

Outline

- ◆ Introduction
- ◆ Theory of frequency conversion
- ◆ Characteristic performances of mixers
- ◆ Active mixers
 - Single Ended (SEM) → Gate Mixer / Drain Mixer
 - Gilbert Cell → DBDM Double Balanced Differential Mixer

- ◆ Passive Mixers
 - Diodes → SEM / SBM / DBM
 - Cold FETs → SEM / SBM
- ◆ IRM: Image Reject Mixers

Passive “Resistive” Mixers

Multiplication: Resistive Mixers

- ◆ **Principle** : Implementing a multiplication by using the Ohm's law

$$V = R.I \quad \text{or} \quad I = G.V$$

$$V_{\text{out}}(t) = R(t).I_{\text{in}}(t) \quad \text{or} \quad I_{\text{out}}(t) = G(t).V_{\text{in}}(t)$$

- ◆ **Varying nonlinear conductance $G(t)$** = nonlinear element driven by a large signal @ LO
→ Obtain a time varying conductance and its required frequency spectrum

- ◆ **Expansion of $G(t)$ in Fourier transform:**

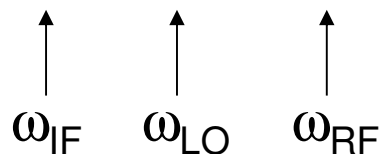
$$G(t) = G_0 + G_1.\cos(\omega_{\text{LO}}.t) + G_2.\cos(2\omega_{\text{LO}}.t) + G_3.\cos(3\omega_{\text{LO}}.t) + \dots$$

Ideal term

Spurs for a fundamental mixer (*However 2nd harmonic can be used for subharmonic mixers*)

- ◆ The mixing is obtained by applying a low signal V_{RF} at the input of the time varying conductance to create the required converted current at IF

$$I_{\text{S}}(t) = G(t) \cdot V_{\text{RF}}(t)$$



Principle of Diode Mixers

Minimum of conversion losses for passive mixers

◆ Ideal case of a diode mixer :

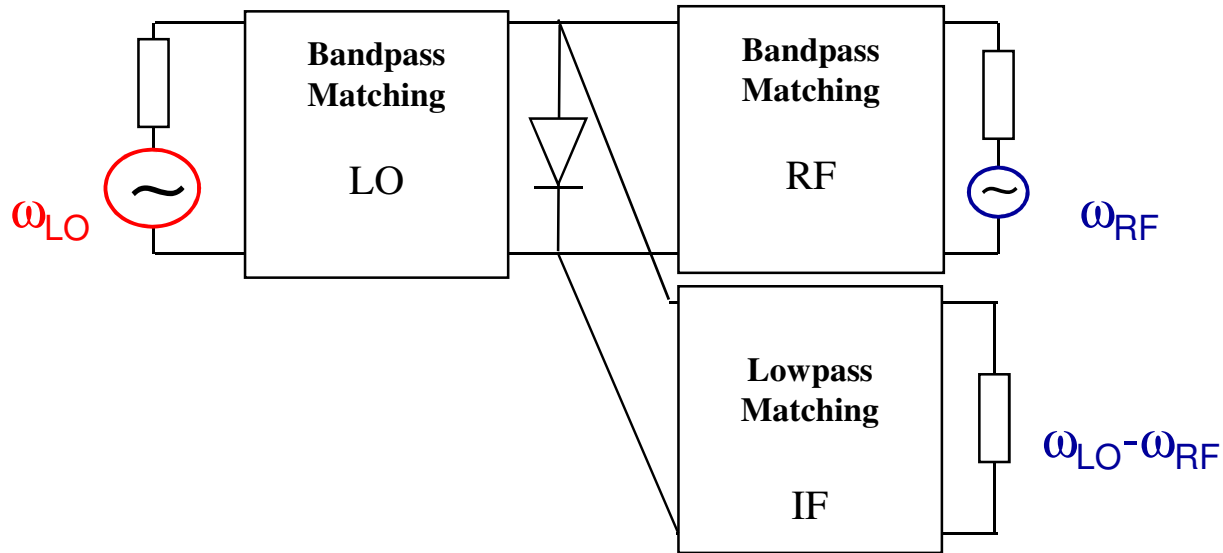
$$\rightarrow L_{C_{\text{MIN}}} \cong 4 \text{ dB}$$

◆ Actual case :

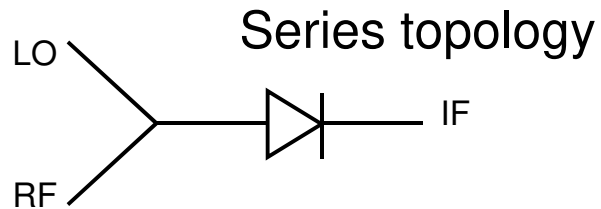
$$L_{C_{\text{MIN}}} \approx 5 \text{ à } 6 \text{ dB}$$

$$L_C = f \left[I-V_{\text{NL}}, V_{\text{LO}}(t), Z_L(\omega_{\text{SPURS}}) \right]$$

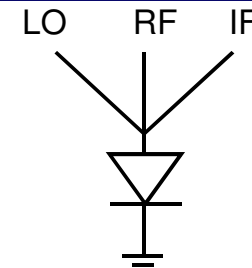
Diode-based SEM



Critical matching constraints for single diode mixers



Parallel topology



Advantages:

- Low L_c and P_{LO}

Disadvantages:

- No suppression of spurs
- Bandwidth and isolation are greatly limited by critical filtering issues
- Filter losses increase $L_c \rightarrow$ Very few diode-based SEM

SBM and DBM diode-based mixers

SBM: Single Balanced Mixer = 2 SEM with couplers or baluns

DBM: Double Balanced Mixer = 2 SBM with couplers or baluns



Advantages

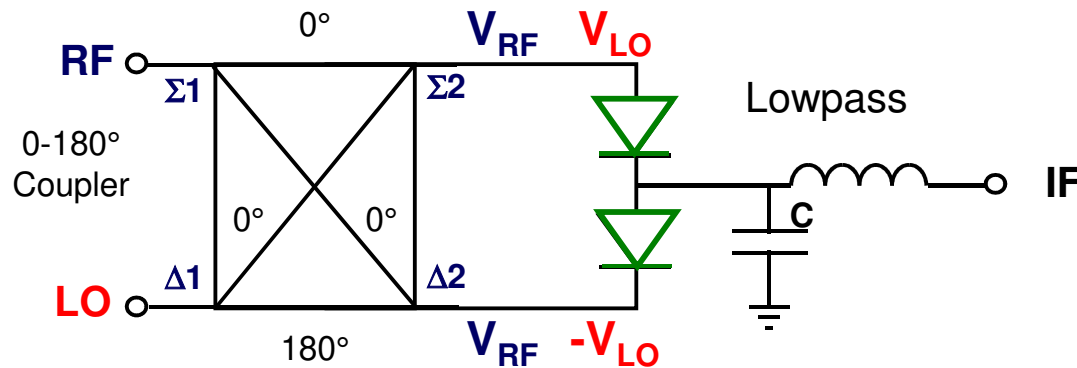
- Suppression of some spurs by out of phase recombination
- Good LO-RF Isolation and sometimes LO-IF isolation without filtering issues

Disadvantages

- Requirement of higher levels of LO power

Example of a diode-based SBM (LO at Δ port)

• Architecture with 180° coupler (LO @ Δ)



180° Coupler

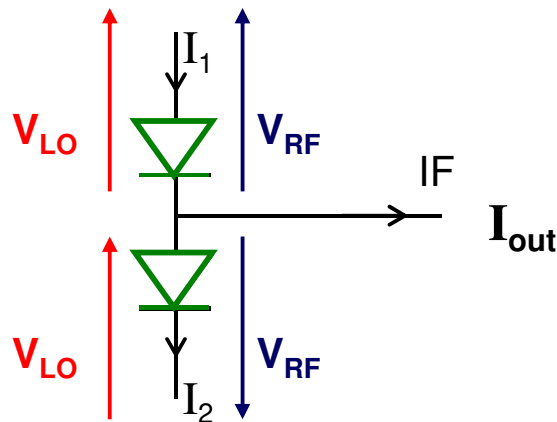
Input Matching @LO/RF \approx Input Matching@LO/RF of coupler

Isolation LO-RF \approx Isolation LO-RF of coupler

LO @ $\Sigma \rightarrow \text{mix}[\text{EH}(\text{LO}), *]$ rejected

LO @ $\Delta \rightarrow \text{mix}[*, \text{EH}(\text{RF})]$ rejected

• Operation mode (LO @ Δ)



Diode current law

$$I(V) = \mathbf{F}(V) = a.V + b.V^2 + c.V^3 + \dots$$

$$I_1 = \mathbf{F}(V_{\text{LO}} + V_{\text{RF}})$$

$$I_2 = \mathbf{F}(V_{\text{LO}} - V_{\text{RF}})$$

$$V_{\text{LO}}^p \cdot V_{\text{RF}}^q \rightarrow \pm p.\omega_{\text{LO}} \pm q.\omega_{\text{RF}}$$

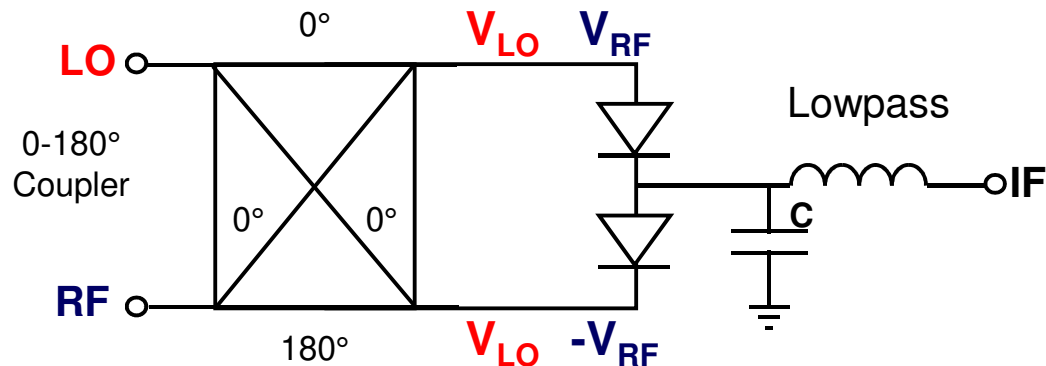
$$I_{\text{OUT}} = I_1 - I_2 = 0 \Leftrightarrow \omega = \pm m.\omega_{\text{LO}} \pm n.\omega_{\text{RF}}$$

If **n is even** because $(V_{\text{RF}})^n = (-V_{\text{RF}})^n$

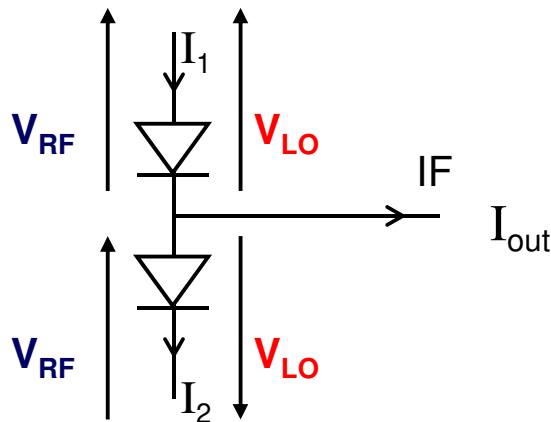
→ $\omega_{\text{LO}}, 2(\omega_{\text{LO}} - \omega_{\text{RF}}), \dots$ suppressed @ IF port \rightarrow (LO-IF Isolation) ...
 $n=0$ $n=2$

Diode-based SBM : LO and RF ports are reversed (LO at Σ port)

• Architecture with 180° coupler (LO @ Σ)



• If LO and RF are reversed



$$I(V) = F(V) = a.V + b.V^2 + c.V^3 + \dots$$

$$I_1 = F(V_{RF} + V_{LO})$$

$$I_2 = F(V_{RF} - V_{LO})$$

$$V_{LO}^p \cdot V_{RF}^q \rightarrow p\omega_{LO} \pm q\omega_{RF}$$

$$I_{OUT} = I_1 - I_2 = 0 \Leftrightarrow \omega = \pm m.\omega_{LO} \pm n.\omega_{RF}$$

$$\text{If } m \text{ is even because } (V_{LO})^m = (-V_{LO})^m$$



$\omega_{RF}, 2(\omega_{LO} - \omega_{RF}), \dots$ suppressed @IF port \rightarrow (RF-IF Isolation) ...

$m=0 \quad m=2$

Less critical

Diode-based SEM

- Properties are linked to the architecture (Baluns, Couplers, ...)
- Conversion losses of SBM are higher than conversion losses of SEM
(Coupler losses, Non ideal phase shift and amplitude balance ...)
- SBM enable to suppress critical spurs and enhance isolations



Diode-based SBM are more efficient than diode-based SEM

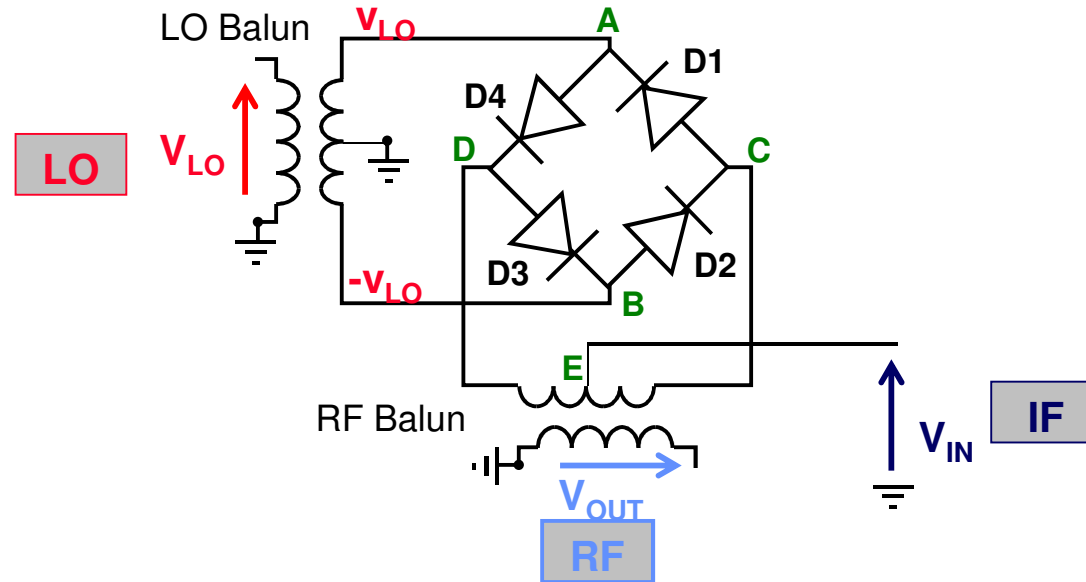
Diode-based DBM

A diode-based DBM
integrates 2 pairs of diodes

Diode-based DBM are preferred to SBM
if the isolation requirements are more critical than the conversion loss specifications

Example of diode-based DBM : Ring oscillator

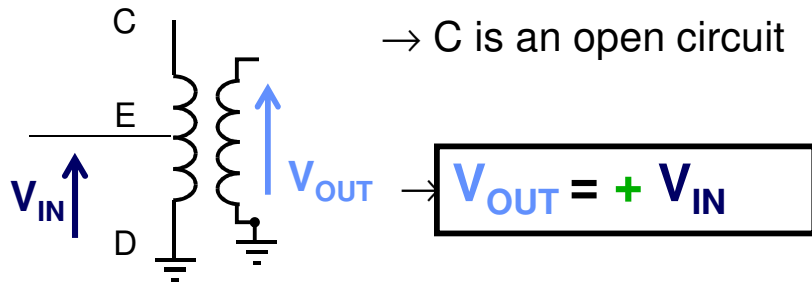
•Architecture



•Operation principle (Diode = switch controlled by LO)

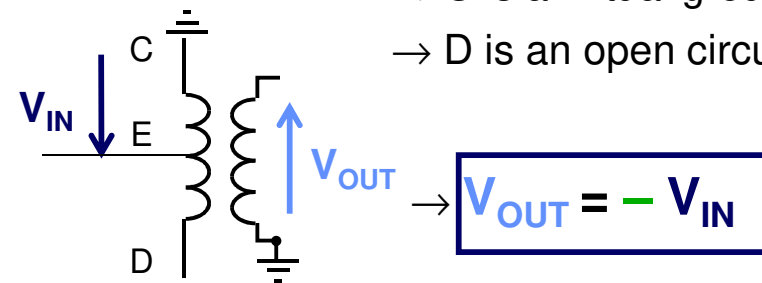
If ($V_{LO} > 0$) $\rightarrow (V_A > V_B) \rightarrow (D_1, D_2) = \text{OFF}$ and $(D_3, D_4) = \text{ON}$

$\rightarrow D$ is a virtual ground
 $\rightarrow C$ is an open circuit



Si ($V_{LO} < 0$) $\rightarrow (V_A < V_B) \rightarrow (D_1, D_2) = \text{ON}$ and $(D_3, D_4) = \text{OFF}$

$\rightarrow C$ is a virtual ground
 $\rightarrow D$ is an open circuit



$$\rightarrow V_{OUT}(t) = \text{sign}[V_{LO}(t)] \times V_{IN}(t) \quad \text{avec} \quad \text{sign}[V_{LO}(t)] = \frac{4}{\pi} \left[\cos(\omega_{LO}t) - \frac{1}{3} \cos(3\omega_{LO}t) + \frac{1}{5} \cos(5\omega_{LO}t) - \dots \right]$$

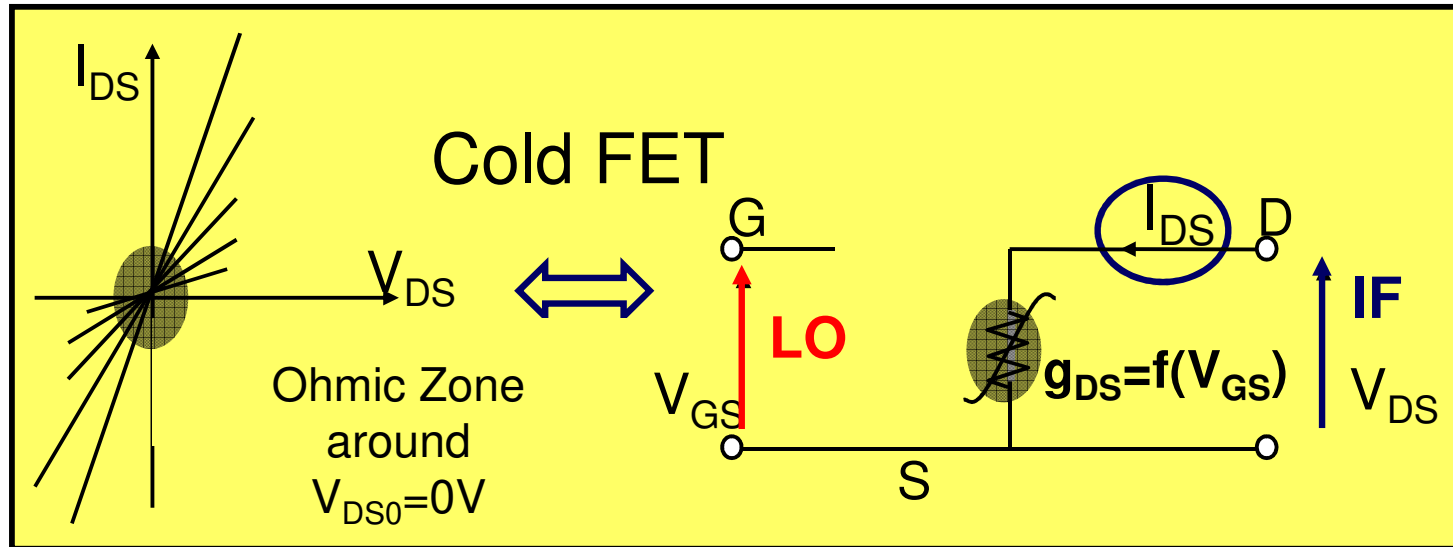


$$V_{OUT} = 0 \Leftrightarrow \omega = m \cdot \omega_{LO} \pm n \cdot \omega_{IF} \quad / \quad (m \text{ or } n) \text{ even} \rightarrow \omega_{LO}, \omega_{IF} \dots \text{ suppressed @ RF port}$$

Cold-FET mixers : Principle

Main advantages : High linearity and No Consumption

Principle of cold-FET resistive mixers

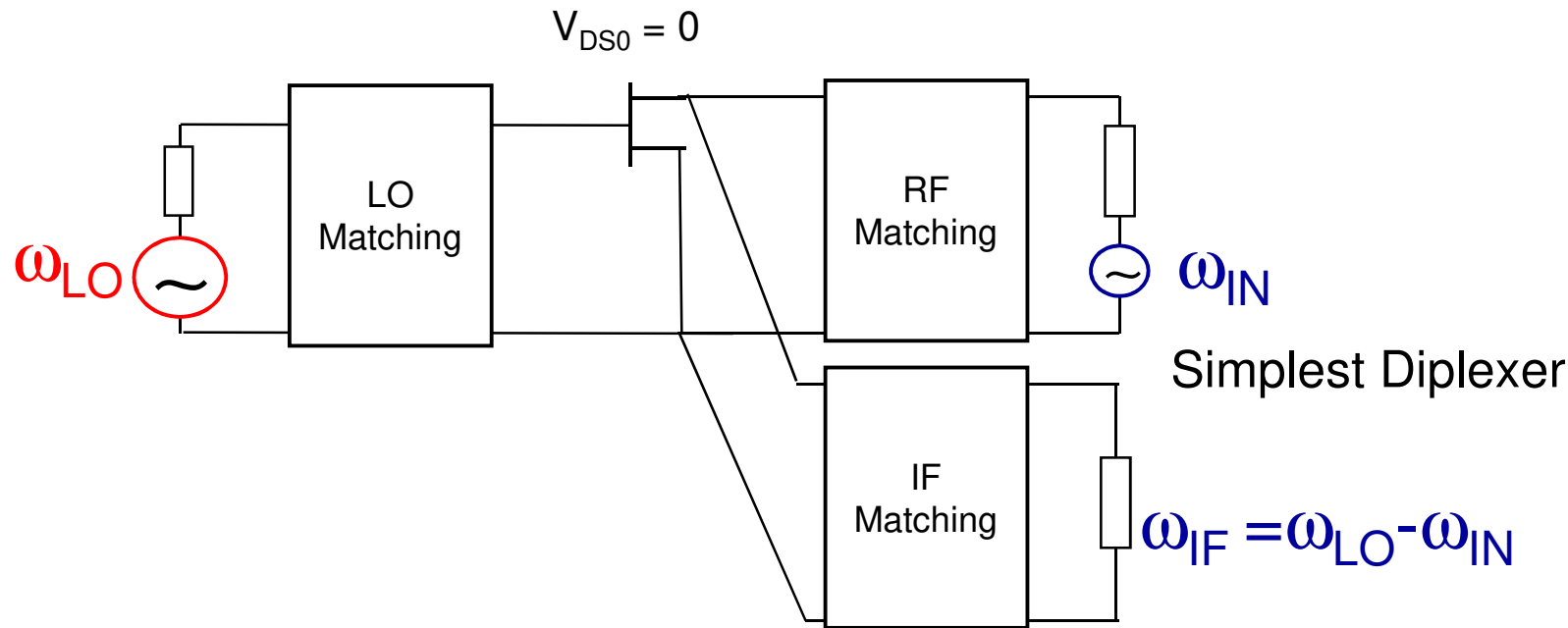


Not biased Drain

→ Transconductance g_m is zero @ $V_{DS0}=0$

→ Resistive Nonlinearity $R_{DS}(V_{GS})$ between drain and source

Cold-FET advantages



→ Simplified design constraints

- better LO-RF isolation due to the intrinsic G-D isolation of FETs (depends on C_{gd} and ω)
- limited interactions between matching circuits (LO @ gate port and $\omega_{RF} \gg \omega_{IF}$ @ drain port)
- higher linear voltage swing of RF signal from 0 to knee voltage → higher linearity
- Only mixer that can be efficiently used in SEM configuration

→ Other solutions: SBM and DBM cold-FET mixers

Comparison (Diode / Cold FET)

- Conversion losses

→ $L_C(\text{Diode Mixers}) < L_C(\text{Cold-FET mixers})$ because $R_{\text{MIN}}(\text{Diode}) < R_{\text{MIN}}(\text{Cold-FET})$

- Linearity/Saturation

- Linearity of diode-based mixer is limited to very low level of RF signal (exponential current)
- Linearity of cold-FET mixer is limited to moderate level of RF signal (ohmic zone)
→ Higher linearity of cold-FET and higher output power

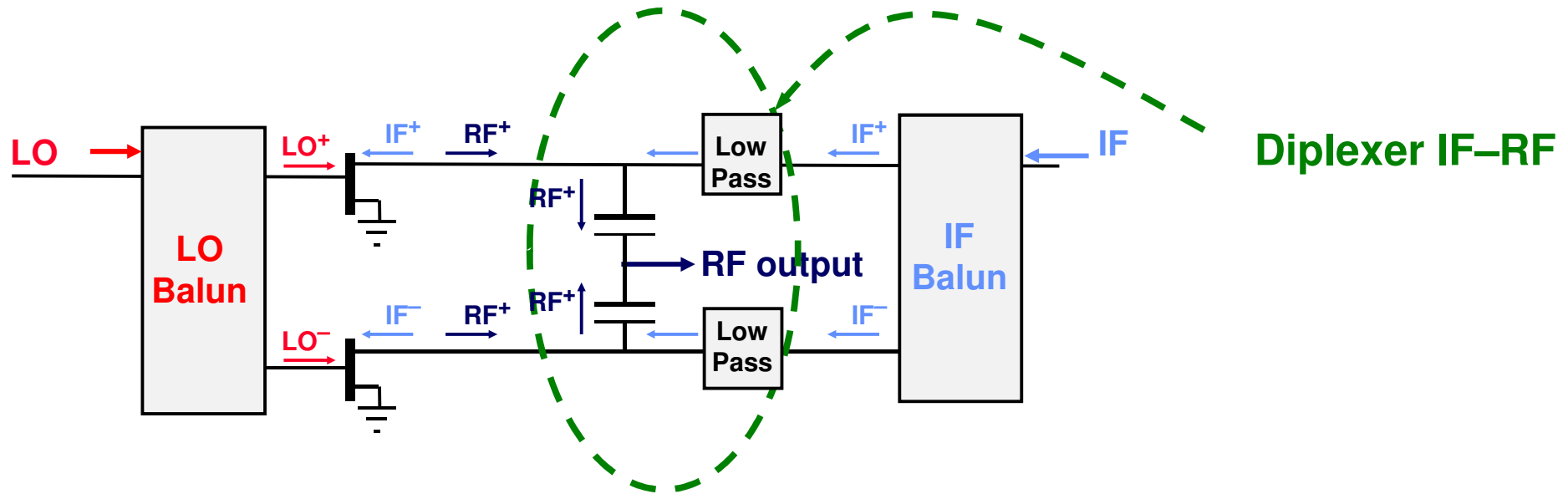
- Isolations

- Diodes do not have intrinsic isolation → can only be used in complex balanced architectures
- Cold-FETs have the intrinsic G-D isolation → can be used as SEM or balanced topologies

Cold-FET SBM

Cold-FET SBM

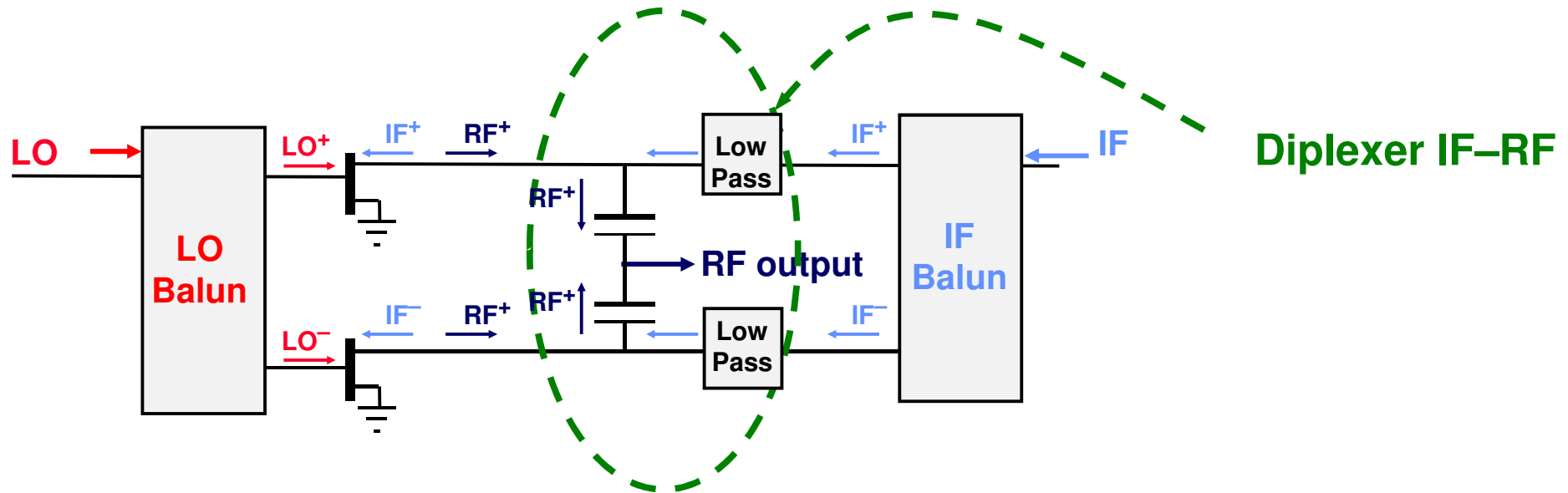
- Example of SBM with LO and IF baluns (emission)
- Pair of cold-FETs



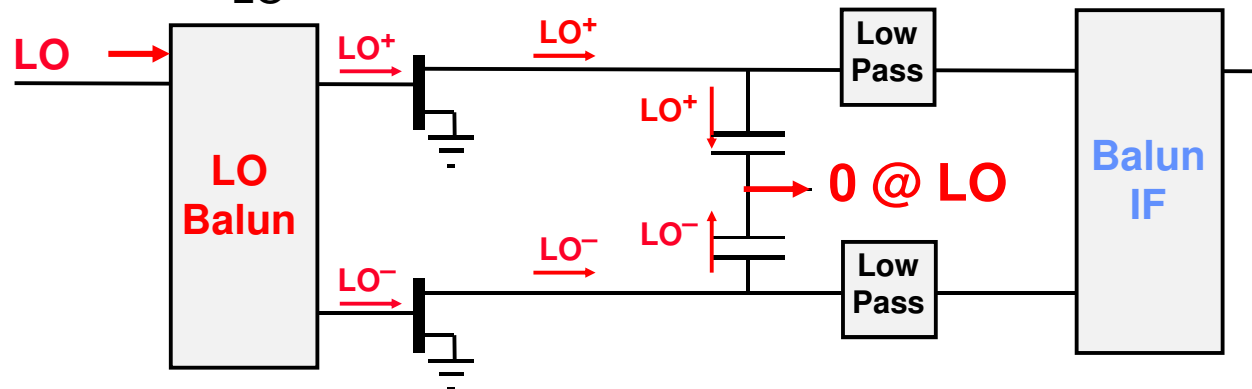
Cold-FET SBM

- Example of SBM with LO and IF baluns (emission)

- Pair of cold-FETs



- Balanced architecture $\Rightarrow \omega_{LO}$ suppressed @ drain port

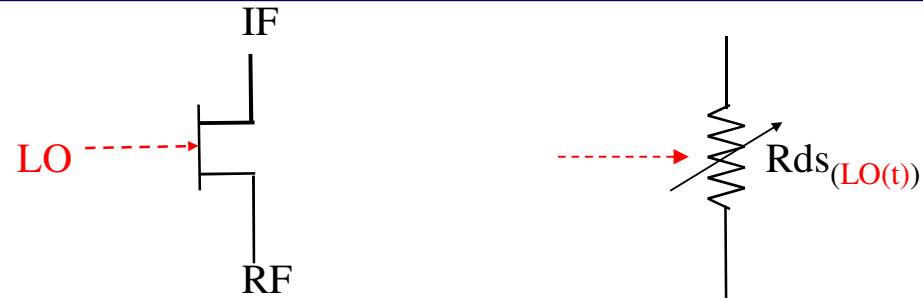


Cold-FET DBM

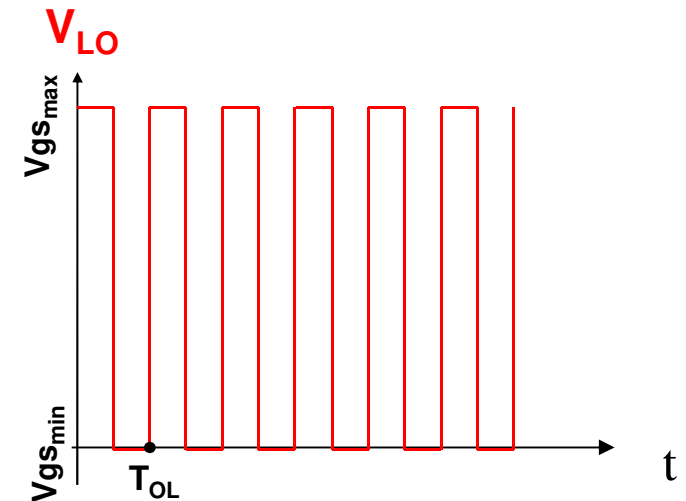
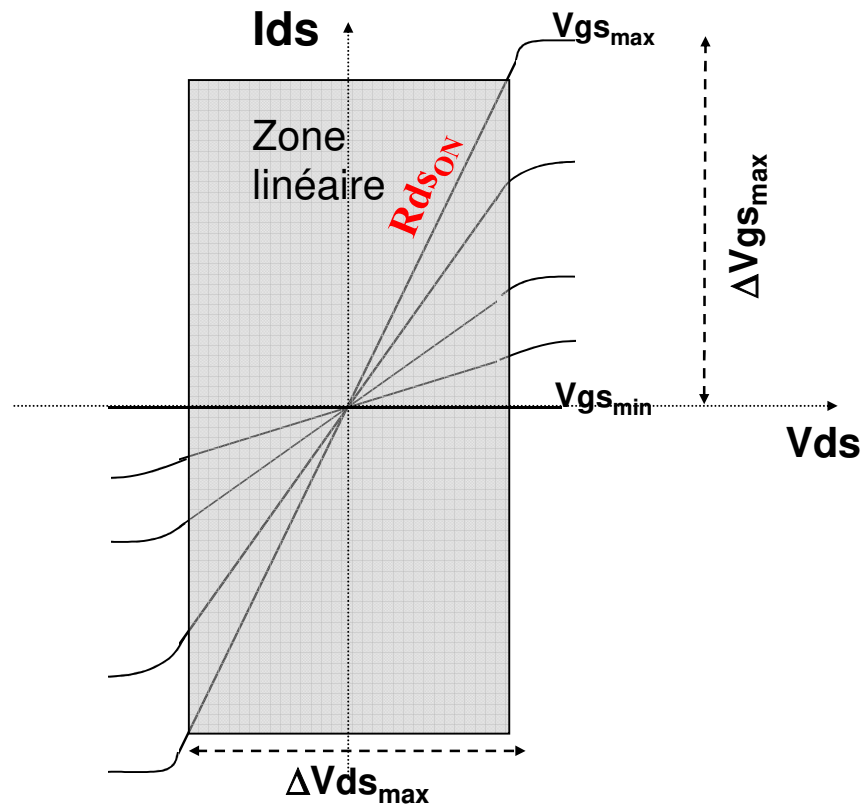
Ring mixer

4 Cold-FETs + 3 Baluns (RF, IF, LO)

Switch mode of Cold-FET

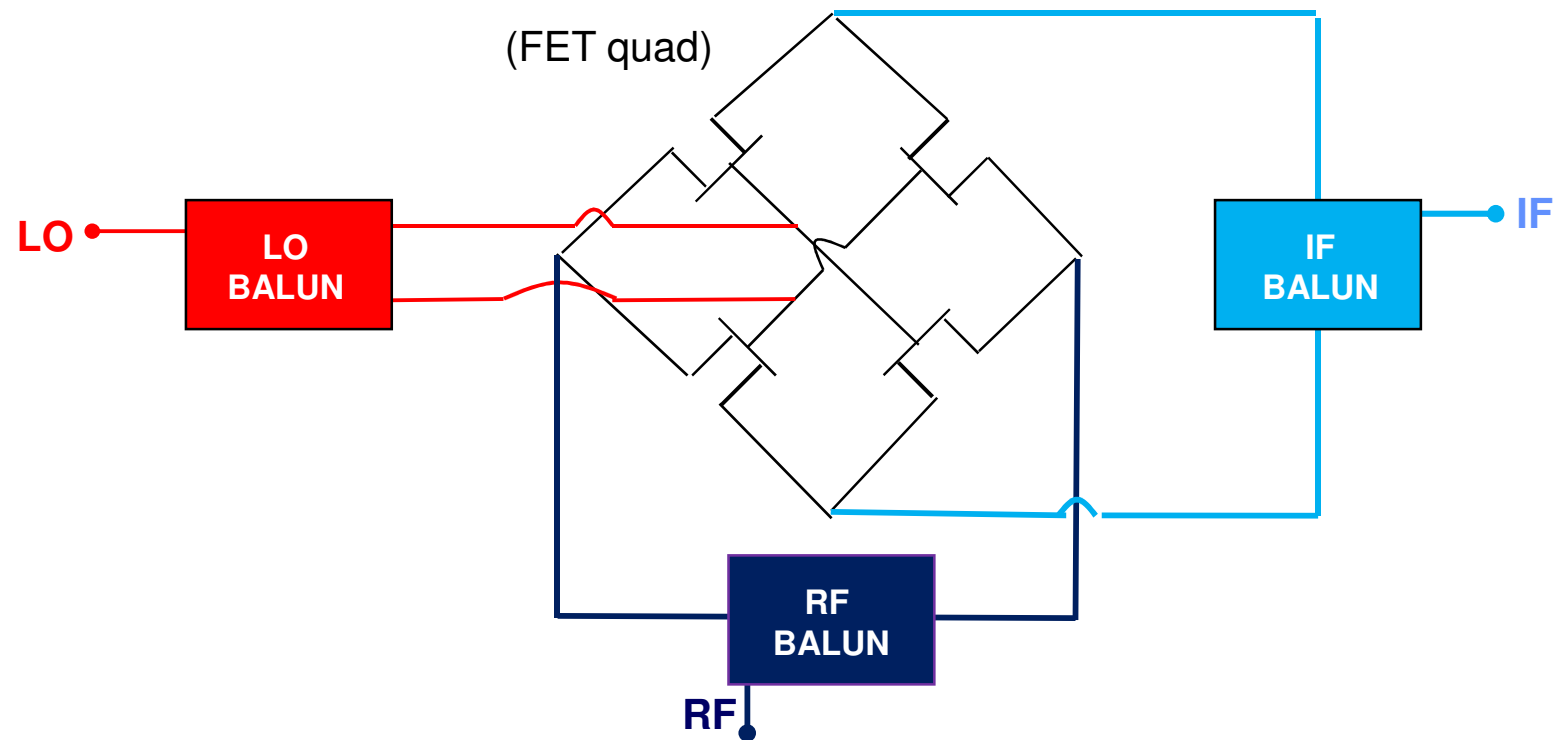


The Cold-FET is switched between $R_{DS_{ON}}$ (minimum value of R_{DS}) and ∞ (maximum value of R_{DS})

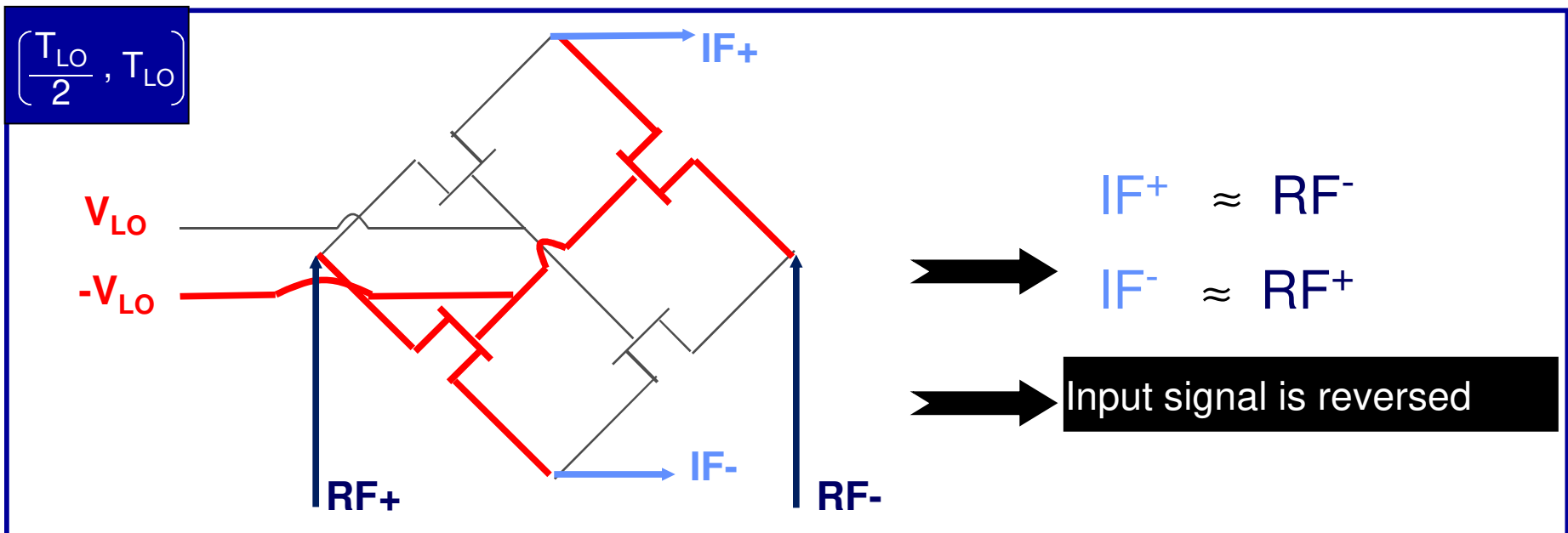
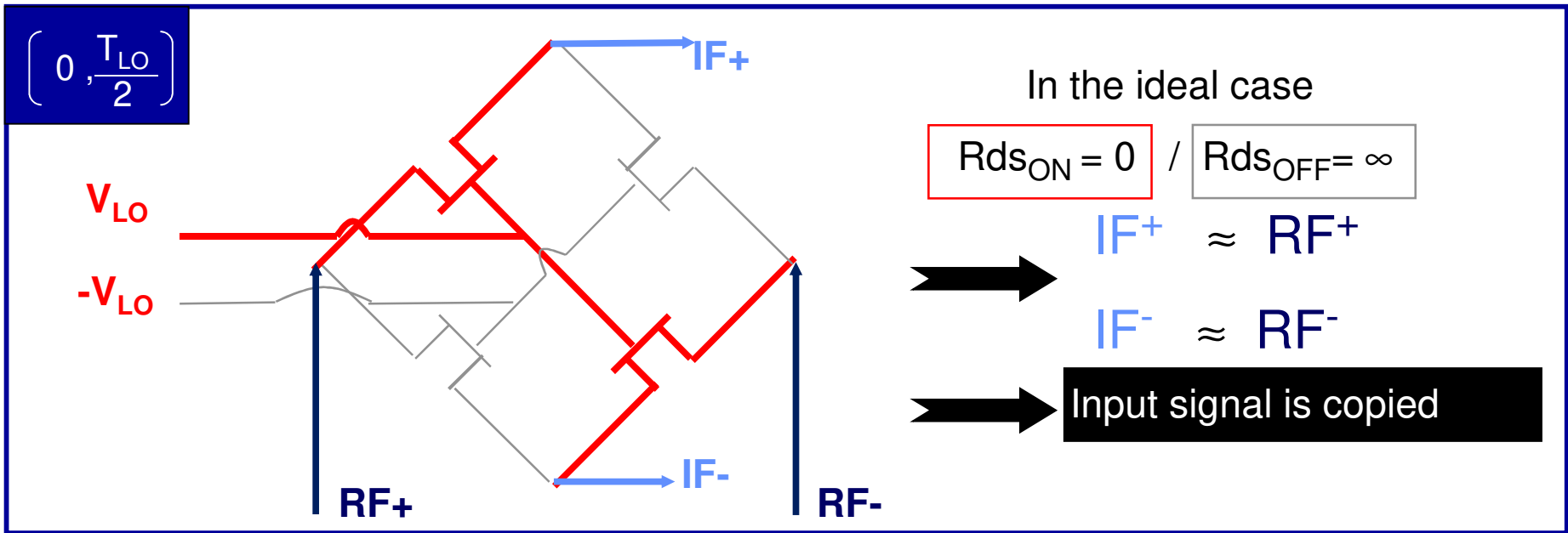


If the transistor size is increased $\rightarrow \left\{ I_{DS_{MAX}} \uparrow \right\} \rightarrow \left\{ R_{DS_{ON}} \downarrow \right\} \rightarrow \left[\text{Conversion losses} \downarrow \right]$
 However $\rightarrow \left\{ C_{GS} \uparrow \right\} \rightarrow \left[\text{Frequency limitation} \uparrow \right]$

Cold-FET « Switch Mode Mixer » : Ring DBM

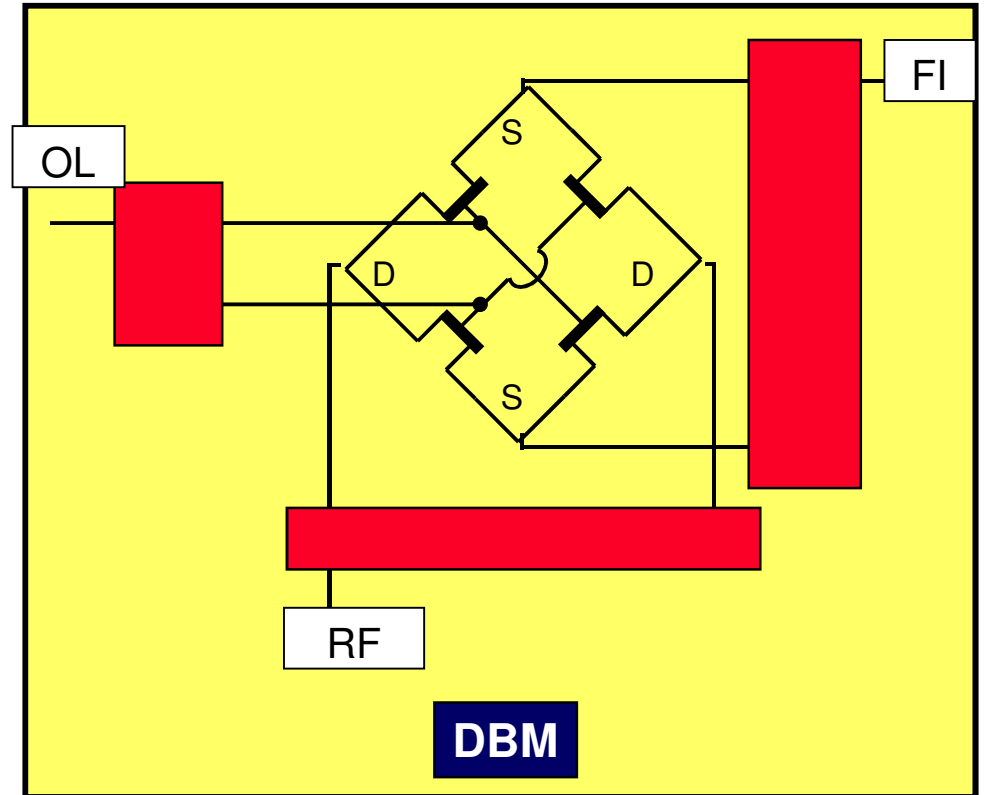
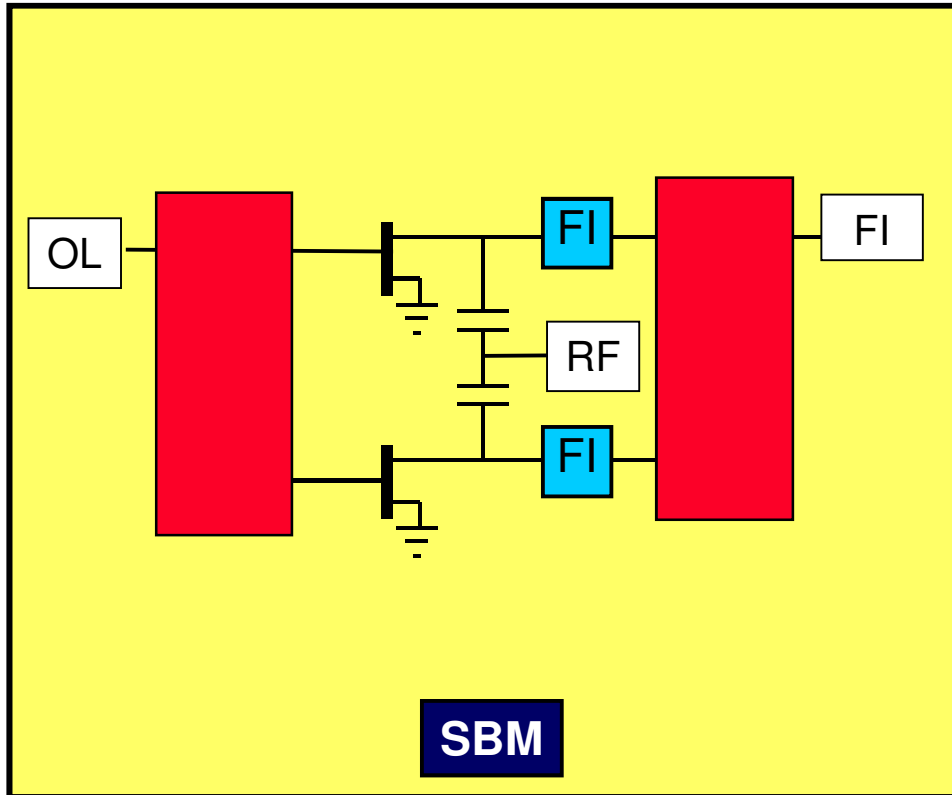


Operating principle of the ring Cold-FET DBM



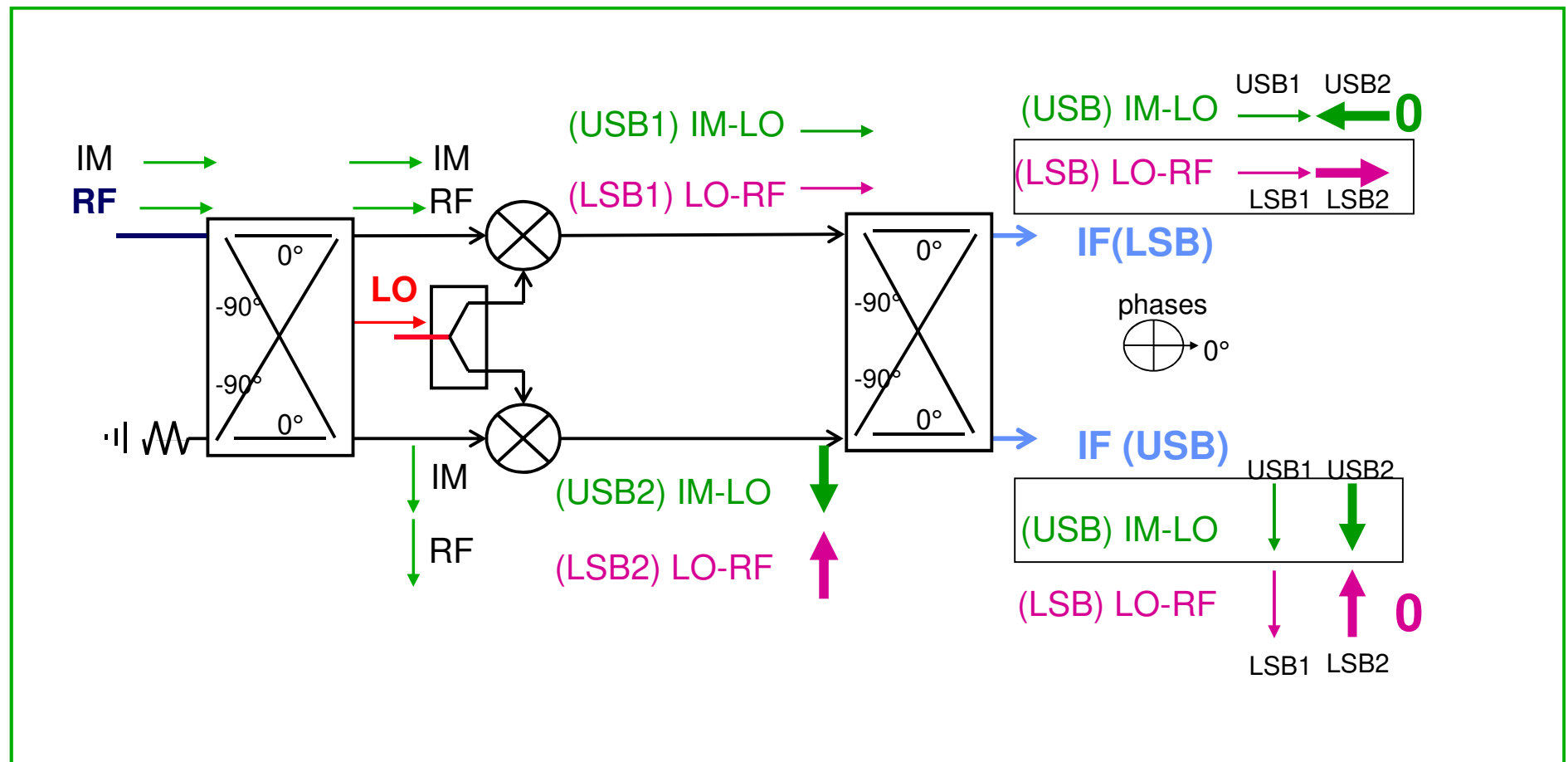
Main Cold-FET mixer architectures

◆ Cold-FET Mixers

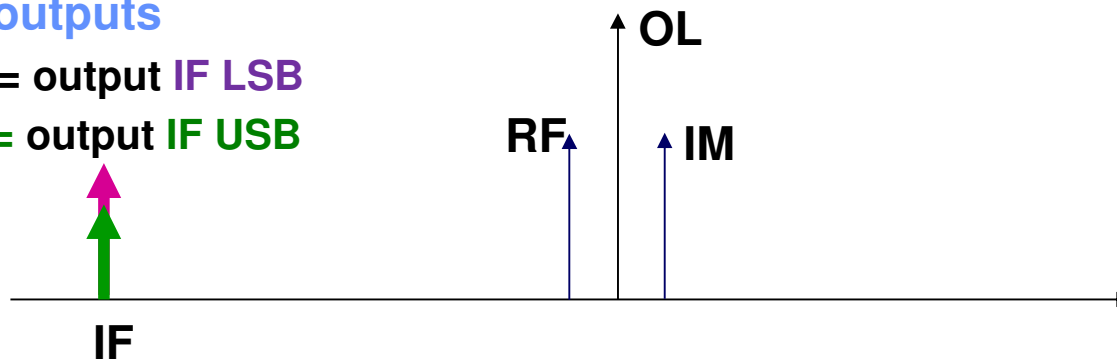


Example of IRM (Image Rejection Mixer)

Example of IRM



IF outputs
 = **(LO-RF)** = output **IF LSB**
 = **(IM-LO)** = output **IF USB**



Mixer