

## Exercise 4: Implementation of a three-dimensional von Mises plasticity model with linear hardening at small strains

### Problem 5.1

The stress-update algorithm for a von Mises plasticity model with linear isotropic and kinematic hardening is given in the algorithmic box 1

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#### Alg. 1 Radial return stress-update algorithm for $J_2$ -plasticity with linear hardening

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... Given: history information  $\{\epsilon_n^p, \alpha_n, \alpha_n\}$  and current total strain  $\epsilon_{n+1}$  ...
... Compute trial elastic state: (elastic prediction) ...
1:  $\text{dev}(\epsilon_{n+1}) = \epsilon_{n+1} - \frac{1}{3} \text{tr}(\epsilon_{n+1}) \mathbf{I}$ 
2:  $\text{dev}(\sigma_{n+1}^{\text{trial}}) = 2\mu \text{dev}(\epsilon_{n+1}^{\text{e,trial}}) = 2\mu [\text{dev}(\epsilon_{n+1}) - \epsilon_n^p]$ 
3:  $\beta_{n+1}^{\text{trial}} = H\alpha_n, \quad \beta_{n+1}^{\text{trial}} = h\alpha_n$ 
4:  $\xi_{n+1}^{\text{trial}} = \text{dev}(\sigma_{n+1}^{\text{trial}}) - \beta_{n+1}^{\text{trial}}$ 
5:  $\mathbf{n}_{n+1}^{\text{trial}} = \frac{\xi_{n+1}^{\text{trial}}}{\|\xi_{n+1}^{\text{trial}}\|}$ 
6:  $\phi_{n+1}^{\text{trial}} = \|\xi_{n+1}^{\text{trial}}\| - \sqrt{\frac{2}{3}} [\sigma_{y0} + \beta_{n+1}^{\text{trial}}]$ 
... Check for elastic-plastic loading ...
7: if  $\phi_{n+1}^{\text{trial}} < 0$  then
... elastic step ...
8:  $\text{dev}(\sigma_{n+1}) = \text{dev}(\sigma_{n+1}^{\text{trial}})$ 
9:  $\mathbb{C}_{n+1}^{\text{dev}} = 2\mu \mathbb{P}_{\text{sym}}$ 
10:  $\epsilon_{n+1}^p = \epsilon_n^p, \quad \alpha_{n+1} = \alpha_n, \quad \alpha_{n+1} = \alpha_n$ 
11: else
... Radial return (plastic correction) ...
12:  $\gamma_{n+1} = \frac{\phi_{n+1}^{\text{trial}}}{2\mu + H + \frac{2}{3}h}$ 
13:  $\text{dev}(\sigma_{n+1}) = \text{dev}(\sigma_{n+1}^{\text{trial}}) - 2\mu \gamma_{n+1} \mathbf{n}_{n+1}^{\text{trial}}$ 
14:  $\epsilon_{n+1}^p = \epsilon_n^p + \gamma_{n+1} \mathbf{n}_{n+1}^{\text{trial}}, \quad \alpha_{n+1} = \alpha_n + \gamma_{n+1} \mathbf{n}_{n+1}^{\text{trial}}, \quad \alpha_{n+1} = \alpha_n + \sqrt{\frac{2}{3}} \gamma_{n+1}$ 
15:  $\beta_1 = 1 - \frac{\phi_{n+1}^{\text{trial}}}{\|\xi_{n+1}^{\text{trial}}\|} \frac{1}{1 + \frac{H}{2\mu} + \frac{h}{3\mu}}, \quad \beta_2 = \left[ 1 - \frac{\phi_{n+1}^{\text{trial}}}{\|\xi_{n+1}^{\text{trial}}\|} \right] \frac{1}{1 + \frac{H}{2\mu} + \frac{h}{3\mu}}$ 
16:  $\mathbb{C}_{n+1}^{\text{dev}} = 2\mu \beta_1 \mathbb{P}_{\text{sym}} - 2\mu \beta_2 \mathbf{n}_{n+1}^{\text{trial}} \otimes \mathbf{n}_{n+1}^{\text{trial}}$ 
17: end if
... Add spherical contribution to stress and moduli: ...
18:  $\sigma_{n+1} = \text{dev}(\sigma_{n+1}) + \kappa \text{tr}(\epsilon_{n+1}) \mathbf{I}$ 
19:  $\mathbb{C}_{n+1} = \mathbb{C}_{n+1}^{\text{dev}} + \kappa \mathbf{I} \otimes \mathbf{I}$ 

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- Implement the stress-update algorithm in the function `vmises.m`, test your implementation for different hardening parameters by running the isochoric tensile test given in `test_suite_isochoric_tension.m`. Compare your results with the analytic solution.
- Extent your function `vmises.m` to include the algorithmic tangent. Run the uniaxial tensile test, implemented in `drive.m`, check the convergence and compare to the analytic solution.