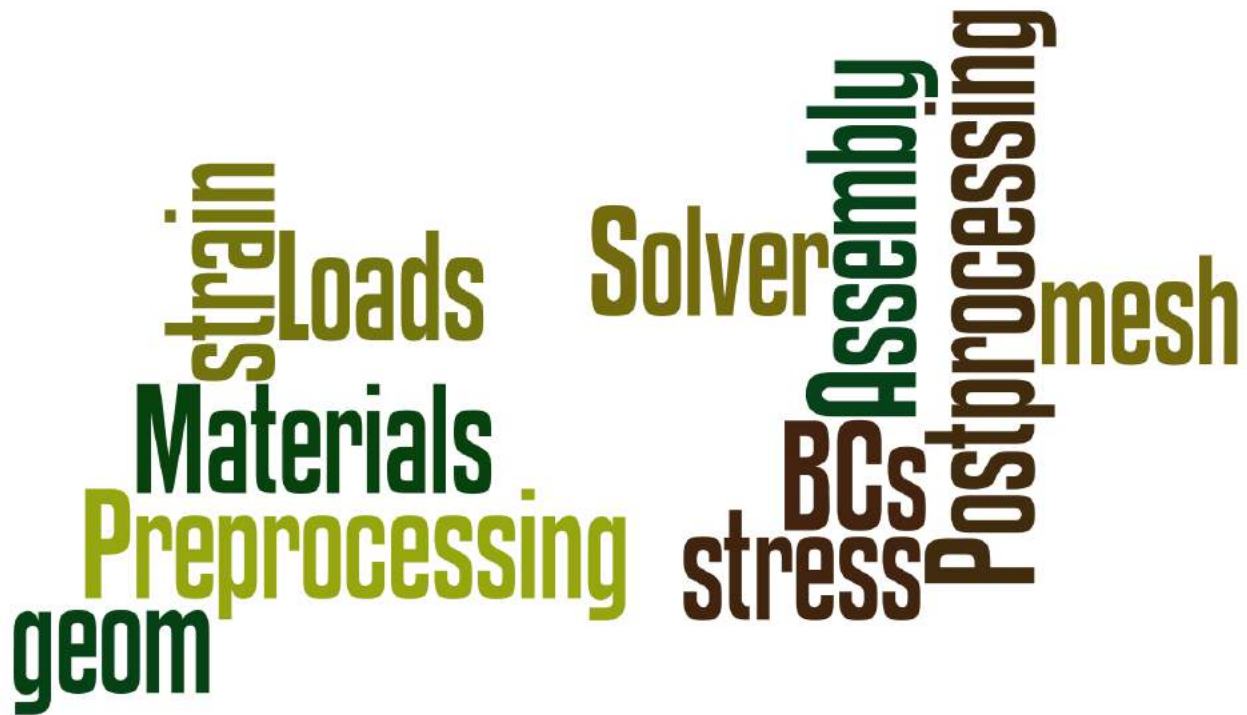
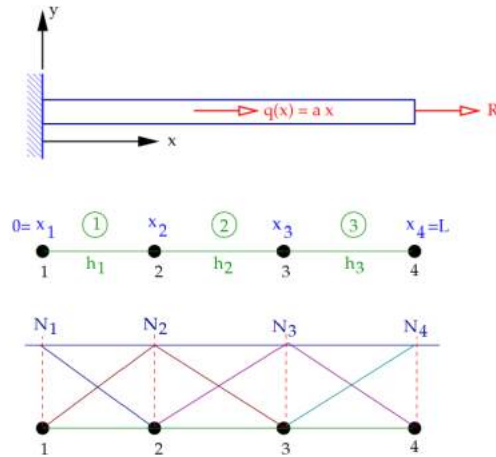


1MAE701 Exercices to be done/started in class

C1: Complete a simple FEA code



Fill the comments with above pictures wordles , specify the units

Copy paste part of the code in the ?? at the right place

B*u	[-1/h 1/h]	inv(Kred)*fred	(A*E/h)*[[1 -1];[-1 1]]	E*eps
-----	------------	----------------	-------------------------	-------

```

function AxialBarFEM
%
%Material and Length
%
    A = 1.0; %cross section mm2
    L = 1.0; %length mm2
    E = 1.0; %Young's modulus MPa (N/mm2)
%loads
    a = 1.0; %distributed force N.m
    R = 1.0; %Force (N)

%
%Prepostfem mesh
%
    e = 3;
    h = L/e;
    n = e+1;

    for i=1:n
        node(i) = (i-1)*h;
    end
    for i=1:e
        elem(i,:) = [i i+1];
    end

%
%Assembly
%
    K = zeros(n);
    f = zeros(n,1);
    for i=1:e
        node1 = elem(i,1);
        node2 = elem(i,2);
        Ke = elementStiffness(A, E, h);
        fe =
elementLoad(node(node1),node(node2), a, h);
        K(node1:node2,node1:node2) =
K(node1:node2,node1:node2) + Ke;
        f(node1:node2) = f(node1:node2) + fe;
    end

%
%BCs &Loads
%
    f(n) = f(n) + 1.0;
    Kred = K(2:n,2:n);
    fred = f(2:n);

%
%Solvers
%
    d = ??;
    dsol = [0 d']; %known solution at x=0
    fsol = K*dsol';
    sum(fsol)

%
%Postprocessing
%
    figure;
    p0 = plotDisp(E, A, L, R, a);
    p1 = plot(node, dsol, 'ro--',
'LineWidth', 3); hold on;
    legend([p0 p1], 'Exact', 'FEM');

    for i=1:e
        node1 = elem(i,1);
        node2 = elem(i,2);
        u1 = dsol(node1);
        u2 = dsol(node2);
        [eps(i), sig(i)] =
elementStrainStress(u1, u2, E, h);

```

```

end

figure;
p0 = plotStress(E, A, L, R, a);
for i=1:e
    node1 = node(elem(i,1));
    node2 = node(elem(i,2));
    p1 = plot([node1 node2], [sig(i)
sig(i)], 'r-', 'LineWidth', 3); hold on;
end
legend([p0 p1], 'Exact', 'FEM');

function [p] = plotDisp(E, A, L, R, a)
    dx = 0.01;
    nseg = L/dx;
    for i=1:nseg+1
        x(i) = (i-1)*dx;
        u(i) = (1/6*A*E)*(-a*x(i)^3 + (6*R +
3*a*L^2)*x(i));
    end
    p = plot(x, u, 'LineWidth', 3); hold
on;
    xlabel('x', 'FontName', 'palatino',
'FontSize', 18);
    ylabel('u(x)', 'FontName', 'palatino',
'FontSize', 18);
    set(gca, 'LineWidth', 3, 'FontName',
'palatino', 'FontSize', 18);

function [p] = plotStress(E, A, L, R, a)
    dx = 0.01;
    nseg = L/dx;
    for i=1:nseg+1
        x(i) = (i-1)*dx;
        sig(i) = (1/2*A*E)*(-a*x(i)^2 + (2*R
+ a*L^2));
    end
    p = plot(x, sig, 'LineWidth', 3); hold
on;
    xlabel('x', 'FontName', 'palatino',
'FontSize', 18);
    ylabel('\sigma(x)', 'FontName',
'palatino', 'FontSize', 18);
    set(gca, 'LineWidth', 3, 'FontName',
'palatino', 'FontSize', 18);

function [Ke] = elementStiffness(A, E, h)

    Ke = ??;

function [fe] = elementLoad(node1, node2,
a, h)
    x1 = node1;
    x2 = node2;
    fe1 = a*x2/(2*h)*(x2^2-x1^2) -
a/(3*h)*(x2^3-x1^3);
    fe2 = -a*x1/(2*h)*(x2^2-x1^2) +
a/(3*h)*(x2^3-x1^3);
    fe = [fe1;fe2];

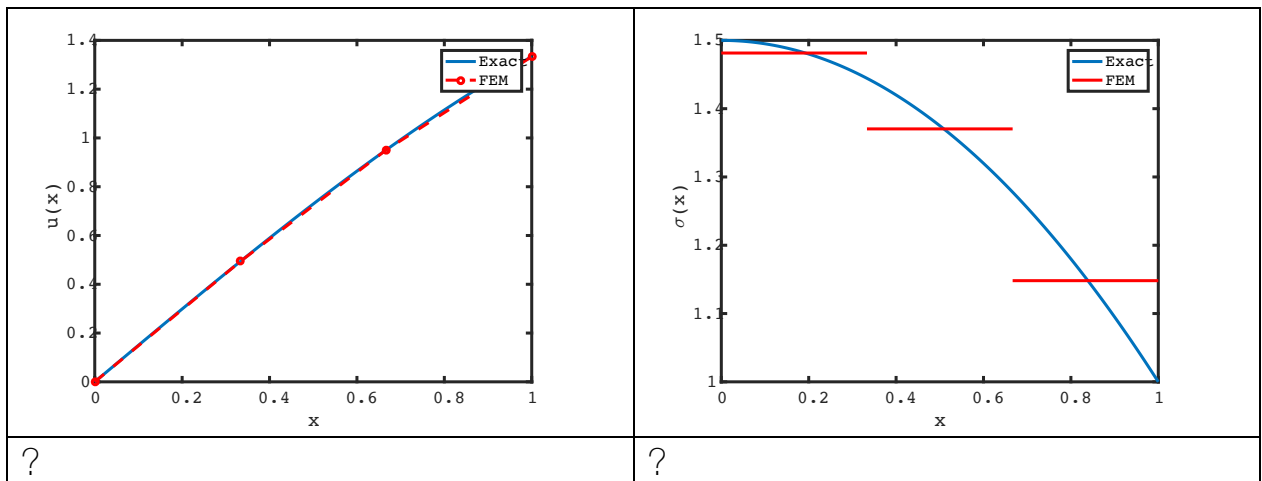
function [eps, sig] =
elementStrainStress(u1, u2, E, h)

    B = ??
    u = [u1; u2];
    eps = ??
    sig = ??;

```

Please also comment some lines %? And the results under

Play with e. Conclude



C2: Fill up a more “complex” FEA code* publish needed on LMS by pair

A cantilever beam of length $L_p = 3$ m and define by a squared section of area $A_p = 30 \times 30$ cm².
The BCs are C-F, and the vertical load is imposed at the free boundary conditions such as $F_0 = 75$ kN.
The materials used is concrete of Young's modulus $E_b = 32000$ MPa.

Matlab will help you A LOT to accelerate learning and deepen understanding. The prof wants that you zip your publish or livescript with m files and upload on LMS.

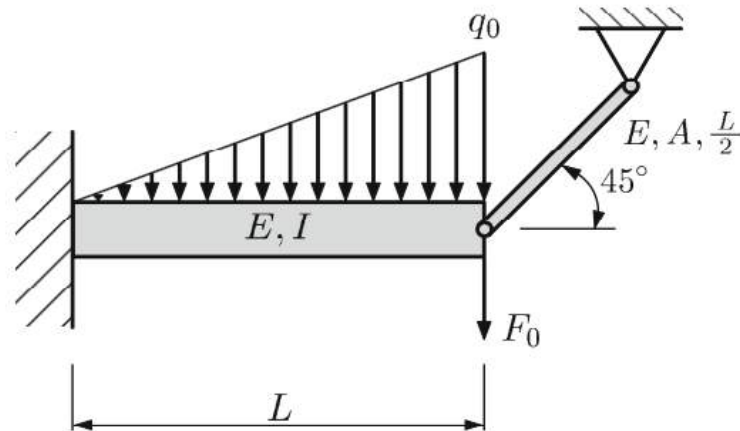


FIGURE 1: STRUCTURE TO BE DISCRETIZED USING 1 BEAM AND 1 BAR ELEMENT

Part 1 : Cantilever ONLY with Load case F_0

- 1) You can then compute the analytical beam deflection (to check)
- 2) Compute the rigidity matrix K_p and handwrite the system of equations respecting the nodes of figure above
- 3) Apply the BC Cantilever and solve the reduced system. Check using Matlab the solution and the resultant forces at the BC using the file “assignment2_student.m” on LMS

Part 2 : Cantilever beam+ inclined bar with the 2 load cases

The free end of the beam is connected to an inclined steel bar as shown in the figure1.

The section of the bar is $A_b = 25$ cm² and the modulus of elasticity of the steel is $E_s = 200000$ MPa.

- 0) Compute first the equivalent load for q_0 with $\max(q_0) = 10$ kN
- 1) Calculate the stiffness matrix K_b of the inclined bar, taking into account the degrees of freedom of transverse displacement and rotation.
- 2) Introduce the axial displacement into the stiffness matrix K_p of the beam.
- 3) Assemble the two matrices K_b and K_p according to the numbering of the nodes given in the figure and write the global force vector (for all nodes of the structure).
- 4) Apply the boundary conditions and write the system of equations to solve.
- 5) Solve the system and give the displacements and rotations of the nodes. Check reactions
- 6) Calculate the axial force in the bar and the beam.

A SMALL HELP

CONCEPTS OF GAUSSIAN INTEGRATION

In Gaussian integration, also called Gaussian quadrature, the integral of a function in natural coordinates is substituted by an equivalent sum of this function evaluated at special points multiplied by a corresponding weight. Commonly, these special points are referred to as sampling points ξ_i .

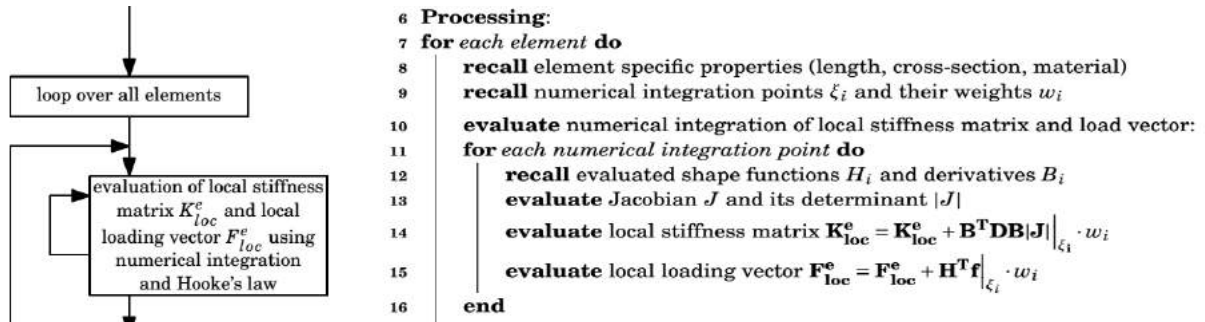
$$\int_{-1}^1 F(\xi) d\xi = \sum_{i=1}^{NG} w_i F(\xi_i)$$

Although there is usually an error term associated with numerical integration, Gaussian quadrature has been shown to yield exact results for polynomials of degree $2m-1$ or lower, where m is equal to the amount of weights / sampling points. This case directly applied to the common shape functions and their associated derivatives. Below is a table summarizing the position of the sampling points for Gaussian quadrature and their associated weights.

rule	point	coordinate	numerical value	weight	numerical value	order
1 point	1	0	0.000000000	2	2.000000000	1
2 points	1	$-\sqrt{\frac{1}{3}}$	-0.5773502692	1	1.000000000	3
	2	$\sqrt{\frac{1}{3}}$	0.5773502692	1	1.000000000	
3 points	1	$-\sqrt{\frac{3}{5}}$	-0.7745966692	$\frac{5}{9}$	0.5555555556	5
	2	0	0.000000000	$\frac{8}{9}$	0.888888889	
	3	$\sqrt{\frac{3}{5}}$	0.7745966692	$\frac{5}{9}$	0.5555555556	
4 points	1	$-\sqrt{\frac{3+2\sqrt{\frac{6}{5}}}{7}}$	-0.8611363116	$\frac{18-\sqrt{30}}{36}$	0.3478548452	7
	2	$-\sqrt{\frac{3-2\sqrt{\frac{6}{5}}}{7}}$	-0.3399810436	$\frac{18+\sqrt{30}}{36}$	0.6521451548	
	3	$\sqrt{\frac{3-2\sqrt{\frac{6}{5}}}{7}}$	0.3399810436	$\frac{18+\sqrt{30}}{36}$	0.6521451548	
	4	$\sqrt{\frac{3+2\sqrt{\frac{6}{5}}}{7}}$	0.8611363116	$\frac{18-\sqrt{30}}{36}$	0.3478548452	

SAMPLING POINTS AND CORRESPONDING WEIGHTS FOR GAUSSIAN QUADRATURE

PSEUDO CODE FOR IMPLEMENTATION IN A FINITE ELEMENT SOFTWARE



PSEUDO CODE FOR NUMERICAL INTEGRATION WITHIN A FINITE ELEMENT SOFTWARE

EXPECTED RESULTS

After first summation

K_local					F_local	
4x4 double					4x1 doub	
	1	2	3	4		1
1	27.6000	43.5349	-27.6000	11.6651	1	8.8490
2	43.5349	68.6697	-43.5349	18.4000	2	2.6289
3	-27.6000	-43.5349	27.6000	-11.6651	3	1.1510
4	11.6651	18.4000	-11.6651	4.9303	4	-0.7044

After second summation

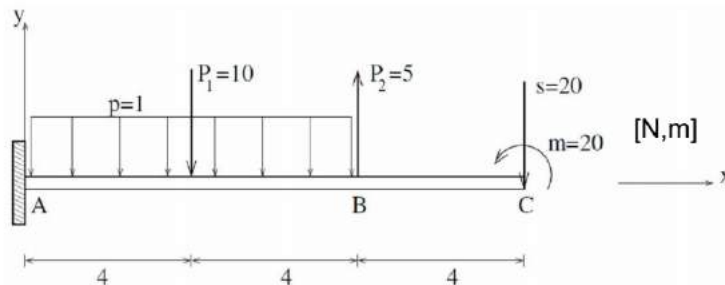
K_local					F_local	
4x4 double					4x1 doub	
	1	2	3	4		1
1	55.2000	55.2000	-55.2000	55.2000	1	10
2	55.2000	73.6000	-55.2000	36.8000	2	3.3333
3	-55.2000	-55.2000	55.2000	-55.2000	3	10
4	55.2000	36.8000	-55.2000	73.6000	4	-3.3333

SOLVING A SAMPLE PROBLEM

Given the following sample beam, find the displacements, moments and shear forces across the beam. Modify your numerical integration method slightly to work within a skeletal finite element program provided, for both the integration of the stiffness matrix as well as the force vector.

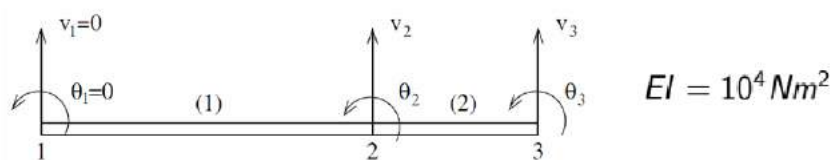
Take a look at the skeletal finite element code provided and complete the sections marked with comments in the code. Some intermediate results are provided below.

Analytical model:



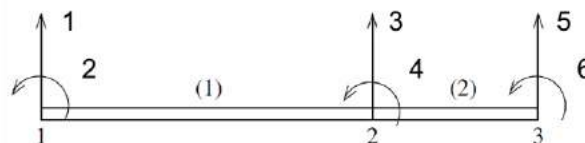
Definition of:

Nodes, Elements, Boundary Conditions and Material properties, etc.



Assign:

DOF identifiers



Some intermediate results are the following:

K_local = (Beam 1)

	1	2	3	4
1	234.3750	937.5000	-234.3750	937.5000
2	937.5000	5.0000e+03	-937.5000	2.5000e+03
3	-234.3750	-937.5000	234.3750	-937.5000
4	937.5000	2.5000e+03	-937.5000	5.0000e+03

K_local = (Beam 2)

	1	2	3	4
1	1.8750e+03	3.7500e+03	-1.8750e+03	3.7500e+03
2	3.7500e+03	1.0000e+04	-3.7500e+03	5.0000e+03
3	-1.8750e+03	-3.7500e+03	1.8750e+03	-3.7500e+03
4	3.7500e+03	5.0000e+03	-3.7500e+03	1.0000e+04

K_system =

	1	2	3	4	5	6
1	234.3750	937.5000	-234.3750	937.5000	0	0
2	937.5000	5.0000e+03	-937.5000	2.5000e+03	0	0
3	-234.3750	-937.5000	2.1094e+03	2.8125e+03	-1.8750e+03	3.7500e+03
4	937.5000	2.5000e+03	2.8125e+03	1.5000e+04	-3.7500e+03	5.0000e+03
5	0	0	-1.8750e+03	-3.7500e+03	1.8750e+03	-3.7500e+03
6	0	0	3.7500e+03	5.0000e+03	-3.7500e+03	1.0000e+04

F_local = (distributed load)

	1
1	-4
2	-5.3333
3	-4
4	5.3333

F_local = (point load)

	1
1	-5
2	-10
3	-5
4	10

F_system_element = (point and distributed load)

	1	2
1	-9	
2	-15.3333	
3	-9	
4	15.3333	
5	0	
6	0	

F_system_nodal = (all nodal loads)

	1	2
1	0	
2	0	
3	5	
4	0	
5	-20	
6	20	

F_system =

	1	2
1	-9	
2	-15.3333	
3	-4	
4	15.3333	
5	-20	
6	20	

d_system =

	1
1	0
2	0
3	-0.5525
4	-0.1125
5	-1.0293
6	-0.1205

C3: Approximation & Gauss Quadrature

Exercise 1

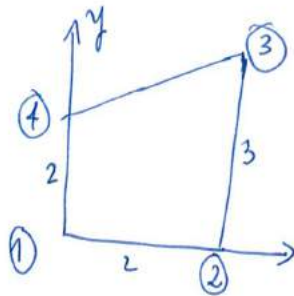
Integrate numerically $f(x) = e^x$ on $[0, 6]$
using Gauss quadrature. compare with 'trapz', 'quad'
Matlab's functions

$$\int_0^6 e^x dx = e^x \Big|_0^6 = e^6 - e^0 = e^6 - 1 \approx 402.43$$

exact solution (see WOLFRAM α)

Compute the relative errors with exact solution

Exercise 2



Evaluate the integral $I = \iint_A (x^2 + y) dx dy$
over the quadrilateral shown.

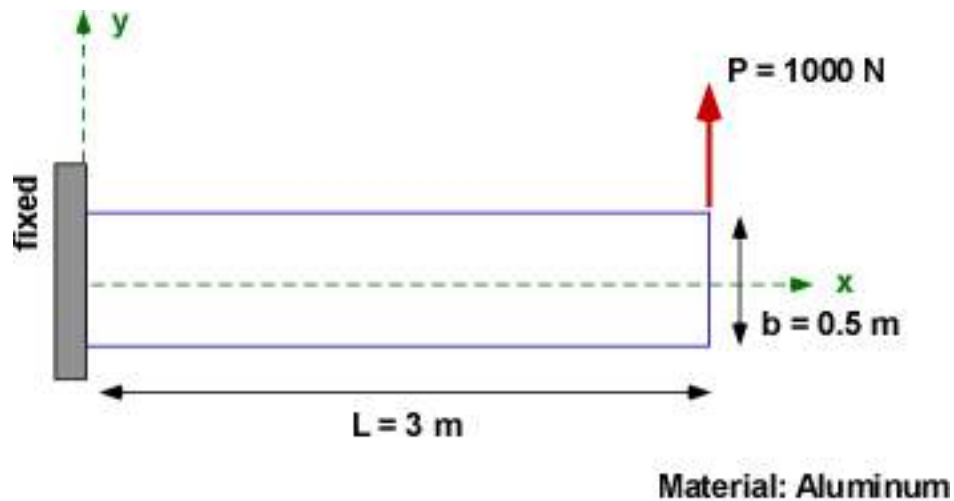
$$\text{corners: } x^T = [0 \ 2 \ 2 \ 0] ; \ y^T = [0 \ 0 \ 3 \ 2]$$

Using the function gaussQuad.m, find the optimal gauss points to reach tolerance 1E-4 for abs(I_exact - I_gauss)

C4: Play with a more “complex” FEA code* publish needed on LMS by pair

Using MATLAB PDE Toolbox

For **elliptical PDEs**, MATLAB provides you with a graphical tool that uses finite elements to solve the problem. However it is available only through the **Partial Differential Equation Toolbox**. The tool is started from the command line with the command ***pdetool***. This is graphical user interface (GUI) tool and requires you to follow a sequence of steps. Knowledge of finite elements is useful. We will use it as a tool to solve the 2D Elasticity problem shown below:



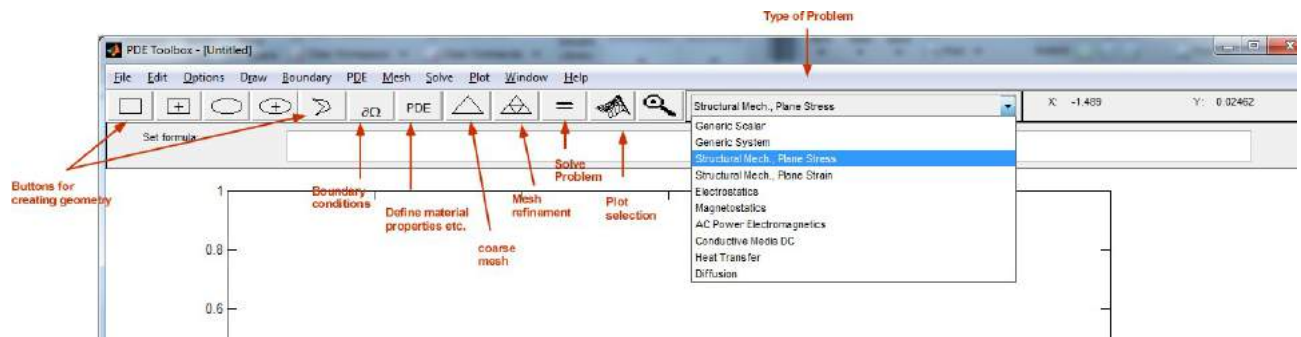
Thickness a is 1m.

The various steps in sequence of applying FEM is detailed below. It should be sufficient to get you started and solve similar problems as long as you remember to do it in sequence. I think the GUI makes it quite painless and interesting and that should be motivation enough.

We will be using the *pdetool* and therefore there is no code for solving this problem. Navigating the tool is through icons or the menu. Our problem is simple and we will use mainly the icons in the following. At the command prompt launch the tool

>> pdetool

Use the drop down menu and choose the Type of Problem : Plane Stress



Like many applications you should see a window with a menu on top, a list of icons below it, a line for formula entry, and a rectangular region for the problem.

Let us setup the problem. Remember you are solving for the displacements. You can get strain and stress from that solution.

Step 1 (Use menu to define problem region)

Options → Axes Limits (slightly more than our rectangle) Set X-axis range [-0.5 3.5]

Set Y-axis range [-0.5 1.0]

Options → Grid (Draw grid) Options → Snap

Click on Rectangle icon

Use mouse to draw rectangle

Click at (0,0.5) and press and drag to (3,0)

Step 2 (Set Boundary condition)

Boundary → remove all subdomain boundaries Click boundary conditions button

(i) Left Edge - Double click left edge (or $x = 0$ edge). There is no displacement ($u = v = 0$). Remember u in the figure below is the vector of u and v . We will use the Dirichlet Boundary condition.

Boundary Condition

Boundary condition equation: $h*u=r$

Condition type:	Coefficient	Value	Description
<input type="radio"/> Neumann	g1	0	Surface tractions
<input checked="" type="radio"/> Dirichlet	g2	0	"
<input type="radio"/> Mixed	q11, q12	0 0	Spring constants
	q21, q22	0 0	"
	h11, h12	1 0	Weights
	h21, h22	0 1	"
	r1	0	Displacements
	r2	0	"

OK Cancel

(ii) Right Boundary: This carries the load P. You cannot set up a point load. You have to specify it as a traction force - or Force/Area on the edge. That is $P/b = 2000$ N. We have to specify traction using the Neumann boundary condition

Double click right edge (or $x = 3$ edge)

Boundary Condition

Boundary condition equation: $n*c*grad(u)+q*u=g$

Condition type:	Coefficient	Value	Description
<input checked="" type="radio"/> Neumann	g1	0	Surface tractions
<input type="radio"/> Dirichlet	g2	2000	"
<input type="radio"/> Mixed	q11, q12	0 0	Spring constants
	q21, q22	0 0	"
	h11, h12	1 0	Weights
	h21, h22	0 1	"
	r1	0	Displacements
	r2	0	"

OK Cancel

(iii) Top Edge ($y = 0.5$) . All traction are zero. Use Neumann to accept default values

Boundary condition equation: $n \cdot c \cdot \text{grad}(u) + q \cdot u = g$

Condition type:	Coefficient	Value	Description
<input checked="" type="radio"/> Neumann			
<input type="radio"/> Dirichlet			
<input type="radio"/> Mixed			
	g1	0	Surface tractions
	g2	0	"
	q11, q12	0 0	Spring constants
	q21, q22	0 0	"
	h11, h12	1 0	Weights
	h21, h22	0 1	"
	r1	0	Displacements
	r2	0	"

OK Cancel

(iv) Same for Bottom edge

Step 3. Click on the PDE button to set the material properties for Aluminum

density = 2710 kg/m^3

Modulus of Elasticity (E) = 70 GPa Modulus of rigidity (G) = 26 GPa

Poisson ratio (ν) : calculate from $G = E/(2(1 + \nu))$

Step 4. Mesh the domain (default meshes) Click on coarse mesh

Refine the mesh twice

This program only uses triangular meshes or elements

Step 5 (Solve the problem) Click on = icon

You will see the solution. We will change the plot properties by clicking the plot button

You can now Export the required variables from pde tool and create a MATLAB script

Question 1: Export the stress fields and compute

VonMises using matlab (check with PDEtool interface)

$$\bar{\sigma} = \sqrt{\frac{3}{2} \cdot \underline{dev}(\underline{\underline{\sigma}}) : \underline{dev}(\underline{\underline{\sigma}})} = \sqrt{\sigma_x^2 + 3 \cdot \tau_{xy}^2}$$

Question 2: Empirically fit with $\sigma_{xx} = K \cdot (L - x) \cdot y$ Please. Comment !

Question 3: (BONUS) Add a hole center in $L/2$, $h/2$ of size defined from the relationship $(D / H = 0.6)$. Make a convergence study on sigma_max. Compare with standard stress concentration factor abaqus if possible.