

CAST 3.0

Conformational Analysis and Search Tool

Tutorial



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1. About this tutorial

2. Getting started: The test molecule

From scratch IN a first step we may want to introduce how to generate TINKER files from scratch. The two programs we will need are molden^[MOLDEN] and tinkers. If there is no PDB file of our target molecule first of all we need to generate this. A very handy program to do so is molden^[MOLDEN].

Using the editor Starting molden there is a button called “ZMAT Editor” shown in figure 1 on the very left of the upper images. Pushing this button opens another window with the option to add a line (figure 1 top middle) which can be clicked to proceed in adding our first atom. The now changed window shows all the atoms in the periodic table. Furthermore next to the section bondlength one can choose whether the added bond is a single, double or triple bond, this only tells molden to use the specific bondlength if molden knows the value. Needless to say that this option will not affect the first atom.

The Molecule In the following we will create a test molecule which is a small peptide made of Alanine and Glycine. So we start by adding a carbon atom as depicted on the very right of the top row in figure 1 which makes a red star appear. To proceed a little faster we may want to add a whole substituent so we click on this little star (figure 1 in the upper middle the very left one). If we successfully pushed the button we see him turning into a sphere (figure 1 in the middle of the upper middle images). Now we choose the “Substitute atom by Fragment” option (figure 1 in the upper middle the very right) and choose CH₃-fragment (figure 1 on the lower middle row the very left). Now three additional H-atoms appear. To go further on we can repeat the actions for substitution to replace one of the hydrogen’s with an amine and another hydrogen with a methyl-group. The last hydrogen stays as it is. Unfortunately, molden does not know what we plan to do so it may create distances between atoms which are not very likely. We deal with this issue later on after we have had a closer look at internal coordinates.

Short look at internal coordinates Now we need another carbon atom which we need to add via the “Add Line” option as we did it for the first carbon. In internal coordinates, which we are using to build our peptide, we need for the first atom no spacial information it just lies in space. For the second one we need the distance from the first atom. The third one needs a distance to one of the former ones and an angle defined through the previous ones. As soon as we reach the fourth atom we need as much spacial information as we do in Cartesian-Coordinates which means three values. Let us say the atom we look at is atom *A*, the first value we need is the distance to another atom *B*, the second the angle over atom *B* to a third atom *C* and the third value is a torsion between *A* and a third atom *D* in respect to the line *B* and *C*. Of course none of these atoms can be the same atoms so $A \neq B \neq C \neq D$.

Add another atom While we add another carbon atom the program will ask us for atom *B* for which we choose our carbon with only four bonds. The next atom *C* will be the methyl carbon and the last one can be one of the methyl hydrogen atoms. To deal with molden’s wrong placements we use our knowledge about internal coordinates and check each atom which is misplaced by clicking on it. In the window showing the internal information the clicked atom is highlighted red as it is marked red in figure 1 on the lower middle

row the right one. Each value can be changed by clicking on the related box and overwriting the old value. If one clicks in the last box all information about bond, angle and torsion partner is revealed. The yellow sphere is atom *B* its distance to atom *A* is marked yellow, the green sphere is atom *C* and the resulting angle is marked green. The light blue sphere is finally atom *D* and the torsion value is marked light blue. In the case shown in figure 1 we can not change the torsion of the misplaced hydrogen for it has no torsion because it is just the third atom (see appendix A). But we can change the position of the amine and the carbon by clicking on them and changing their torsion. Now we need to proceed to substitute and add atoms till we got the Ala-Gly-Peptide. If we want to use the OPLS-AA-Force field (FF)- and we will - we got to create a zwitterionic peptide.

Saving as tinker-file After finishing the structure we click on close to close the Z-Matrix editor and click on write on the main window and choose tinker as output (figure 1 bottom pictures). We enter the directory and the filename we wish to use and save it. In this case the filename is “AlaGly.xyz”. Now we have a tinker file with MM3 forcefield parameters changing these to OPLS-AA is desired.

Generating the final tinker-file The most straight forward way to change the MM3 parameters to OPLS-AA ones is to look inside the tinker file and, for each atom, look up the kind of atom molden has assigned it to. So let’s take this little example:

1	N	-0.679000	1.176000	-0.480000	39	2	6	12	13
---	---	-----------	----------	-----------	----	---	---	----	----

This may be the first atom of the molden generated file. The first integer is the atom number followed by the atom’s abbreviation. The three floating point numbers are the x, y and z coordinate values and in the sixth row the atom type is placed. The last integers assign the connected atoms. We need the type and look that up in an MM3 FF file and scroll to the lines beginning with “atom” and choose the 39th. The line reads:

atom	39	N+	"NSP3 AMMONIUM"	7	14.003	4
------	----	----	-----------------	---	--------	---

So now we need a equivalent atom number in the OPLS-AA FF in which are plenty of more atom types as in the MM3 parameter file. So we need to find which atom type this might be. MM3 say ammonium sp3 in OPLS-AA we find:

atom	230	53	N3	"Ammonium RNH3+"	7	14.007	4
------	-----	----	----	------------------	---	--------	---

So we change the atom type to 230 changing the atom’s abbreviation is optional. The first atom now looks like:

1	N3	-0.679000	1.176000	-0.480000	230	2	12	6	13
---	----	-----------	----------	-----------	-----	---	----	---	----

We need to proceed through the whole molden generated MM3 file and end up with something like the file in appendix A.

3. First look at CAST

Now we are ready to set up the first calculation. The CAST configuration file is shown in appendix C. This file is part of the downloaded package and is contained in the downloaded main directory. The easiest

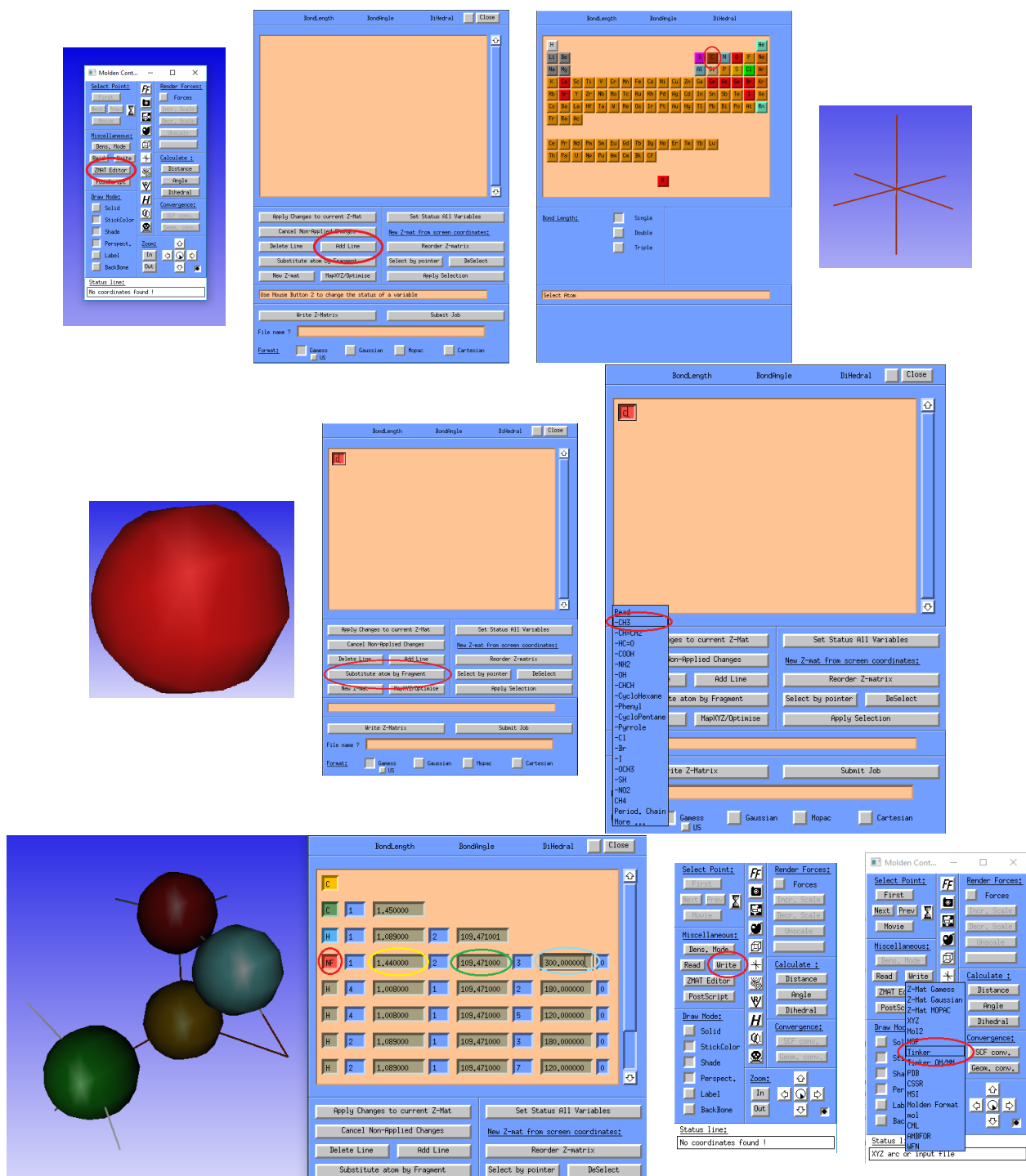


Figure 1: - Molden structure generation process within the "ZMAT Editor"

way is to copy the configuration file directly to the tinker file we want to use otherwise the total path to the file got to be defined in the command prompt by using `-status="C:\PATH\TO\FILE\filename.txt"` or `-s "C:\PATH\TO\FILE\filename.txt"` after calling CAST. There are two options to start CAST either with a configuration file or using the command prompt alone. Of course one can mix these two possibilities up. In this tutorial we focus on using the configuration file rather than using the second option. There is no particular order in which the configurations in the configuration file are sorted but it is advised to use the predefined configuration file in order to keep things easy. The configuration file is used by giving each keyword a value. In general:

keyword	value
---------	-------

So each value for each keyword can be changed to adjust the settings to each respective task which is desired. So let us take a look at the predefined configuration file. The first section contains general settings starting at line 4 like the amount of information which is printed during the execution which can be changed in line 12 by altering the value next to **verbosity**. The next value depends on the cores which your PC can spend for the desired calculation. With an *i*-X-Processor there are four cores available and thus the value next to **cores** in line 17 reads 4.

The next section is for determining the input and output options beginning at line 23 and starting with the name of the molecules file name in our case we got to write next to **name** the name of the Alanine Glycine peptide, so **AlaGly.xyt** will do. The next option in line 34 decides in which file the final output is written. In this case we use **AlaGly_final**. Keep in mind that there is no ending needed depending on the method there is a ending generated. As we use a tinker-file as input format we write in line 38 **TINKER**. Of course there are other input types, too. At line 52 begins a listing of all possible tasks which we depict in this tutorial and which are possible to undergo. The task we desire is to write in line 84 next to **task**. In a first step we want to start a local optimization for which we choose **LOCOPT**. This is the only configuration we can change in this section. The next section concentrates on the energy interfaces e. g. **OPLS-AA** which we desire to use. To do so we need to write **OPLS-AA** next to **interface** in line 101. We do not need a preinterface (for preoptimization) so we let the value in line 105 unchanged. The path to the parameter files needs to be adjusted as well and so the desired parameter file needs to be defined in line 110. So we change the value to **OPLS-AA.prm** and copy the FF file to the directory with the **CAST.txt** and the **AlaGly.xyz**. Everything is set up for the first optimization so we open a command prompt and enter:

```
cd "C:\PATH\TO\TUTORIAL"
"C:\PATH\TO\CAST\CAST.exe"
```

CAST starts and prints the local optimized structure in the desired outputfile with a **_LOCOPT.arc** extension. Opening this shows the result in appendix B.

4. Available energy interfaces

CAST posses in principle three different types of energy interfaces. Starting with force fields which are directly included in the CAST code. Therefore, the CHARMM, AMBER, OPLS-AA and AMOEBA force fields (FF) are available. In addition to the standard AMOEBA FF. The improved SAPT-FF is included (details will be given in the specific paragraph). The second type are semi-empirics, whereas we use a an

interface to the MOPAC program from the Stewart group. The third interface offers the possibility to do DFT calculations on GPUs by using an MPI interface with the Terachem (V1.5) program from Todd Martinez group.

OPLSAA, AMBER and CHARMM CAST includes three standard FFs which possess more or less same functional description, but are different in terms of parametrization. The interface is chosen by the following **interface** keywords: **OPLSAA**, **AMBER**, **CHARMM**. Besides The interface keyword each of these FFs needs a tinker-parameter file. The keyword is **paramfile** this is defined in line 110 in the example input file. A typical parameter file in Tinker-format looks like:

```

1
2 #####
3 ##                               ##
4 ## Force Field Definition      ##
5 ##                               ##
6 #####
7
8
9 forcefield                      OPLS-AA
10
11 vdwindex                      TYPE
12 vdwtype                       LENNARD-JONES
13 radiusrule                    GEOMETRIC
14 radiustype                    SIGMA
15 radiussize                    DIAMETER
16 epsilonrule                  GEOMETRIC
17 torsionunit                   0.5
18 vdw-14-scale                  2.0
19 chg-14-scale                  2.0
20 electric                      332.06
21 dielectric                    1.0
22
23
24 #####
25 ##                               ##
26 ## Literature References      ##
27 ##                               ##
28 #####
29
30
31 The parameters supplied with TINKER are from "OPLS All-Atom Parameters
32 for Organic Molecules, Ions, Peptides & Nucleic Acids, July 2008" as
33 provided by W. L. Jorgensen, Yale University during June 2009. These
34 parameters are taken from those distributed with BOSS Version 4.8.
35
36 Note that "atom type" numbers and not "atom class" numbers are used
37 to index van der Waals parameters, see the "vdwindex" keyword above
38
39 The atom types with (UA) in the description are "united atom" values,
40 ie, OPLS-UA, where any nonpolar hydrogen atoms are combined onto their

```

```

41 attached atoms. All other parameters are "all-atom", OPLS-AA, including
42 explicit hydrogen atoms.
43
44
45 #####
46 ##                                     ##
47 ## Atom Type Definitions             ##
48 ##                                     ##
49 #####
50
51
52 atom      1      1      F      "Fluoride -CH2-F (UA)"      9      18.998      1
53 atom      2      2      C2     "Fluoride -CH2-F (UA)"      6      14.027      2
54 atom      3      3      C      "Acetic Acid -COOH (UA)"      6      12.011      3
55 atom      4      4      O      "Acetic Acid >C=O (UA)"      8      15.999      1
56 atom      5      5      OH     "Acetic Acid -OH (UA)"      8      15.999      2
57 atom      6      6      C3     "Acetic Acid CH3- (UA)"      6      15.035      1
58 atom      7      7      HO     "Acetic Acid -OH (UA)"      1      1.008      1
59 .....

```

The first block after the FF definition defines several input parameters for the calculations of the potential energy functions like vdw-combination rules and further on.

AMOEBA and SAPT-FF The AMOEBA FF belongs to the class of polarizable FFs. The energy description should not be described in detail. A detailed description can be found in [Ponder2010]. The SAPT-FF is a specialized kind of the AMOEBA FF, whereas the short-range electrostatics are treated within a partitioning scheme. For the description of the electrostatic energy it is a common approach to use a finite expansion over atomic multipoles. The simple multipole expansion underestimates the electrostatic energy and for a better description a penetration energy can be included by using the Coulombic energy between pro molecular charge densities. The classical electrostatic energy (Coulomb) between two molecules A and B is described by the following expression,

$$E_{es} = \int \int \rho_A(r_A) \rho_B(r_B) |r_A - r_B|^{-1} dr_A dr_B \quad (1)$$

where $\rho_A(r_A)$ and $\rho_B(r_B)$ are the molecular charge distributions, containing nuclear and electronic contributions. In most cases in computational work the electron distribution is approximated by a set of multipole moments.[Stone1996] But it is shown that they underestimate the exact energies which can be calculated by exact integration methods. This is related due to the fact that the penetration of the electronic distribution of molecule A inside molecule B is not included in these approaches.

The penetration energy is affected by the Coulombic charge density between pro molecular charge distributions (atomic charge distributions), which means that it is the dominant part. Therefore, the charge distribution can be split into a sum of atomic and deformation terms. The atomic charge distributions are described by spherical ones. In consequence the Coulombic energy is relatively easy to compute. It can be

calculated as functions depending on the distance and several parameters. Then the contribution term of atom A can be written in the following way^[Spackman1986a],

$$\rho_A(r_A) = \sum_{i \in A} [\rho_{A,i}^{atomic}(r_A) + \Delta\rho_{A,i}^{elec}(r_A)] = \rho_A^{pro}(r_A) + \Delta\rho_{A,i}^{elec}(r_A) \quad (2)$$

which describes the partitioning of the molecular electronic distribution. The pro molecular charge distribution of spherical atom A is $\rho_A^{pro}(r_A)$ and $\Delta\rho_{A,i}^{elec}(r_A)$ is the deformation term. Now it is possible to rewrite E_{es} and fill in $\rho_A\rho_B$ in eq. 1 For this $\rho_A\rho_B$ is shown.

$$\begin{aligned} \rho_A\rho_B &= \sum_{i \in A} \sum_{j \in B} [\rho_{A,i}^{atomic} \rho_{B,i}^{atomic} + \rho_{B,j}^{atomic} \Delta\rho_{A,i}^{elec} + \rho_{A,i}^{atomic} \Delta\rho_{B,j}^{elec} + \Delta\rho_{A,i}^{elec} \Delta\rho_{B,j}^{elec}] \\ &= \rho_A^{pro} \rho_B^{pro} + \rho_A^{pro} \Delta\rho_B^{elec} + \rho_B^{pro} \Delta\rho_A^{elec} + \Delta\rho_A^{elec} + \Delta\rho_B^{elec} \end{aligned} \quad (3)$$

In consequence E_{es} can be expressed in three terms containing pro molecule and deformation depending energies.

$$E_{es} = E_{pro-pro} + E_{pro-def} + E_{def-def} \quad (4)$$

The description with pseudo atomic spheres leads to zero multipole moments for the spherical atom. Only the deformation term $E_{def-def}$ includes multipole moments. If no atomic multipole moments are used all other terms are zero for spherical pseudoatoms, so it is necessary to use an atomic description. This is the case for the Bader's atoms in molecules (AIM) theory. There the electronic distribution is divided into discrete atomic fragments. In the case of fitted charge/multipole expansions derived from electrostatic potentials it would generally work, but there are cases for which this approach fails. It is important to know that there are many differences between the partitioning schemes and how they are implemented. Especially the multipole expansion and the convergence criteria can be very different. For instance, AIM uses a formally infinite expansion, truncated at some level for the multipole expansion or in the evaluation of the energy. AIM stops at the hexadecapole level and the energy calculation at $L = l_A + l_B = 8$ (hexadecapole-hexadecapole). The $E_{pro-pro}$ term in eq. 4 describes the Coulomb interaction between pairs of spherical atomic charge densities. $E_{pro-pro}$ can be the constitutive term in the expression for E_{es} which is related to the large contribution in the description of an attractive interaction and is substantial at normal bindings and Van-der-Waals separations. This energy can be expressed as a function of the distance between two atomic centers

$$E^{a,b}(R) = \frac{Z_A Z_B}{R} - \int_{-\infty}^{\infty} \frac{Z_a \rho_b(r_2)}{|R_a - r_2|} dr_2 - \int_{-\infty}^{\infty} \frac{Z_b \rho_a(r_1)}{|R_b - r_1|} dr_1 - \int \int_{-\infty}^{\infty} \frac{\rho_a(r_1) \rho_b(r_2)}{|r_1 - r_2|} dr_1 dr_2 \quad (5)$$

with the nuclear charges Z and the charge distributions $\rho(r)$. The first term represents the coulomb interactions between two atomic centers with their charges, the second and the third term represents the coulomb interaction between the atomic charges and the atomic charge densities (spherical), and the last term is the interaction between the charge densities. This three dimensional problem can be reduced to a one-dimensional integral for integration in reciprocal space (in atomic units)^[Spackman1986],

$$E_{es}^{a,b} = \frac{2}{\pi} \int_0^{\infty} [Z_a - f_a(s)][Z_b - f_b(s)] j_0(sR) ds \quad (6)$$

where Z_a is a nuclear charge, $f_i(s)$ are the atomic scattering factors with the scattering vector $s = (4\pi \sin\Theta/\lambda)$ and $j_0(sR)$ the spherical Bessel function of zero order^[Tafipolsky2011]. The atomic scattering factors

$$f_a(s) = 4\pi \int_0^\infty \rho_a(r) \frac{\sin(sr)}{sr} dr \quad (7)$$

are obtained from analytical atomic ground state wave functions. The scattering factors can be expanded with linear combinations of Slater-type functions. There are a few commonly known possibilities for the ground state wave function available. For a appropriate description of aromatic dimers, as noted by Spackman^[Spackman2006], a contraction scheme of the hydrogen atom charge density is needed (for the reproduction of reference data). In consequence to this a description for the contraction is needed. This can be done by rewriting eq. 6 and obtain

$$E_{es}^{a,b} = \frac{2}{\pi} \int_0^\infty [Z_a - f_a(s)/\kappa_a][Z_b - f_b(s)/\kappa_b] j_0(sR) ds \quad (8)$$

where κ_a and κ_b are contraction parameters for the charge densities of atoms a and b . In the original paper of Spackman^[Spackman2006] this contraction parameter has been set to the value of 1. If $\kappa > 1$ then a contraction is the result and if $\kappa < 1$ an expansion is realized. The integral in eq. 8 can be solved numerically by a one dimensional numerical strategy.

The $E_{pro-def}$ term in eq. 4 characterizes the interaction between the charge density of one molecule and the atomic deformation term in another. This term is very small and only notable for small separations between atoms. For dimers of small molecules the energy is always positive and in the range of 1.5 kJ/mol. In conclusion, it can be said that $E_{pro-pro}$ is one of the most important terms for the electrostatic energy description and is called the **Spackman-correction** in this work. The deformation energy $E_{def-def}$ is also one of the key terms in the description of intermolecular interactions. For this term the description depends on the used force field or the used multipole moments (for example DMA multipoles).

- **How to run a SAPT-FF/AMOEBA calculation?**

For running an AMOEBA or the SAPT-FF calculation the **interface** keyword should be set to AMOEBA. The SAPT-FF is activated by using the **Spackman** keyword (see line 122). This keywords needs three input parameters: activation (0/1), interpolated gradients (0/1) and cutoff radius for the elect. interactions (standard=10.0).

- **Spackman 1 1 10.0** - short-range correction activated, interpolative calculation activated and cutoff is set to 10.0 Å

The SAPT-FF calculation needs several additional input files. The minimum which requested is the Spackman.prm file which contains the κ and the atomic basis information. If one would like to use the interpolative variant the precalculated energy and gradient lists are needed. These files are called XY_EN.in or XY_GRAD.in. For a successful calculation one needs all the .in files (at the moment 20 files). The Spackman.prm file is given in the appendix (see line 51). Within the parameter files the κ values can be changed (see line 3. The first number indicates the atom type by the atomic charge value.

MOPAC By using the the **MOPAC** interface keyword one needs to install the latest Version of MOPAC (MOPAC2012/16) to do calculations. For academic groups MOPAC can be freely downloaded from: <http://openmopac.net/downloads.html>. The MOPAC interface is an file I/O interface and needs some input parameters to generate the appropriate input file. Generally the MOPAC interface can be combined with all existing tasks which need an energy or gradient evaluation. The most important keywords are:

- **MOPACpath** *Character String* - defines the absolute pathway to the binary installed on the system
- **MOPACkey** *Character String* - delivers the essential input parameters like method (standard = PM7)
- **MOPACdelete** *bool* - decision about saving or deleting temporarily generated files

TERACHEM description under construction....

5. Go through tasks

SP Now we may compare the total energy of our “initial guess” and the local minimum we found. To do so we can look at the `AlaGly_final_LOCOPT.txt` file to obtain the energy of the local minimum which reads -125.525 kcal/mol but if we close the command prompt the energy of the initial structure is gone. So we can compute this by doing a SP calculation by just changing the task to **SP**. Remember the task was in line 84 in the input file seen in appendix C and again running CAST with

```
cd "C:\PATH\TO\TUTORIAL"  
"C:\PATH\TO\CAST\CAST.exe "
```

and we obtain a total energy of 5.204 kcal/mol. The same way one could calculate the gradients by using **GRAD**.

MD A MD simulation is to describe the behavior of an ensemble of particles during a period of time by integrating over the classical Newton laws of mechanics. To use CAST to do so we take a closer look at the input file in appendix C. The MD part starts at line 606 a few lines below we see the **MDsteps** option in line 612 which we can assign the value of how many steps we want to perform. This may depend on the size of the time step we want to take which can be determined later. Keep in mind that a MD simulation needs very little time steps. We set the step number to 50000. The **MDintegrater** option in line 619 let us choose which integrator we want to use. We can choose between the Velocity-Verlet^[VelVer] implementation and the Beeman^[Beeman] one. Let's use the Velocity-Verlet one known from basic computational chemistry textbooks. The **MDveloscale** option in line 623 is set to one. A thermostat would be nice to observe MD on one specific temperature so we choose for **MDthermostat** in line 627 the one to let a Nose-Hoover^[NoseHoover] algorithm take care of keeping the same temperature. In line 631 is the option to choose the time step in picoseconds by writing the desired value next to the option **MDtimestep**. We choose 0.001 ps. The next option in line 635 makes the MD simulation start again if the molecule gets broken. We choose not to do so and hope it will work either way. To do so we write a 0 next to **MDrestart_if_broken**. After that we go forth to line 639 and write next to **MDtrack** a one to enable tracking and allowing us to make several snapshots. This makes it possible to make a little video. The next three options in line 648, 650 and 652 are determining the snapshots we want. So **MDsnap** is set to 1000 to get 1000 snapshots the **MDsnap_buffer** option is set to 100 to sample 100 snapshots before writing them into a file. The last option is to optimize each snapshot which would be **MDsnap_opt** is disabled, too. In line 656 we can determine the temperature and can change it at a specific step. This can be done by adding lines in the form of line 656. So e. g. if we want to have a start temperature of 298.15 K and increase the temperature by 50 K every 10000 steps we write something like written in line 658 to 662. One could also use a **RATTLE**^[RATTLE] option which considers internal constraints. This is done by enabling the **MDrattle** option in line 684. We do not need this now so we turn it off.

Enough explanation on the input file lets try this MD simulation. First of all you may want to copy the optimized file `AlaGly_final_LOCOPT.arc` file and the modified `CAST.txt` to a separate folder to keep your workspace clean now you got to change the input filename in the `CAST.txt` to the new `AlaGly_final_LOCOPT.arc` or rename `AlaGly_final_LOCOPT.arc` to `AlaGly.xyz`. Open a command prompt and write

```
cd "C:\PATH\TO\MD"
```

```
"C:\PATH\TO\CAST\CAST.exe"
```

hit enter and let CAST work. The result are two files one is `AlaGly_final_MD_SNAP` with the snapshots which can be opened by molden. If we do so we can click the movie button in molden and see the MD simulation visualized. The other file is a tracking file showing the energy and temperature after each step. The temperature is never exact on the level we demanded but is kept to value. It is pretty evident that the potential energy can get higher with more energy because we offer more thermal energy to get to not minimized states. Some other examples of MD-simulation are shipped with CAST

MC The MC^[MC] option is to globally scan the hyperplane. If we use MCM we scan the hyperplane and optimize afterward in order to find new minima. To do so we change the task on line 84 of the configuration file in appendix C to MC and proceed to the configurations beginning at line 374. In line 382 in which we can choose the temperature. We choose to write 298.15 new to `Temperature` to set it to 298.15 K. We choose 2000 iterations in line 386. In line 400 we can decide which found minima are saved by applying a value which says how great the energy difference of the local to the global minima is allowed to be. We choose 10 kcal/mol. To use the current local minima as metropolis criterion in our MCM simulation we write 0 new to `G0metrolocal` in line 405. We look at `STARTOPT` later so we choose the zero next to the startopt option in line 410. We do not want to have our temperature scaled once a new minimum is found so we choose in line 416 the default 1.0. The next option in line 420 let's us determine how precise the floating point numbers are printed. We may choose 6. With the option which fallback type we prefer we can choose to which structure we fall back in case the simulation got stuck. We want to go back to the last global minimum and thus choose `LAST_GLOBAL` next to `G0fallback` in line 427. The fall back limit in line 433 is set to 500 so we want CAST to try hard before it decides it got stuck. The `fallback_fr ...` options are just for other fall back types than returning to the last global minimum so we skip line 440, 445 and 452. We choose the main grid in Å with 60.0 at line 461 and the step size determining the maximum value MC moves the atom by 1.4 in Å. In most of the cases a MC is not enough so we choose to perform a MCM by setting the option `MCminimization` in line 476 to 1. There are several reasons why would prefer to optimize in internal rather than cartesian coordinates so we choose the `MCmovetype` to be dihedral by setting the value in line 480 to 1. At last we want the greatest possible change in torsion between two steps to be 180° so that each torsion can be scanned. To do so we write 180.0 next to `MCmax_dihedral`. Do perform the calculation save the `CAST.txt` in a separate folder and add the optimized `AlaGly_final_LOCOPT.arc` either change the name of `AlaGly_final_LOCOPT.arc` to `AlaGly.xyz` or change line 30. Now only CAST needs to be started. To do so open a command prompt and type

```
cd "C:\PATH\TO\MC"  
"C:\PATH\TO\CAST\CAST.exe"
```

due to the fact that this is a statistical approach there is a small change in not getting another global minimum. If this is the case rerun the program. There got to be another one. In this example CAST found another minimum with a total energy of -135.289 kcal/mol which differs in 9.764 kcal/mol from the starting point. If we look inside molden and load the .arc file we see the nitrogen of the amide group aligned its hydrogen next to the amide carbonyl oxygen. This seems legit to be in a greater minimum.

TS The TS-algorithm^[TS:1986] has an MCM-method as underlying principle with a tabuisation as suggested by **TS:1986**. This makes a smart sampling of global minima possible. As mentioned a MCM-method is part of the TS so we keep the settings described in the MC part. So we look again at appendix C and skip the MC-part and start at line 489 the first option is at line 495 we do not want to do that so we choose the value 0 and look at line 499 in which the value is said which commands on how many steps got to fail before a new diversification. We choose 10. The key `TSdivers_threshold` in line 503 defines how much steps for the diversification are performed. We choose 30. If the diversification got to be executed too often a termination is required which is defined in line 507. We choose the limit to be 30 and so we write 30 next to `TSdivers_limit`. So with a already setup MC we are ready to start CAST again. Save the `CAST.txt` in a separate folder, add the parameter file and the optimized structure of `AlaGly.xyz`. Remember to apply the actual filename to `CAST.txt`. Now open a command prompt and type

```
cd "C:\PATH\TO\TS"
"C:\PATH\TO\CAST\CAST.exe"
```

to start TS. After a few seconds the calculation is done and looking at the `accepted_final.log` file we see the obtained minima. In this case three minima could be found. one is the initial with -125.525 kcal/mol, one with -130.077 kcal/mol and the global minimum, which was found by MCM, too, with -135.289 kcal/mol. Opening molden again and looking at the picture with -125.525 kcal/mol one sees the interaction with amonium and the carboxylate group. In -130.077 kcal/mol the amide hydrogen and the amide carbonyl oxygen are arranged to benefit from each others interactions. But the hydrogen of the CH and the amide carbonyl oxygen have a dihedral angle of 0° . The global minimum with -135.289 kcal/mol is almost like the local with -130.077 kcal/mol but the dihedral between the CH and the amide carbonyl oxygen has increased to 150° .

NEB NEB is a double ended or chain of states method in which the start and the end position has to be known in order to generate a reaction path. In the appendix C the settings for NEB and pathopt, which is discussed in the next paragraph, start at line 289. The following NEB methods are included in the CAST program: Standard method Henkelman and Jonsson^[JonssonH.1998], improved tangent estimate^[Henkelman2000], climbing image variant^[Henkelman2000a], temperature dependent neb^[Crehuet2003] and image dependent pair potential for improved interpolation^[Smidstrup2014]. In the following the procedure how to do a NEB calculation should be illustrated on the example of the rotation of pentane.

• First steps

The first step is the preparation of the Input structures. They should be presented in Tinker (.arc) or AMBER () like Format (for Tinker structure generation see also chapter 1). For exclusion of translational and rotational degrees of freedom the structures should aligned beforehand. This can be done by using the `TASK ALIGN` in CAST or e.g. VMD for this purpose. It is also important that the ordering of atoms is identical in both structures which are used. The first structure is defined as the standard input structure by using the keyword `name` (-name=input1.arc). The second structure is defined by the keyword `NEB-PATHOPT-FINAL` at line 295. For all methods applying an optimization via the NEB scheme the following keywords have to be assigned:

NEB-PATHOPT-IMAGES *integer value* - defines the total number of interpolated structures which define the band (see line 298)

NEB-PATHOPT-SPRING *floating point value* - defines the strength of the force which couples the structures of the band and is defined in kcal/molÅ² (see line 302)

global variables (see also **task=LOCOPT**):

BFGSgrad - assigns the convergence threshold for the L-BFGS optimizer which defines also the convergence for the NEB optimization (see line 283)

BFGSmaxstep - maximum number of steps carried out in a NEB optimization (see line 283)

- **Standard NEB method**

In NEB the band is defined by $N+1$ structures $\{R_0, R_1, \dots, R_N\}$. The start (R_0) and the final structure (R_N) remain unchanged by the optimization process. They serve as the anchor points of the band. The force which acts on a projected structure is the sum of the perpendicular component with respect to the derivative of the potential energy function $\nabla E(R_i^\perp)$ and the tangential component F_i^\parallel . In this way the force F_i on the projected structure is

$$F_i = F_i^\parallel - \nabla E(R_i^\perp), \quad (9)$$

thereby one can write the resulting force (derived from the potential energy function) as:

$$\nabla E(R_i^\perp) = \nabla E(R_i) - \nabla E(R_i) \cdot \hat{\tau}_i. \quad (10)$$

Within these equations E describes the potential energy of the system which is a function of the atomic coordinates. The normalized tangent vector is denoted by $\hat{\tau}_i$, whereas i stands for the projected structure although the calculation is atom wise defined. The force component along the band (tangential) is the spring force and defined as

$$F_i^\parallel = k (|R_{i+1} - R_i| - |R_i - R_{i-1}|) \hat{\tau}_i, \quad (11)$$

with k the spring constant. The modified force is then used by the optimizer to find the relaxed pathway.

– NEB-PATHOPT-TAU is set to 0 using the standard tangent approach (see line 308).

- **Climbing image and improved tangent estimate**

Various improvements of the standard NEB approach exist. One example is the climbing image (CI) variant which is only a small correction with respect to the standard approach. The information

about the MEP is included as well, as the better convergence to the TS. Within the CI calculation the maximum energy image is calculated within the optimization procedure, whereas the calculation is repeated for each step. This projected structure is then called $i(MAX)$. For this special structure the force acting on it is computed in a modified approach:

$$F_{i(MAX)} = -\nabla E(R_{i(MAX)}) + 2\nabla E(R_{i(MAX)}^{\parallel}). \quad (12)$$

In detail this equation can be written as:

$$F_{i(MAX)} = -\nabla E(R_{i(MAX)}) + 2\nabla E(R_{i(MAX)}) \cdot \hat{\tau}_{i((MAX))} \hat{\tau}_{i((MAX))}. \quad (13)$$

Within the CI variant the maximum energy structure is not influenced by the spring forces during the optimization step.

- NEB-PATHOPT-CI *bool value* - is set to 1 to use the climbing image variant (see line 305).

Within the improved tangent estimate the connecting vectors τ are defined in the following manner:

$$\tau_i = \frac{R_i - R_{i-1}}{|R_i - R_{i-1}|} + \frac{R_{i+1} - R_i}{|R_{i+1} - R_i|}. \quad (14)$$

- NEB-PATHOPT-TAU *bool value* - is set to 1 using the improved tangent approach (see line 308).

- **Temperature dependent NEB (MAXFLUX)**

The temperature dependent NEB method accordingly to Crehuet and Field is based on the maximization of the flux related to the Smoluchowski equation^[Smoluchowski1916]. The method applies a differential equation and is directly inherited within the NEB algorithm. Starting from the Smoluchowski equation, Berkowitz and co-workers^[Berkowitz1983] showed how the flux j of an optimal reaction path P can be expressed

$$j_p = \frac{const}{y \int_p exp(\beta U) ds}, \quad (15)$$

whereas along an ideal pathway (which is assumed to exist) all particles will flow and the friction y is constant for all positions. Hereby U is the potential energy and s the position of the particles along the path. The factor β is equal to $1/k_b T$. One way to optimize the flux is the discretization of the integral, $\int_p exp(\beta U) ds$ given in Equation 15. This can be done using the Euler formalism leading to the function F :

$$F(R_1 \dots R_N) = \sum_{i=0}^{N-1} \frac{1}{2} (e^{\beta U(R_{i+1})} + e^{\beta U(R_i)}) |R_{i-1} - R_i|. \quad (16)$$

Within this equation, R_i is the coordinates vector of the i -th image along the pathways. N is the total number of images/configurations. Starting from the discrete function, also gradients can be derived numerically. Still instabilities may arise during the optimization due to the presence of the exponential terms. Crehuet and Field^[Crehuet2003a] present a different approach to circumvent this issue. They start with the differential equation related to the Euler-Lagrange equation for the above mentioned

integral (see Equation 15). Therefore, one obtains the equation of Berkowitz and co-workers in the following form:

$$\kappa \hat{t} + \hat{n}(\nabla \beta U \cdot \hat{t}) - \nabla \beta U = 0. \quad (17)$$

Within this equation, the gradient along the reaction pathway is defined as $g = \nabla U$ and the curvature of the RP is κ . The tangent and the normal vectors are \hat{t} and \hat{n} . In a next step one can split the gradient into its components along and perpendicular to the band $g = g_{||} + g_{\perp}$. The perpendicular component can be described as follows:

$$g_{\perp} = \frac{\kappa}{\beta} \hat{n}. \quad (18)$$

Using this equation, the transition between steepest descent pathways and finite temperature pathways is obtained. For $T \rightarrow 0K$ the equation is equal to $g_{\perp} = 0$. At infinite temperatures the path is straight, because all existing barriers can be overcome. Also κ must be zero, as $\beta \rightarrow 0$ and g_{\perp} is not allowed to be singular. This new scheme for the perpendicular gradient component can be easily applied to the existing NEB scheme using the projection scheme. The force component which defines the perpendicular acting part of the NEB forces can be redefined,

$$F_i^{\perp} = g_i^{\perp} - \frac{\kappa}{\beta} \hat{n} \quad (19)$$

whereas the force acting on the i-th atom is shown. The curvature of the band is defined by,

$$\kappa_i = \frac{\arccos(\hat{\tau}_{i-1} \cdot \hat{\tau}_{i+1})}{|R_i - R_{i-1}| + |R_{i+1} - R_i|} \quad (20)$$

with τ_i the tangential vector along the band. The temperature dependent calculation is carried out by inclusion of the following flag:

- **NEB-PATHOPT-MAXFLUX** *bool value* - setting the value to 1 enable the temperature dependent calculation (see line 360).

Besides this flag also the temperature values have to be assigned using the specific flag.

- **NEB-PATHOPT-TEMP** *floating point value* - assigns temperature value in K (see line 311).

- **IDPP**

One of the first steps within a NEB calculation is the generation of the initial pathway which is built up by $N - 2$ intermediate projected structures. Normally, this initial band is built up using a linear interpolation between the two starting minimum structures. Within this approach the interpolated structures can be far from being reasonable in terms of the internal coordinates (bonds, angles and dihedrals). Therefore, Smidstrup et al.^[Smidstrup2014] introduced a new method for the calculation of the initial band of projected structures. This method is based on the interpolation of pairwise distances which are calculated for the whole band and additional acting forces which are deduced from these distances. The linearly projected structures (R_i) can be defined via their position vector (r),

whereas each structure is built up by N atoms. By using $i - 2$ projected structures and the *start* and *end* structure, the interpolated distances between atom n and m at structure i are given as

$$\begin{aligned} d_{nm}^i &= d_{nm}^{start} + \frac{i (d_{nm}^{end} - d_{nm}^{start})}{N}, \\ &= \sqrt{\sum_{\sigma} (r_n - r_m)^2} \\ &\quad + \frac{i}{N} \left(\sqrt{\sum_{\sigma} (r_n - r_m)^2}^{end} - \sqrt{\sum_{\sigma} (r_n - r_m)^2}^{start} \right). \end{aligned} \quad (21)$$

For finding the improved pathway the objective function for a projected structure can be defined as follows:

$$\begin{aligned} S_i^{IDPP}(r) &= \sum_n^N \sum_{n>m}^N \omega(d_{nm}) \left(d_{nm}^i - \sqrt{\sum_{\sigma} (r_n - r_m)^2} \right)^2, \\ &= \sum_n^N \sum_{n>m}^N \frac{1}{d_{nm}^4} \left(d_{nm}^i - \sqrt{(x_n - x_m)^2 + (y_n - y_m)^2 + (z_n - z_m)^2} \right)^2, \\ &= \sum_n^N \sum_{n>m}^N \frac{(d_{nm}^i - d_{nm})^2}{d_{nm}^4}, \\ &= \frac{1}{2} \sum_n^N \sum_m^N \frac{(d_{nm}^i - d_{nm})^2}{d_{nm}^4}. \end{aligned} \quad (22)$$

Therefore, the objective function $S_i^{IDPP}(r)$ can be described as the square deviation of the interpolated distances d_{nm}^i with respect to the Euclidean distances d_{nm} . So it acts like the pairwise potential that is related to an effective energy surface. This function is then applied to the NEB method for finding the optimal initial pathway. The function $\omega(d_{nm}) = 1/d_{nm}^4$ is a weight function which takes into account that shorter distances within the overall description stronger contribute. The resulting force acting on atom n in structure i can be assigned to

$$\begin{aligned} F_n^i(r) &= -\nabla_n S_i^{IDPP}, \\ &= - \left(\begin{array}{c} \frac{\partial}{\partial x_n} \\ \frac{\partial}{\partial y_n} \\ \frac{\partial}{\partial z_n} \end{array} \right) \sum_n^N \sum_{n>m}^N \frac{1}{d_{nm}^4} \left(d_{nm}^i - \sqrt{(x_n - x_m)^2 + (y_n - y_m)^2 + (z_n - z_m)^2} \right)^2. \end{aligned} \quad (23)$$

The force on atom n in the projected structure i can be written as the sum of all forces derived from IDPP along the bonds n, m .

- NEB-PATHOPT-IDPP *bool* - de/-activates the image dependent pair potential approach (see line 367).

- **Complete Pathway (NEB) calculations**

Instead of using two starting structures it is possible to use a complete pathway and optimize this pathway within the prescribed NEB methods. The Input structures have to be prepared, as aligned ones.

- NEB-PATHOPT-NEB-COMPLETE *bool* - de/-activates the complete pathway calculation (see line 370).

- **Example: Pentane rotation**

Input structure (input1.arc):

1																			
2	17																		
3	1	C	-6.016091	3.306270	-0.044295	77	2	15	16	17									
4	2	C	-6.778675	2.465777	-1.077584	78	1	3	13	14									
5	3	C	-8.140709	1.957359	-0.577027	78	2	4	6	7									
6	4	C	-8.034142	0.895299	0.529129	78	3	5	11	12									
7	5	C	-9.403430	0.349131	0.949511	77	4	8	9	10									
8	6	H	-8.681389	1.530106	-1.422866	82	3												
9	7	H	-8.742763	2.798324	-0.229801	82	3												
10	8	H	-9.916658	-0.120884	0.110039	82	5												
11	9	H	-10.044670	1.143560	1.332613	82	5												
12	10	H	-9.298851	-0.399878	1.734959	82	5												
13	11	H	-7.538002	1.315575	1.404241	82	4												
14	12	H	-7.408510	0.069934	0.186786	82	4												
15	13	H	-6.939622	3.075131	-1.967939	82	2												
16	14	H	-6.162287	1.624598	-1.397608	82	2												
17	15	H	-6.610481	4.157228	0.289636	82	1												
18	16	H	-5.091402	3.696309	-0.470451	82	1												
19	17	H	-5.747204	2.718713	0.833407	82	1												

Input structure 2 (input2.arc):

1																			
2	17																		
3	1	C	-6.179615	3.774843	-0.656810	77	2	15	16	17									
4	2	C	-6.460412	2.282163	-0.449732	78	1	3	13	14									
5	3	C	-7.882438	2.017213	0.064828	78	2	4	6	7									
6	4	C	-8.162536	0.522049	0.272529	78	3	5	11	12									
7	5	C	-9.581823	0.256642	0.787283	77	4	8	9	10									
8	6	H	-8.606359	2.427775	-0.640663	82	3												
9	7	H	-8.033377	2.549135	1.005388	82	3												
10	8	H	-10.331673	0.623674	0.085798	82	5												
11	9	H	-9.752187	0.745973	1.746782	82	5												
12	10	H	-9.752121	-0.811450	0.925346	82	5												
13	11	H	-7.441250	0.108091	0.978529	82	4												
14	12	H	-8.015375	-0.012835	-0.666770	82	4												
15	13	H	-6.306552	1.753784	-1.391617	82	2												
16	14	H	-5.733473	1.874287	0.253980	82	2												
17	15	H	-6.864957	4.208449	-1.385756	82	1												
18	16	H	-5.164381	3.932621	-1.021933	82	1												
19	17	H	-6.286357	4.330141	0.275567	82	1												

– **standard calculation**

In the standard case a calculation would be carried out by using 10-20 images (NEB-PATHOPT-IMAGES) and using the standard method for estimating the tangents (NEB-PATHOPT-TANGENT). The force constant (NEB-PATHOPT-SPRING) can be set to a value of 1.0 kcal/molÅ² (see line 302) and the climbing image variant can be used (NEB-PATHOPT-CI 1). The optimizer settings can be chosen to be the default values. The most important settings are given:

```

1 name input1.arc
2
3 task NEB
4
5 interface OPLS-AA
6 paramfile          OPLS-AA_mod.prm
7
8 BFGSgrad            0.0001
9 BFGSmaxstep         1000
10
11
12 NEB-PATHOPT-FINAL input1.arc
13 NEB-PATHOPT-IMAGES 20
14 NEB-PATHOPT-SPRING 1.0
15 NEB-PATHOPT-TAU 1

```

After a normal NEB run one should obtain the following files: IMAGES_START.arc, IMAGES_FINAL.arc and ENERGIES_COMPLETE.dat.

– improved calculation

For an improved tangent estimate or temperature dependent calculations the input file has to be modified according to the specifications explained in the related sections.

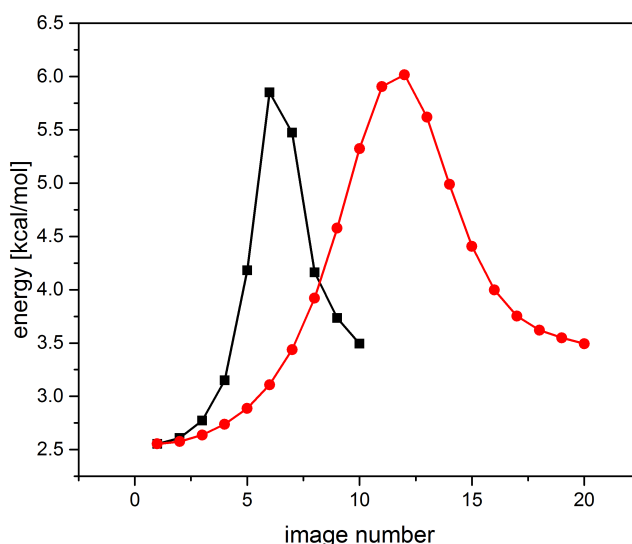


Figure 2: NEB pathway from a optimization carried out for 10/20 structures using the standard tangent-estimate. The OPLS-AA force field parameters were used.

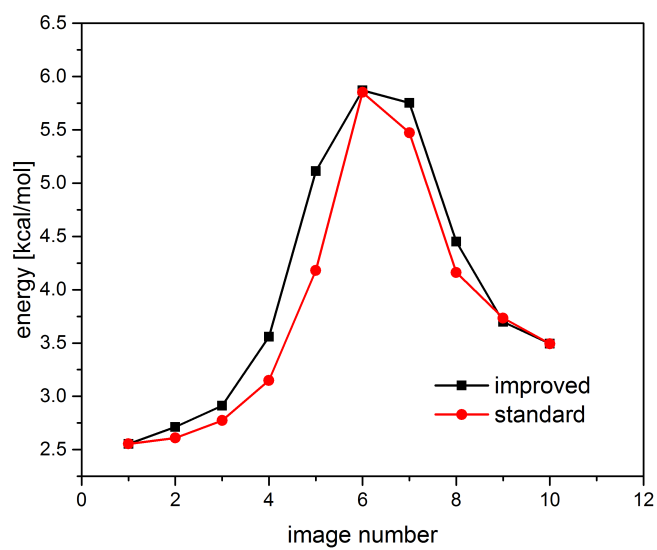


Figure 3: Comparison between pathways obtained for a standard tangent estimate and an improved estimate calculation for the pentane transition.

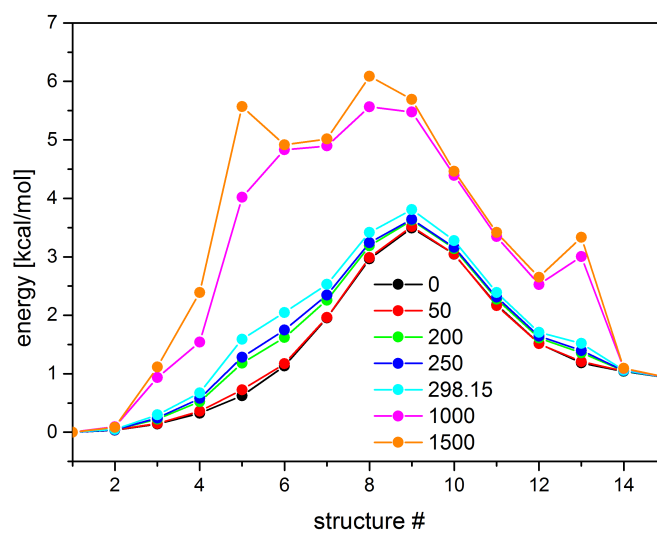


Figure 4: The temperature dependent pathways for the pentane transition are shown.

PATHOPT PO [Grebner2013b, Weber2016] is a newly developed algorithm for finding reaction paths. It is a double-ended method that means, two structures are used. The main idea of the algorithm is, to make an initial guess between the start and final structure. This is performed by using the Nudged Elastic Band (NEB) approach. In a next step, this initial path is divided by perpendicular (n-1) dimensional hyperplanes. Subsequently, we perform global optimization on these hyperplanes. This is done with projected gradients (see figure 5). The resulting minima are traces of possible reaction paths between the start and final structure. The number of planes can be varied and depends on the system, which is investigated. In addition, the connection method for the found traces of pathways can also be chosen. This pathways can be obtained in a direct manner via RMSD criterion or by using additional NEB simulations. The movement within the global optimization scheme can be chosen by using a distortion in Cartesian space or by applying a mixed move strategy (see figure 6) and distorting dihedral angles as well.

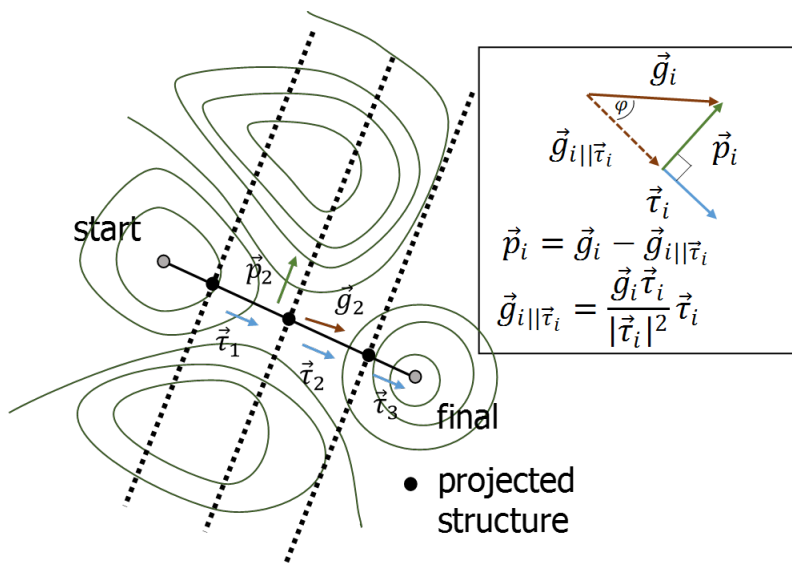


Figure 5: Schematic representation of the Pathopt algorithm

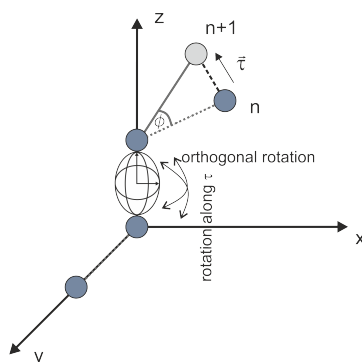


Figure 6: The mixed move strategy is illustrated by rotating only main dihedrals perpendicular to the connecting vectors τ .

PO calculations can be carried out by using various optional configurations. For the MCM procedure within PO the following settings can be varied: Steps, number of total MCM runs, Temperature criterion,

stepsize, acceptance criteria, move-type and optimization settings (standard L-BFGS settings are used e.g. convergence).

- NEB-PATHOPT-ITER *integer* - number of constraint MCM steps (see line 314).
- NEB-PATHOPT-GLOBITER *integer* - number of total MC runs for multiple calculations (see line 317).
- NEB-PATHOPT-TEMP *floating point value* - assigns temperature value in K (see line 311).
- NEB-PATHOPT-STEPSIZE *floating point value* - Cartesian step size in Å (see line 332).
- NEB-PATHOPT-MAXVAR *floating point value* - maximum allowed displacement in Å (see line 332).
- NEB-PATHOPT-ENERGY_RANGE *floating point value* - maximum allowed energy difference with respect to starting structure (see line 332).
- NEB-PATHOPT-MIXMOVE *bool* - de/-activates the dihedral movement approach (see line 335).
- NEB-PATHOPT-MODE *character string* - assigns the gradient calculation scheme: PROJECTED=projected gradients / BIAS=bias potential (needs a bias constant to be set (see line 320)).
- NEB-PATHOPT-BIAS *floating point value* - bias constant in kcal/molÅ² (see line 323).
- NEB-PATHOPT-MF_PATHOPT *bool* - de/-activates the temperature dependent MAXFLUX optimization of PO pathways (uses standard temp. criterion) (see line 363).
- **Example calculation on Tridecaalanine and GlyAla-petide**

In the following the standard parameters for the tridecaalanine calculation are given. The OPLS-AA method is used and for the PATHOPT procedure the standard gradient projection scheme is used.

```

1 name ala1.xyz
2
3 task NEB
4
5 interface OPLS-AA
6 paramfile          OPLS-AA_mod.prm
7
8 BFGSgrad            0.0001
9 BFGSmaxstep         1000
10
11
12 NEB-PATHOPT-FINAL ala2.arc
13 NEB-PATHOPT-IMAGES 22
14 NEB-PATHOPT-SPRING 1.0
15 NEB-PATHOPT-CLIMBING 1
16 NEB-PATHOPT-TAU 1
17 NEB-PATHOPT-TEMP 298.15
18 NEB-PATHOPT-ITER 1000
19 NEB-PATHOPT-GLOBITER 1

```

```

20 NEB-PATHOPT-MODE PROJECTED
21 NEB-PATHOPT-BIASCONSTANT 0.1
22 NEB-PATHOPT-MAXVAR 20.0
23 NEB-PATHOPT-ENERGY_RANGE 20.0
24 NEB-PATHOPT-STEPSize 1.4
25 NEB-PATHOPT-MIXMOVE 1
26 NEB-PATHOPT-NEBCONN 0
27 NEB-PATHOPT-CONSTRAINT_GLOBAL 0

```

Input structure (ala1.arc):

1									
2	133								
3	1	N3	0.000000	-0.000000	0.000000	227	2	5	6
4	2	CT	1.461000	-0.000000	0.000000	233	1	3	8
5	3	C	1.963000	1.449000	-0.000000	174	2	4	13
6	4	O	1.497000	2.242000	-0.816000	175	3		
7	5	H3	-0.415000	0.588000	-0.722000	230	1		
8	6	H3	-0.401000	-0.931000	0.019000	230	1		
9	7	H3	-0.282000	0.410000	0.903000	230	1		
10	8	HC	1.767000	-0.516000	0.907000	82	2		
11	9	CT	1.994000	-0.758000	-1.227000	77	2	10	11
12	10	HC	1.661000	-1.797000	-1.225000	82	9		12
13	11	HC	3.084000	-0.765000	-1.241000	82	9		
14	12	HC	1.658000	-0.300000	-2.158000	82	9		
15	13	N	2.910000	1.851000	0.852000	177	3	14	17
16	14	CT	3.485000	1.181000	2.013000	163	13	15	18
17	15	C	4.172000	2.273000	2.841000	174	14	16	19
18	16	O	4.612000	3.278000	2.275000	175	15		23
19	17	H	3.253000	2.800000	0.770000	180	13		
20	18	HC	2.700000	0.727000	2.619000	82	14		
21	19	CT	4.535000	0.148000	1.565000	77	14	20	21
22	20	HC	4.097000	-0.681000	1.012000	82	19		22
23	21	HC	5.049000	-0.279000	2.428000	82	19		
24	22	HC	5.298000	0.605000	0.933000	82	19		
25	23	N	4.282000	2.066000	4.154000	177	15	24	27
26	24	CT	4.963000	2.945000	5.092000	163	23	25	28
27	25	C	6.085000	2.158000	5.781000	174	24	26	29
28	26	O	6.117000	0.926000	5.742000	175	25		33
29	27	H	3.903000	1.214000	4.560000	180	23		
30	28	HC	5.403000	3.804000	4.581000	82	24		
31	29	CT	3.938000	3.434000	6.129000	77	24	30	31
32	30	HC	3.130000	3.982000	5.644000	82	29		32
33	31	HC	4.393000	4.102000	6.859000	82	29		
34	32	HC	3.489000	2.601000	6.672000	82	29		
35	33	N	6.998000	2.863000	6.459000	177	25	34	37
36	34	CT	8.095000	2.282000	7.235000	163	33	35	38
37	35	C	7.584000	1.800000	8.608000	174	34	36	39
38	36	O	8.047000	2.254000	9.651000	175	35		43
39	37	H	6.906000	3.866000	6.472000	180	33		
40	38	HC	8.496000	1.413000	6.708000	82	34		

41	39	CT	9.222000	3.323000	7.358000	77	34	40	41	42
42	40	HC	9.592000	3.625000	6.378000	82	39			
43	41	HC	10.068000	2.915000	7.913000	82	39			
44	42	HC	8.888000	4.218000	7.886000	82	39			
45	43	N	6.606000	0.890000	8.585000	177	35	44	47	
46	44	CT	5.929000	0.304000	9.735000	163	43	45	48	49
47	45	C	5.080000	-0.881000	9.268000	174	44	46	53	
48	46	O	5.202000	-1.981000	9.798000	175	45			
49	47	H	6.325000	0.563000	7.664000	180	43			
50	48	HC	6.683000	-0.073000	10.429000	82	44			
51	49	CT	5.051000	1.346000	10.456000	77	44	50	51	52
52	50	HC	5.655000	2.145000	10.884000	82	49			
53	51	HC	4.501000	0.886000	11.278000	82	49			
54	52	HC	4.324000	1.801000	9.783000	82	49			
55	53	N	4.211000	-0.652000	8.276000	177	45	54	57	
56	54	CT	3.287000	-1.630000	7.717000	163	53	55	58	59
57	55	C	2.906000	-1.201000	6.294000	174	54	56	63	
58	56	O	3.223000	-0.091000	5.861000	175	55			
59	57	H	4.192000	0.254000	7.828000	180	53			
60	58	HC	3.779000	-2.604000	7.661000	82	54			
61	59	CT	2.035000	-1.720000	8.610000	77	54	60	61	62
62	60	HC	2.297000	-2.028000	9.623000	82	59			
63	61	HC	1.323000	-2.452000	8.227000	82	59			
64	62	HC	1.521000	-0.761000	8.676000	82	59			
65	63	N	2.211000	-2.084000	5.574000	177	55	64	67	
66	64	CT	1.689000	-1.857000	4.237000	163	63	65	68	69
67	65	C	0.317000	-2.528000	4.147000	174	64	66	73	
68	66	O	0.128000	-3.615000	4.694000	175	65			
69	67	H	1.941000	-2.966000	5.989000	180	63			
70	68	HC	1.582000	-0.788000	4.046000	82	64			
71	69	CT	2.653000	-2.493000	3.223000	77	64	70	71	72
72	70	HC	3.644000	-2.045000	3.290000	82	69			
73	71	HC	2.293000	-2.366000	2.203000	82	69			
74	72	HC	2.764000	-3.565000	3.397000	82	69			
75	73	N	-0.615000	-1.886000	3.445000	177	65	74	77	
76	74	CT	-1.936000	-2.384000	3.087000	163	73	75	78	79
77	75	C	-2.108000	-2.295000	1.558000	174	74	76	83	
78	76	O	-1.127000	-2.322000	0.807000	175	75			
79	77	H	-0.370000	-0.953000	3.084000	180	73			
80	78	HC	-2.006000	-3.443000	3.341000	82	74			
81	79	CT	-3.016000	-1.624000	3.882000	77	74	80	81	82
82	80	HC	-2.798000	-1.650000	4.950000	82	79			
83	81	HC	-4.001000	-2.070000	3.749000	82	79			
84	82	HC	-3.079000	-0.578000	3.586000	82	79			
85	83	N	-3.354000	-2.202000	1.081000	177	75	84	87	
86	84	CT	-3.728000	-2.293000	-0.330000	163	83	85	88	89
87	85	C	-4.103000	-0.934000	-0.952000	174	84	86	93	
88	86	O	-4.781000	-0.917000	-1.976000	175	85			
89	87	H	-4.099000	-2.073000	1.747000	180	83			
90	88	HC	-2.900000	-2.689000	-0.921000	82	84			
91	89	CT	-4.897000	-3.290000	-0.433000	77	84	90	91	92

92	90	HC	-4.628000	-4.260000	-0.014000	82	89			
93	91	HC	-5.180000	-3.458000	-1.473000	82	89			
94	92	HC	-5.782000	-2.928000	0.090000	82	89			
95	93	N	-3.674000	0.195000	-0.371000	177	85	94	97	
96	94	CT	-3.900000	1.538000	-0.902000	163	93	95	98	99
97	95	C	-2.551000	2.162000	-1.304000	174	94	96	103	
98	96	O	-1.583000	1.450000	-1.587000	175	95			
99	97	H	-3.105000	0.165000	0.477000	180	93			
100	98	HC	-4.505000	1.502000	-1.810000	82	94			
101	99	CT	-4.666000	2.368000	0.145000	77	94	100	101	102
102	100	HC	-5.575000	1.855000	0.459000	82	99			
103	101	HC	-4.968000	3.339000	-0.247000	82	99			
104	102	HC	-4.059000	2.539000	1.033000	82	99			
105	103	N	-2.481000	3.496000	-1.323000	177	95	104	107	
106	104	CT	-1.267000	4.283000	-1.487000	163	103	105	108	109
107	105	C	-0.922000	4.822000	-0.095000	174	104	106	113	
108	106	O	-1.811000	5.315000	0.600000	175	105			
109	107	H	-3.304000	4.011000	-1.053000	180	103			
110	108	HC	-0.448000	3.676000	-1.874000	82	104			
111	109	CT	-1.547000	5.435000	-2.463000	77	104	110	111	112
112	110	HC	-1.842000	5.057000	-3.442000	82	109			
113	111	HC	-0.657000	6.050000	-2.603000	82	109			
114	112	HC	-2.343000	6.089000	-2.102000	82	109			
115	113	N	0.344000	4.698000	0.321000	177	105	114	117	
116	114	CT	0.915000	5.067000	1.626000	163	113	115	118	119
117	115	C	0.554000	4.059000	2.729000	174	114	116	123	
118	116	O	1.417000	3.679000	3.515000	175	115			
119	117	H	0.964000	4.194000	-0.302000	180	113			
120	118	HC	1.995000	4.986000	1.496000	82	114			
121	119	CT	0.625000	6.522000	2.038000	77	114	120	121	122
122	120	HC	0.916000	7.222000	1.255000	82	119			
123	121	HC	1.185000	6.783000	2.937000	82	119			
124	122	HC	-0.430000	6.685000	2.262000	82	119			
125	123	N	-0.705000	3.613000	2.763000	177	115	124	127	
126	124	CT	-1.175000	2.467000	3.524000	222	123	125	128	129
127	125	C	-1.049000	1.269000	2.583000	210	124	126	133	
128	126	O2	-0.000000	0.593000	2.580000	211	125			
129	127	H	-1.352000	4.033000	2.107000	180	123			
130	128	HC	-0.545000	2.292000	4.399000	82	124			
131	129	CT	-2.622000	2.709000	3.981000	77	124	130	131	132
132	130	HC	-2.679000	3.559000	4.661000	82	129			
133	131	HC	-3.011000	1.838000	4.508000	82	129			
134	132	HC	-3.284000	2.909000	3.140000	82	129			
135	133	O2	-1.948000	0.995000	1.762000	211	125			

Input structure 2 (ala2.arc):

1										
2	133									
3	1	N3	0.364558	0.471283	0.336934	227	2	5	6	7
4	2	CT	1.122582	1.089650	-0.746370	233	1	3	8	9

5	3	C	1.146753	2.607327	-0.523589	174	2	4	13
6	4	O	0.195284	3.286015	-0.892547	175	3		
7	5	H3	-0.551878	0.916236	0.436559	230	1		
8	6	H3	0.248087	-0.532694	0.230849	230	1		
9	7	H3	0.844314	0.603110	1.244630	230	1		
10	8	HC	2.135483	0.693100	-0.722507	82	2		
11	9	CT	0.517872	0.722197	-2.111722	77	2	10	11 12
12	10	HC	-0.523885	1.039957	-2.186698	82	9		
13	11	HC	0.549508	-0.354270	-2.282869	82	9		
14	12	HC	1.065509	1.201189	-2.924284	82	9		
15	13	N	2.178818	3.198847	0.078918	177	3	14	17
16	14	CT	3.360642	2.626253	0.713958	163	13	15	18 19
17	15	C	3.624637	3.422485	1.998460	174	14	16	23
18	16	O	3.042835	4.493614	2.194802	175	15		
19	17	H	2.107424	4.198450	0.213656	180	13		
20	18	HC	3.211407	1.586949	0.987211	82	14		
21	19	CT	4.553856	2.731182	-0.251321	77	14	20	21 22
22	20	HC	4.366982	2.190381	-1.179116	82	19		
23	21	HC	5.456575	2.309133	0.195797	82	19		
24	22	HC	4.775412	3.769312	-0.505135	82	19		
25	23	N	4.519136	2.906682	2.840358	177	15	24	27
26	24	CT	5.087370	3.567480	4.004334	163	23	25	28 29
27	25	C	6.494805	4.049839	3.625106	174	24	26	33
28	26	O	7.030457	3.698424	2.571618	175	25		
29	27	H	4.973399	2.030264	2.593019	180	23		
30	28	HC	4.471251	4.415991	4.308886	82	24		
31	29	CT	5.187810	2.545480	5.151654	77	24	30	31 32
32	30	HC	4.236290	2.046753	5.323468	82	29		
33	31	HC	5.466822	3.031885	6.085630	82	29		
34	32	HC	5.924932	1.769640	4.949651	82	29		
35	33	N	7.138436	4.823954	4.502583	177	25	34	37
36	34	CT	8.502830	5.318054	4.311728	163	33	35	38 39
37	35	C	9.538332	4.250856	4.729180	174	34	36	43
38	36	O	10.441898	4.535352	5.510622	175	35		
39	37	H	6.668968	5.063956	5.361579	180	33		
40	38	HC	8.671517	5.542422	3.256022	82	34		
41	39	CT	8.652719	6.629782	5.102295	77	34	40	41 42
42	40	HC	7.910101	7.364754	4.792393	82	39		
43	41	HC	9.635228	7.073381	4.937232	82	39		
44	42	HC	8.543637	6.469602	6.175397	82	39		
45	43	N	9.395425	3.023613	4.208162	177	35	44	47
46	44	CT	10.244640	1.854708	4.443575	163	43	45	48 49
47	45	C	9.709152	0.648583	3.662193	174	44	46	53
48	46	O	10.418255	0.065462	2.847102	175	45		
49	47	H	8.647085	2.914834	3.529037	180	43		
50	48	HC	11.244686	2.077642	4.067388	82	44		
51	49	CT	10.343337	1.494004	5.943323	77	44	50	51 52
52	50	HC	10.896908	2.246758	6.503313	82	49		
53	51	HC	10.874704	0.551449	6.083693	82	49		
54	52	HC	9.361106	1.392308	6.404749	82	49		
55	53	N	8.456738	0.267755	3.938931	177	45	54	57

56	54	CT	7.780402	-0.917558	3.412811	163	53	55	58	59
57	55	C	6.480516	-0.509419	2.704498	174	54	56	63	
58	56	O	6.164809	0.674931	2.602772	175	55			
59	57	H	7.914744	0.864838	4.541159	180	53			
60	58	HC	8.408601	-1.426403	2.678910	82	54			
61	59	CT	7.497036	-1.874031	4.587200	77	54	60	61	62
62	60	HC	8.417115	-2.125172	5.116006	82	59			
63	61	HC	7.059615	-2.813506	4.246516	82	59			
64	62	HC	6.809230	-1.431906	5.309753	82	59			
65	63	N	5.705359	-1.481334	2.218842	177	55	64	67	
66	64	CT	4.410346	-1.260682	1.593704	163	63	65	68	69
67	65	C	3.494957	-2.433629	1.943255	174	64	66	73	
68	66	O	3.929572	-3.584104	1.895072	175	65			
69	67	H	5.971179	-2.450641	2.333016	180	63			
70	68	HC	3.964351	-0.342119	1.975834	82	64			
71	69	CT	4.599259	-1.159192	0.070395	77	64	70	71	72
72	70	HC	5.204584	-0.291195	-0.192066	82	69			
73	71	HC	3.641606	-1.066086	-0.440318	82	69			
74	72	HC	5.095883	-2.044413	-0.330540	82	69			
75	73	N	2.239053	-2.131947	2.276170	177	65	74	77	
76	74	CT	1.147929	-3.077935	2.478659	163	73	75	78	79
77	75	C	-0.019828	-2.701127	1.547386	174	74	76	83	
78	76	O	0.204484	-2.197456	0.441798	175	75			
79	77	H	2.000773	-1.138366	2.369876	180	73			
80	78	HC	1.468071	-4.074025	2.166706	82	74			
81	79	CT	0.771341	-3.146007	3.971787	77	74	80	81	82
82	80	HC	1.649657	-3.348590	4.584754	82	79			
83	81	HC	0.057678	-3.946006	4.168827	82	79			
84	82	HC	0.332423	-2.213599	4.323866	82	79			
85	83	N	-1.263229	-2.950015	1.971071	177	75	84	87	
86	84	CT	-2.473146	-2.867312	1.152417	163	83	85	88	89
87	85	C	-3.304358	-1.588192	1.371095	174	84	86	93	
88	86	O	-4.413471	-1.511518	0.848514	175	85			
89	87	H	-1.374335	-3.241278	2.929597	180	83			
90	88	HC	-2.209490	-2.886553	0.092862	82	84			
91	89	CT	-3.320446	-4.118431	1.447917	77	84	90	91	92
92	90	HC	-2.760216	-5.031725	1.245898	82	89			
93	91	HC	-4.214431	-4.145521	0.822299	82	89			
94	92	HC	-3.649694	-4.145640	2.487668	82	89			
95	93	N	-2.807654	-0.592545	2.115630	177	85	94	97	
96	94	CT	-3.489448	0.673989	2.378454	163	93	95	98	99
97	95	C	-2.716813	1.817295	1.697869	174	94	96	103	
98	96	O	-1.977067	1.598757	0.736396	175	95			
99	97	H	-1.861679	-0.651159	2.503034	180	93			
100	98	HC	-4.496007	0.675019	1.955690	82	94			
101	99	CT	-3.606547	0.866181	3.904455	77	94	100	101	102
102	100	HC	-4.076518	0.000539	4.371517	82	99			
103	101	HC	-4.213848	1.735413	4.159394	82	99			
104	102	HC	-2.625540	1.000019	4.363578	82	99			
105	103	N	-2.872020	3.037369	2.212580	177	95	104	107	
106	104	CT	-2.040404	4.204959	1.961449	163	103	105	108	109

107	105	C	-1.420102	4.527654	3.326096	174	104	106	113
108	106	O	-2.109778	4.406381	4.337814	175	105		
109	107	H	-3.503535	3.138145	2.995083	180	103		
110	108	HC	-1.257001	3.990102	1.233080	82	104		
111	109	CT	-2.927789	5.352463	1.461079	77	104	110	111 112
112	110	HC	-3.422729	5.081486	0.527936	82	109		
113	111	HC	-2.337436	6.248877	1.270187	82	109		
114	112	HC	-3.699764	5.611467	2.186989	82	109		
115	113	N	-0.127719	4.879004	3.360365	177	105	114	117
116	114	CT	0.736446	5.025222	4.545331	163	113	115	118 119
117	115	C	1.286007	3.676335	5.043901	174	114	116	123
118	116	O	2.289860	3.652879	5.751564	175	115		
119	117	H	0.353827	4.976612	2.478811	180	113		
120	118	HC	1.606845	5.579677	4.192718	82	114		
121	119	CT	0.116651	5.853197	5.688308	77	114	120	121 122
122	120	HC	-0.309309	6.786982	5.322712	82	119		
123	121	HC	0.877475	6.103701	6.428798	82	119		
124	122	HC	-0.664217	5.303137	6.214447	82	119		
125	123	N	0.637609	2.569695	4.667622	177	115	124	127
126	124	CT	1.085960	1.196638	4.798430	222	123	125	128 129
127	125	C	0.800266	0.557306	3.440574	210	124	126	133
128	126	O2	1.682175	0.555939	2.556020	211	125		
129	127	H	-0.223874	2.692482	4.159419	180	123		
130	128	HC	2.160370	1.156144	4.976397	82	124		
131	129	CT	0.341473	0.507421	5.953095	77	124	130	131 132
132	130	HC	0.536811	1.014794	6.897783	82	129		
133	131	HC	0.670773	-0.525842	6.060726	82	129		
134	132	HC	-0.736624	0.498476	5.793444	82	129		
135	133	O2	-0.322015	0.078066	3.186905	211	125		

After a successful PO calculation one should obtain the following files and folders: PATHOPT_BASIN_ENERGIES_ PATHOPT_STRUCTURES_X_Y.arc, arrhenius_global.dat and folders 1-3. X and Y stand for the global run and concerning hyperplane.

- PATHOPT_BASIN_ENERGIES - contains the energies of the accepted structures with mcstep number, hyperplane number and energy in kcal/mol.
- PATHOPT_STRUCTURES - contains the structures found on each hyperplane in TINKER format.
- FOLDERS 1-3 - the connected pathways sorted as energy and structure files, whereas folder 1 contains next minimum RMSD moves along the hyperplanes and further on by increasing order.
- arrhenius_global.dat - the arrhenius rates are given, but without any preexponential factor included.

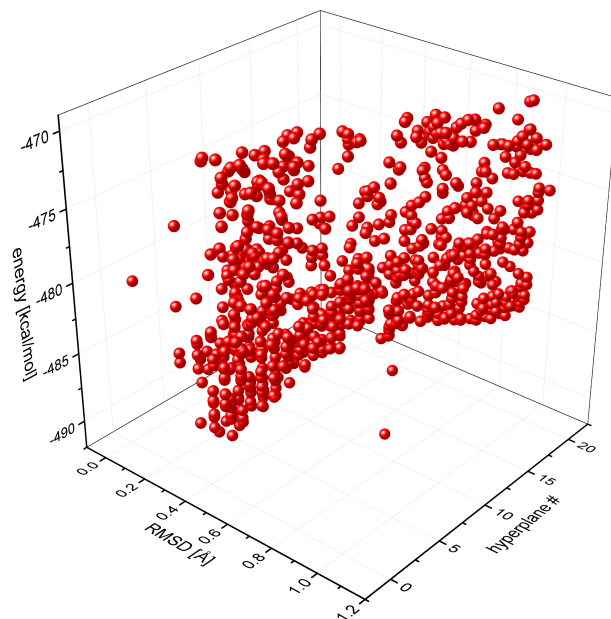


Figure 7: Distribution of found minima along the hyperplanes. The RMSD values are referenced to frame 0 on hyperplane 1.

The next example is the alanine-glycine dipeptide molecule. For the dipeptide two structures (given in the Appendix) should be connected via NEB or PO which are a little problematic. Within the FF description and the NEB method no reasonable pathway is found due to convergence failures which stem from the energy description. The initial and the final structure possess zwitterionic character and the linear transition from one to another structure leads to configurations which are not favorable within the zwitterionic FF description. One way to circumvent this failure is to use a QM description. A different way would be to carry out a PO optimization.

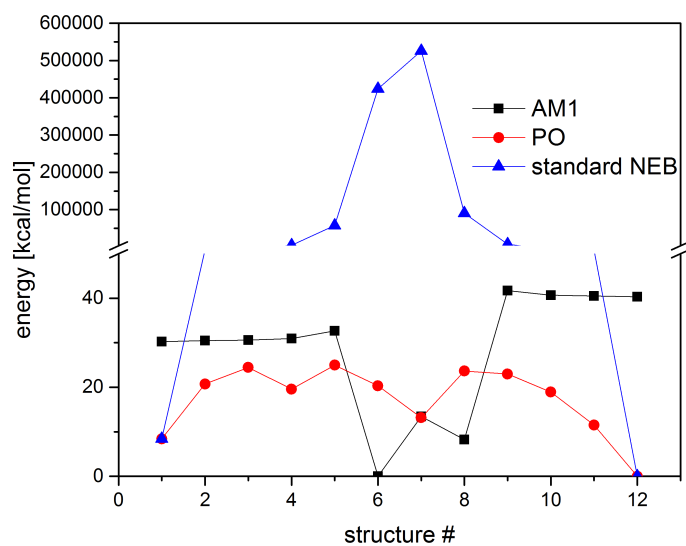


Figure 8: The figure shows the not converged NEB pathway (blue) which is obtained by using standard parameters and the OPLS-AA FF description. In red, one of the PO pathways (OPLS-AA) is depicted and in black the NEB pathway by using the AM1 energy description.

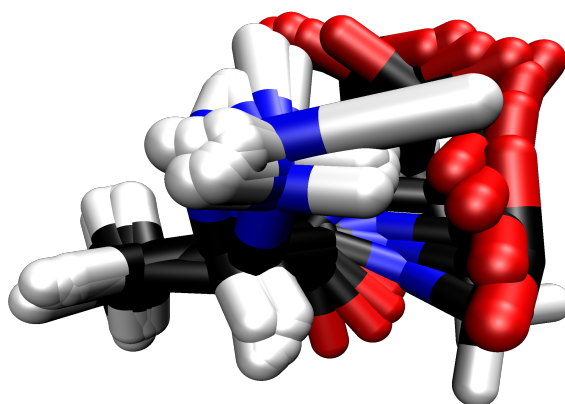


Figure 9: The structures which form the AM1 NEB pathway are given.

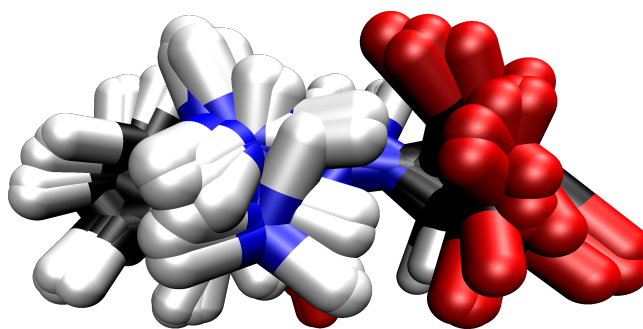


Figure 10: The structures which form the PO pathway built upon the OPLS-AA description are given.

In this case it was possible to create a different pathway by varying the energy description and in addition PO shows the capability to find pathways around the initial linear pathway within the same FF description. In figure 8 the AM1 pathway structures show that the abstraction of the proton from the ammonium group (positively charged) and attach it to the carboxylate (negatively charged) is more stable along the linear pathway.

Abbreviations

Å Angström

CAST Conformational Analysis and Search Tool

e. g. exempli gratia

MC Monte Carlo

MCM Monte Carlo with minimization

MD Molecular Dynamic

NEB Nudged Elastic Band

PO PATHOPT

SP Single Point

TS Tabu Search

A. AlaGly.xyz

1			20						
2	1	N3	-0.679000	1.176000	-0.480000	230	2	12	6 13
3	2	CT	0.000000	-0.000000	0.000000	774	1	3	7 8
4	3	C	-0.684000	-1.184000	-0.483000	177	2	5	4
5	4	N	-2.062000	-1.412000	-0.135000	180	14	3	18
6	5	O	-0.267000	-2.292000	-0.189000	178	3		
7	6	H3	-1.629001	1.176004	-0.144002	233	1		
8	7	CH	0.000000	0.000000	1.450000	80	2	9	10 11
9	8	HC	1.027000	0.000000	-0.363000	892	2		
10	9	HC	-1.027000	0.000000	1.813000	85	7		
11	10	HC	0.513000	-0.889000	1.813000	85	7		
12	11	HC	0.513000	0.889000	1.813000	85	7		
13	12	H3	-0.679000	1.176000	-1.488000	233	1		
14	13	H3	-0.203783	1.999027	-0.144054	233	1		
15	14	C	-2.510000	-2.644000	-0.731000	186	4	15	19 20
16	15	C	-2.384000	-2.557000	-2.173000	213	14	17	16
17	16	O2	-1.885000	-1.390000	-2.763000	214	15		
18	17	O2	-2.712000	-3.502000	-2.872000	214	15		
19	18	H	-2.150000	-1.472000	0.867000	183	4		
20	19	HC	-3.553000	-2.816000	-0.468000	741	14		
21	20	HC	-1.902000	-3.468000	-0.362000	741	14		

B. AlaGly_final_LOCOPT.arc

1			20						
2	1	N3	-0.716463	0.459942	-0.932396	230	2	6	12 13
3	2	CT	0.014710	-0.225311	0.153634	774	1	3	7 8
4	3	C	-0.226806	-1.731938	0.013408	177	2	4	5
5	4	N	-1.484582	-2.148443	0.200041	180	3	14	18
6	5	O	0.667603	-2.452458	-0.411433	178	3		
7	6	H3	-0.585983	1.450174	-1.006646	233	1		
8	7	CH	-0.392379	0.309041	1.539094	80	2	9	10 11
9	8	HC	1.082733	-0.056052	0.005354	892	2		
10	9	HC	-1.467155	0.226887	1.710368	85	7		
11	10	HC	0.109266	-0.246858	2.333236	85	7		
12	11	HC	-0.118419	1.357731	1.656718	85	7		
13	12	H3	-1.723112	0.228853	-0.862306	233	1		
14	13	H3	-0.533031	-0.013551	-1.815384	233	1		
15	14	C	-2.225781	-2.763760	-0.896804	186	4	15	19 20
16	15	C	-2.703848	-1.535683	-1.677994	213	14	16	17
17	16	O2	-3.158228	-0.607857	-0.961833	214	15		
18	17	O2	-2.018062	-1.231682	-2.673249	214	15		
19	18	H	-2.114284	-1.484003	0.632037	183	4		
20	19	HC	-3.077660	-3.334666	-0.528435	741	14		
21	20	HC	-1.602043	-3.410428	-1.516725	741	14		

C. CAST.txt

```
1 #####
2 #
3 #
4 # CAST CONFIGFILE #
5 #
6 #
7 #####
8
9 # Verbosity
10 # Amount of output information from CAST [0-5] (do not use verbosity > 4 :-)
11
12 verbosity 4
13
14 # Cores
15 # Number of OpenMP Threads (if compiled with openmp support)
16
17 cores 4
18
19
20 #####
21 #
22 #
23 # I/O: FILES & TYPES #
24 #
25 #
26 #####
27
28 # Input file name
29
30 name AlaGly.xyz
31
32 # Output file name
33
34 outname AlaGly_final
35
36 # Input file type
37
38 inputtype TINKER
39
40 ### AMBER I/O OPTIONS
41
42 #amber_mdcrd min.rst
43 #amber_mdvel
44 #amber_inpcrd
45 #amber_restrt
46 #amber_trajectory_at_constant_pressure
47
48
49
```

```

50 #####
51 #                                     #
52 #          PROGRAM TASK              #
53 #                                     #
54 #####
55
56 # SP                               Single point energyg calculation
57 # GRAD                             Single point energy calculation
58 # LOCOPT                           Local optimization using Lib-LBFGS
59 # MD                               Molecular dynamics simulation
60 # GOSOL                             Combined Solvation + Global Optimization
61 # MC                               Monte Carlo
62 # CENTER                           Center of mass/geometry
63 # TS                               Tabu Search (CAST: GOTS)
64 # RMSD                             Root mean square deviation
65 # DIMER                             Dimer method using torsional space
66 # NEB                               Nudged elastic band calculation
67 # INTERNAL                         Create Z-Matrix
68 # STARTOPT
69 # UMBRELLA                         Umbrella Sampling
70 # PROFILE                         Repeated Gradient Calculation of first input structure
71 # FEP                             Alchemical transformations using FEP
72 # ALIGN                           Trajectory Alignment (Kabsch algorithm)
73 # PCAgen                          Principal Component Analysis
74 # PCAproc
75 # ENTROPY                         Configurational and Conformational Entropy Calculations
76 # GRID                             Grid Search
77 # PATHOPT                         Global reaction path search by constraint optimization on n-1 dim.
78 #                                hyperplane(s)
79 # ADJUST
80 # GRID
81 # PATHSAMPLING
82 # REMOVE_EXPLICIT_WATER
83
84 task                                LOCOPT
85
86
87 #####
88 #                                     #
89 #          ENERGY INTERFACES        #
90 #                                     #
91 #####
92
93 # AMBER                            AMBER force field
94 # (AMOEBA)                         AMOEBA03 force field
95 # CHARMM22                         CHARMM22 force field
96 # OPLS-AA                          OPLS all atoms force field
97 # TERACHEM                         Terachem MPI Interface
98 # (TINKER)                         Tinker syscall interface
99 # MOPAC                            MOAPC2012 syscall Interface
100

```

```

101 interface                OPLS-AA
102
103 # Interface for preoptimizations
104
105 preinterface              0
106
107 # PARAMETER FILE FOR forcefield
108 # paramfile                amber.prm, amoeba.prm, OPLS-AA.prm, charmm22.prm
109
110 paramfile                  OPLS-AA.prm
111
112 # Keywords for MOPAC Call
113
114 MOPACkey                   PM7
115
116 # Delete temporary MOPAC comm files?
117
118 MOPACdelete                1
119
120 #MOPAC executable path
121
122 MOPACpath                   "C:\Program Files\mopac\MOPAC2012.exe "
123
124 #MOPACversion
125
126 # Short-range electrostatics correction 0/1 activate interpolative energies/gradients (0/1) and cutoff
127
128 Spackman 1 1 10.0
129
130 #####
131 #                               #
132 #          CUTOFF RADIUS       #
133 #                               #
134 #####
135
136 cutoff                      400.0
137 switchdist                  10.0
138
139
140 #####
141 #                               #
142 #          ATOM FIXATIONS      #
143 #                               #
144 #####
145
146 # Exclude nonbondeds between two fixed atoms in internal force fields
147
148 FIXexclude                  0
149
150 # Remove rotations of hydrogens from main torsional angles
151

```

```

152 REMOVEHROT          0
153
154 # Fix a range of atoms
155 #FIXrange             <start index> <end index>
156
157 #FIXrange             1 213
158
159 # Fixation of single atoms
160 #ATOMFIX              <INDEX>
161
162 #ATOMFIX              1
163 #ATOMFIX              3
164
165
166 #####
167 #                      #
168 #          Boundary Bias      #
169 #                      #
170 #####
171
172 # Quadratic Dihedral Bias Potential
173 #BIASspherical         <radius> <force> <exponent>
174 #BIAScubic             <x> <y> <z> <force> <exponent>
175
176 #BIASspherical  25.0 1.0 2.0
177 #BIAScubic  40.0 40.0 40.0 1.0 2.0
178
179
180 #####
181 #                      #
182 #          DIHEDRAL FIXATIONS      #
183 #                      #
184 #####
185
186 # Quadratic Dihedral Bias Potential (quadratic in degrees)
187
188 #BIASdih              <atom 1> <atom 2> <atom 3> <atom 4> <angle> <force> <all atoms>
189
190 #BIASdih              1 2 3 5 0.0 10.0 1
191 #BIASdih              2 5 6 9 150.0 5.0 1
192 #BIASdih              1 2 5 6 150.0 5.0 1
193 #BIASdih              1 2 5 6 95.0 10.0 1
194
195 #BIASdih              1 2 5 6 60.0 0.01
196
197 #BIASdih              1 2 5 6 30.0 1.0 1
198
199
200
201 #####
202 #                      #

```

```

203 #                MAINlists                #
204 #                #
205 #####
206
207 # Black- or Whitelist a rotation around a bond
208 # for the selection as main rotation
209
210 #MAINblacklist 2 5
211
212 #MAINwhitelist 2 5
213
214
215 #####
216 #                #
217 #      Periodic Boundaries                #
218 #                #
219 #####
220
221 #Periodics          <Active 1(on)/0(off)> <box-x> <box-y> <box-z>
222 #Periodics          0 70.0 70.0 70.0
223
224 # Print periodic boundary dummy atoms to output?
225 #Periodicp          <Active 1(on)/0(off)>
226
227 #Periodicp          0
228
229
230 #####
231 #                #
232 #      INTERACTION OPTIONS                #
233 #                #
234 #####
235
236 # The interaction of substructures that are not bound to each other can be calculated
237 # IAlimits <Start Index Substructure> <End Index Substructure>
238
239 #IAlimits            1 122
240
241
242
243 #####
244 #                #
245 #      Implicit Solvation                #
246 #                #
247 #####
248
249 # solvmethod : VAC          (default) Vacuum
250 #                ONION      Numerical Still method
251 #                STILL       Analytical Still method
252 #                HCT         HCT method
253 #                OBC         OBC method

```

```

254 #          GRYPK      Grycuk's method
255 #          ACE        ACE method
256 # surface    : TINKER  (default) TINKER's accessible surface area calculation
257 #          SASASTILL  Still's surface area calculation
258 #          GAUSS      SASA according to the global theorem of Gauss-Bonnet
259 #
260 # ONION should only be combined with GAUSS
261
262 solvmethod          VAC
263 surface             TINKER
264
265
266 #####
267 #                                     #
268 #          PROFILE RUNS             #
269 #                                     #
270 #####
271
272 # Number of repeated gradient calculations for PROFILE task
273
274 profileruns          10
275
276
277 #####
278 #                                     #
279 #          libLBFGS OPTIONS          #
280 #                                     #
281 #####
282
283 BFGSgrad              0.0001
284 BFGSmaxstep           5000
285
286
287 #####
288 #
289 #          NEB &
290 #                                     PATHOPT OPTIONS          #
291 #
292 #
293 #####
294 # Second structure for double-ended search
295 NEB-PATHOPT-FINAL input.xyz
296
297 # Number of NEB images
298 NEB-PATHOPT-IMAGES 12
299
300 # Force constant in kcal/molA^2 for NEB calculation defining the force component along the
301 # connecting band
302 NEB-PATHOPT-SPRING 1.0

```



```

303
304 # Climbing image in NEB 0/1 (off/on)
305 NEB-PATHOPT-CLIMBING 1
306
307 # Standard tau or improved tau method in NEB 0/1 (standard/improved)
308 NEB-PATHOPT-TAU 1
309
310 # Definition of the Temperature settings for the Monte Carlo run
311 NEB-PATHOPT-TEMP 298.15
312
313 # MCM iterations in Pathopt
314 NEB-PATHOPT-ITER 60
315
316 # Number of multiple MCM simulations
317 NEB-PATHOPT-GLOBITER 1
318
319 # Optimization mode BIAS/GRADIENT Projection
320 NEB-PATHOPT-MODE PROJECTED
321
322 # Bias constant (Pathopt)
323 NEB-PATHOPT-BIASCONSTANT 0.1
324
325 # Maximum displacement in Angstrom for accepted coordinates in MCM
326 NEB-PATHOPT-MAXVAR 3.0
327
328 # Maximum energy range in kcal/mol for MCM in Pathopt
329 NEB-PATHOPT-ENERGY_RANGE 20.0
330
331 # MCM stepsize in Angstrom
332 NEB-PATHOPT-STEPSIZE 1.4
333
334 # Move strategy by applying dihedral changes at several steps of MCM 0/1 (off/on)
335 NEB-PATHOPT-MIXMOVE 0
336
337 # Using NEB connection within Pathopt 0/1 (off/on)
338 NEB-PATHOPT-NEBCONN 0
339
340 # Number of NEB images within Pathopt-NEB connection procedure
341 NEB-PATHOPT-NEBCONN_NUMBER 12
342
343 # Constraint global optimization (MCM standard) by fixation of
344 # dihedrals which change the most during NEB
345 NEB-PATHOPT-CONSTRAINT_GLOBAL 0
346
347 # Number of dihedrals within constraint global optimization
348 # (MCM standard) which should be fixed along the NEB path
349 NEB-PATHOPT-CONSTRAINT_NUMBER_DIHEDRALS 1
350
351 # Interpolation via spline method between the linear constructed NEB pathway
352 # by locally optimizing with perpendicular force projection 0/1 (off/on)
353 NEB-PATHOPT-INT_PATH 0

```

```

354
355 #step size of interpolated images via spline interpolation approach
356 NEB-PATHOPT-INT_IT 0.5
357
358 # choose if the MaxFlux method is used to simulate a NEB method with temperature dependencies
359 # (0/1 no/yes)
360 NEB-PATHOPT-MAXFLUX 1
361
362 # determine if a neb calculation is performed for every found path in PATHOPT (0/1: no/yes)
363 NEB-PATHOPT-MF_PATHOPT 1
364
365 # image dependent pair potential approach for generation of initial pathway in NEB optimization
366 # (0/1: no/yes)
367 NEB-PATHOPT-NEB-IDPP 1
368
369 # complete pathway NEB calculation (0/1: no/yes)
370 NEB-PATHOPT-NEB-COMPLETE 1
371
372 #####
373 #
374 #          SIMULATION OPTIONS          #
375 #          (MC, TS)                    #
376 #                                     #
377 #####
378
379 # Simulation Temperature
380 # for TS and MC important for Metropolis Criterion
381
382 Temperature          298.15
383
384 # Number of iterations in global optimization routine
385
386 Iterations           2000
387
388
389 #####
390 #
391 #          GLOBOPTIONS                 #
392 #          (MC, TS)                    #
393 #                                     #
394 #####
395
396 # Save all (minimized) structures
397 # which are within "Erangle" kcal/mol from the final global minimum
398 # default = 0.0
399
400 GOorange              10.0
401
402 # use the current local minimum energy for metropolis criterion?
403 # default = 0
404

```

```

405 GOfmetrolocal          0
406
407 # startopt before starting simulation/optimization?
408 # default = 0
409
410 GOfstartopt            0
411
412 # Temperature Scaling Factor applied to the Temperature,
413 # once a new minimum is found during GlobOpt
414 # default = 1.0
415
416 Tempscale              1.0
417
418 # Precision of values printed
419
420 GOfprecision           6
421
422 # Fallback type
423 #
424 # LAST_GLOBAL (default) = fall back to last minimum and then to global minimum if stuck
425 # EVOLUTION = select new minimum via evolutionary algorithm if stuck
426
427 GOfallback             LAST_GLOBAL
428
429 # Maximum number of tries from one structure before it is set
430 # tabu as a starting point
431 # default = 20
432
433 GOfallback_limit       500
434
435 # Fitness function type for evolutionary fallback
436 #
437 # LINEAR (default) = linear ranking
438 # EXPONENTIAL = exponential ranking
439
440 GOfallback_fr_fit      EXPONENTIAL
441
442 # Number of minima included in the ranking for evolutionary fallback
443 # default = 10
444
445 GOfallback_fr_minima   10
446
447 # Lower and upper bounardy for fitness value
448 # rank 1 is assign second value, rank X
449 # (determined via GOfincluded_minima) is assigned the first value
450 # default = 0.5 1.0
451
452 GOfallback_fr_bounds   0.5 1.0
453
454
455 #####

```

```

456 | #                                     #
457 | #             GRID OPTIONS          #
458 | #                                     #
459 | #####
460 |
461 | GMain_grid           60.0
462 |
463 |
464 | #####
465 | #                                     #
466 | #             MCM OPTIONS          #
467 | #                                     #
468 | #####
469 |
470 | # Step size in cartesian space
471 |
472 | MCstep_size          1.4
473 |
474 | # Use minimization
475 |
476 | MCminimization        1
477 |
478 | # Use dihedral (1), cartesian (2) or biased dihedral (0) randomization
479 |
480 | MCmovetype            1
481 |
482 | # Maximum dihedral deviation
483 |
484 | MCmax_dihedral        30.0
485 |
486 |
487 | #####
488 | #                                     #
489 | #             TS OPTIONS          #
490 | #                                     #
491 | #####
492 |
493 | # Do diversification before first TS steps?
494 |
495 | TSmc_first            0
496 |
497 | # How many TS steps need to fail in finding new minimum before diversification?
498 |
499 | TSdivers_threshold     10
500 |
501 | # How many diversification steps are applied?
502 |
503 | TSdivers_iter          30
504 |
505 | # How often will diversification be applied before termination?
506 |

```

```

507 TSdivers_limit          20
508
509
510 #####
511 #                          #
512 #          STARTOPT OPTIONS      #
513 #                          #
514 #####
515
516 # startopt type
517 # 0          Ringsearch
518 # 1          Solvadd [default]
519 # 2          Ringsearch + Solvadd
520
521 Sotype          1
522
523 # startopt structure count
524 # number of structures generated by startopt routines
525
526 SOstructures          10
527
528
529 #####
530 #                          #
531 #          RINGSEARCH OPTIONS      #
532 #                          #
533 #####
534
535 # Force, applied to close rings
536 # (multiplied with quadratic in degrees of dihedral deviation)
537
538 RSbias_force          10.0
539
540 # Chance to close a ring in the initial random population generation
541
542 RSchance_close          0.33
543
544 # Number of individuals in the ringsearch evolution
545
546 RSpopulation          10
547
548 # Number of propagated generations during ringsearch evolution
549
550 RSgenerations          10
551
552
553 #####
554 #                          #
555 #          SOLVADD OPTIONS      #
556 #                          #
557 #####

```

```

558
559 # Hydrogen bond length parameter [default: 1.8]
560
561 SAhb                1.8
562
563 # number of desired water molecules [default: 0(=no limit)]
564
565 SAlimit             20
566
567 # water boundary type
568 #
569 # 0    layer [default]
570 # 1    sphere
571 # 2    box
572
573 SAboundary          0
574
575 # water boundary extent [default: 10.0] and push length (elongation of radius if limit is
576 # not reached)
577
578 SARadius            10.0
579
580 # force field parameter types of oxygen and hydrogen
581 #
582 # 53 54    OPLS-AA
583 # 101 88   CHARMM
584 # 2001 2002 AMBER
585
586 SAtypes              53 54
587
588 # Intermediate optimizations
589 #
590 # 0    none
591 # 1    each "shell"
592 # 2    all waters
593 # 3    1+2
594
595 SAopt               0
596
597 # fix initial structure
598
599 SAfixinit           1
600
601
602
603
604 #####
605 #
606 #          MD OPTIONS
607 #
608 #####

```

```

609
610 # Number of Steps
611
612 MDsteps                50000
613
614 # Integrator
615 #
616 # 0                      Velocity-Verlet
617 # 1                      Beeman
618
619 MDintegrator            0
620
621 # Velocity Scaling
622
623 MDveloscale             1
624
625 # Thermostat (Nose-Hoover)
626
627 MDthermostat            1
628
629 # Timestep in picoseconds
630
631 MDtimestep              0.001
632
633 # start MD again from beginning if molecule gets destroyed
634
635 MDrestart_if_broken     0
636
637 # Activate Tracking (Log and Snapshots)
638
639 MDtrack                 1
640
641 #MDtrackoffset          0
642
643 #
644 #   Snapshots
645 #
646
647 # Number
648 MDsnap                  1000
649 # Buffer size
650 MDsnap_buffer           100
651 # Optimize snapshots
652 MDsnap_opt              0
653
654 # Heating process control
655 #
656 # MDheat                 <step> <temperature at that step>
657
658 MDheat                  0 298.15
659 MDheat                  10000 348.15

```

```

660 MDheat                20000  398.15
661 MDheat                30000  448.15
662 MDheat                40000  498.15
663
664 # Pressure control
665
666 #MDpress                0
667
668 #MDpcompress
669 #MDpdelay
670 #MDptarget
671
672 # Spherical boundaries' options
673 #
674 # MDspherical           <Active 0/1> <Radius 1> <Radius 2> <Force 1> <Force 2> <Exp 1> <Exp 2>
675
676 #MDspherical           0 34.0 34.1 10.0 10.0 2.0 4.0
677
678 # H bond constraints
679 #
680 # 0                      No Constraints
681 # 1                      All Hydrogend Bonds
682 # 2                      Specific Hydrogen Bonds
683
684 MDrattle                0
685
686 #MDrattpar
687
688 # Rattle bond specification
689 #
690 # MDrattlebond          <H index>
691
692 #MDrattlebond           7 12
693
694 #apply a biased potential
695 #MDbiased potential     <0/1>
696
697 MDbiased_potential      0
698
699 #atom number(s) of active site <every atom a new line>
700 #MDactive_site          1
701
702 #cutoff around active site <inner/outer>
703 #MDcutoff               1 2
704
705 #adjust active center + distances with every step
706 #MDadjust_by_step      <0/1>
707
708 MDadjust_by_step        1
709
710 # Iteration offset for restart files

```



```

711
712 MDrestart_offset      10000
713
714 # Resume simulation from restart file?
715
716 MDresume               0
717
718 #MDpre_optimize
719
720
721 #####
722 #                               #
723 #           FEP OPTIONS        #
724 #                               #
725 #####
726
727 FEPlambda      1.0
728 FEPdlambda     0.05
729 FEPvdwcouple   1.0
730 FEPeccouple    0.5
731 FEPvshift      0.1
732 FEPcshift      2.0
733 FEPequil       100
734 FEPsteps       500
735 FEPfreq        1000
736
737
738 #####
739 #                               #
740 #           PATH OPTIONS        #
741 #                               #
742 #####
743
744 # File containing the desired path end
745
746 PRendfile      PATHREL_END.xyz
747
748 # Maximum Energy distance within the path
749
750 PRdeltae       0.5
751
752 # Maximum structure distance with the path
753
754 PRdeltax       0.5
755
756
757 #####
758 #                               #
759 #           DIMER OPTIONS        #
760 #                               #
761 #####

```

```

762 #
763 # Distance between dimer start end endpoint
764
765 DIMERdistance          0.001
766
767 # Maximum absolute of rotational force during dimer translation
768
769 DIMERtflimit           0.01
770
771 # Convergence criterion for the dimer rotation
772
773 DIMERrotconvergence    5.0
774
775 # Maximum number of rotation and translation iterations
776
777 DIMERmaxit             50 250
778
779
780
781 #####
782 #                               #
783 #          UMBRELLA SAMPLING    #
784 #                               #
785 #####
786
787
788 USsteps                 60
789
790 # definition of strained torsion
791
792 #USTorsion              <index 1> <index 2> <index 3> <index 4> <force> <phi0>
793 #                      <flat bottom 0/1> <width>
794 #[int] 1-4              atom indices
795 #[float] force          potential force constant
796 #[float] phi0           start angle
797 #[float] phi1           ending angle
798 #[int] steps            number of sampling steps
799 #[bool/int]            switch to activate fixation of all torsions around the specified
800
801 #USTorsion              1 2 5 6 100.0 180.0 120.0 1
802
803 # definition of strained bond
804
805 #USBond                 <index 1> <index 2> <force> <r0> <flat bottom 0/1> <width>
806 #USBond                 1 2 155.0 1.09 1 0.2
807
808 # Offset for taking snapshots
809
810 USSnap                  5
811
812

```

```

813 #####
814 #                                     #
815 #             ADJUST                 #
816 #                                     #
817 #####
818
819
820 #ADJUSTdih 1 2 3 4 180.0
821 #ADJUSTdih 2 3 4 5 180.0
822
823
824 #####
825 #                                     #
826 #   TRAJECTORY ALIGNMENT OPTIONS   #
827 #                                     #
828 #####
829
830 # Should alignment be performed?
831 traj_align_bool                true
832 # Should distance measures be calculated and printed?
833 traj_print_bool                false
834
835
836 # Should we align to an external reference structure? If yes, give file name
837 align_external_file            reference.xyz
838
839 # Reference frame for alignment (using Kabsch algorithm)
840 # default is "0"
841 ref_frame_num                  110
842
843
844 # Desired distance measurement unit for output
845 # 0: RMSD (default)
846 # 1: dRMSD
847 # 2: Hold and Sander Score
848
849 dist_unit                      0
850
851 # if Holm and Sander Score is chosen, pick value for r_c
852 # (contact cutoff distance)
853 # default is "20", as in original publication
854
855 holm_sand_r0                   5
856
857
858 #####
859 #                                     #
860 #   ENTROPY-CALC OPTIONS             #
861 #                                     #
862 #####
863

```

```

864 # Should alignment (Kabsch algorithm, minimizes RMSD) be performed
865 # prior to calculations? (options: false / true; true is default)
866 # entropy_ref_frame_num gives reference frame for alignment (default is 0)
867 entropy_alignment                true
868 entropy_ref_frame_num            0
869
870 # Specify first frame to be used in entropy calculations
871 # default is 0
872 entropy_start_frame_num          0
873 # Specify offset value (only every n'th frame will be used in calculations)
874 entropy_offset                   1
875
876 # Temperature needed for Entropy etc. calculations in K
877 entropy_temp                     300.00
878
879 # Should the removal of degrees of freedom for rotation / translation be attempted?
880 entropy_remove_dof               true
881
882 # Use internal coordinates instead of cartesian coordinates?
883 # Use the CAST task to display the internal z-mat and then enter desired atom-indexes of
884 # bondlengths (bnd), angles (ang) and dihedral angles (dih). "none" also possible
885 entropy_use_internal             false
886 entropy_internal_bnd             none
887 entropy_internal_ang             none
888 entropy_internal_dih             4-23
889
890 # Should only specific atoms be used for entropy calculations?
891 # (only use with cartesian coordinates)
892 entropy_trunc_atoms_bool         false
893 entropy_trunc_atoms_num          3,4
894
895 # Specify method used in entropy-calculations:
896 # 1 : Quasi-Harmonic-Approx., configurational entropy, according to Karplus et. al.
897 #     (DOI 10.1021/ma50003a019)
898 # 2 : Quasi-Harmonic-Approx., conformational entropy, according to Knapp et. al. without
899 #     corrections (Genome Inform. 2007;18:192-205.)
900 # 3 : Quasi-Harmonic-Approx., conformational entropy, according to Knapp et. al. with
901 #     corrections (Genome Inform. 2007;18:192-205.)
902 # 4 : Nearest-Neighbor Nonparametric Method, configurational entropy, according to
903 #     Hnizdo et. al. (DOI: 10.1002/jcc.20589)
904 # 5 : Nearest-Neighbor Nonparametric Method - Sum of Marginal Entropies, configurational
905 #     entropy, according to Hnizdo et. al. (DOI: 10.1002/jcc.20589)
906 # 6 : Quasi-Harmonic-Approx., conformational entropy, according to Schlitter (use cartesians
907 #     only)
908 # 0 : All of the above
909 entropy_method                   0
910 # if entropy_method = 3 || 4 || 5 : specify value for k in kNN-Algorithm (default is 4)
911 entropy_method_knn_k             4
912
913
914 #####

```

```

915 #                                     #
916 #          PCAgen OPTIONS                #
917 #                                     #
918 #####
919
920 # Should alignment (Kabsch algorithm, minimizes RMSD) be performed
921 # prior to PCA-Analysis? (options: false / true; true is default)
922 # pca_ref_frame_num gives reference frame for alignment (default is 0)
923 pca_alignment                true
924 pca_ref_frame_num            0
925
926 # Specify first frame to be used in PCA-Analysis
927 # default is 0
928 pca_start_frame_num          0
929
930 # Specify offset value (only every n'th frame will be used in calculations)
931 #pca_offset                    1
932
933 # Should PCA-Mode-Coordinates and Eigenvalues of the covariance-matrix be written to file?
934 # If false, we are expecting to read Eigenvectors and PCA-Modes from a previously
935 # CAST-generated file.
936 pca_read_vectors              false
937 pca_read_modes                false
938
939 # Use internal coordinates instead of cartesian coordinates? If yes, should they converted
940 # to metric coordinate space?
941 # Use the CAST task to display the internal z-mat and then enter desired atom-indexes of
942 # bondlengths (bnd), angles (ang) and dihedral angles (dih). "none" also possible.
943 # Atom indices start at 0.
944 pca_use_internal              true
945 pca_internal_dih              5-20
946 pca_internal_ignore_hydrogen  false
947
948 # Should only specific atoms be used for PCA-Analysis?
949 pca_trunc_atoms_bool          true
950 pca_trunc_atoms_num           5-50
951 pca_trunc_atoms_ignore_hydrogen false
952
953 # Print probability density of generated PCA modes?
954 pca_print_probability_density true
955 # If true, specify the number of bins or a bin-width for histogramming the data
956 pca_histogram_width           0
957 pca_histogram_number_of_bins  42
958 pca_dimensions_for_histogramming 1,2
959
960
961 #####
962 #                                     #
963 #          PCAproc OPTIONS                #
964 #                                     #
965 #####

```

```
966 |
967 | # Desired range of coordinates as principal components to be written.
968 | # Specify as such: 5.0,7.0,9.0 (this means: dim1, dim2, dim3 etc....)
969 | proc_desired_start      -5.0
970 | proc_desired_stop       5.0
```

```

1
2
3 forcefield spackman
4
5 n 1 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0
6 n 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0
7 n 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0
8 n 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0
9 n 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0
10 n 1 1 2 2 2 2 3 1 1 2 2 2 2 3 2 2 2 2 2 2 2
11 n 1 1 2 2 2 2 3 1 1 2 2 2 2 3 2 2 2 2 2 2 2
12 n 1 1 2 2 2 2 3 1 1 2 2 2 2 3 2 2 2 2 2 2 2
13 n 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0
14 n 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0
15 zeta 1.0 2.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0
16 zeta 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0
17 zeta 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0
18 zeta 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0
19 zeta 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0
20 zeta 8.567411 4.888048 6.992217 2.263845 1.475269 1.164113 15.468297 8.493580 4.879055 7.049887
21 2.263881 1.475239 1.163509 15.466018 7.047132 3.224676 2.182796 1.439708 1.023369
22 zeta 10.34086 5.90729 8.38254 2.75805 1.80300 1.48481 17.99319 9.90512 5.74365 8.30856 2.76159
23 1.82269 1.41970 17.98161 8.34900 3.88269 2.59205 1.69455 1.19122
24 zeta 11.38904 6.58916 9.45755 3.24871 2.16127 1.64181 20.50524 9.90281 5.87197 8.28914 3.03043
25 1.91090 1.56290 17.97671 9.64711 4.33213 2.75051 1.75250 1.24654
26 zeta 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0
27 zeta 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0
28 c 1.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0
29 c 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0
30 c 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0
31 c 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0
32 c 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0
33 c 0.363110 0.437999 0.234039 0.005501 0.015065 -0.005056 -0.000015 -0.066035 0.441836 -0.087353
34 -0.393509 -0.578609 -0.125934 -0.000496 0.007068 0.071982 0.231920 0.410597 0.349870
35 c 0.30997 0.50753 0.20963 0.02966 -0.07656 0.07353 0.00149 -0.06167 0.43690 -0.07645 -0.37468
36 -0.52264 -0.20704 -0.00046 0.00643 0.08300 0.26010 0.41827 0.30836
37 c 0.35854 0.46329 0.21278 -0.01355 0.02844 0.00140 0.00083 0.07478 0.19686 0.05240 -0.51069

```

38		-0.52007	-0.07553	-0.00389	0.00583	0.12660	0.32926	0.39488	0.23210											
39	c	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
40	c	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
41	o	1	0	0																
42	o	0	0	0																
43	o	0	0	0																
44	o	0	0	0																
45	o	0	0	0																
46	o	2	2	2																
47	o	2	2	3																
48	o	2	2	4																
49	o	0	0	0																
50	o	0	0	0																
51	6	1.00238																		
52	1	1.44743																		
53	5	1.0																		
54	8	1.0																		
55	e																			