

Example 3: Multiaxial plasticity (rate independent)

$$\begin{aligned} \sigma_{ij}^{m+1} &= C_{ijkl} (\varepsilon_{kl}^{m+1} - \varepsilon_{kl}^{pl}) & \sigma_{ij}^{m+1} &= C_{ijkl} (\varepsilon_{kl}^{m+1} - \varepsilon_{kl}^{pl^{m+1}}) \\ \dot{\varepsilon}_{kl}^{pl} &= \Lambda \frac{\partial \Phi}{\partial \sigma_{kl}} & \xrightarrow{\text{Euler-backward}} & \varepsilon_{kl}^{pl^{m+1}} = \varepsilon_{kl}^{pl^m} + \Delta \Lambda \frac{\partial \Phi}{\partial \sigma_{kl}} \Big|^{m+1} \\ \Phi(\sigma_{ij}) \leq 0, \quad \Lambda \geq 0, \quad \Phi \Lambda &= 0 & \Phi(\sigma_{ij}^{m+1}) \leq 0, \quad \Delta \Lambda \geq 0, \quad \Phi \Delta \Lambda &= 0 \end{aligned} \quad (1)$$

Plastic corrector in general: nonlinear system of equations for $\varepsilon_{kl}^{pl^{m+1}}$, $\Delta \Lambda$ and hardening variables

Mises plasticity with isotropic hardening

$$\Phi = \sigma_{eq} - \sigma_y(\bar{\varepsilon}^{pl}) \quad \text{with} \quad \sigma_{eq} = \sqrt{\frac{3}{2} \sigma_{kl}^d \sigma_{kl}^d} \quad \rightarrow \quad \dot{\varepsilon}_{kl}^{pl} = \Lambda \frac{3}{2} \frac{\sigma_{kl}^d}{\sigma_{eq}} \quad (2)$$

$$\dot{\bar{\varepsilon}}^{pl} = \sqrt{\frac{2}{3} \dot{\varepsilon}_{kl}^{pl} \dot{\varepsilon}_{kl}^{pl}} = \Lambda \quad (3)$$

with isotropic elastic behavior $C_{ijkl} = \lambda \delta_{ij} \delta_{kl} + \mu (\delta_{ik} \delta_{jl} + \delta_{il} \delta_{jk}) = \frac{K}{3} \delta_{ij} \delta_{kl} + 2\mu I_{ijkl}^d$ with $I_{ijkl}^d = 1/2(\delta_{ik} \delta_{jl} + \delta_{il} \delta_{jk}) - 1/3 \delta_{ij} \delta_{kl}$

Euler-backward discretization of flow rule:

$$\sigma_{ij}^{m+1} = C_{ijkl} \left(\varepsilon_{kl}^{m+1} - \varepsilon_{kl}^{pl^m} - \Delta \Lambda \frac{3}{2} \frac{\sigma_{kl}^d}{\sigma_{eq}} \Big|^{m+1} \right) = \underbrace{C_{ijkl} (\varepsilon_{kl}^{m+1} - \varepsilon_{kl}^{pl^m})}_{\sigma_{ij}^{tr}} - 3\mu \Delta \Lambda \frac{\sigma_{ij}^d}{\sigma_{eq}} \Big|^{m+1} \quad (4)$$

split into hydrostatic and deviatoric part

$$\sigma_{kk}^{m+1} = \sigma_{kk}^{tr}, \quad \sigma_{ij}^{d^{m+1}} = \sigma_{ij}^{d^{tr}} - 3\mu \Delta \Lambda \frac{\sigma_{ij}^d}{\sigma_{eq}^{m+1}} \quad (5)$$

rearranging

$$\sigma_{eq}^{m+1} = \sigma_{eq}^{tr} - 3\mu \Delta \Lambda \quad (6)$$

$$\sigma_{ij}^{d^{m+1}} = \frac{\sigma_{eq}^{m+1}}{\sigma_{eq}^{tr}} \sigma_{ij}^{d^{tr}} = \frac{\sigma_{eq}^{tr} - 3\mu \Delta \Lambda}{\sigma_{eq}^{tr}} \sigma_{ij}^{d^{tr}} \quad (7)$$

- hydrostatic part is purely elastic
- stress deviator $\sigma_{ij}^{d^{m+1}}$ is colinear to its trial value $\sigma_{ij}^{d^{tr}}$

\Rightarrow only necessary in plastic corrector: (numerical) determination of $\Delta \Lambda$ from yield condition $\Phi^{m+1} = \sigma_{eq}^{tr} - 3\mu \Delta \Lambda - \sigma_y(\bar{\varepsilon}^{pl^m} + \Delta \Lambda) = 0$

"radial return mapping"

- stress update: $\sigma_{ij}^{m+1} = \frac{1}{3} \delta_{ij} \sigma_{kk}^{tr} + \frac{\sigma_{eq}^{tr} - 3\mu \Delta \Lambda}{\sigma_{eq}^{tr}} \sigma_{ij}^{d^{tr}}$
- algorithmically consistent tangent stiffness:
 - implicit differentiation of $\Phi^{m+1} = 0$: $1 - \frac{\partial \Delta \Lambda}{\partial \sigma_{eq}^{tr}} (3\mu + h) = 0$

$$C_{ijkl}^t = \frac{d\sigma_{ij}^{m+1}}{d\varepsilon_{kl}^{m+1}} = \frac{1}{3} K \delta_{ij} \delta_{kl} + 2\mu \frac{\sigma_{eq}^{tr} - 3\mu \Delta \Lambda}{\sigma_{eq}^{tr}} I_{ijkl}^d - 3\mu \frac{3\mu}{3\mu + h} \frac{\sigma_{eq}^{tr} - \Delta \Lambda h}{(\sigma_{eq}^{tr})^3} \sigma_{ij}^{d^{tr}} \sigma_{kl}^{d^{tr}}$$

\Rightarrow to Voigt notation $\underline{\underline{C}}_t$