

Final Exam

Friday, 11th 10:30-12:30

- Same style as the midterm
- T/F, MC, Short Ans, Long Ans
- Comprehensive: Focused on things after-midterm
- Equation sheet provided before the exam
- pencil / non-programable calculator
and rulers/protractors/compass
- no notes, no book
- review notes, book sections, homework

4-1 to 4-13

5-1 to 5-11, 5-13

6-1 to 6-4, 6-7 to 6-15

6-12: Langer line (yielding) and modified Goodman

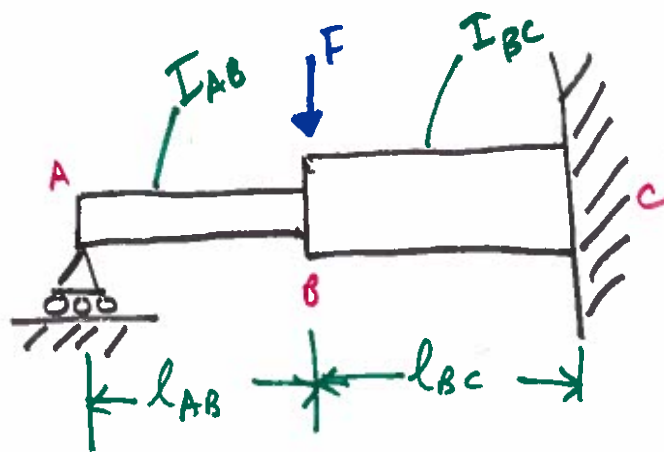
+ sections for
midterm

Requested Review Topics

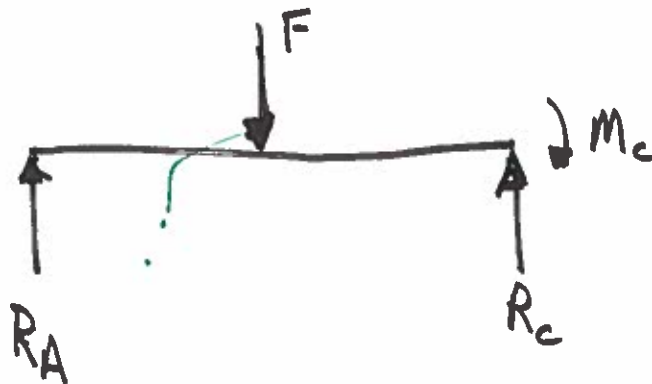
fluctuating stress	6
strain energy deflection	5
compound loading	5
brittle fracture	3
fatigue	3
non ferrous fluctuating stress	2
fatigue stress concentration	2
buckling	2
stress cube/multi axial	2
FoS for fatigue	1
transverse shear stress (Q)	1
finite life fluctuating stress	1
compound stress strain	1
statically indeterminate	1
probability	1
conceptual questions	1
cumulative loading	1
curved beam	1
kf marin	1
material after midterm	1
sample problems	1
static failure theories	1
equation sheet	1

Ex

What is the deflection at point B?



FBD



$$\sum F = 0: R_A + R_C - F = 0$$

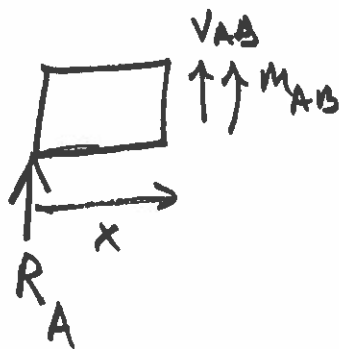
$$\sum M_C = 0: M_C + R_A(l_{AB} + l_{BC}) - F(l_{BC}) = 0$$

} 3 unknowns
only 2 equations

$$y_A = 0 = \frac{\partial U}{\partial R_A}$$

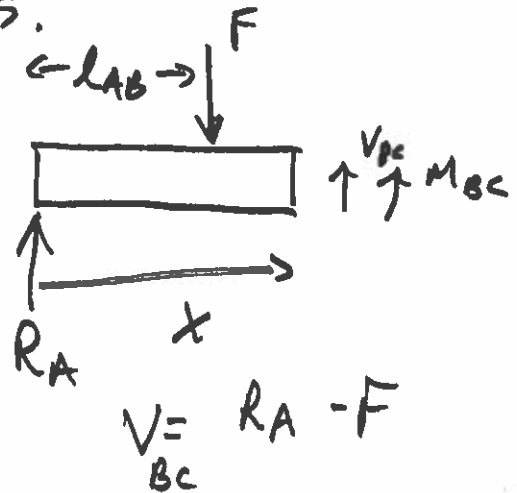
Castiglione's theorem
to get a ~~se~~ third equation

Take x from the l.h.s can avoid dealing reactions @ r.h.s.



$$V_{AB} = R_A$$

$$M_{AB} = R_A x$$



$$V_{BC} = R_A - F$$

$$M_{BC} = R_A x - F(x - l_{AB})$$

Neglect shear: long slender beam the stress/strain due to bending dominates.

$$y_A = 0 = \frac{\Delta u}{2R_A} = \int_0^{l_{AB}} \frac{1}{EI_{AB}} \left(M_{AB} \frac{\partial M_{AB}}{\partial R_A} \right) dx$$

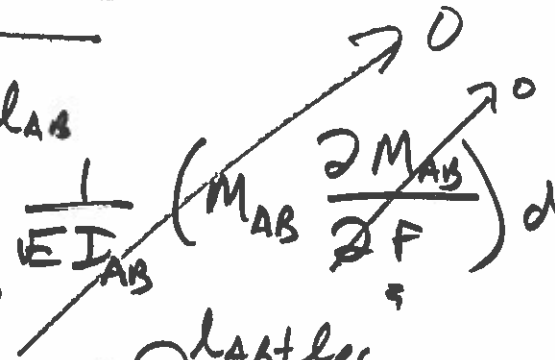
$$+ \int_{l_{AB}}^{l_{AB}+l_{BC}} \frac{1}{EI_{BC}} \left(M_{BC} \frac{\partial M_{BC}}{\partial R_A} \right) dx$$

$$0 = \int_0^{l_{AB}} \frac{R_A x^2}{EI_{AB}} dx + \int_{l_{AB}}^{l_{AB}+l_{BC}} \frac{x [F(l_{AB} - x) + R_A x]}{EI_{BC}} dx$$

Solve for R_A !

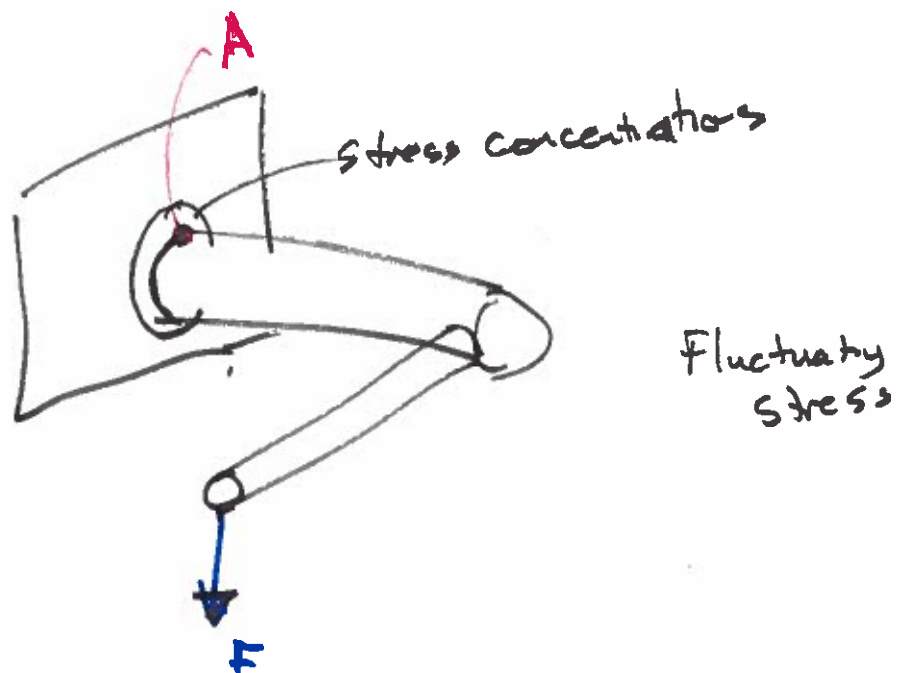
$$R_A = \frac{F I_{AB} [l_{AB}^3 - 3l_{AB}(l_{AB}+l_{BC})^2 + 2(l_{AB}+l_{BC})^3]}{2(-I_{AB}l_{AB}^3 + I_{AB}(l_{AB}+l_{BC})^3 + I_{BC}l_{AB}^3)}$$

Deflection @ B

$$y_B = \frac{\partial u}{\partial F} = \int_0^{l_{AB}} \frac{1}{EI_{AB}} \left(M_{AB} \frac{\partial M_{AB}}{\partial F} \right) dx + \int_{l_{AB}}^{l_{AB}+l_{BC}} \frac{1}{EI_{BC}} \left(M_{BC} \frac{\partial M_{BC}}{\partial F} \right) dx$$


$$y_B = \int_{l_{AB}}^{l_{AB}+l_{BC}} \frac{(l_{AB}-x)[-F(x-l_{AB})+R_A x]}{EI_{BC}} dx$$

$$y_B = \frac{F l_{AB}^2 l_{BC} (3I_{AB} l_{BC} + 4I_{BC} l_{AB})}{12 EI_{BC} (3I_{AB} l_{AB}^2 l_{BC} + 3I_{AB} l_{AB} l_{BC}^2 + I_{AB} l_{BC}^3 + I_{BC} l_{AB}^3)}$$



Find state of stress @ A

Torsional shear τ_{max} τ_{min}
 Bending normal σ_{max} σ_{min}



σ_A , σ_m

- Stress concentration factors
- Endurance limit
- von mises fluctuating stress
- modified Goodman to check for failure

$$K_f \quad K_{fs} =$$

$$K_f = 1 + q(K_t - 1)$$

$$K_{fs} = 1 + q(K_{ts} - 1)$$

Notch size $1/8''$ weld

$$\sigma_a = K_f \sigma_{a0} \quad \sigma_m = K_f \sigma_{m0}$$

$$\tau_a = K_{fs} \tau_{a0} \quad \tau_m = K_{fs} \tau_{m0}$$

$\left\{ \begin{array}{l} K_a \Rightarrow \text{surface finish} \\ K_b \Rightarrow \text{size} \end{array} \right.$

$K_c \Rightarrow$ don't use it

$$\sigma'_a = [\sigma_a^2 + 3(\tau_a)^2]^{1/2}$$

$$\sigma'_m = [\sigma_m^2 + 3(\tau_m)^2]^{1/2}$$

$\frac{\sigma'_a + \sigma'_m}{\text{yielding}}$