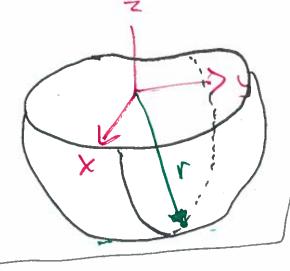
Assumptions

- loads are perpendicular to the surface
- No friction, smooth, continous surface
- Small strain theory

Coneral Case

- general curved Surface z



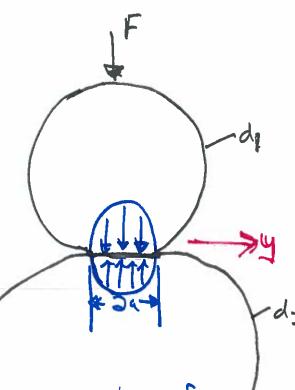
- circular area of contact

- hemispherical stress/pressure at the contact

Surface

Special Cases

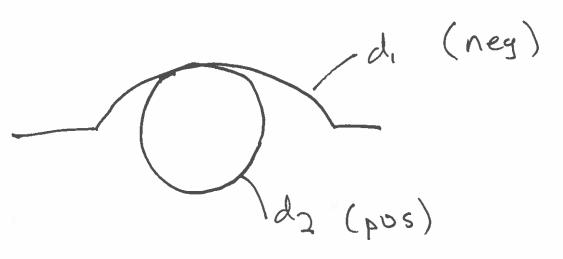
Two Spheres



a = radius of contact on a

↑F 1_z

L-17-2

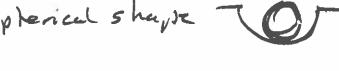


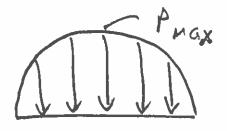
$$0 = \frac{3}{8} \frac{3F}{(1-\nu_1^3)/E_1 + (1-\nu_2^3)/E_3}$$

flut surface

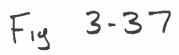
internal

Spherical shape





The stress is a function of Z 0,= 02 = 0x = 0y = - P (1- 12/al) (1+V)



Sphere contact stress as function of depth into sphere

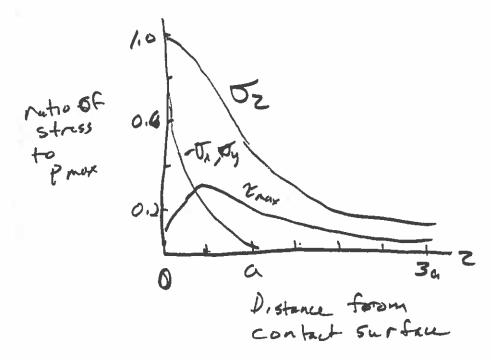
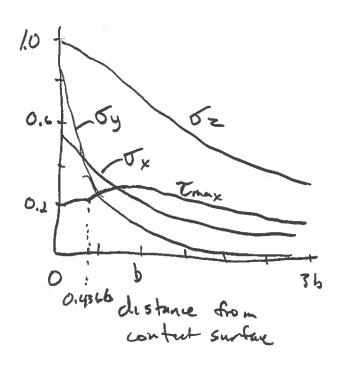


Fig 3-31

Cylindrical



Spalling! flaking of material from the surface

brinelling: permanent indentation of a hard surface

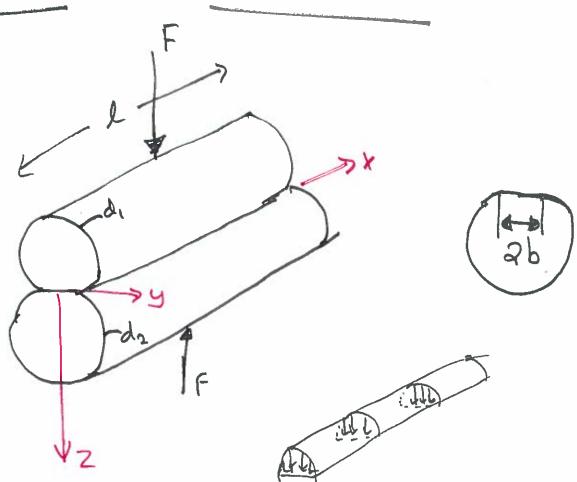
Pitting: Spalling due to fatigue in roller bearings

**

* See website resources page for examples

Max-sheur below surface is attributed to spelling and pitting failures

Special Case: Cylindrical Contact



$$b = \sqrt{\frac{2F}{TTR}} \frac{(1-V_1^2)/E_1 + (1-V_4^2)/E_2}{V_{d_1} + V_{d_2}}$$

$$P_{max} = \frac{2F}{TTbR}$$

$$\nabla_x = -2V P_{max} \left(\sqrt{1+\frac{2^2}{b^2}} - \frac{2}{b}\right) \frac{3-75}{3-75}$$

$$\nabla_y = -P_{max} \left(\sqrt{1+\frac{2^2}{b^2}} - 2\frac{2}{b}\right) \frac{3-75}{3-75}$$

$$\sqrt{1+\frac{2^2}{b^2}} \frac{3-75}{3-75}$$