-a) f(a) dt = f(a)$

(provided t=a lies within the range of integration) (i) $\int \delta(t-3) dt = 1$ since t=3 his between 0 and 3

(ii) $\int \delta(i) \sin(a) da = \sin 0 = 0$

because $O < T_4 < 1$ = exp (us (474)) = 1.3407 $S(x+T_4) coss dx = 0 since -T_4 is not in the range <math>O \rightarrow 1$ 3 (i) of is the square ware All jumps of magnitude 4. definitions, from these jumps 45(t-1) 45(t-3) etc -45(t-1) -45(t-1)At = (0 tco Denset to Note jump at t=0 $\frac{d^2t}{dt} = \begin{cases} 0 + < 0 \\ \sqrt{25(t)} - \sqrt{25(t)} - \sqrt{25(t)} \end{cases}$ 40For tCO f=0, and y=0 is a solution For t>0 f=1 and the equation is dy + 3y = 1 Complementary function: solve ij + 3y = 0 to $y
et y = Ae^{-3t}$ Particular integral: try $y = \lambda$ (combant)

Then from $0 \quad 3\lambda = 1$, so $\lambda = V_3$ So general solution is CF+FI, $y = Ae^{-3t} + 1/3$ Now at t = 0 y must be continuous: it y had a jump, is would have a delta function, and nothing else in (1) could balance thin. So at t=0 we have y=0 to A+t/s=0The response is $y=\begin{cases} 0' & t<0 \\ t<0 \end{cases}$ The response t=0 (step response) t=0 t<0 t<0 t<0

4(ii) Same method as (i). For t < 0, y = 0.

For t > 0 we have y + ty = 1C.F.: $y + ty = 0 \rightarrow y = A \cos 2t + B \sin 2t$ P.I. In y = L, then reed (4t = 1), so t = 1/4So general solution is $y = \frac{1}{4}t + A \cos 2t + B \sin 2t$ At t = 0: if y had a jump, y would have a dittation and y would have $\frac{1}{2}t(S|\theta)$. This could not satisfy the equation, so y is continuous.

Similarly, if y had a jump, y would have S(t), and is y much be continuous.

So at t = 0 ($y = 0 \rightarrow 1/4 + A = 0 \rightarrow A = -1/4$)

So step response $y = 0 \rightarrow 1/4 + A = 0 \rightarrow A = -1/4$ To pulse response $y = 0 \rightarrow 1/4 + A = 0 \rightarrow A = -1/4$ Timpulse response $y = 0 \rightarrow 1/4 + A = 0 \rightarrow 0$ Timpulse response $y = 0 \rightarrow 0$ Timpulse response $y = 0 \rightarrow 0$ Timpulse response $y = 0 \rightarrow 0$

5. (i) For t < 0 f = 0, and y = 0For t > 0 f = 1 and equation is $y + \alpha y = 1$ CF. is $y = Ae^{-\alpha t}$ PI.: try $y = B \Rightarrow \alpha B = 1 \Rightarrow B = 1/\alpha$ So general solution is $y = 1/\alpha + Ae^{-\alpha t}$ At t = 0 y = 0, so $1/\alpha + A = 0 \Rightarrow A = -1/\alpha$ So step response is $y = \frac{1}{\alpha}(1 - e^{-\alpha t})$ for t > 0

(ii) If the unit step function is H(t) the required input is $f(t) = \frac{1}{T} (H(t) - H(t-T))$ The output thus a superposition of two step responses, as found in (i)

5 cont. Output
$$y = \begin{cases} 0 & t < 0 \\ \frac{1}{Td} \left(1 - e^{-dt} \right) & 0 \le t \le T \end{cases}$$

$$\frac{1}{Td} \left[\left(1 - e^{-dt} \right) - \left(1 - e^{-d(t-T)} \right) \right] \qquad t > T$$

The last part simplifies to
$$\frac{1}{Td}e^{-dt}(e^{dT}-1)$$

As
$$T \to 0$$
, $e^{\lambda T} \approx 1 + \lambda T + (\lambda T)^2 + \dots$

So $\frac{1}{\lambda T} e^{-\lambda t} \left(e^{\lambda T} - 1 \right) \approx e^{-\lambda t} \frac{\lambda T + \lambda^2 T_2^2 \dots}{\lambda T}$

So response tends to $y = \begin{cases} 0 & t < 0 \\ e^{-\lambda t} & t \neq 0 \end{cases}$

which is indeed the impulse response.

6 Impulse response from 4(i) was 9(t) = (0)(i) Input $f(t) = \begin{cases} 0 & t < 0 \\ e^{-2t} & t > 0 \end{cases}$ Output is $y(t) = \frac{1}{2}g(t-\tau)f(\tau)d\tau$ for the $=\int e^{3(t-\tau)} e^{-2\tau} d\tau = e^{-3t} \left[e^{\tau}\right]^{t}$ $= e^{-2t} - e^{-3t}$ Chech: $\dot{y} = -2e^{-2t} + 3e^{-3t}$ So $\dot{y} + 3\dot{y} = e^{-2t} = +4$

6 (ii) In put
$$f(t) = \begin{cases} 0 & t < 0 \\ sint & t > 0 \end{cases}$$

Output $y(t) = \int g(t-\tau) f(\tau) d\tau$

$$= \int e^{-3(t-\tau)} sin\tau d\tau$$

$$= e^{-3t} \int e^{3\tau} \left(\frac{e^{i\tau} - e^{-i\tau}}{2i} \right) d\tau$$

$$= \frac{e^{-3t}}{2i} \left[\frac{e^{(3+\frac{0}{2})\tau}}{3+i} - \frac{e^{(3-i)\tau}}{3-i} \right] t$$

$$= \frac{e^{-3t}}{2i} \left[e^{3t} \left(\frac{e^{i\tau}}{3+i} - \frac{e^{-i\tau}}{3-i} \right) - \frac{1}{3+i} + \frac{1}{3-i} \right]$$

$$= \frac{(3-i)e^{i\tau} - (3+i)e^{-i\tau}}{2i(3^2+1^2)} - \frac{e^{-3t}}{2i} \left(\frac{3-i-3-i}{3^2+1^2} \right)$$

$$= \frac{1}{10} \left(3 \sin t - \cot t + e^{-3t} \right) \qquad \text{for } t > 0$$
Chedi: $\dot{y} = \left(3 \cot t + \sin t - 3 e^{-3t} \right) / 10 \qquad \text{for } t > 0$

$$\dot{y} + 3y = \sin t \qquad \qquad \qquad$$

7(1)
$$\frac{1}{6}\ddot{y} + \frac{11}{12}\dot{y} + \dot{y} = 1$$
 for $\frac{6}{7}$ 0
C.F.: Try $y = e^{\lambda t} \Rightarrow \frac{1}{6}\lambda^2 + \frac{11}{12}\lambda + 1 = 0 \Rightarrow \lambda = -4$ or $-\frac{3}{2}$
50 C.F. is $Ae^{-\frac{7}{2}t} + Be^{-4t}$

P.T: Try
$$y = x \Rightarrow x = 1$$

50 general solution is $y = 1 + Ae^{-\frac{3}{2}t} + Be^{-4t}$

At
$$t=0$$
, $y=\dot{y}=0 \Rightarrow 1+A+B=0$ and $\frac{-3A}{2}-4B=0$
Thus $A=-85$ and $B=35$

So the step response is
$$y = 1 - \frac{8e}{5} + \frac{3e}{5}$$
 for $t > 0$.

7 (ii) Inpulse response =
$$\frac{d}{dt}$$
 (step response)

if $g(t) = 12e^{-3t/2} - 12e^{-4t}$ for $t > 0$

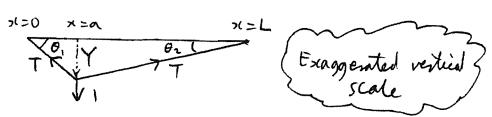
(iii) Now impose input $f(t) = \begin{cases} 0 & t < 0 \\ e^{-t} & t > 0 \end{cases}$

Output is $y(t) = \begin{cases} f(t) = f(t) & d = t \\ f(t) = t = t \end{cases}$

$$= \frac{12}{5} \begin{cases} e^{-3(t-t)/2} - e^{-4(t-t)} \end{cases} e^{-7} dt$$

$$= \frac{e^{-3t/2}}{5} \cdot \frac{12}{5} \cdot \frac{12$$

8 (i) Stretched custain wire in response to a point load moves to a displaced shape consisting of two straight lines.



 θ_1, θ_2 are around small, so that $\int \sin \theta_1 \simeq \theta_1 \simeq \tan \theta_1 = \frac{1}{\alpha}, \cos \theta_1 \simeq 1$ $\int \sin \theta_2 \simeq \theta_2 \simeq \tan \theta_2 = \frac{1}{1-\alpha}, \cos \theta_2 \simeq 1$ A unit bond is applied, so force balence requires $\int \sin \theta_1 \simeq \theta_2 \simeq \tan \theta_2 = \frac{1}{1-\alpha}$

8 cont.
i.e.
$$TY \begin{bmatrix} 1 \\ L-a \end{bmatrix} \approx 1$$

$$TYL = 1, \text{ so } Y = \alpha(L-a)$$

$$So g(x,a) = \begin{cases} (L-a)x & x < a \\ LT & a(L-x) \\ LT & x > a \end{cases}$$

(ii) For a continuous load f(x), we can apprecimate it by a now at small point boads (think of the curtain as a bead curtain!) tach point boad produces a suitably scaled venion of $g(x_1,a)$ as found in (i). By superposition, total displacement is the sum of there. In the limit, this sum becomes an integral, just as for the time-vanying case from lecture. So $y(x) = \int g(x_1,a) f(a) da$

(iii) For $0 \le x \le \frac{1}{2}$: $y(x) = \int_{0}^{x} \frac{Fa(L-x)}{LT} dx + \int_{x}^{x} \frac{F(L-a)x}{LT} dx$ $= \int_{0}^{x} \frac{F(L-a)x}{LT} dx + \int_{x}^{x} \frac{F(L-a)x}{LT} dx$ $= \int_{0}^{x} \frac{F(L-a)x}{LT} dx + \int_{0}^{x} \frac{F(L-a)x}{LT} dx$ $= \int_{0}^{x} \frac{F(L-a)x}{LT}$

8 cont.
For
$$x > \frac{1}{2}$$
: $y(x) = \int_{0}^{2} Fa(L-n) da$

$$= \frac{F(L-n)}{LT} \cdot \frac{L^{2}}{8} = \frac{FL(L-n)}{8T}$$

Check: At
$$x = \frac{1}{2}$$
, wire should be not broken.
From first solution, $y = \frac{FL}{16T}(3L-2L) = \frac{FL^2}{16T}$
From second solution, $y = \frac{FL^2}{16T}$

Note that this problem involving convolution in space is a bit more tricky than problems involving time. The reason is that an injudic response in time is always zero for t < 0, but a spatial "impulse response" like $g(s_1, a_1)$ here has non-zero values on both sides of the delta function. This means that more case is needed to get the convolution integral right.

TPH/JW