

Electronic Circuits

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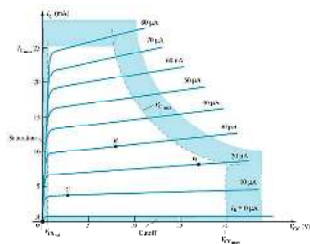
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Biassing

Biassing: The DC voltages applied to a transistor in order to turn it on so that it can amplify the AC signal.

Operating Point

The DC input establishes an operating or *quiescent point* called the **Q-point**.



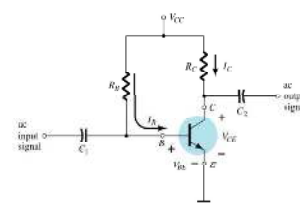
The Three States of Operation

- **Active or Linear Region Operation**
Base-Emitter junction is forward biased
Base-Collector junction is reverse biased
- **Cutoff Region Operation**
Base-Emitter junction is reverse biased
- **Saturation Region Operation**
Base-Emitter junction is forward biased
Base-Collector junction is forward biased

DC Biasing Circuits

- Fixed-bias circuit
- Emitter-stabilized bias circuit
- Collector-emitter loop
- Voltage divider bias circuit
- DC bias with voltage feedback

Fixed Bias



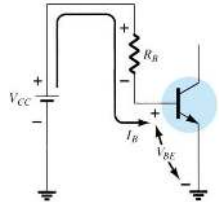
The Base-Emitter Loop

From Kirchhoff's voltage law:

$$+V_{CC} - I_B R_B - V_{BE} = 0$$

Solving for base current:

$$I_B = \frac{V_{CC} - V_{BE}}{R_B}$$



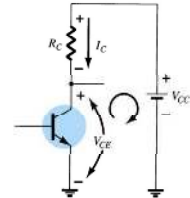
Collector-Emitter Loop

Collector current:

$$I_C = \beta I_B$$

From Kirchhoff's voltage law:

$$V_{CE} = V_{CC} - I_C R_C$$



Saturation

When the transistor is operating in saturation, current through the transistor is at its *maximum* possible value.

$$I_{Csat} = \frac{V_{CC}}{R_C}$$

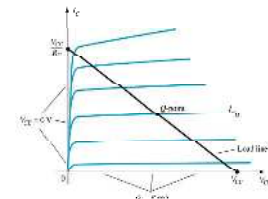
$$V_{CE} \approx 0 \text{ V}$$

Load Line Analysis

The end points of the load line are:

$$I_{Csat} \\ I_C = V_{CC} / R_C \\ V_{CE} = 0 \text{ V}$$

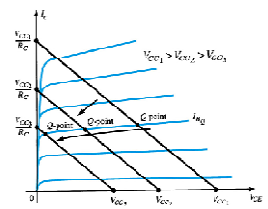
$$V_{CEcutoff} \\ V_{CE} = V_{CC} \\ I_C = 0 \text{ mA}$$



The *Q*-point is the operating point:

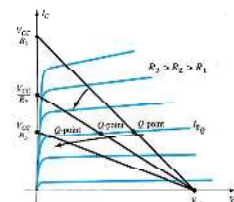
- where the value of R_B sets the value of I_B
- that sets the values of V_{CE} and I_C

Circuit Values Affect the Q-Point



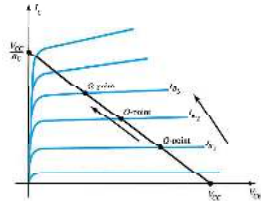
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Circuit Values Affect the Q-Point



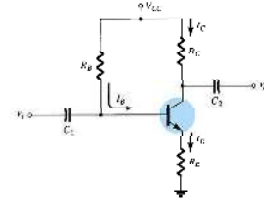
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Circuit Values Affect the Q-Point



Emitter-Stabilized Bias Circuit

Adding a resistor (R_E) to the emitter circuit stabilizes the bias circuit.



Base-Emitter Loop

From Kirchhoff's voltage law:

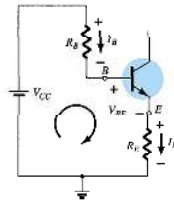
$$+V_{CC} - I_E R_E - V_{BE} - I_E R_E = 0$$

Since $I_E = (\beta + 1)I_B$:

$$V_{CC} - I_B R_B - (\beta + 1)I_B R_E = 0$$

Solving for I_B :

$$I_B = \frac{V_{CC} - V_{BE}}{R_B + (\beta + 1)R_E}$$



Collector-Emitter Loop

From Kirchhoff's voltage law:

$$I_E R_E + V_{CE} + I_C R_C - V_{CC} = 0$$

Since $I_E \cong I_C$:

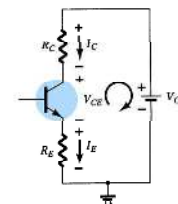
$$V_{CE} = V_{CC} - I_C(R_C + R_E)$$

Also:

$$V_E = I_E R_E$$

$$V_C = V_{CE} + V_E = V_{CC} - I_C R_C$$

$$V_B = V_{CC} - I_B R_B = V_{BE} + V_E$$

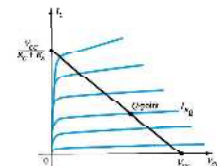
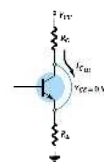


Improved Biased Stability

Stability refers to a circuit condition in which the currents and voltages will remain fairly constant over a wide range of temperatures and transistor Beta (β) values.

Adding R_E to the emitter improves the stability of a transistor.

Saturation Level



The endpoints can be determined from the load line.

$V_{CE\text{cutoff}}:$

$$V_{CE} = V_{CC}$$

$$I_C = 0 \text{ mA}$$

$I_{C\text{sat}}:$

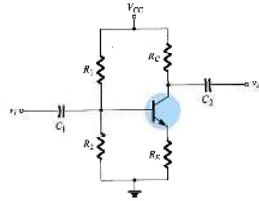
$$V_{CE} = 0 \text{ V}$$

$$I_C = \frac{V_{CC}}{R_C + R_E}$$

Voltage Divider Bias

This is a very stable bias circuit.

The currents and voltages are nearly independent of any variations in β .



Approximate Analysis

Where $I_B \ll I_1$ and $I_1 \cong I_2$:

$$V_B = \frac{R_2 V_{CC}}{R_1 + R_2}$$

Where $\beta R_E > 10R_2$:

$$I_E = \frac{V_E}{R_E}$$

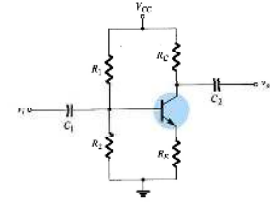
$$V_E = V_B - V_{BE}$$

From Kirchhoff's voltage law:

$$V_{CE} = V_{CC} - I_C R_C - I_E R_E$$

$$I_E \cong I_C$$

$$V_{CE} = V_{CC} - I_C (R_C + R_E)$$



Voltage Divider Bias Analysis

Transistor Saturation Level

$$I_{Csat} = I_{Cmax} = \frac{V_{CC}}{R_C + R_E}$$

Load Line Analysis

Cutoff:

$$V_{CE} = V_{CC}$$

$$I_C = 0 \text{ mA}$$

Saturation:

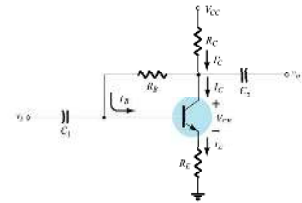
$$I_C = \frac{V_{CC}}{R_C + R_E}$$

$$V_{CE} = 0 \text{ V}$$

DC Bias with Voltage Feedback

Another way to improve the stability of a bias circuit is to add a feedback path from collector to base.

In this bias circuit the Q-point is only slightly dependent on the transistor beta, β .



Base-Emitter Loop

From Kirchhoff's voltage law:

$$V_{CC} - I_C' R_C - I_B R_B - V_{BE} - I_E R_E = 0$$

Where $I_B \ll I_C$:

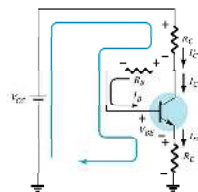
$$I_C' = I_C + I_B \cong I_C$$

Knowing $I_C = \beta I_B$ and $I_E \cong I_C$, the loop equation becomes:

$$V_{CC} - \beta I_B R_C - I_B R_B - V_{BE} - \beta I_B R_E = 0$$

Solving for I_B :

$$I_B = \frac{V_{CC} - V_{BE}}{R_B + \beta(R_C + R_E)}$$



Collector-Emitter Loop

Applying Kirchhoff's voltage law:

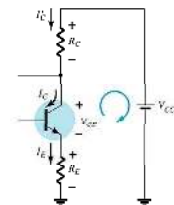
$$I_E + V_{CE} + I_C' R_C - V_{CC} = 0$$

Since $I_C' \cong I_C$ and $I_C = \beta I_B$:

$$I_C (R_C + R_E) + V_{CE} - V_{CC} = 0$$

Solving for V_{CE} :

$$V_{CE} = V_{CC} - I_C (R_C + R_E)$$



Base-Emitter Bias Analysis

Transistor Saturation Level

$$I_{Csat} = I_{Cmax} = \frac{V_{CC}}{R_C + R_E}$$

Load Line Analysis

Cutoff:

$$V_{CE} = V_{CC}$$

$$I_C = 0 \text{ mA}$$

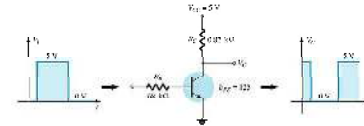
Saturation:

$$I_C = \frac{V_{CC}}{R_C + R_E}$$

$$V_{CE} = 0 \text{ V}$$

Transistor Switching Networks

Transistors with only the DC source applied can be used as electronic switches.



Switching Circuit Calculations

Saturation current:

$$I_{Csat} = \frac{V_{CC}}{R_C}$$

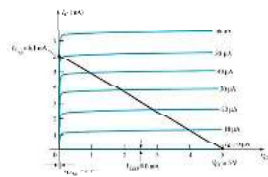
To ensure saturation:

$$I_B > \frac{I_{Csat}}{\beta_{dc}}$$

Emitter-collector resistance at saturation and cutoff:

$$R_{sat} = \frac{V_{CEsat}}{I_{Csat}}$$

$$R_{cutoff} = \frac{V_{CC}}{I_{CEO}}$$

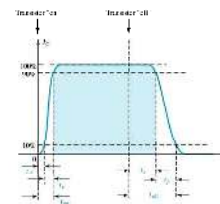


Switching Time

Transistor switching times:

$$t_{on} = t_r + t_d$$

$$t_{off} = t_s + t_f$$



Troubleshooting Hints

- Approximate voltages
 - $V_{BE} \approx 0.7 \text{ V}$ for silicon transistors
 - $V_{CE} \approx 25\% \text{ to } 75\% \text{ of } V_{CC}$
- Test for opens and shorts with an ohmmeter.
- Test the solder joints.
- Test the transistor with a transistor tester or a curve tracer.
- Note that the load or the next stage affects the transistor operation.

PNP Transistors

The analysis for *pnp* transistor biasing circuits is the same as that for *npn* transistor circuits. The only difference is that the currents are flowing in the opposite direction.