

Documentation 2023

Version 4.3

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#### Introduction

ANYstructure is a free structural optimization tool. It can be used for multiple purposes. The software can be downloaded various ways:

For python users

PIP install ANYstructure

For windows version

Download at <a href="https://github.com/audunarn/ANYstructure/releases">https://github.com/audunarn/ANYstructure/releases</a> or <a href="https://sourceforge.net/projects/anystructure/">https://sourceforge.net/projects/anystructure/</a>

The code is located on github and is open source (<a href="https://github.com/audunarn/ANYstructure">https://github.com/audunarn/ANYstructure</a>)

# Theory

All calculations are according to the following DNV standards and recommended practices:

- DNVGL-OS-C101 Design of offshore steel structures, general LRFD method
  - http://rules.dnvgl.com/docs/pdf/DNVGL/OS/2018-07/DNVGL-OS-C101.pdf
- DNV-RP-C203 Fatigue design of offshore steel structures
- DNV-RP-C201 BUCKLING STRENGTH OF PLATED STRUCTURES
  - https://rules.dnvgl.com/docs/pdf/DNV/codes/docs/2010-10/RP-C201.pdf
- DNV-RP-C202 Buckling Strength of Shells
- PULS (Panel Ultimate Limit State)
- DNVGL-CG-0128 Buckling

# Modeling

Modeling is done in the Geometry tab.

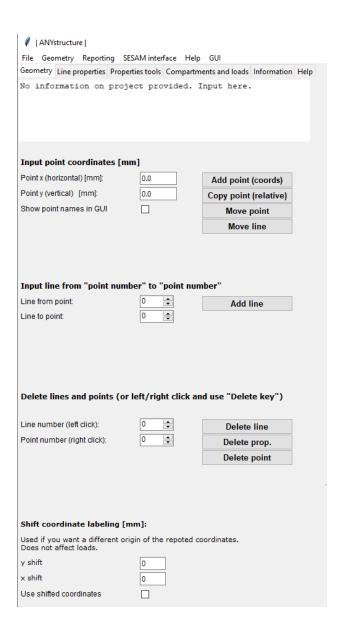
Right click: select point

You can copy or move the selected point by shortcut or clicking

Buttons.

Left click: select line

A line is made by right clicking two points (or input point number)



Speed up your modeling significantly by using the shortcuts:

CTRL-Z Undo modeling

CTRL-P Copy a selected point

CTRL-M Move a selected point

CTRL-Q New line between two selected points

CTRL-S Assign properties to a selected line

CTRL-DELETE Delete the structural properties from the selected line

DELETE Delete selected line/point

CTRL-E Select a line and copy the properties of this line

CTRL-D Paste structural properties to a selected line

Arrows up/down Toggle point in model

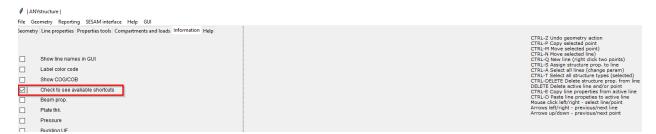
Arrows left/right Toggle lines in model

CTRL-A Select all lines in model for changing a selected parameter for all

CTRL-T Select all lines of a specific structure type for changing a parameter

for multiple lines.

The shortcuts can be shown in the GUI as seen next.



# Assigning properties

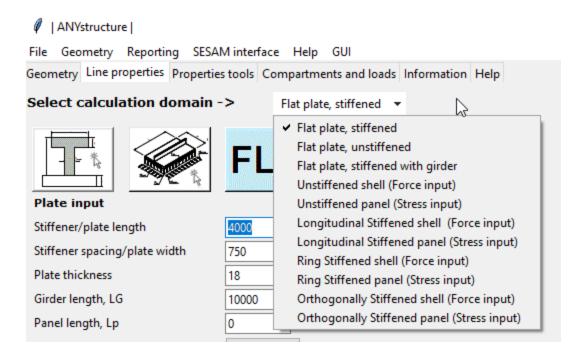
Input properties manually or click the button indicated below to set the values.

Values are set by clicking "Add structure to line". This also applies to fatigue properties.

If you have added a property to a line and want to use the same for the next line, just

press "Add structure to line" on the new line.

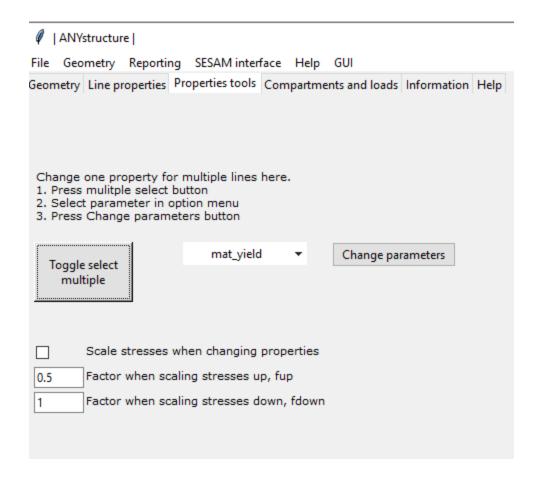
The first value to be set is the structure type. The selection is either a flat plate or some type of cylindrical structure (all others). The dropdown list is shown next. More details on the cylindrical structures.



All beam sections are recorded. If you want to apply an existing, choose it from the drop down menu. Then press "Save and return structure".

#### Scale stresses

Stresses can be automatically scaled when changing a property, for example plate thickness. The parameters fup and fdown specify the factor to be applied to the scaling when scaling up (thicker plate) or down (thinner plate).



The formula applied is referenced next. The factor depends on your case.

If panel thickness (T) is changed (dT), stress may be scaled by a factor (f) according to the formula:

$$newStress = \left(\frac{T}{T + f * dT}\right) * oldStress$$

- f = 0.0 -> stress does not depend on local thickness change.
- f = 1.0 -> stress is proportional to local thickness change.

Stresses to be scaled are axial stress (SigmaX), transversal stress(SigmaY) and shear stress (TauXY).

The parameters fdown = 1 and fup = 0.5 are by default. The general idea is that it is conservative to accept lower stress reduction when increasing thicknesses.

## Cylinder input

#### **Variables**

Thickness of cylinder

Yield stress fy Material yield stress

Shell Radius (middle of plate) r Radius of cylinder

Distance between rings I Distance between ring stiffeners. If there are no ring

stiffeners, the value is the same as cylinder length.

Length of shell Length of the cylinder.

Total cylinder length Lc Used when the input is a complete cylinder (not

panel). Total length of cylinder.

Eff. Buckling length factor k Effective length buckling factor.

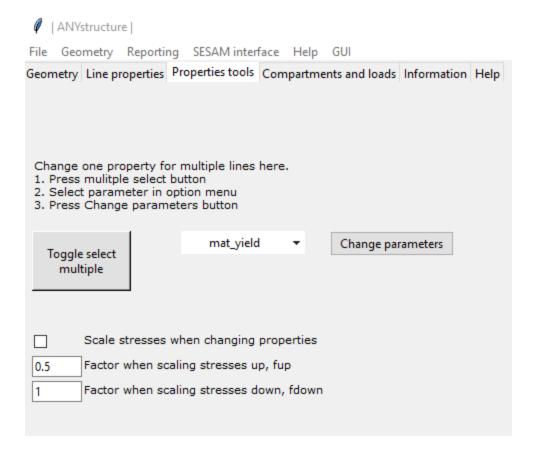
Length between girders Lh Used when a heavy ring frame is applied. Distance

between the girders/heavy ring frames.

#### Changing multiple properties

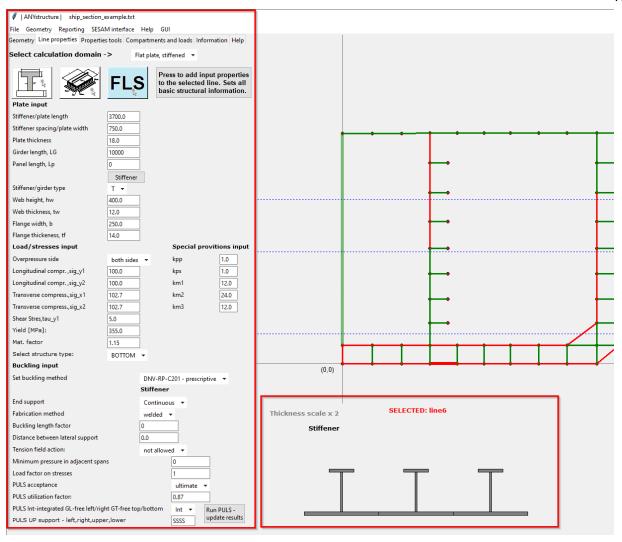
If you want to change a single property for multiple lines. How to do it:

- 1. Press Toggle select multiple
- 2. Select the parameter to change
- 3. Select the lines to change. Click single lines, CTRL-A or CTRL-T (see shortcuts)
- 4. Press Change multi. param.



#### Display properties

If you click a line properties are shown in the input fields under the "Line properties" tab. In addition a visual representation of the structure is shown.



Also it is recommended to use color coding to review your input.

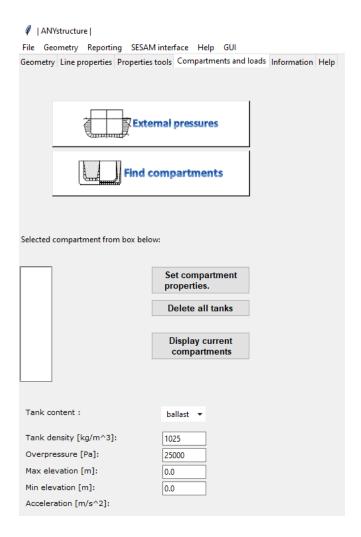
### Define tanks

Compartment and loads found in the "Compartments and loads" tab.

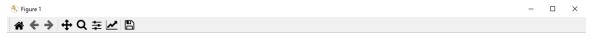
Tanks are searched for when clicking "Find compartments". Non watertight structures are ignored. For information on structure types click "Show structure types".

By default tank content density is set to 1025 (water).

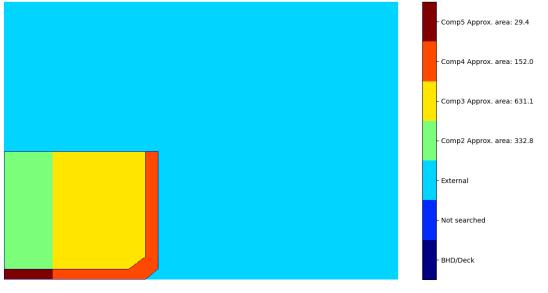
Other tanks are found content and overpressure must be defined as seen next.



If you press "Display current compartments" after doing a compartment search, the result of the search is illustrated as seen next. Approximate area of the respective compartments is also shown.



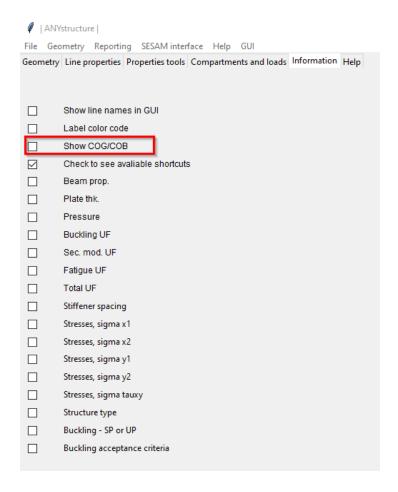
#### Compartments returned from search operation displayed below

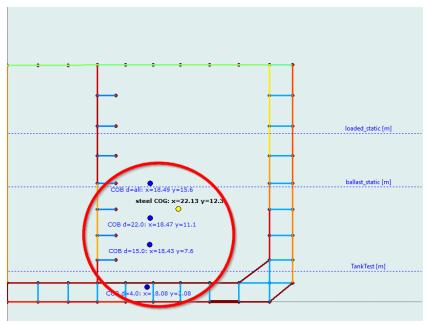


\*area calculation inaccuracies due to thickness of barriers (BHD/Deck)

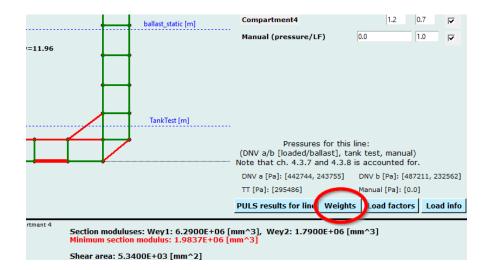
#### COB and COG

COG is calculated when structure properties are defined. COB for various drafts is calculated when tank search is completed.

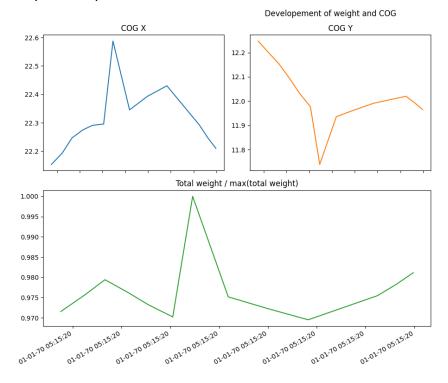




Development of weight and COG is recorded each time the structure changes. The resulting plot can be seen by pressing the "weights" button.



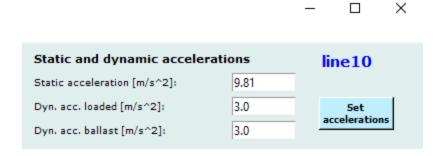
#### Output example is seen next.



Plates in model	Beams in model
18.0 mm	T_400_0x12_0_200_0x20_0
25.0 mm	T_400_0x12_0250_0x14_0
12.0 mm	T_400_0x12_0250_0x12_0
20.0 mm	T_400_0x12_0_200_0x18_0
14.0 mm	T_400_0x12_0150_0x20_0
30.0 mm	T_500_0x12_0_150_0x20_0
15.0 mm	T_340_0x12_0200_0x20_0
	T_340_0x12_0150_0x16_0
	T_250_0x12_0150_0x14_0
	T_450_0x12_0150_0x20_0
	T_375_0x12_0150_0x18_0
	T_500_0x12_0150_0x25_0
	T_325_0x12_0150_0x16_0
	FB_250_0x18_0
	FB_400_0x18_0
	T_350_0x12_0150_0x20_0
	T_320_0x12_0150_0x20_0
	T_300_0x12_0150_0x20_0

# Setting accelerations

Accelerations apply to tank content. It is set in the upper right corner as seen next.



# Define external pressures

Click "External pressures" to define pressures acting on the structures.

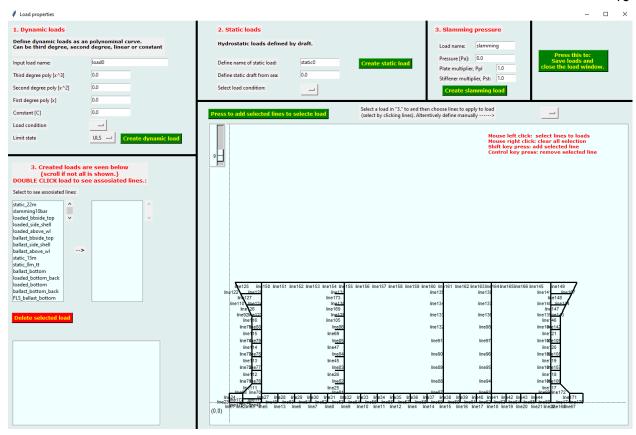
#### NOTE:

#### FOR DYNAMIC EQUATION THE FOLLOWING APPLIES

X (horizontal) used for BOTTOM, BBT, HOPPER, MD Z (vertical) used for BBS, SIDE\_SHELL, SSS

#### After new window is opened:

- 1. Make dynamic loads
  - a. Dynamic loads are made by defining up to 3rd degree equations. X or Y
    direction depends on the defined structure type.
  - b. Note that you can define a constant dynamic load by using Constant (Constant (C)) only.
- 2. Static loads are calculated according to depth.
- 3. To apply a defined load to a line or multiple lines:
  - a. a. Select load by clicking the created load
- 4. Click the lines that shall have the load. Click the button "Press to add selected lines to selected load"
- 5. When finished press the button in the upper right corner.



Slamming loads can be specified separately. The multiply factors are the slamming pressure to be used on plate and stiffener respectively. For example for a 10 bar pressure:

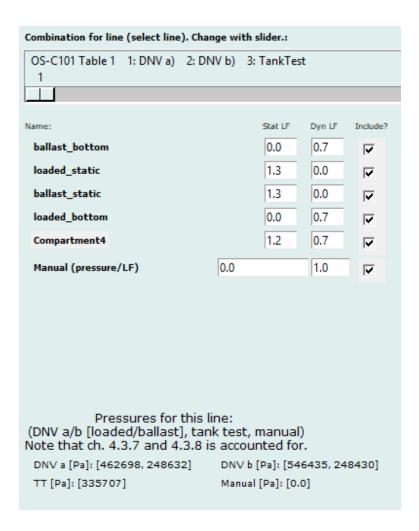
Pplate = 10 bar \* factor\_plate

Pstf = 10 bar \* factor\_stiffener

## Load combinations

Load combinations are created automatically after external pressures are defined. Some comments on the loads.

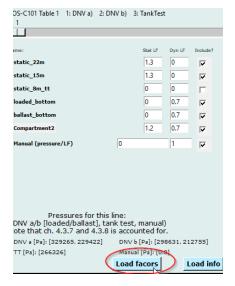
- 1. According to DNVGL-OS-C101
- 2. Highest pressure is chosen w.r.t. tank filling.
- 3. You can deselect a load by manually inputting load factor to 0 or deselect include.

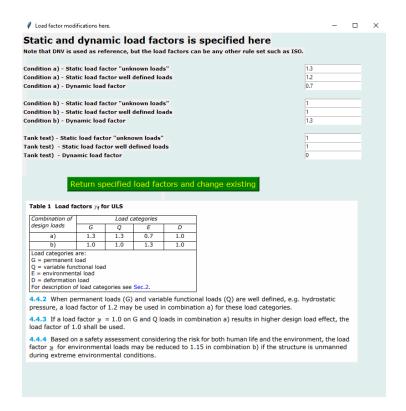


## Changing load factors

You can change default load factors and existing load factors using the button seen in the next illustration.

Load factors are based on standard DNV LRFD factors, but any values can be used.



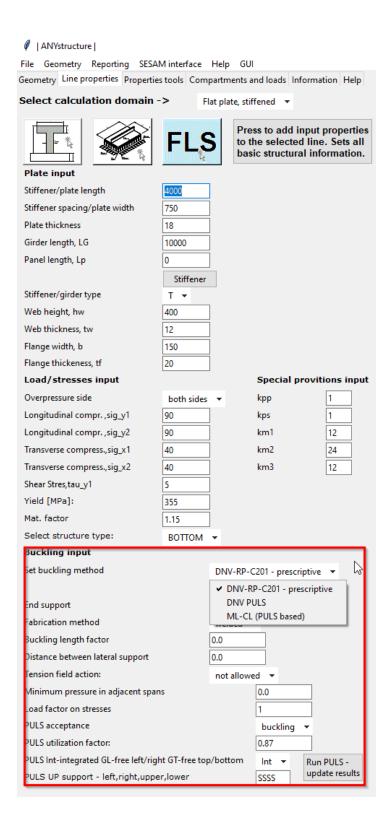


# **Buckling**

ANYstructure has 3 options for calculating buckling.

# Prescriptive

Buckling calculations as per DNV-RP-C203.



## **PULS** integration

ANYstructure can use PULS software to calculate buckling. PULS is a licensed DNV software. Consequently, PULS integration will not work if you do not have the license. Specifically ANYstructure uses the PULS Excel sheet to calculate. Macros must be enabled for the sheet. The sheet may require a 32 bit version of Microsoft Office. Using PULS is activated by clicking

the button seen next. When running a line for the first time, you will be asked to provide the location of the PULS excel sheet. The sheet should be empty and macros should be enabled.

PULS parameters are set for each line.

- 1. Stiffened panel (SP) or unstiffened plate (UP).
  - a. If UP is chosen you can specify the boundary conditions. The conditions consist of four letters, representing left side, right side, top and bottom (in this order). 'S' means simply supported and 'C' means Clamped. 'SSSS' is consequently all simply supported and for example 'SSCC' is simply supported sides with clamped top and bottom.
- 2. Integrated (Int) or girder panels (GL/GT)
- 3. Continuous or Sniped stiffener
- 4. Ultimate or buckling acceptance. In general ultimate acceptance is more representative for larger plate fields where loads can be redistributed. Reference is made to DNV standards.

For theory check out PULS manual and/or Part 1, chapter 8 of the IACS Common structural rules for bulk carriers and oil tankers:

https://iacs.org.uk/publications/common-structural-rules/csr-for-bulk-carriers-and-oil-tankers/

Detailed PULS results can be viewed by selecting a line a pressing the "PULS results for line" button:

```
| ANYstructure | ship_section_example.txt
                                                                     Identification : line8
Plate geometry
  Length of panel: 3500.0 mm
  Stiffener spacing: 750.0 mm
  Plate thick. : 18.0 mm
Primary stiffeners
 Number of stiffeners: 10.0
  Stiffener type : T-bar
  Stiffener boundary : Cont
  Stiff. Height: 400.0 mm
  Web thick. : 12.0 mm
  Flange width: 250.0 mm
  Flange thick. : 12.0 mm
  Flange ecc. : 0.0 mm
  Tilt angle : 0.0 degrees
Secondary stiffeners
  Number of sec. stiffeners: 0.0
   Secondary stiffener type : Flatbar
  Stiffener boundary : SS
  Stiff. Height: 0.0 mm
  Web thick. : 0.0 mm
  Flange width: 0.0 mm
  Flange thick. : 0.0 mm
Model imperfections
  Imp. level : Default
  Plate : 3.75 mm
  Stiffener: 3.5 mm
  Stiffener tilt : 3.5 mm
Material
  Modulus of elasticity: 210000.0 MPa
  Poisson's ratio : 0.3
  Yield stress plate : 355.0 MPa
  Yield stress stiffener: 355.0 MPa
Aluminium prop
  HAZ pattern :
  HAZ red. factor : -
Applied loads
  Axial stress: 102.0 MPa
  Trans. stress : 100.0 MPa
  Trans. stress 2 : 100.0 MPa
  Shear stress : 5.0 MPa
  Pressure (fixed) : 0.438508 MPa
Bound cond.
  In-plane support : Integrated
Global elastic buckling
  Axial stress : 367.0 MPa
  Trans. Stress: 362.0 MPa
  Trans. stress: 362.0 MPa
  Shear stress : 18.0 MPa
Local elastic buckling
 Axial stress : 134.0 MPa
  Trans. Stress: 132.0 MPa
  Trans. stress: 132.0 MPa
  Shear stress : 7.0 MPa
Ultimate capacity
 Actual usage Factor: 0.73
  Allowable usage factor: 1.0
  Status : Ok
Failure modes
  Plate buckling: 37.0 %
```

## ML buckling

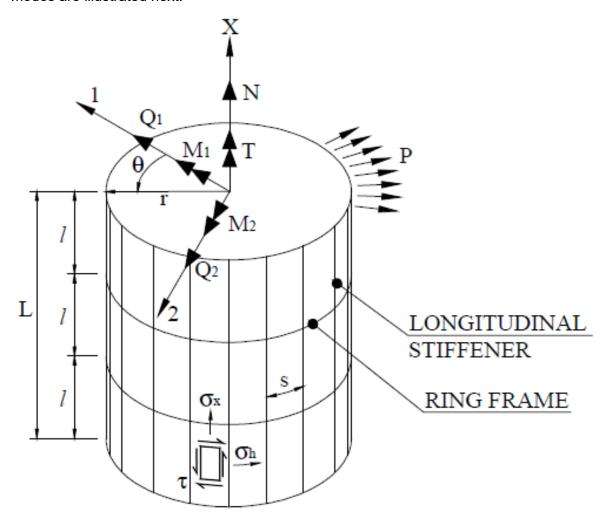
The buckling ML option is an implementation of PULS using a neural network. It uses the same input as PULS. Note that the "PULS utilization factor" does not apply. The CL (classification) neural network will use 1/1.15 =0.87 as material factor and get the acceptance from that. If you need other acceptance criterias, contact Audun (<u>audunarn@gmail.com</u>). In that case the neural networks must be retrained for other acceptance levels.

The results should be used with care, as a neural network typically can give an incorrect prediction. The accuracy is currently in the range of 97%.

ML buckling can be used for all optimization options.

# Cylinder buckling

Prescriptive buckling calculations according to DNV-RP-C202. The various calculated buckling modes are illustrated next.



Buckling mode	s for different types of cylinders  Type of structure geometry			
Successing mode	Ring stiffened (unstiffened circular)	Longitudinal stiffened	Orthogonally stiffened	
a) Shell buckling				
		#0 0 B		
	Section 3.4	Section 3.3	Section 3.3	
b) Panel stiffener buckling				
		. 401100		
		Section 3.6	Section 3.7	
c) Panel ring buckling	Section 3.5		Section 3.7	
d) General buckling				
\ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \			Section 3.7	
e) Column buckling				
	Section 3.8	Section 3.8	Section 3.8	

# Reviewing data

# Color coding

All color coding options are indicated next.

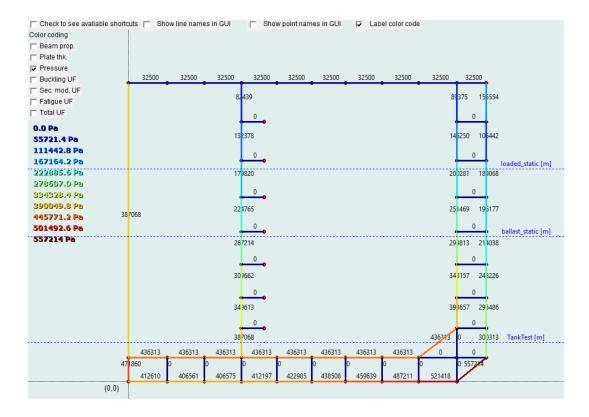
Geometry   Line properties   Properties tools   Compartments and loads   Information   Help		ANYstructure   Geometry Reportir	na SESAM inter	face Help	GUI		
Label color code   Show COG/COB   Check to see avaliable shortcuts   Beam prop.   Plate thk.   Pressure   Buckling UF   Sec. mod. UF   Fatigue UF   Total UF   Stiffener spacing   Stresses, sigma x1   Stresses, sigma x2   Stresses, sigma y1   Stresses, sigma tauxy   Structure type   Buckling - SP or UP			_			Information	Help
Label color code   Show COG/COB   Check to see avaliable shortcuts   Beam prop.   Plate thk.   Pressure   Buckling UF   Sec. mod. UF   Fatigue UF   Total UF   Stiffener spacing   Stresses, sigma x1   Stresses, sigma x2   Stresses, sigma y1   Stresses, sigma tauxy   Structure type   Buckling - SP or UP							
Label color code   Show COG/COB   Check to see avaliable shortcuts   Beam prop.   Plate thk.   Pressure   Buckling UF   Sec. mod. UF   Fatigue UF   Total UF   Stiffener spacing   Stresses, sigma x1   Stresses, sigma x2   Stresses, sigma y1   Stresses, sigma tauxy   Structure type   Buckling - SP or UP							
□ Label color code   □ Show COG/COB   ☑ Check to see avaliable shortcuts   □ Beam prop.   □ Plate thk.   □ Pressure   □ Buckling UF   □ Sec. mod. UF   □ Total UF   □ Stiffener spacing   □ Stresses, sigma x1   □ Stresses, sigma x2   □ Stresses, sigma y1   □ Stresses, sigma tauxy   □ Structure type   □ Buckling - SP or UP   □ Buckling acceptance criteria							
Show COG/COB    Check to see avaliable shortcuts   Beam prop.   Plate thk.   Pressure   Buckling UF   Sec. mod. UF   Fatigue UF   Total UF   Stiffener spacing   Stresses, sigma x1   Stresses, sigma x2   Stresses, sigma y2   Stresses, sigma tauxy   Structure type   Buckling acceptance criteria		Label color cod	е				
Check to see avaliable shortcuts   Beam prop.   Plate thk.   Pressure   Buckling UF   Sec. mod. UF   Fatigue UF   Total UF   Stiffener spacing   Stresses, sigma x1   Stresses, sigma x2   Stresses, sigma y1   Stresses, sigma tauxy   Structure type   Buckling - SP or UP   Buckling acceptance criteria		Show COG/COE	3				
□ Beam prop.   □ Plate thk.   □ Pressure   □ Buckling UF   □ Fatigue UF   □ Total UF   □ Stiffener spacing   □ Stresses, sigma x1   □ Stresses, sigma x2   □ Stresses, sigma y1   □ Stresses, sigma tauxy   □ Structure type   □ Buckling - SP or UP   □ Buckling acceptance criteria	☑	Check to see av	aliable shortcut	3			
Plate thk.   Pressure   Buckling UF   Sec. mod. UF   Fatigue UF   Total UF   Stiffener spacing   Stresses, sigma x1   Stresses, sigma x2   Stresses, sigma y1   Stresses, sigma y2   Stresses, sigma tauxy   Structure type   Buckling - SP or UP   Buckling acceptance criteria		Beam prop.					
□ Pressure   □ Buckling UF   □ Sec. mod. UF   □ Fatigue UF   □ Total UF   □ Stiffener spacing   □ Stresses, sigma x1   □ Stresses, sigma x2   □ Stresses, sigma y1   □ Stresses, sigma tauxy   □ Structure type   □ Buckling - SP or UP   □ Buckling acceptance criteria		Plate thk.					
Buckling UF Sec. mod. UF Total UF Stiffener spacing Stresses, sigma x1 Stresses, sigma x2 Stresses, sigma y1 Stresses, sigma y2 Stresses, sigma tauxy Structure type Buckling - SP or UP Buckling acceptance criteria		Pressure					
Sec. mod. UF Fatigue UF Total UF Stiffener spacing Stresses, sigma x1 Stresses, sigma x2 Stresses, sigma y1 Stresses, sigma y2 Stresses, sigma tauxy Structure type Buckling - SP or UP Buckling acceptance criteria		Buckling UF					
Fatigue UF Total UF Stiffener spacing Stresses, sigma x1 Stresses, sigma x2 Stresses, sigma y1 Stresses, sigma y2 Stresses, sigma tauxy Structure type Buckling - SP or UP Buckling acceptance criteria		Sec. mod. UF					
Total UF Stiffener spacing Stresses, sigma x1 Stresses, sigma x2 Stresses, sigma y1 Stresses, sigma y2 Stresses, sigma tauxy Structure type Buckling - SP or UP Buckling acceptance criteria		Fatigue UF					
Stiffener spacing Stresses, sigma x1 Stresses, sigma x2 Stresses, sigma y1 Stresses, sigma y2 Stresses, sigma tauxy Structure type Buckling - SP or UP Buckling acceptance criteria		Total UF					
Stresses, sigma x1 Stresses, sigma x2 Stresses, sigma y1 Stresses, sigma y2 Stresses, sigma tauxy Structure type Buckling - SP or UP Buckling acceptance criteria		Stiffener spacing	)				
Stresses, sigma x2 Stresses, sigma y1 Stresses, sigma y2 Stresses, sigma tauxy Structure type Buckling - SP or UP Buckling acceptance criteria		Stresses, sigma	d				
Stresses, sigma y1 Stresses, sigma y2 Stresses, sigma tauxy Structure type Buckling - SP or UP Buckling acceptance criteria		Stresses, sigma >	ι2				
Stresses, sigma y2 Stresses, sigma tauxy Structure type Buckling - SP or UP Buckling acceptance criteria		Stresses, sigma y	/1				
Stresses, sigma tauxy Structure type Buckling - SP or UP Buckling acceptance criteria		Stresses, sigma y	/2				
Structure type Buckling - SP or UP Buckling acceptance criteria		Stresses, sigma t	auxy				
Buckling - SP or UP Buckling acceptance criteria		Structure type					
Buckling acceptance criteria		Buckling - SP or	UP				
		Buckling accept	ance criteria				
					1		

#### Shifting coordinates for visual purposes

You can shift the coordinates displayed for visual purposes. This does NOT affect the calculations of loads. This feature is included to better be able to review coordinates using different origins. Input magnitude of the shift in the lower left corner and check "Use shifted coordinates" to activate.

#### Loads

Pressure magnitude can be reviewed by using color coding. The highest total pressure used in calculations is shown.



Load calculations and results can be reviewed by clicking the "Load info" button. An example is seen in the next illustration.

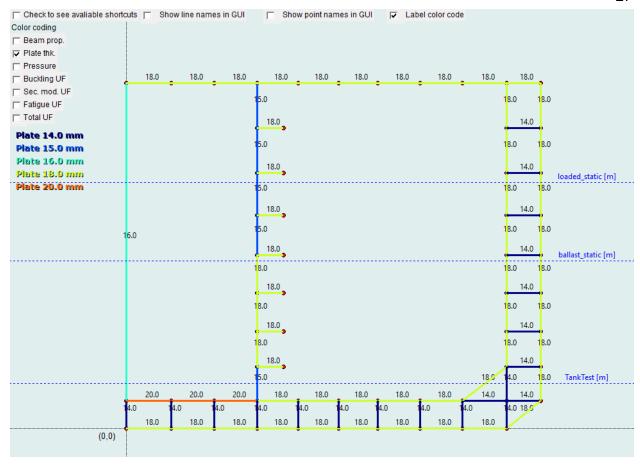
Х

```
| ANYstructure | ship_section_example.txt
```

```
Load results for line8
Loads for condition: loaded - dnva
 static with acceleration: 9.81 is:
 1*1.3*221215.5 = 287580.2
 dynamic with acceleration: 3.0 is:
 1*0.7*181077.2 = 126754.1
RESULT: 287580.2 + 126754 = 414334.2
Loads for condition: ballast - dnva
 dynamic with acceleration: 3.0 is:
 1*0.7*57425.2 = 40197.6
 static with acceleration: 9.81 is:
 1*1.3*150828.8 = 196077.4
comp4 - static: 1*1.2*310707.22500000003 + 25000.0*1.3 = 405348.67000000004
comp4 - dynamic: 1*0.7*95017.50000000001 + 25000.0*0 = 66512.25
RESULT: 40197.6 + 196077 = 236275.0
Loads for condition: loaded - dnvb
 static with acceleration: 9.81 is:
 1*1.0*221215.5 = 221215.5
 dynamic with acceleration: 3.0 is:
 1*1.2*181077.2 = 217292.7
RESULT: 221215.5 + 217293 = 438508.2
Loads for condition: ballast - dnvb
 dynamic with acceleration: 3.0 is:
 1*1.2*57425.2 = 68910.2
 static with acceleration: 9.81 is:
 1*1.0*150828.8 = 150828.8
comp4 - static: 1*1.0*310707.22500000003 + 25000.0*1.3 = 343207.22500000003
comp4 - dynamic: 1*1.3*95017.50000000001 + 25000.0*0 = 123522.75000000003
RESULT: 68910.2 + 150829 = 219739.0
Tank test for: t
1 * 1.0 * 40221.0 + 0 = 40221
Tank test for: comp4
1 * 1.0 * 310707.2 + 25000.0 * 1 = 335707
Manual pressure:
0.0 * 1.0 * 1 = 0.0
```

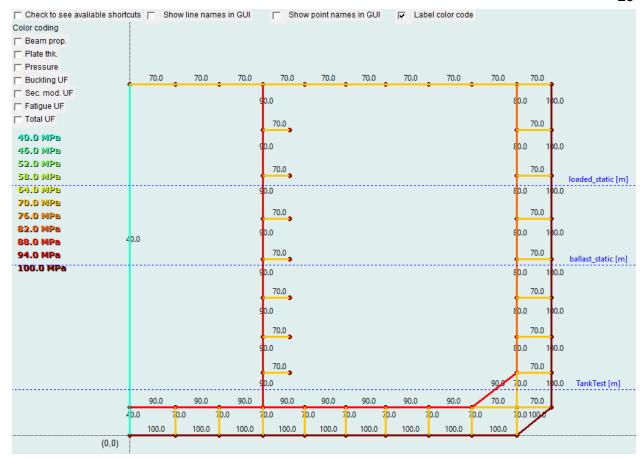
#### Thickness and beam properties

Line plate thicknesses and beam properties can be reviewed using color coding. Plate thicknesses are exemplified next.



# Global stresses (buckling) and structure types

Stresses used in buckling calculations can be reviewed by checking as illustrated next.



# Results

When clicking a line, results as presented in the window below. If the result for the clicked line is OK, the color of the line and text is green. If the result is NOT OK, the color of the line and text is red. Two examples are seen next.

Special provisions - DNV-OS-C101 - checks for section, web thickness and plate thickness.			
	Minimum value	Actual value	Accepted?
Section modulus check	1.8617E+06 [mm^3]	1.9600E+06 [mm^3]	Ok
Shear area check	3.6307E+03 [mm^2]	5.2320E+03 [mm^2]	Ok
Plate thickness check	14.4 [mm]	18.0 [mm]	Ok
Buckling results DNV-RP-C201 -	prescriptive - (plate, st	iffener, girder):	
	Plate	Stiffener	Girder
Overpressure plate side	0.574	1.244	0
Overpressure stiffener side		1.112	0
Resistance between stiffeners		0.832	0
Shear capacity		0.684	
Maximum web height [mm]		410.0	0
Maximum flange width [mm]		205.0	0
Fatigue results (DNVGL-RP-C203):			
Total damage (DFF not included): 0.137   With DFF = 2.0> Damage: 0.275			
	•		

Special provisions - DNV-OS-C	101 - checks for se	ction, web thickness and	l plate thickness.
	Minimum value	Actual value	Accepted?
Section modulus check	8.1018E+05 [mi	m^3] 1.7400E+06 [mm	1^3] Ok
Shear area check	1.7920E+03 [mi	m^2] 4.5360E+03 [mm	1^2] Ok
Plate thickness check	11.0 [mm]	18.0 [mm]	Ok
Buckling results DNV-RP-C201	- prescriptive - (pla	ite, stiffener, girder):	
	Plate	Stiffener	Girder
Overpressure plate side	0.352	0.641	0
Overpressure stiffener side		0.554	0
Resistance between stiffeners		0.865	0
Shear capacity		0.411	
Maximum web height [mm]		410.0	0
Maximum flange width [mm]		228.0	0
Fatigue results (DNVGL-RP-C2	03):		
Total damage: NO RESULTS			
_			

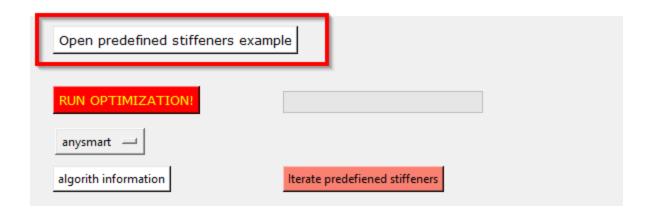
A combined utilization can be reviewed using color coding.

# Optimization

## Optimization iteration by predefined stiffeners

From 0.5 you can iterate by a defined set of stiffeners. Press the button marked below. Open a csv (or json) file. Then start your iterations. The only other input is the stiffener spacing and plate thickness.

To see how the input format is, click the "open predefined stiffeners example" button. See illustrations next.



Note that the weight of your initial structure is ignored even though it is calculated. If the initial structure is in your predefined set it will be included in the evaluations.

Press the button indicated below to activate. An open file window will open when running the optimization.



#### Single optimization

Single optimization is done by clicking a line and clicking the "OPTIMIZE" button.

- 1. Set the upper and lower bounds of the optimization.
- 2. Set the delta to be used for the search. This is the step size of the optimization when using brute force method (for example anysmart).
- Run the optimization.
- 4. If you are happy, return the properties by clicking the top button

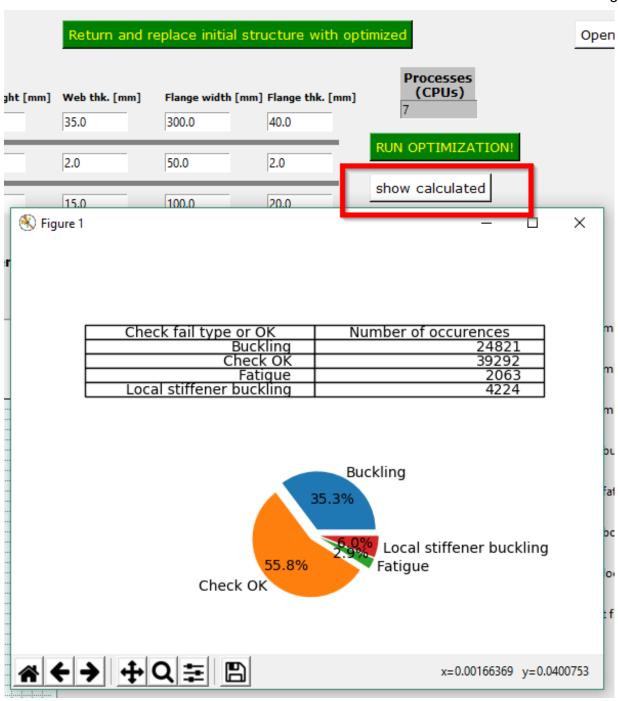
Various checks in the optimization module:

You can select the checks to be performed. PULS buckling can be used in optimization. Remember to check the running time.

The weight filter ensures that only sections with a lower weight than the current minimum weight. This significantly speeds up the calculations, but if you want to see the full distribution of the various checks this must be unchecked.

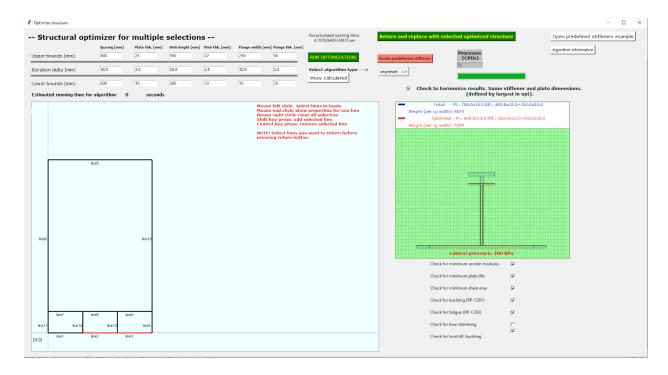
Check for minimum section modulus	<b>~</b>
Check for minimum plate thk.	<b>~</b>
Check for minimum shear area	<b>V</b>
Check for buckling (RP-C201)	✓
Check for fatigue (RP-C203)	<b>~</b>
Check for bow slamming	
Check for local stf. buckling	<b>~</b>
Use weight filter (for speed)	<b>~</b>
Check for buckling (PULS)	

If you press the "show calculated" button, you will get an overview of how many are ok and how many failed (and what criteria first failed). One "occurence" is a one checked plate/stiffener combination.



You will also be asked to save to a csv file. If you do not cancel, a csv file will ALL results will pre saved to your chosen location. If you open the file in excel you should see something like show next

#### Multiple optimization



Multiple optimization is done by clicking the "MultiOpt" button.

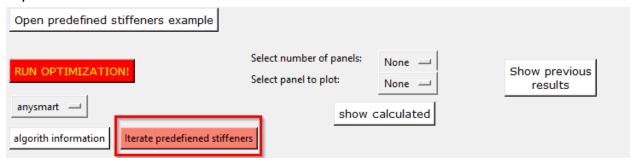
- 1. Same input on upper bounds, lower bounds and delta.
- 2. Click all the lines you want to include in the optimization.
- Run the optimization.
- Check the properties by middle clicking the line you ran.
- If you are happy, return the properties by clicking the top button. Remember to select the lines you want to return. Lines that have been optimized are marked orange.

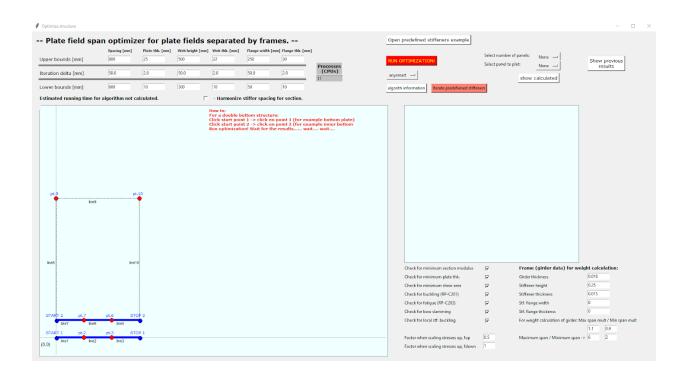
The optimization can be harmonized. That means that the largest dimension found in the multiple optimization is used for all selected. This is done after all plates/stiffeners are checked. Harmonization can only be done in the multiopt option. Note that the weight filter is not used when harmonizing, i.e. running will take some more time.

Other options that can be set are explained in the single optimization chapter. When showing calculated you must have selected a line (middle click).

## Span optimization

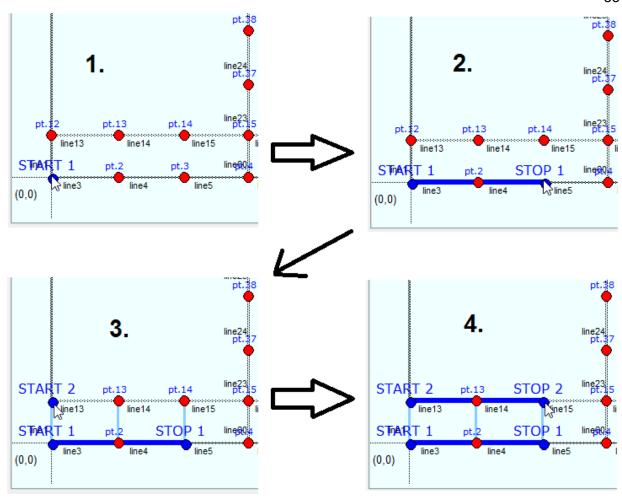
NOTE: The span optimization is computationally heavy. It is recommended to use a set of predefined stiffeners.





The optimization is started as follows.

1. Start by clicking as illustrated next:



#### 2. Check the input and checkboxes in the lower right corner

You can, similar to single optimization, select the checks that shall be runned. Also you can set the girder (frame) properties. This is used for calculating the weights.

Check for minimum section modulus	<b>▽</b>	Frame (girder data) for weight calculation:		
Check for minimum plate thk.	✓	Girder thickness	0.018	
Check for minimum shear area	✓	Stiffener height	0.25	
Check for buckling (RP-C201)	<b>▽</b>	Stiffener thickness	0.015	
Check for fatigue (RP-C203)	✓	Stf. flange width	0	
Check for bow slamming	✓	Stf. flange thickenss	0	
Check for local stf. buckling	<b>V</b>	For weight calculation of girder: Ma:	x span mult / Min span mult	
			1.1 0.9	
Factor when scaling stresses up, fup	0.5	Maximum span / Minimum span ->	6 2	
Factor when scaling stresses up, fdown	1			

#### 3. Start the calculation

The program will calculate variations of even spans in your structure as illustrated next.

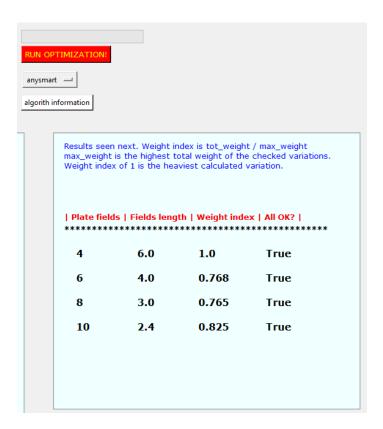
This is an example and the number of plate fields may vary.

# 4 plate fields 6 plate fields 8 plate fields 10 plate fields

With reference to the previous example, max span mult is the multiplicator for the 4 plate fields set up and min span mult is the weight multiplication for the 10 plate field set up. This is adopted because one can assume the required dimensions for the girder will reduce when more girders are added.

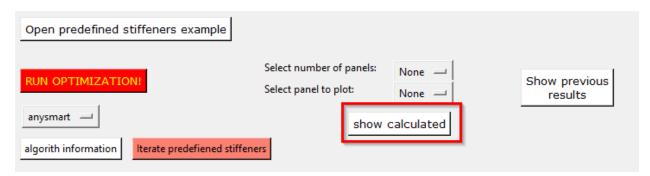
Minimum span and maximum span is the minimum and maximum span of the plate fields in meters.

Results are presented as seen next.



In this case 8 plate fields with length of 3 meters will give the lowest weight. 6 plate fields are almost equal.

When the analysis has been runned you should save your results. Just specify a file name in the save file dialog. You can also get detailed individual results for a specified panel. Select the number of plate fields in the iteration you want to look at, then choose which panel to get data from. Order of the panels is the same as printed in the left result canvas.

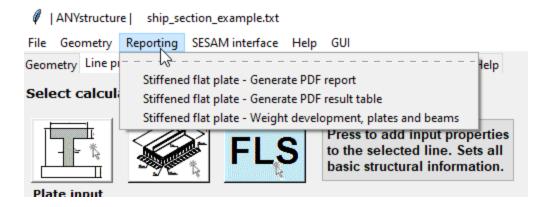


Now close the window. Results are not currently returned to the main window.

Detailed results, printed after running, looks like this:

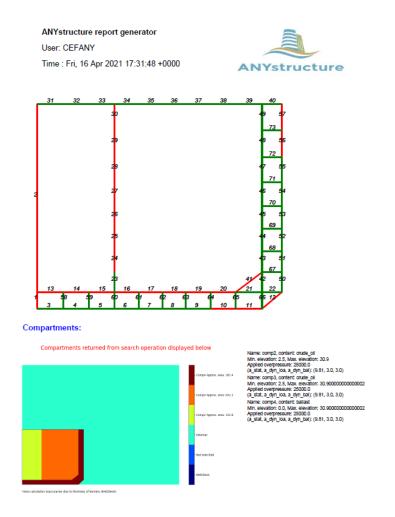
Plate fields: 22 Frames: 10 pl\_650.0x14.0 stf\_L180.0x8.0+33.0x17.8 span: 1.0636 structure type: BOTTOM stf. type: L pressure side: p | sigma\_y1: 128.6 sigma\_y2: 128.6 sigma\_x: 177.9 tauxy: 6.4 START 1 OK! pl\_650.0x14.0 stf\_L180.0x8.0+33.0x17.8 span: 1.0636 structure type: BOTTOM stf. type: L pressure side: p | sigma\_y1: 128.6 sigma\_y2: 128.6 sigma\_x: 177.9 tauxy: 6.4 ------ OK! pl\_650.0x14.0 stf\_L180.0x8.0+33.0x17.8 span: 1.0636 structure type: BOTTOM stf. type: L pressure side: p | sigma\_y1: 128.6 sigma\_y2: 128.6 sigma\_x: 177.9 tauxy: 6.4 ------ OK! pl\_650.0x14.0 stf\_L180.0x8.0+33.0x17.8 span: 1.0636 structure type: BOTTOM stf. type: L pressure side: p | sigma\_y1: 128.6 sigma\_y2: 128.6 sigma\_x: 177.9 tauxy: 6.4 ----- OK! pl\_650.0x14.0 stf\_L180.0x8.0+33.0x17.8 span: 1.0636 structure type: BOTTOM stf. type: L pressure side: p | sigma\_y1: 128.6 sigma\_y2: 128.6 sigma\_x: 177.9 tauxy: 6.4 ------ OK! pl\_650.0x14.0 stf\_L180.0x8.0+33.0x17.8 span: 1.0636 structure type: BOTTOM stf. type: L pressure side: p sigma\_y1: 128.6 sigma\_y2: 128.6 sigma\_x: 177.9 tauxy: 6.4 ----- OK! pl\_650.0x14.0 stf\_L180.0x8.0+33.0x17.8 span: 1.0636 structure type: BOTTOM stf. type: L pressure side: p | sigma\_y1: 128.6 sigma\_y2: 128.6 sigma\_x: 177.9 tauxy: 6.4 ------ OK! pl\_650.0x14.0 stf\_L180.0x8.0+33.0x17.8 span: 1.0636 structure type: BOTTOM stf. type: L pressure side: p | sigma\_y1: 128.6 sigma\_y2: 128.6 sigma\_x: 177.9 tauxy: 6.4 ------ OK! pl\_650.0x14.0 stf\_L180.0x8.0+33.0x17.8 span: 1.0636 structure type: BOTTOM stf. type: L pressure side: p | sigma\_y1: 128.6 sigma\_y2: 128.6 sigma\_x: 177.9 tauxy: 6.4 ------ OK! pl 650.0x14.0 stf L160.0x8.0+36.0x18.7 span: 1.0636 structure type: BOTTOM stf. type: L pressure side: p | sigma\_y1: 128.6 sigma\_y2: 128.6 sigma\_x: 174.9 tauxy: 6.4 ------ OK! pl\_650.0x14.0 stf\_l160.0x8.0+36.0x18.7 span: 1.0636 structure type: BOTION stf. type: L pressure side: p | sigma\_y1: 128.6 sigma\_x: 170.0 tauxy: 6.4 -END 1 - OK! pl\_750.0x14.0 stf\_l160.0x8.0+36.0x18.7 span: 1.0636 structure type: GENERAL\_INTERNAL\_WT stf. type: L pressure side: p | sigma\_y1: 115.7 sigma\_y2: 115.7 sigma\_y2: 115.7 sigma\_x: 144.9 tauxy: 6.4 START 2 OK! pl\_750.0x14.0 stf\_l160.0x8.0+36.0x18.7 span: 1.0636 structure type: GENERAL\_INTERNAL\_WT stf. type: L pressure side: p | sigma\_y1: 115.7 sigma\_y2: 115.7 sigma\_x: 144.9 tauxy: 6.4 ------ OK! pl\_750.0x14.0 stf\_1160.0x8.0+36.0x18.7 span: 1.0636 structure type: GENERAL\_INTERNAL\_WT stf. type: L pressure side: p | sigma\_y1: 115.7 sigma\_x: 144.9 tauxy: 6.4 ------ OK| pl\_750.0x14.0 stf\_1160.0x8.0+36.0x18.7 span: 1.0636 structure type: GENERAL\_INTERNAL\_WT stf. type: L pressure side: p | sigma\_y1: 115.7 sigma\_x: 144.9 tauxy: 6.4 ------ OK| pl\_750.0x14.0 stf\_1160.0x8.0+36.0x18.7 span: 1.0636 structure type: GENERAL\_INTERNAL\_WT stf. type: L pressure side: p | sigma\_y1: 115.7 sigma\_y2: 115.7 sigma\_x: 144.9 tauxy: 6.4 ------ OK| pl\_750.0x14.0 stf\_1160.0x8.0+36.0x18.7 span: 1.0636 structure type: GENERAL\_INTERNAL\_WT stf. type: L pressure side: p | sigma\_y1: 115.7 sigma\_x: 144.9 tauxy: 6.4 ------ OK| pl\_750.0x14.0 stf\_1160.0x8.0+36.0x18.7 span: 1.0636 structure type: GENERAL\_INTERNAL\_WT stf. type: L pressure side: p | sigma\_y1: 115.7 sigma\_x: 144.9 tauxy: 6.4 ------ OK| pl\_750.0x14.0 stf\_L160.0x8.0+36.0x18.7 span: 1.0636 structure type: GENERAL\_INTERNAL\_WT stf. type: L pressure side: p | sigma\_y1: 115.7 sigma\_y2: 115.7 sigma\_x: 144.9 tauxy: 6.4 ------ OK| pl\_750.0x14.0 stf\_L160.0x8.0+36.0x18.7 span: 1.0636 structure type: GENERAL\_INTERNAL\_WT stf. type: L pressure side: p | sigma\_y1: 115.7 sigma\_y2: 115.7 sigma\_x: 144.9 tauxy: 6.4 ------ OK| pl\_750.0x14.0 stf\_L160.0x8.0+36.0x18.7 span: 1.0636 structure type: GENERAL\_INTERNAL\_WT stf. type: L pressure side: p | sigma\_y1: 115.7 sigma\_y2: 115.7 sigma\_x: 144.9 tauxy: 6.4 ------ OK| pl\_750.0x14.0 stf\_L160.0x8.0+36.0x18.7 span: 1.0636 structure type: GENERAL\_INTERNAL\_WT stf. type: L pressure side: p | sigma\_y1: 115.7 sigma\_y2: 115.7 sigma\_x: 144.9 tauxy: 6.4 ------ OK! pl 750.0x14.0 stf L160.0x8.0+36.0x18.7 span: 1.0636 structure type: GENERAL\_INTERNAL\_WT stf. type: L pressure side: p | sigma\_y1: 115.7 sigma\_y2: 115.7 sigma\_x: 144.9 tauxy: 6.4 -END 2- OK! Weight details for this solution: Weight of main structure: ['1423.0', '1423.0', '1423.0', '1423.0', '1423.0', '1423.0', '1423.0', '1423.0', '1423.0', '1423.0', '1423.0', '1423.0', '1423.0', '1423.0', '1423.0', '1423.0', '1413.8', '1381.1',

# Reporting



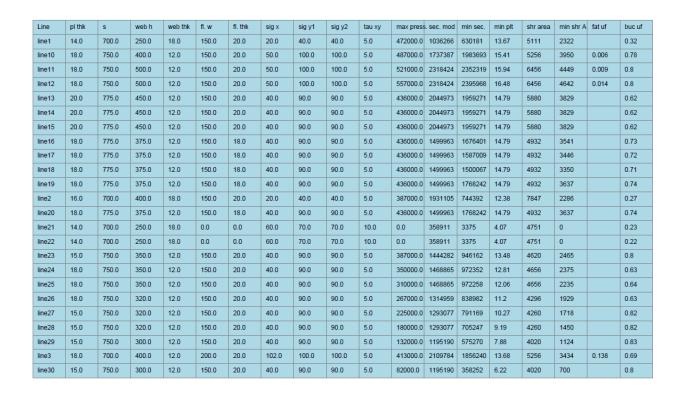
#### General

A pdf report can be created by clicking "Reporting - Generate PDF report". The report will include all information for all lines. An example is seen next.



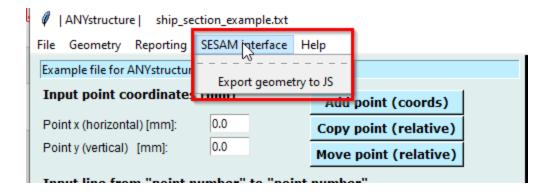
#### **Table**

A report in table format can be created using "Generate PDF result table". This report is a compressed version of all results.

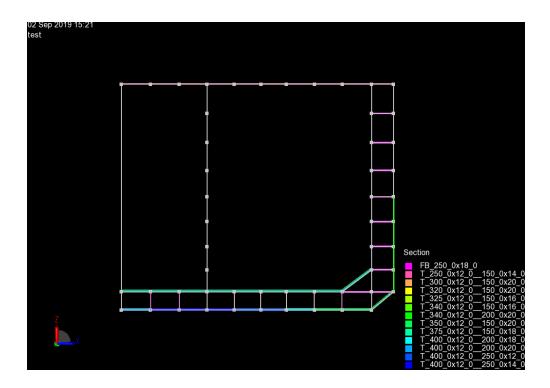


# Export to JS

ANYstructure can export points, lines and section properties to SESAM GeniE. A dialog will request a location to save the JS file. After that you can read the js file into GeniE.



The result is illustrated next:



# Changing the GUI

Various GUI modifications can be selected as seen next.

