1 ABSTRACT

3	Plant simulation models are abstractions of plant physiological processes. They are useful for
4	investigating the responses of plants to changes in their environment and physical structure.
5	Photosynthesis is a basic plant process that drives growth and biomass accumulation. Thus the
6	simulation of photosynthetic processes is a basic requirement for any plant simulation model.
7	The objective of this work is to develop and document a computer software module that
8	encapsulates equations and parameters to simulate the process of light capture, gas exchange of
9	CO <sub>2</sub> and water vapor, and production of carbohydrate by a plant leaf. The module is written in
10	C++. The program simulates leaf gas exchange processes by coupling photosynthesis with leaf
11	energy balance through stomatal conductance for both $C_3$ and $C_4$ crops. The coupled-model
12	approach can describe the photosynthetic behavior of leaves by taking into account the
13	biochemical limitation for CO <sub>2</sub> assimilation (demand) as well as the stomatal limitation to the
14	supply of CO <sub>2</sub> , linked to transpiration and canopy temperature. The module's input and output
15	data are documented and complete, compilable code is presented along with a simple interface
16	written in C# to interact with the module. The environmental input required by the module
17	includes net radiation, ambient air temperature, relative humidity, and atmospheric $\mathrm{CO}_2$
18	concentration. The module outputs transpiration rate, net and gross CO2 assimilation rates,
19	respiration rate, leaf temperature, internal CO <sub>2</sub> concentration and stomatal conductance.
20	Measured photosynthesis data and parameters for maize, potato and rose are also presented to
21	allow evaluation of the gas exchange simulations. Parameters for other crops are also included.
22	Users will be able to easily incorporate this module into a larger plant simulation model in order
23	to add the ability to simulate photosynthesis. The module is also useful as a teaching aid.

- 25 Photosynthesis includes the processes of CO<sub>2</sub> assimilation and water vapor release by plant
- leaves. It is one of the more important processes for life on Earth as it provides carbohydrate for
- food and oxygen for respiration. Because plant growth depends on photosynthesis it is an
- 28 essential building block of plant simulation models. Photosynthesis models range in complexity
- from correlative models based on radiation use efficiency (Monteith, 1977) where carbon
- 30 assimilation is proportional to total irradiance absorbed by leaf surfaces to models based on
- enzyme kinetics (Farguhar et al., 2001).
- 32 A coupled approach to photosynthesis-stomatal conductance-transpiration modeling for C<sub>3</sub> plants
- has been presented by a number of authors (Collatz et al., 1991; Harley et al., 1992; Leuning et
- al., 1995; Nikolov et al., 1995). This approach combines the FvCB (Farquhar-von Caemmerer-
- 35 Berry) C<sub>3</sub> photosynthesis model (Farquhar et al., 1980; Farquhar and von Caemmerer, 1981)
- with a model of stomatal conductance (Ball et al., 1987; Leuning, 1995) and an energy balance
- 37 equation. The coupled-model approach can describe the photosynthetic behavior of leaves by
- taking into account the biochemical limitation for CO<sub>2</sub> assimilation (demand) as well as the
- stomatal limitation to CO<sub>2</sub> (supply), linked to transpiration and canopy temperature. These
- 40 models describe photosynthesis mechanistically based on its key biochemical and anatomical
- 41 characteristics. A comprehensive biochemical model for C<sub>4</sub> photosynthesis was developed more
- 42 recently by von Caemmerer and Furbank (1999).
- The parameterization for these models is reasonably stable over a range of environments and
- practical to carry out. Many of the important parameters can be derived from measurements with
- portable photosynthesis systems such as LI-COR 6400 (Li-Cor Biosciences, Lincoln, NE, USA).
- Furthermore, the temperature dependence of photosynthesis and its key enzyme activities has
- been determined experimentally for both C<sub>3</sub> and C<sub>4</sub> plants (Bernacchi et al., 2001; Kubien, 2003;
- 48 Kim, 2006, 2007; Massad et al., 2007; Sage and Kubien, 2007). Dubois et al., (2007) discuss
- 49 methods for statistical estimation of the parameters. Parameters determined using the Li-Cor
- 50 6400 and published values were successfully used in a simulation model to estimate field level

- 51 maize yields in Maryland, USA (Kim et al., 2012), potato in growth chambers (Fleisher et al.,
- 52 2010), and greenhouse crops (Kim and Lieth, 2003; Kim et al., 2007b).

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### **Model Descriptions and Governing Equations**

- 55 The  $C_3$  model:
- The basis of this module is the biochemical model for C<sub>3</sub> photosynthesis by Farquhar et al.
- 57 (1980) as modified by Harley et al. (1992) and de Pury and Farquhar (1997). Photosynthesis in
- 58 C<sub>3</sub> plants is mathematically abstracted as three processes. These are the rates of carboxylation
- 59 catalyzed by Rubisco electron transport, and triose phosphate utilization. As irradiance
- 60 increases, CO<sub>2</sub> fixation becomes less limited by light and more limited by rate of carboxylation
- 61 governed primarily by Rubisco kinetics (von Caemmerer and Farquhar, 1981, 1982). Similarly,
- at low CO<sub>2</sub> levels, CO<sub>2</sub> fixation is limited by Rubisco while at higher CO<sub>2</sub> levels, it is limited by
- RuBP regeneration. Sharkey (1985) identified the rate of triose phosphate utilization (TPU) as
- 64 the third limiting process in photosynthesis. Harley et al. (1992) implemented the TPU limitation
- 65 in their model.
- The external variables that determine steady state leaf photosynthetic rate include intercepted
- 67 light, CO<sub>2</sub>, temperature and vapor pressure deficit (calculated from relative humidity and
- temperature). Net CO<sub>2</sub> assimilation rate,  $A_n$ , in C<sub>3</sub> plants is assumed to be limited by three
- processes: Rubisco-catalyzed carboxylation rate  $[(A_v)$ , regeneration of RuBP  $(A_i)$  controlled by
- electron transport rate, or the triose-phosphate utilization, TPU  $(A_n)$ . Thus net photosynthetic
- 71 rate  $(A_n, \mu mol CO2 m-2 s-1)$  is the minimum of  $A_v$ ,  $A_i$  or  $A_p$  and can be expressed as:

$$A_n = \min\{A_v, A_i, A_p\} - R_d$$

- 73 where  $R_d$  is the mitochondrial respiration rate in light or day respiration (for brevity, the units are
- specified with the variable listing in the appendix).
- 75 Rubisco limited photosynthetic rate is calculated as:

$$A_{v} = V_{c \max} \frac{C_{i} - \Gamma^{*}}{C_{i} + K_{c}(1 + O/K_{o})}$$

- 76 where  $V_{c max}$  is the temperature dependent maximum rate of Rubisco carboxylation,  $C_i$  is the
- intercellular CO<sub>2</sub> partial pressure, O is the partial pressure of oxygen (210 mbars),  $\Gamma^*$  is the CO<sub>2</sub>
- compensation point in the presence of  $R_d$ ,  $K_c$  is the temperature dependent Michaelis-Menten
- 79 constant of Rubisco for  $CO_2$ , and  $K_o$  is the Michaelis-Menten constant of Rubisco for  $O_2$ .  $C_i$  is
- 80 calculated as:

$$C_i = C_a - A_n \cdot \left(\frac{1.6}{g_{sw}} + \frac{1.37}{g_b}\right) \cdot P_a$$

- where  $C_a$  is atmospheric CO<sub>2</sub> content,  $A_n$  is net photosynthesis,  $g_{sw}$  is stomatal conductance to
- water vapor,  $g_b$  is the boundary layer conductance to water vapor, and  $P_a$  is the partial pressure
- of the atmosphere. In practice, an iterative method is used to solve for  $C_i$  using a search
- algorithm (e.g., secant, bisectional) since  $A_n$  is also needed to calculate stomatal conductance as
- will be described later.
- 87 The  $CO_2$  compensation point in the absence of day respiration ( $\Gamma^*$ ) is temperature dependent and
- 88 calculated as:

$$\Gamma^* = 36.9 + 1.88 \cdot (T_L - 25) + 0.036 \cdot (T_L - 25)^2$$

- where  $T_L$  is leaf temperature in °C.
- 90 RuBP regeneration limited photosynthetic rate (Aj) through electron transport is:

$$A_{j} = \frac{J \cdot (C_{i} - \Gamma^{*})}{4 \cdot (C_{i} + 2\Gamma^{*})}$$

- 92 where J is the electron transport rate, and the other variables defined as above. The light
- dependence of the rate of electron transport, J, can be expressed as:

$$\theta J^2 - (I_a + J_{\text{max}})J + I_a J_{\text{max}} = 0$$

- Where  $\theta$  is curvature of response of electron transport to photosynthetically active radiation
- 96 (PAR),  $J_{max}$  is the maximum electron transport rate at the temperature of the leaf,  $I_2$  is PAR
- effectively absorbed by Photosystem II. The variable  $I_a$  is calculated as:

$$I_2 = \alpha I(1-f)/2$$

- Where I is the incident light in photosynthetic flux density ( $\mu$ mol photons m<sup>-2</sup> s<sup>-1</sup>) (PFD),  $\alpha$  is
- leaf absorbance in PAR, and f is the spectral correction factor (0.2). The value of J in Eq. [6] is
- obtained using a quadratic equation.
- $A_p$ , the TPU limited photosynthetic rate, is calculated as:

$$A_p = 3 \cdot P_u$$

- where P<sub>u</sub> is the rate of TPU. An Arrhenius function is used to calculate the temperature
- dependence of  $K_c$ ,  $K_o$ ,  $R_d$ ,  $V_{cmax}$  and  $P_u$ . For example,

$$K_c = K_{c25} \exp[E_a \cdot (T_L - 25) / \{298 \cdot R \cdot (T_L + 273)\}]$$

- Where  $E_a$  is the activation energy (varies by process),  $T_L$  is the leaf temperature, and R is the
- universal gas constant. Each temperature dependent parameter has a value at 25C, i.e.,  $K_{c 25}$ ,

- $V_{Cmax25}$ , etc. Eq. [9] scales the variable for the current leaf temperature as a function of the value
- 107 at 25 °C.
- The parameter  $J_{max}$  in the light dependence function is also temperature dependent and varies as:

$$J_{\text{max}} = J_{m25} \cdot \exp \left[ \frac{(T_L - 25) \cdot E_a}{R \cdot (T_L + 273) \cdot 298} \right] \cdot \frac{\left[ 1 + \exp \left( \frac{S \cdot 298 - H}{R \cdot 298} \right) \right]}{\left[ 1 + \exp \left( \frac{S \cdot (T_L + 273) - H}{R \cdot (T_L + 273)} \right) \right]}$$

- Where  $E_a$  and R are as defined above, H is the curvature parameter determining the rate of  $J_{\text{max}}$
- decrease above the peak temperature, S is the entropy factor.
- The leaf age dependence function for  $J_{max}$ ,  $V_{cmax}$  and  $P_u$  is given as:

$$f(t) = \max \left[ 0.0, \frac{t}{t_{opt}} \exp \left( 1.0 - \frac{t}{t_{opt}} \right) \right]$$

- Where t is leaf age (days, physiological age, or GDD),  $t_{opt}$  is the optimal age for photosynthesis
- to peak. This function scales between 0 and 1, and has also been used for scaling final leaf size in
- response to temperature in maize (Kim et al., 2012).
- 115 *The C*<sub>4</sub> *Model:*
- 116 The biochemical demand for CO<sub>2</sub> assimilation is adapted from von Caemmerer and Furbank
- 117 (1999). The rate of net  $CO_2$  assimilation  $(A_n)$  is represented by the minimum of enzyme limited
- 118  $(A_c)$  and electron transport limited  $(A_i)$  assimilation rates.

$$A_n = \min h \left\{ A_c, A_i \right\}$$

- Where  $A_c$  is the enzyme limited CO<sub>2</sub> assimilation rate, and  $A_i$  is the electron transport limited
- 120 CO<sub>2</sub> assimilation rate. The transition between  $A_c$  and  $A_i$  is calculated using a hyperbolic
- minimum (minh) which is equivalent to taking the lower root of quadratic solution with a
- curvature factor which may be interpreted as a parameter of co-limitation (Kirschbaum, 1994;

- Buckley et al., 2003).  $A_c$  can be approximated by the minimum of phosphoenol pyruvate
- carboxylase (PEPC) and Rubisco activities taking into account the bundle-sheath leakage rate
- and mitochondrial respiration.

$$A_c = \min\{(V_p + g_{bs}C_m - 0.5R_d), (V_{c \max} - R_d)\}$$

- Where  $V_p$  is the rate of C<sub>4</sub> carboxylation,  $g_{bs}$  is the bundle sheath conductance to CO<sub>2</sub>,  $C_m$  is the
- mesophyll CO<sub>2</sub> partial pressure, and  $R_d$  is mitochondrial respiration. In the model,  $A_c$  is solved
- using a quadratic expression as described by von Caemmerer (2000) which was not introduced
- here for brevity. Provided that the resistance for CO<sub>2</sub> from intercellular spaces to mesophyll cells
- is negligible,  $C_m$  can be estimated by:

$$C_m \cong C_i = C_s - A_n \left( \frac{1.6}{g_s} + \frac{1.37}{g_b} \right)$$

- Where  $C_m$  and  $C_i$  are as defined above,  $g_s$  is stomatal conductance,  $A_n$  is net carbon assimilation
- rate, and  $C_s$  is the CO<sub>2</sub> concentration at the leaf surface inside the boundary layer. As is done in
- the  $C_3$  model, an iterative method is used to solve for  $C_m$  using a search algorithm since  $A_n$  is also
- needed to calculate stomatal conductance.
- The rate of  $C_4$  carboxylation  $(V_p)$  is assumed to be limited either by PEPC activity or PEP
- 136 regeneration.

$$V_p = \min\left\{\frac{C_m V_{p \max}}{C_m + K_p}, V_{pr}\right\}$$

- Where  $V_{pmax}$  is the maximum PEP carboxylation rate,  $K_p$  is the Michaelis-Menton constant for
- 138 CO<sub>2</sub> of PEPC, and  $V_{pr}$  is PEP regeneration rate.
- The assimilation rate limited by electron transport  $(A_i)$  can be approximated similarly to  $A_c$  by the
- minimum of electron transport limited rates in C<sub>4</sub> and C<sub>3</sub> cycles.

$$A_{j} = \min \left\{ \left( \frac{xJ}{2} - R_{m} + g_{bs}C_{m} \right), \left( \frac{(1-x)J}{3} - R_{d} \right) \right\}$$

- where J is the electron transport rate, x is a partitioning factor of J,  $R_m$  is mitochondrial
- respiration in the mesophyll,  $g_{bs}$  is bundle-sheath conductance to  $CO_2$ ,  $R_d$  is mitochondrial
- respiration in the light,  $C_m$  is as defined above. Total rate of electron transport (J) was modeled
- using the non-rectangular hyperbolae which can be described as a hyperbolic minimum (*minh*)
- 145 (Buckley et al., 2003).

$$J = \min\{I_2, J_{\text{max}}, \theta\} \text{ where } \theta J^2 - J(I_2 + J_{\text{max}}) + I_2 J_{\text{max}} = 0$$

- Where  $I_2$  is effective radiation absorbed by PSII (Eqn. [7]),  $\theta$  is curvature of response of electron
- transport to PAR, and  $J_{max}$  is the maximum rate of electron transport.
- The temperature dependence of  $Vp_{max}$ ,  $Vc_{max}$ ,  $K_o$ ,  $K_c$ , and  $R_d$  was approximated by the Arrhenius
- 149 equation  $(k_T)$  normalized at 25 °C.

$$k_T = \exp[E_a(T_K - 298)/(298RT_K)]$$
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- The temperature dependence of  $K_p$  and  $Vp_r$  was assumed to be  $Q_{10}$  of 2.0. The temperature
- dependence of  $J_{max}$  was modeled using a peaked function (Medlyn, 2002).

$$k_{Tpeak} = k_T \left[ 1 + \exp\left(\frac{298S - H}{298R}\right) \right] \left[ 1 + \exp\left(\frac{ST_K - H}{RT_K}\right) \right]^{-1}$$

- Where H and S are defined as in the  $C_3$  model (Eq.[10]]) and temperature is in Kelvin.
- The effect of leaf nitrogen content ( $N_1$  in g m<sup>-2</sup>) on photosynthetic capacity is described using a
- logistic function (Vos et al., 2005).

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$$k_N = \frac{2.0}{1.0 + \exp(-\chi_n(N_l - N_b))} - 1.0$$
 (7)

- 156  $N_b$  is base N content below which the leaf is non photosynthetic,  $\chi_n$  determines the rate of change
- in photosynthesis in response to  $N_1$ .
- Finally,  $Vp_{max}$ ,  $Vc_{max}$ , and  $J_{max}$  were modeled as:

$$V_{p \max} = V_{pm25} \cdot k_N \cdot k_T \tag{20}$$

$$V_{c \max} = V_{cm25} \cdot k_N \cdot k_T$$
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$$J_{\text{max}} = J_{m25} \cdot k_N \cdot k_{Tneak}$$

- 160 Stomatal Conductance Model
- Both the  $C_3$  and  $C_4$  models share the same code for the stomatal conductance  $(g_s)$  model. This
- model is based on the work of Ball et al. (1987) and is called the BWB model. The main form of
- the conductance model is given as:

$$g_s = g_0 + g_1 \cdot A_n \cdot \frac{h_s}{\left(C_s / P_a\right)}$$
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- Where  $g_0$  is residual stomatal conductance to water vapor at the light compensation point in
- BWB model,  $g_1$  is the empirical coefficient for the sensitivity of  $g_s$  to  $A_n$ ,  $C_s$  and  $h_s$ ;  $h_s$  is relative
- humidity at the leaf surface (as a fraction),  $A_n$  is net photosynthesis,  $C_s$  is CO<sub>2</sub> concentration at
- the leaf surface, and  $P_a$  is the partial pressure of the atmosphere.  $C_s$  is estimated as:

$$C_s = C_a - A_n \cdot \frac{1.37}{g_{hw}} \cdot P_a$$

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- Where  $g_{bw}$  is boundary layer conductance to water vapor.
- Boundary layer conductance  $(g_{bw})$  in relation to wind speed (u) and leaf dimension (d) is:

$$g_{bw} = 0.147 \sqrt{\frac{u}{d}}$$

 $d = 0.72 \cdot w$ 

- 171 Where w is leaf width (m).
- 172 A quadratic equation is used to obtain  $h_s$  by combining  $g_s$  with the diffusion equation (Eq. [24])

$$a_{h} \cdot h_{s}^{2} + b_{h} \cdot h_{s} + c_{h} = 0$$

$$\begin{cases}
a_{h} = \frac{g_{1} \cdot A_{n}}{C_{s}} \\
b_{h} = g_{0} + g_{bw} - (g_{1} \cdot A_{n}/C_{s}) \\
c_{h} = (-h_{a} \cdot g_{bw}) - g_{0}
\end{cases}$$
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- And  $g_0$ ,  $g_1$  and  $g_{bw}$  are defined as above. The vapor pressure deficit,  $D_s$ , at the leaf surface is
- given as:

$$D_s = (1 - h_s) \cdot e_s \tag{27}$$

- 175 Where  $e_s$  is vapor pressure at the leaf surface (assumed saturated).
- Leaf temperature,  $T_L$ , is determined using a linearized solution (Norman and Campbell, 1998) of
- the energy budget equation for temperature at the leaf surface:

$$T_{L} = T_{a} + \frac{\gamma^{*}}{s + \gamma^{*}} \left[ \frac{R_{abs} - \varepsilon \cdot \sigma \cdot T_{a}^{4}}{g_{hr} c_{p}} - \frac{D}{p_{a} \gamma^{*}} \right]$$

$$\gamma^{*} = \frac{\gamma \cdot g_{hr}}{g_{v}}$$
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$$g_{hr} = g_h + g_r$$

- Where  $T_a$  is air temperature,  $R_{abs}$  is absorbed long-wave and short-wave radiation per surface leaf
- area,  $\varepsilon$  is leaf thermal emissivity (set to 0.97),  $\sigma$  is the Stefan-Boltzmann constant (5.67x 10-8
- Watts  $m^{-2}$  K<sup>-4</sup>), D is vapor pressure deficit, s is the slope of the slope of the vapor pressure
- deficit-temperature curve  $\Delta$  divided by atmospheric pressure:

$$s = \frac{\Delta}{p_a}$$

$$\Delta = \frac{d(e_s)}{dT} = \frac{e_s(T) \cdot 17.502 \cdot 240.97}{(c+T)^2}$$

- 182  $\gamma$  is the psychrometric constant (6.66 x 10<sup>-4</sup>). Total water vapor conductance per surface leaf area,
- 183  $g_{\nu}$ , is calculated as:

$$g_{v} = 0.5 \frac{g_{s} \cdot g_{bw}}{g_{s} + g_{bw}}$$

Heat conductance for the boundary layer is:

$$g_h = \frac{0.135}{0.147} \cdot g_{bw}$$
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185 Radiative conductance is:

$$g_r = \frac{4 \cdot \varepsilon \cdot \sigma \cdot T_L^3}{C_p}$$

186 Saturated water vapor pressure at temperature (*T*) is:

$$e_s(T) = 0.611 \cdot \exp\left(\frac{17.502 \cdot T}{240.97 + T}\right)$$

187 Where *T* is temperature.

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188 Transpiration rate, E, is calculated as:

$$E = 2 \cdot g_v \cdot \left( \frac{e_s(T_L) - e_a}{P_a} \right)$$

Where all variables are defined as before.

191 Coupling Photosynthesis and Transpiration

The  $C_3$  and  $C_4$  photosynthesis models use light,  $CO_2$ , air temperature, and relative humidity as environmental input variables. Since photosynthetic rate is necessary to calculate stomatal conductance, leaf temperature and  $C_i$  or  $C_m$ , an iterative method is used to arrive at a solution (Fig. 1). The BWB model requires the net photosynthetic rate  $(A_n)$  as an input (Eq. [1] for  $C_3$  and Eq. [12] for  $C_4$ ), while  $C_i$  or  $C_m$  results from the interaction of  $A_n$  and  $a_n$  and

diffusion equation is used to relate  $C_a$ ,  $C_s$  and  $C_i$  using A,  $g_s$  and  $g_b$  [Eqns. [3] and [14] for the  $C_3$  and  $C_4$  models respectively, and [26]). Therefore, the three sub-models (photosynthesis, stomatal conductance, and energy balance) are interdependent. A nested iterative procedure was used to solve this relation numerically (Fig. 1). Initially, leaf temperature and  $C_i$  were assumed to be equal to  $T_a$  and 0.7  $C_a$ , respectively, so as to obtain an estimate of  $A_n$ . The estimate of  $A_n$  is then used to obtain  $g_s$ .  $C_i$  was estimated using the resulting  $A_n$  and  $g_s$  (Eqns. [3] and [14] depending on the model). This process is solved iteratively using the Newton-Raphson method until  $C_i$  was stable. Subsequently, leaf temperature is computed using  $T_a$  and  $g_s$  (Eq. [28]) and compared with the initial leaf temperature. When the new leaf temperature agreed to within 0.1 °C with the initial value, the iteration was assumed to have converged.

### **Parameterization**

We used a stepwise calibration of individual components of the photosynthesis model rather than fitting all parameters simultaneously (Kim and Lieth, 2003; Kim, 2006, 2007). That is, the photosynthetic parameters ( $V_{cm25}$ ,  $J_{m25}$ ,  $R_{d25}$ ) were first determined by fitting the biochemical model of photosynthesis (Farquhar et al., 1980) to the A/C<sub>i</sub> response using measured C<sub>i</sub> at controlled steady state conditions where PAR is fixed (typically 1500 µmol·m<sup>-2</sup>·s<sup>-1</sup>), and relative humidity and leaf temperature controlled to around 50%, and 25 °C respectively. In addition,  $V_{cmax}$  and  $J_{max}$  were estimated for individual leaves over a range of temperatures (usually growth temperatures). Temperature dependence of  $V_{cmax}$  and  $V_{cmax}$  and  $V_{cmax}$  are then determined by fitting Eqs. [18]- [22]. Temperature dependence of  $V_{cmax}$  are then determined by fitting Eq. [8] with the net photosynthesis data collected between 10 to 20 °C at 1500 µmol·mol<sup>-1</sup> of CO<sub>2</sub> and 1500 µmol·m<sup>-2</sup>·s<sup>-1</sup> of PAR, assuming that  $V_{cmax}$  are primarily governed by the rate of TPU when temperature is low while CO<sub>2</sub> and light are not limiting (Sharkey, 1985).  $V_{cmax}$  was estimated for the rose data by extrapolating Eq. [9] to 25 °C (see Fig. 3c in Kim and Lieth, 2003). Temperature

dependencies of  $K_c$ ,  $K_o$ ,  $\Gamma^*$ , and  $R_d$  were adopted from de Pury and Farquhar (1997), assuming that those parameters were invariant across species. The parameter values of the stomatal conductance model also come from gas exchange data. No parameter values in the energy balance equation are specifically calibrated. The parameterization data included a range of  $CO_2$  concentrations, relative humidities, PAR levels, and temperatures including those conditions where A might approach zero (PAR < 50  $\mu$ mol·m<sup>-2</sup>·s<sup>-1</sup> a<sup>-1</sup>. Specific details on parameterizing the model for other crops can be found in Kim and Lieth (2003) for rose, Fleisher et al. (2010) for potato, Kim et al. (2007b) for *Scaevola*, and Kim et al. (2012) for garlic. More details on parameterizing the FvCB model in general can be found in Dubois et al. (2007).

#### Validation of the Module Code

The biochemical models of photosynthesis for both  $C_3$  and  $C_4$  plants have been studied extensively and results have been published in a number of studies (Lenz et al., 2010; Fleisher et al., 2010; Massad et al., 2007; Kim and Lieth, 2003; Kim et al., 2006, 2007). The goal of the validation for this paper is to ensure that the equations for the model have been implemented correctly in the computer code and that the published parameters will give realistic results. This version of the code has been parameterized and tested for Rose (*Rosa hybrida* L.) by Kim and Lieth (2003), potato by Fleisher et al. (2010) and corn by Kim et al. (2006, 2007). Some of the simulations for Rose are repeated here to show that the current version of the code for  $C_3$  crops gives similar results as those published by Kim and Lieth (2003). Simulations for net photosynthesis response to light, internal  $CO_2$  and leaf temperature for Rose are shown in Figures 2a, 2b, and 2c. The responses and errors are similar to those shown in Kim and Lieth (2003). Note that the measurement errors for leaf temperature are higher than those for  $CO_2$  and light response. This is because it is difficult to control leaf temperature in the LiCor 6400 chamber.

Figure 3 shows a CO<sub>2</sub> response curve for potato estimated by the photosynthesis module for the calibration data from Fleisher et al (2010). Figure 4 shows CO<sub>2</sub> and light response curves for potato grown in sunlit growth chambers in a later study from unpublished data. The same parameters from Fleisher et al. (2010) were used from these simulations. Figure 5 shows estimated and observed leaf level transpiration as a function of stomatal conductance from leaves from the same unpublished data. The simulated values are slightly greater than observed at higher values of stomatal conductance. Since transpiration is affected by other variables in addition to stomatal conductance there tends to be more variance in the observed and simulated values. Also, the stomatal conductance submodel has not been calibrated to the same extent as the photosynthesis model. Net photosynthesis data for maize as a function of internal CO<sub>2</sub> concentration (C<sub>i</sub>) is shown in Figure 6. The parameters for the C<sub>4</sub> corn model were calibrated data reported in Kim et al. (2006 and 2007). The observed data in this figure were taken from corn grown in a field experiment in Beltsville, MD, U.S.A in 2002 and may have been subject to water stress. Note the shape of the curve and photosynthetic rates simulated by the model are within the range of the measured data. The corn model was calibrated under optimum growing conditions for corn as was present in the growth chambers. As a result, the net photosynthesis rates were in the high range as compared to other publications. Massad et al. (2007) in a study on C<sub>4</sub> model parameters noted that leaf photosynthesis rates for corn can be variable due to different growing conditions and stresses that may occur. It should be noted that the errors are largest at maximal light levels. At the canopy level, not all the leaves will be light saturated. As a result the errors of maximal photosynthesis may not translate to large errors for canopy level photosynthesis where light levels vary over time and over canopy position. Figure 7 shows simulated net photosynthesis and transpiration as a function of PAR. The data for this figure come from a field experiment carried out in Beltsville, MD, U.S.A in 2002 (unpublished). Note that the variability mainly occurs at high light or internal CO<sub>2</sub> levels. Again net photosynthesis is estimated well at all light levels but the simulated values range toward the high end. The differences for ET are larger at the high light

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levels. Again, the model has not been extensively calibrated and tested for the stomatal conductance submodel.

#### **Scaling to Canopy Level**

The coupled leaf physiology model can be scaled to estimate canopy level values of photosynthesis and transpiration. One approach is to calculate the light and temperature regime for individual leaves in the canopy depending on their location in the canopy and aggregating leaf level photosynthesis rates over the canopy. A simpler approach is to divide the canopy into sunlit and shaded components (de Prury and Farquhar, 1997) and calculate gas exchange rates for each component and sum them. Canopy level gas exchange rates have been calculated using this method for sunlit growth chamber grown plants by Kim et al (2007) for corn and Fleisher et al. (2010) for potato. The code has also been used to estimate dry matter and leaf area production of corn grown under field conditions (Kim et al., 2012).

### **Conclusions and Further Applications**

The comprehensive model described here that couples key leaf gas exchange processes is a critical tool in plant physiological and ecological research. This model can be used to evaluate the interactions between plants and the environment, and to forecast global carbon and water budgets in response to climate change. Because the gas exchange processes are not only sensitive to the microclimate surrounding the plant canopy but also closely related to soil and root processes in addition to endogenous biochemical regulations, a leaf gas exchange model should account for the interrelationships among carbon, water and nitrogen economies of above and below ground parts. That is, the model needs account for biochemical demand for CO<sub>2</sub> assimilation, physical supply of CO<sub>2</sub> and loss of water through stomata, supply of water from the

soil through transpiration stream, and stomatal control to balance these interrelated processes. Consequently, such model should also account for soil water status. In addition, the dependence on leaf physiological status like water potential, nitrogen content and age, which are key determinants of plant performance, should be also accounted for. This can be accomplished by numerically combining the component models of photosynthesis, stomatal conductance, and energy balance as described here and their response functions to various conditions. Such response functions have not been included here but the reader can find a number of them in the literature. For example, the Tardieu-Davies (TD) model of stomatal regulation as a function of Abscisic acid (ABA) concentration (Tardieu and Davies, 1993) has been used to model stomatal response to water stress. The TD model has been used in conjunction with the BWB model (Dewar, 2002; Gutschick, 2002).

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402	Figure Captions
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404	Figure 1. Flow chart for the model (from Kim and Lieth, 2003)
405	Figure 2. Simulated and observed carbon assimilation rates as a function of light (a), internal
406	CO <sub>2</sub> concentration (b), and leaf temperature (c) in Rose (Rosa hybrida L.) from Kim and Lieth
407	(2003).
408	Figure 3. Simulated and observed carbon assimilation rates for potato (Solarium tuberosum L.)
409	as a function of internal CO <sub>2</sub> concentration. These are calibration data from Fleisher et al. (2010).
410	Figure 4. Simulated and observed carbon assimilation rates for potato as a function of internal
411	CO <sub>2</sub> concentration (a) and light (b) using parameters from the data in Figure 3.
412	Figure 5. Simulated and observed transpiration rates for potato as a function of stomatal
413	conductance.
414	Figure 6. Simulated and observed carbon assimilation rates for maize (Zea Mays L.) as a
415	function of internal CO <sub>2</sub> concentration.
416	Figure 7. Simulated and observed carbon assimilation rates (a) and transpiration (b) as a function
417	of light for maize.
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Variables, parameters, and their values used in the model. The values with the superscript 'a' are from de Pury and Farquhar (1997). All parameters are projected leaf area basis unless stated otherwise.

Symbol	Value	Units	Description			
Photosyn	Photosynthesis model					
Γ	-	μbar	$CO_2$ compensation point in the presence of $R_d$			
$\Gamma^*$	-	μbar	$CO_2$ compensation point in the absence of $R_d$			
ξ	-	day	Leaf age counted as days after unfolding			
$\theta$	$0.7^{a}$	-	Curvature of response of electron transport to PAR			
δ	0.15	-	Leaf reflectance plus transmittance			
$A_n$	-	µmol·m <sup>-</sup> <sup>2</sup> ·s <sup>-1</sup>	Net CO <sub>2</sub> assimilation rate (photosynthetic rate)			
$A_c$	-	$\mu \text{mol·m}^{-1}$	Rubisco limited CO <sub>2</sub> assimilation rate			
$A_j$	-	µmol·m <sup>-</sup> <sup>2</sup> ·s <sup>-1</sup>	Electron transport limited CO <sub>2</sub> assimilation rate			
$A_{max}$	-	$\mu mol \cdot m^{-2} \cdot s^{-1}$	Light saturated CO <sub>2</sub> assimilation rate at ambient [CO <sub>2</sub> ]			

$A_p$	-	$\mu \text{mol·m}^{-1}$	Triose phosphate utilization limited CO <sub>2</sub> assimilation rate (C3 model only)
$C_i$	-	μbar	Intercellular CO <sub>2</sub> partial pressure (C3 model only)
$C_m$	-	μbar	Mesophyll CO <sub>2</sub> partial pressure (C4 model only)
$d_0$	1.296	-	Scaling factor of leaf age effect
$d_I$	0.1468	-	Empirical coefficient to determine growth of leaf age effect
$d_2$	0.0103	-	Empirical coefficient to determine downward slope of leaf age effect
$E_a$	-	kJ·mol <sup>-1</sup>	Activation energy
f	0.15 <sup>a</sup>	-	Spectral correction factor
$g_{bs}$	0.003	$\mu mol_{s^1} m^2$	Bundle sheath conductance to CO <sub>2</sub> , mol m <sup>2</sup> s <sup>1</sup>
Н	219.4	kJ·mol⁻¹	Curvature parameter of the temperature dependence of $J_{max}$
I	-	µmol quanta·m <sup>-</sup> <sup>2</sup> ·s <sup>-1</sup>	Incident PAR (Photosynthetically Active Radiation)
J	-	μmol electrons· m <sup>-2</sup> ·s <sup>-1</sup>	Electron transport rate

$J_{Max}$		$\mu mol \cdot m^{-2} \cdot s^{-1}$	Maximum rate of electron transport when temperature is at the optimum
$K_{c25}$	- 404 <sup>a</sup>	μbar	Michaelis-Menten constant of Rubisco for CO <sub>2</sub>
$K_{o25}$	- 248 <sup>a</sup>	mbar	Michaelis-Menten constant of Rubisco for O <sub>2</sub>
0	205 <sup>a</sup>	mbar	Oxygen partial pressure
$P_{u25}$	- 11.55	$\underset{\overset{2}{\cdot}s^{-1}}{\operatorname{mol}\cdot m}$	Rate of tirose phosphate utilization at 25 °C
R	8.314	$\underset{1}{\text{J-mol}}^{-1} \cdot \text{K}^{-}$	Universal gas constant
$R_{d25}$	1.260	$\mu mol \cdot m^{-2} \cdot s^{-1}$	Mitochondrial respiration in the light at 25 °C
S	704.2	J·mol <sup>-1</sup> ·K	Electron transport temperature response parameter
$T_L$	-	°C	Leaf temperature
$V_c$	-	µmol·m⁻²·s⁻¹	Carboxylation rate
$V_{cm25}$	102.4	µmol·m⁻²·s⁻¹	Photosynthetic Rubisco capacity at 25 °C
$V_{cmax}$	-	$\mu mol \cdot m^{-2} \cdot s^{-1}$	Maximum rate of rubisco carboxylation

 $V_{pmax}$  \_  $\frac{\text{umol·m}^2}{2 \cdot \text{g}^{-1}}$  Maximum PEP carboxylation rate (C4 model only)

 $V_{pr}$  \_  $\frac{\mu \text{mol·m}}{2 \cdot \text{s}^{-1}}$  PEP regeneration rate (C4 model only)

 $V_o$  -  $\frac{\mu \text{mol·m}}{2 \cdot \text{s}^{-1}}$  Oxygenation rate

# Variables with temperature dependence

 $K_c$  -  $\underset{^2\cdot s^{-1}}{\operatorname{umol \cdot m}}$  Michaelis-Menten constant of rubisco for  $CO_2$ 

 $K_o$  -  $\frac{\mu \text{mol·m}}{^2 \cdot \text{s}^{-1}}$  Michaelis-Menten constant of rubisco for  $O_2$ 

 $P_u$  -  $\underset{2\cdot s^{-1}}{\operatorname{umol} \cdot m}$  Triose phosphate utilization rate (C3 model only)

 $K_p$   $\underset{^2\cdot \text{S}^{-1}}{\text{µmol}\cdot \text{m}}$  Michaelis-Menten constant for CO<sub>2</sub> of PEPC

 $R_d$  -  $\frac{\mu \text{mol·m}}{2 \cdot \text{s}^{-1}}$  Mitochondrial respiration in the light

## Stomatal conductance model

 $g_0$  0.0960- mol·m<sup>-1</sup>·s<sup>-</sup> Minimum stomatal conductance to water vapor at the light compensation point in BWB model

*g*<sub>1</sub> - -

 $C_a$  -  $\mu$ bar Ambient  $CO_2$  partial pressure

 $C_s$  -  $\mu$ bar  $CO_2$  partial pressure at the leaf surface

 $g_b$  -  $\frac{\text{mol · m}^{-2} \cdot \text{s}^{-}}{1}$  Boundary layer conductance to water vapor

 $g_s$  -  $\frac{\text{mol} \cdot \text{m}^{-2} \cdot \text{s}^{-}}{1}$  Stomatal conductance to water vapor

 $h_a$  - Relative humidity of the ambient air

 $h_s$  - Relative humidity at the leaf surface

m 10.055 - Empirical coefficient for the sensitivity of  $g_s$  to A,  $C_s$  and  $h_s$  in BWB model

## Energy balance model

 $\varepsilon$  0.97 - Leaf thermal emissivity

 $\sigma$   $0^{-8}$   $W \cdot m^{-2} \cdot K^{-4}$  Stefan-Boltzmann constant per surface area

 $\lambda$  44.0 kJ·mol<sup>-1</sup> Latent heat of vaporization at 25 °C

 $C_p$  29.3  $J \cdot \text{mol}^{-1} \cdot C^{-1}$  Specific heat of air

D - kPa Vapor pressure deficit of the ambient air

 $D_s$  - Vapor pressure deficit at the leaf surface

E -  $\text{mol·m}^{-2} \cdot \text{s}^{-1}$  Transpiration rate per projected leaf area

 $e_a$  - kPa Vapor pressure in the ambient air

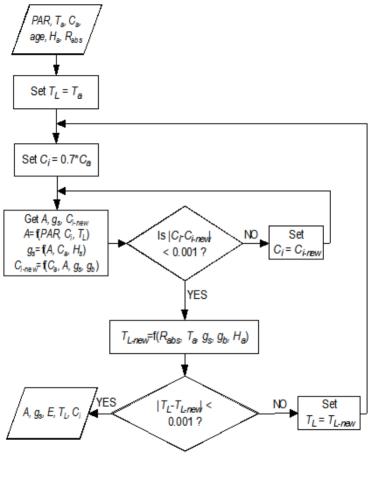
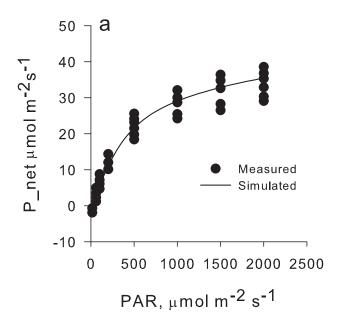
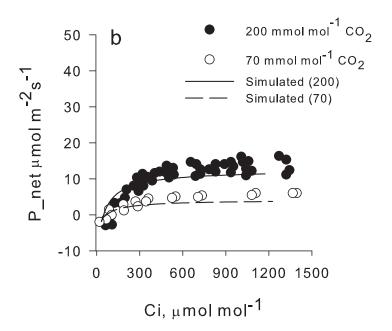


Figure 1





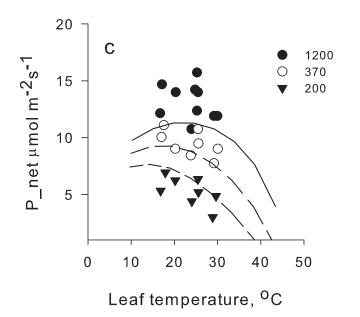


Figure 2

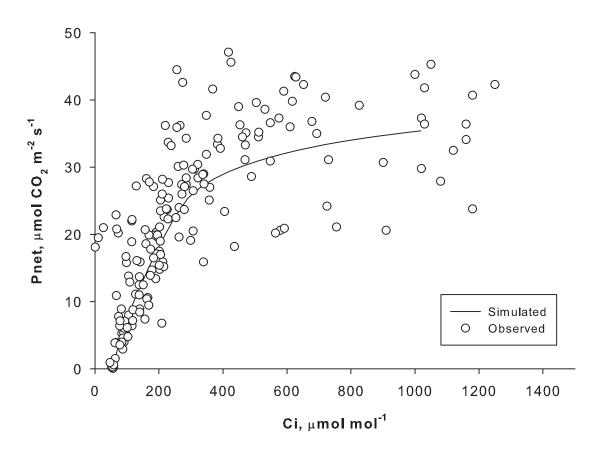
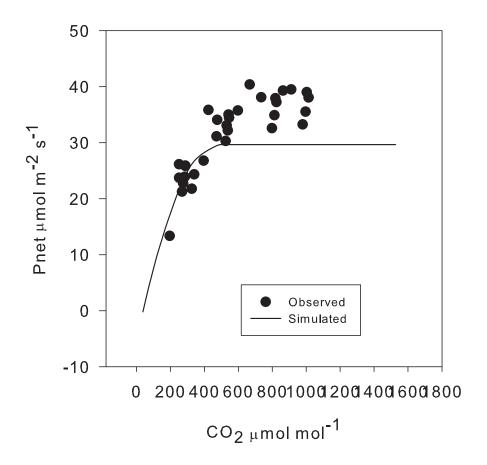
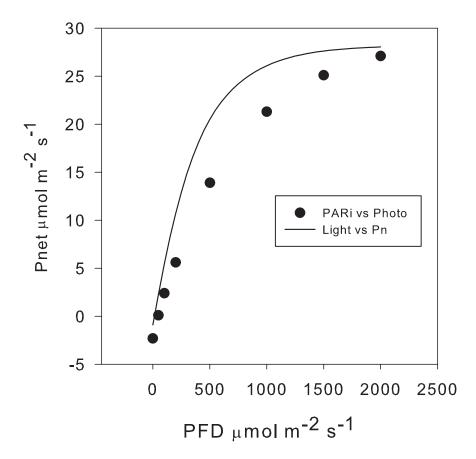


Figure 3





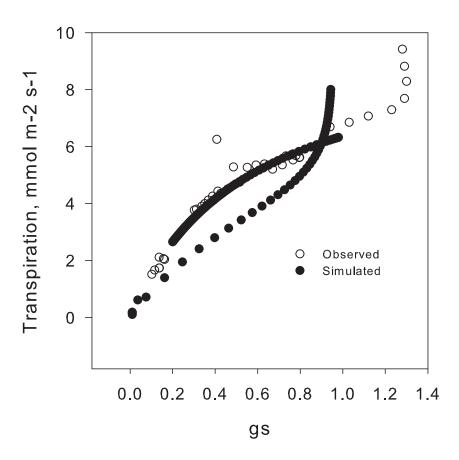


Figure 5

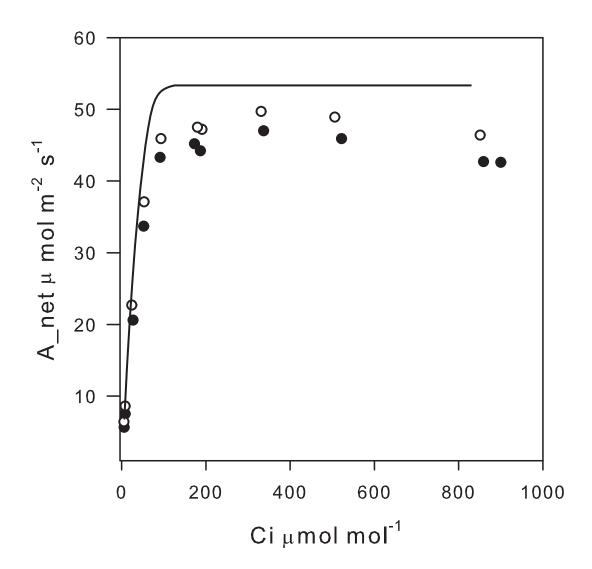


Figure 6

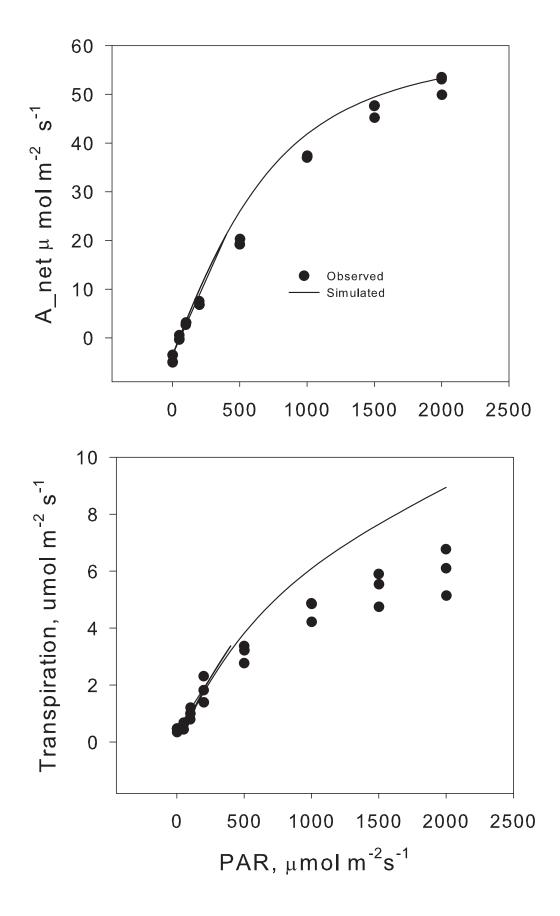


Figure 7