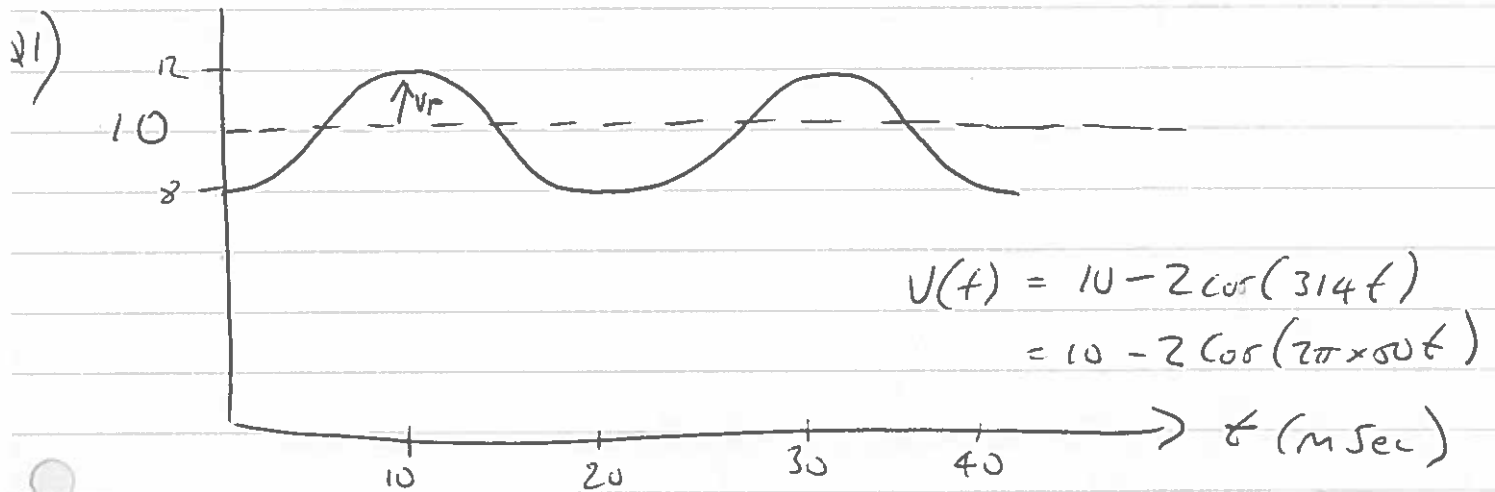


IA P3 Analyser of Cct Ex #2 CRIB



a) Amplitude $V_p = 2V$ b) Ph.-Ph Amplitude
 $V_{p-p} = 4V$

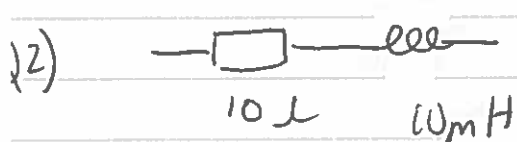
c) Time average value = $10V$

d) RMS amplitude: general case $a + b \cos(\omega t)$

$$RMS = \sqrt{a^2 + \frac{b^2}{2}} = \sqrt{102} = 10.1 V_{rms}$$

e) Freq $f = 50 \text{ Hz}$

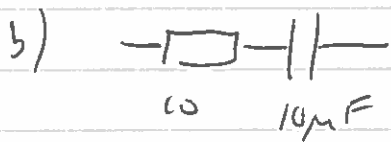
f) Angular freq $\omega = 2\pi f = 314 \text{ rad s}^{-1}$



$$\begin{aligned}
 Z_L &= j\omega L = j2\pi \times 10^3 \times 10 \times 10^{-3} \\
 &= j62.8 \Omega
 \end{aligned}$$

$$\Rightarrow Z_T = 10 + j62.8 \Omega$$

$$|Z_T| = 63.6 \quad \angle Z_T = 81^\circ$$



$$Z_C = \frac{1}{j\omega C} = -j \times \frac{1}{2\pi \times 10^3 \times 10 \times 10^{-6}}$$

$$= -j15.9 \Omega$$

$$Z_T = 10 - j15.9 \Omega$$

$$|Z_T| = 18.8 \Omega \quad \angle Z_T = -57.8^\circ$$

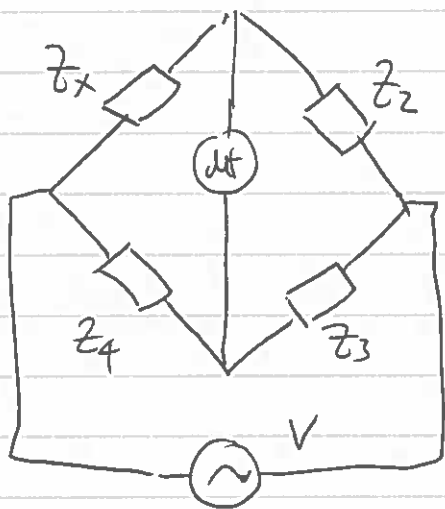
$$c) Z_T = (15 + j5.3) + (10 + j62.8) // (20 - j15.9)$$

$$= 15 + j5.3 + 28.2 - j7.52$$

$$= 43.2 - j2.22 \Omega$$

$$|Z_T| = 43.3 \Omega \quad \angle Z_T = -2.94^\circ$$

Q3) Balance condition can be gained from the data book but ideally should be derived via algebra



Balance when there is no current through detector "det"

\Rightarrow 2 potential dividers which will create the same voltage at top & bottom nodes

$$\Rightarrow \text{Top node } \frac{Z_2}{Z_x + Z_2} V = \text{Bot node } = \frac{Z_3}{Z_4 + Z_3} V$$

$$Z_2 (Z_4 + Z_3) = Z_3 (Z_x + Z_2)$$

$$Z_2 Z_4 = Z_3 Z_x \quad Z_x = \frac{Z_2 Z_4}{Z_3}$$

(2)

a) Maxwell $Z_x = R_x + j\omega L_x$

$$Z_2 = R_2 \quad Z_4 = R_4 \quad Z_3 = R_3 \parallel \frac{1}{j\omega C_3} = \frac{R_3 \frac{1}{j\omega C_3}}{R_3 + \frac{1}{j\omega C_3}} \times \frac{j\omega C_3}{j\omega C_3}$$

$$= \frac{R_3}{1 + j\omega C_3 R_3}$$

at balance

$$Z_x = R_x + j\omega L_x = \frac{R_2 R_4 (1 + j\omega C_3 R_3)}{R_3}$$

Compare real parts

$$\Rightarrow R_x = \frac{R_2 R_4}{R_3} \quad \cancel{j\omega} L_x = \frac{\cancel{j\omega} C_3 R_3 R_2 R_4}{\cancel{R_3}}$$

$$L_x = R_2 R_4 C_3$$

b) Wein $Z_x = R_x + \frac{1}{j\omega C_x}$

$$Z_2 = R_2 \quad Z_3 = R_3 \quad Z_4 = R_4 + \frac{1}{j\omega C_4}$$

At balance

$$R_x + \frac{1}{j\omega C_x} = \frac{R_2 (R_4 + \frac{1}{j\omega C_4})}{R_3}$$

$$R_x = \frac{R_2 R_4}{R_3} \quad \frac{1}{\cancel{j\omega} C_x} = \frac{R_2}{\cancel{j\omega} C_4 R_3}$$

$$C_x = \frac{C_4 R_3}{R_2}$$

Q4 a) $V_1 = 10 + 3j = 10.44 \angle 16.7^\circ$

$$b) \quad i_2 = \frac{V_2}{6-3j} \quad V_2 = \frac{V_1(6-3j)}{5+j+6-3j} = \frac{V_1(6-3j)}{11-2j}$$

$$\Rightarrow i_2 = \frac{V_1(6-3j)}{(11-2j)(6-3j)} = \frac{10+3j}{11-2j} = 0.832 + j0.424 \text{ A}$$

$$V_2 = (6-3j)i_2 = 6.26 + j0.048 \text{ V}$$

$$= 6.25 \angle 0.439^\circ$$

$$\text{phase difference} = \angle V_2 - \angle V_1 = 0.439 - 16.7 = -16.26^\circ$$

$$G_{av} = |V_2|/|V_1| = 6.26/10.44 = 0.6$$

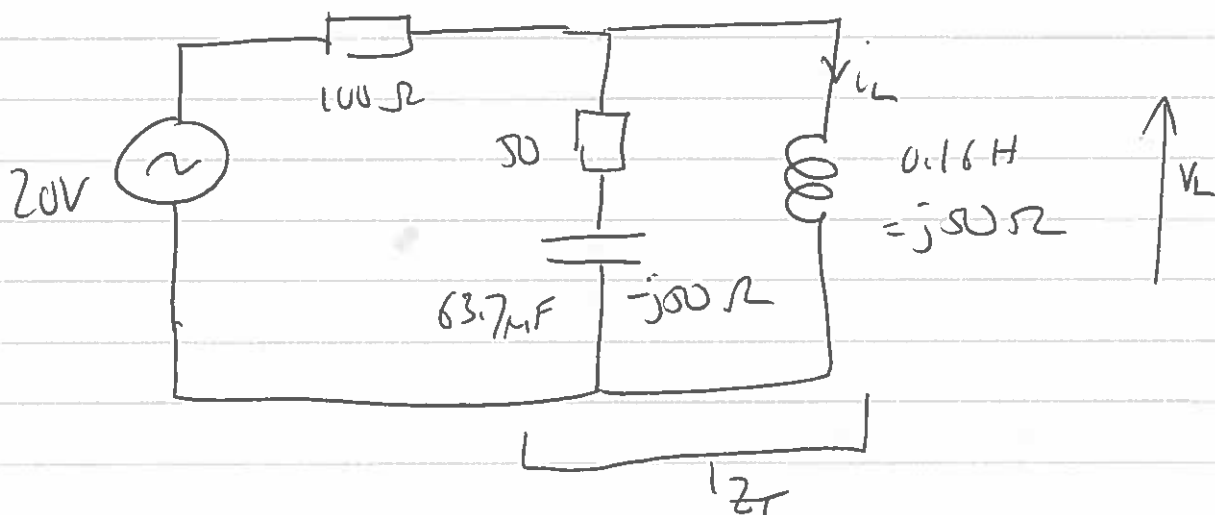
d) Thévenin voltage V_T is just $V_2 = 6.26 + j0.048 \text{ V}$

Thévenin impedance $Z_T = Z_1 \parallel Z_2$ as voltage source has no impedance

$$= \frac{(5+j)(6-3j)}{5+j+6-3j}$$

$$= 3.048 - j0.264 \Omega$$

Q5)



$$\Rightarrow i_L = \frac{V_L}{j50} \quad V_L \rightarrow \text{potential divider}$$

$$V_L = 20 \times \frac{Z_T}{100 + Z_T}$$

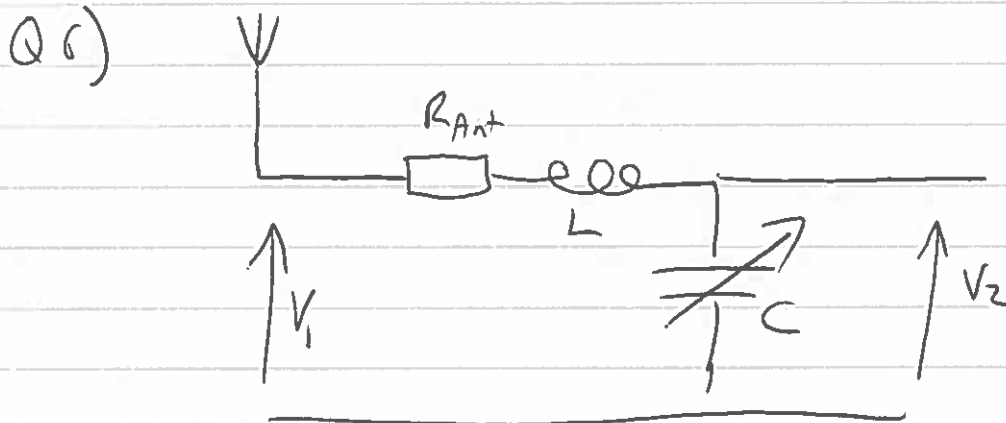
$$Z_T = \frac{j\cancel{50}(\cancel{50} - 50j)}{\cancel{50} - j\cancel{50} + \cancel{50}j} \neq$$

$$= 50 + 50j$$

$$i_L = \frac{20(50 + j50)}{j50(100 + 50 + j50)}$$

$$= \frac{2 + 2j}{-5 + 15j} = 0.08 - j0.16$$

$$|i_L| = 0.179 \angle -63.4^\circ$$



Pot divider

$$V_2 = V_1 \frac{1/j\omega C}{R_{Ant} + j\omega L + 1/j\omega C} \times \frac{j\omega C}{j\omega C}$$

$$= \frac{V_1}{\underbrace{1 - \omega^2 LC + j\omega C R_{Ant}}_{\text{Resonant term}}}$$

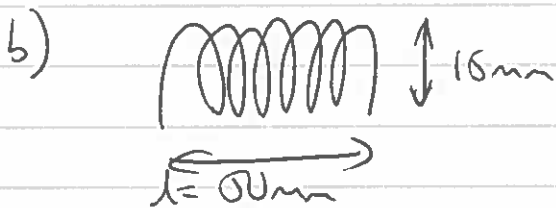
V_2 max when resonant term = 0

$$\Rightarrow 1 = \omega^2 LC \quad \Rightarrow \omega = \frac{1}{\sqrt{LC}}$$

$$f = 198 \text{ kHz} \quad L = 8 \text{ mH} \quad \Rightarrow \quad C = 81 \text{ pF}$$

$$\begin{aligned} \text{At resonance} \quad V_2 &= \frac{V_1}{j\omega C R_{\text{ant}}} = \frac{100 \times 10^{-6}}{j 2\pi \times 198 \times 10^3 \times 30 \times 81 \times 10^{-12}} \\ &= -j 3.31 \times 10^{-3} \text{ V} \end{aligned}$$

$$33.1 \text{ mV} \quad \angle -90^\circ$$



From PPE Lecture, inductance of an air filled solenoid

$$L = \frac{\mu_0 N^2 A}{l}$$

$$\begin{aligned} \Rightarrow N &= \sqrt{\frac{l L}{\mu_0 A}} = \sqrt{\frac{80 \times 10^{-3} \times 8 \times 10^{-3}}{4\pi \times 10^{-7} \times \pi (7.5 \times 10^{-3})^2}} \\ &= 1342 \text{ Turns} \end{aligned}$$

c) Long wave tuning range $148 \text{ kHz} \rightarrow 284 \text{ kHz}$

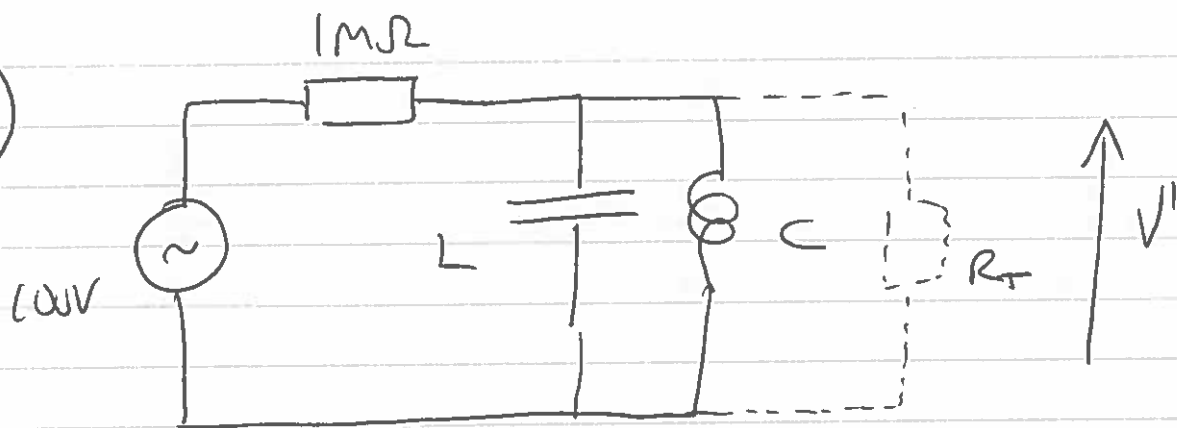
\Rightarrow Variable C has to tune resonance across this range $\Rightarrow C_1$ at lowest freq

$$C_1 = \frac{1}{\omega_1^2 L} = 145 \text{ pF} \quad C_2 = 39.3 \text{ pF}$$

Either Air filled variable capacitor or varactor

(6)

Q7)



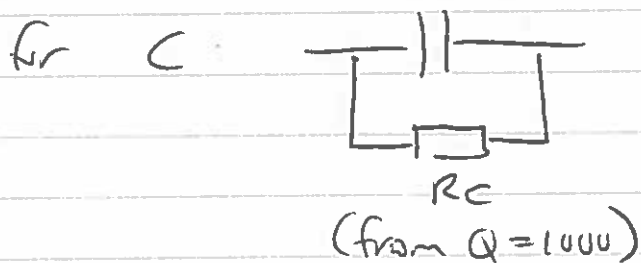
L & C are non-ideal and we want to represent the components as an ideal L & C in parallel with resistance R_T which represents the imperfections. Imperfection or via Q -factor

if ~~that~~ Resonant frequency only depends on L & C

$$\Rightarrow f_0 = \frac{1}{2\pi\sqrt{LC}} = 159 \text{ kHz}$$

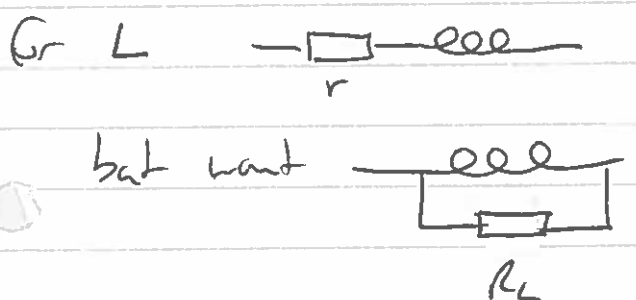
At resonance L & C cancel leaving R_T

$$\Rightarrow V' = \frac{R_T}{1 \times 10^6 + R_T} \times 100$$



$$Q = \omega_0 R_C C$$

$$\Rightarrow R_C = 1 \times 10^{-7} \Omega \quad (10 \text{ m}\Omega)$$



both have same

$$Q = \frac{\omega_0 L}{r} = \frac{R_L}{\omega_0 L}$$

$$\Rightarrow R_L = \frac{\omega_0^2 L^2}{r} = 1 \times 10^{-7} \Omega$$

$$R_T = R_L // R_C$$

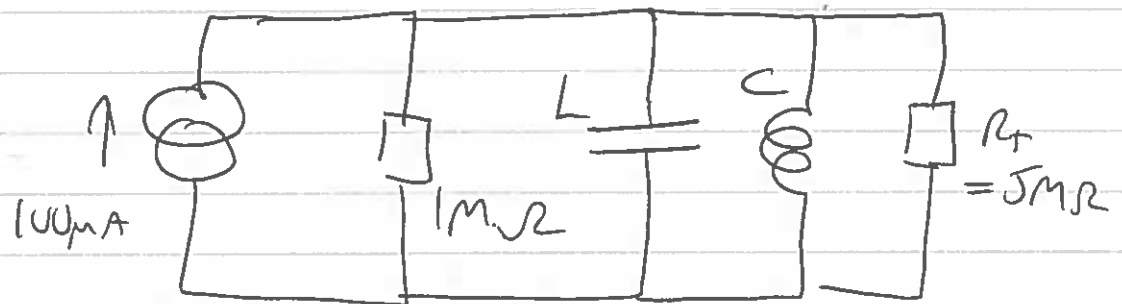
$$= 5 \text{ M}\Omega$$

$$\Rightarrow V' = \frac{5 \times 10^6}{1 \times 10^6 + 5 \times 10^6} \times 100 = 83.3 \text{ V}$$

c) $Q_T = \frac{f_0}{\Delta f}$ $\Delta f = \text{half power B/W}$

Q_T is a result of the Q from the L & the C as well as the source resistance.

\Rightarrow Norton equivalent



$$\Rightarrow \text{total parallel } R' = R_T // 1 \text{ M}\Omega$$

$$= 5 \times 10^6 // 1 \times 10^6 = 830 \text{ k}\Omega$$

$$\Rightarrow \text{get total } Q_T = \omega_0 R' C$$

$$= 1 \times 10^6 \times 830 \times 10^3 \times 100 \times 10^{-12}$$

$$= 83$$

$$\Rightarrow \Delta f = \frac{159 \times 10^3}{83} = 1.92 \text{ kHz}$$

