

# MICROWAVE ENGINEERING

Lecture 22:

Microwave  
Resonators



# Series and parallel resonant circuits

## Series Resonant Circuit

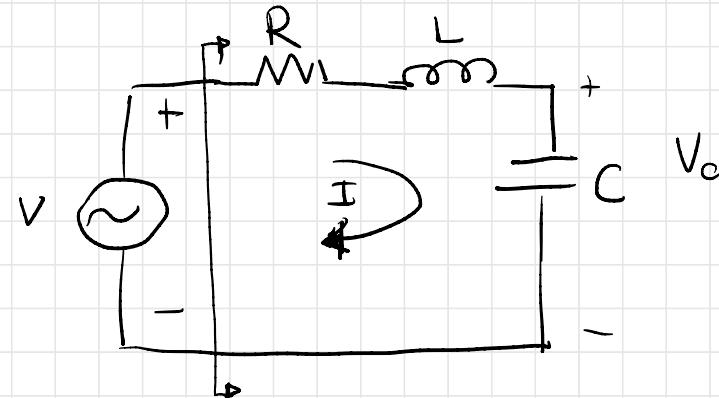
The input impedance is:

$$Z_{IN} = R + j\omega L - j/\omega C = \frac{2P_{IN}}{|I|^2}$$

$\curvearrowleft$

Power delivered to the resonator is

$$\begin{aligned}
 P_{IN} &= \frac{1}{2} VI^* = \underbrace{\frac{1}{2} Z_{IN} |I|^2}_{=} = \frac{1}{2} Z_{IN} \left| \frac{V}{Z_{IN}} \right|^2 = \\
 &= \frac{1}{2} |I|^2 \left( \underline{R + j\omega L - \frac{j}{\omega C}} \right) = P_{loss} + 2j\omega (W_m - W_e)
 \end{aligned}$$



Power dissipated by the resistor is:

$$P_{\text{loss}} = \frac{1}{2} |I|^2 R$$

Stored magnetic energy  $W_m = \frac{1}{4} |I|^2 L$

Stored electric energy  $W_e = \frac{1}{4} |V_c|^2 C = \frac{1}{4} |I|^2 \frac{1}{\omega^2 C}$

The circuit is at resonance when  $\boxed{W_m = W_e}$



$$P_{IN} = P_{\text{loss}}$$

$$Z_{IN} = \frac{2 P_{IN}}{|I|^2} = \frac{2 P_{\text{loss}}}{|I|^2} = 2 \frac{\frac{1}{2} |I|^2 R}{|I|^2} = R \quad \text{PURELY REAL}$$

When  $W_m = W_e \Rightarrow \frac{1}{4} |I|^2 L = \frac{1}{4} |I|^2 \frac{1}{W^2 C} \Rightarrow$

$$W_0 = \frac{1}{\sqrt{LC}}$$

RESONANCE  
FREQUENCY

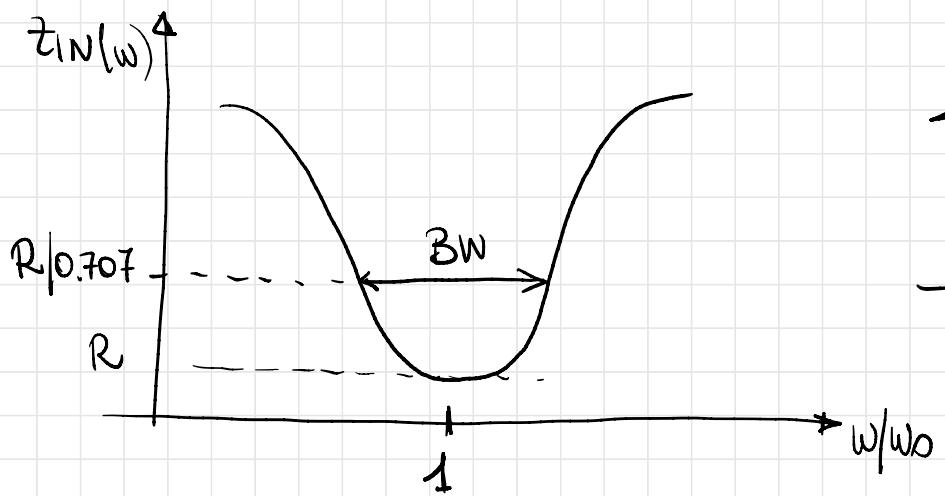
### Quality Factor

$$Q = \omega \frac{\text{average energy stored}}{\text{energy loss/sec}} = \omega \frac{W_m + W_e}{P_{loss}}$$

AT resonance :

$$Q = \omega_0 \frac{2W_m}{P_{loss}} = \omega_0 \frac{2 \frac{1}{4} |I|^2 L}{\frac{1}{2} |I|^2 R} = \omega_0 \frac{L}{R} =$$

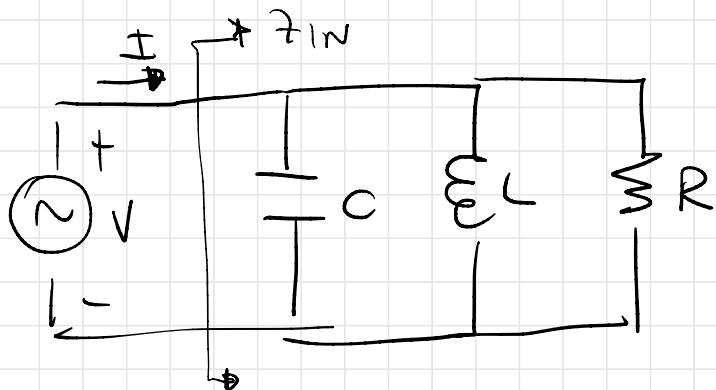
$$= \frac{1}{\sqrt{LC}} \cdot \frac{L}{R} = \frac{1}{R} \sqrt{\frac{L}{C}}$$



$$BW = \frac{1}{Q}$$

### PARALLEL RESONANT CIRCUIT

$$Z_{IN} = \left( \frac{1}{R} + \frac{1}{j\omega L} + j\omega C \right)^{-1}$$



Power delivered at the resonator is:

$$\begin{aligned} P_{IN} &= \frac{1}{2} VI^* = \frac{1}{2} Z_{IN} |I|^2 = \frac{1}{2} \underbrace{\frac{|V|^2}{Z_{IN}^*}}_{\text{ }} = \frac{1}{2} |V|^2 \left( \frac{1}{R} + \frac{1}{\omega L} - j\omega \right) \\ &= P_{loss} + \omega \left( W_m - W_e \right) \end{aligned}$$

Power loss  $P_{loss} = \frac{1}{2} \frac{|V|^2}{R}$

Stored electric energy  $W_e = \frac{1}{4} |V|^2 C$

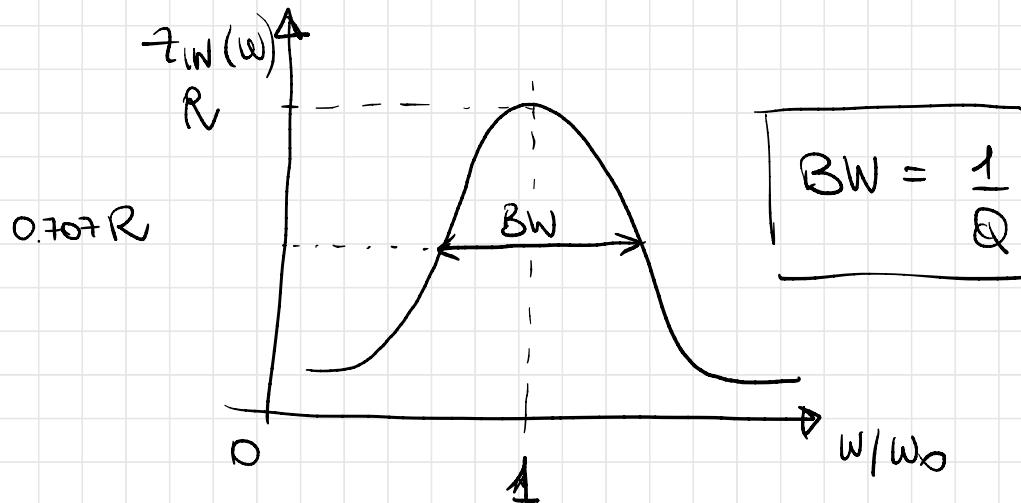
Stored magnetic energy  $W_m = \frac{1}{4} |I|^2 L = \frac{1}{4} |V|^2 \frac{1}{\omega^2 L}$

Resonance occurs when  $\omega_m = \omega_e \Rightarrow \frac{1}{\sqrt{LC}} C = \frac{1}{\sqrt{L}} \frac{1}{\sqrt{C}} \frac{1}{\omega^2 L}$

$$\omega_0 = \frac{1}{\sqrt{LC}}$$

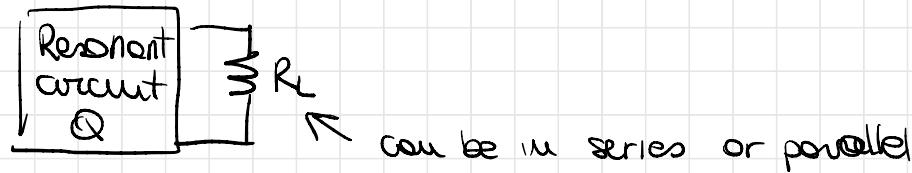
### Quality factor

$$Q = \omega_0 \frac{\omega_m + \omega_e}{P_{loss}} = \omega_0 \frac{2\omega_m}{P_{loss}} = \omega_0 \frac{\cancel{\frac{1}{\sqrt{LC}} \frac{1}{\sqrt{L}} \frac{1}{\omega^2 L}}}{\cancel{\frac{1}{2} \frac{V^2}{R}}} = \omega_0 \frac{1}{\omega_0^2 L} \cdot R = \frac{R}{L} \sqrt{LC} = R \sqrt{\frac{C}{L}}$$



## LOADED AND UNLOADED Q

UNLOADED Q  $\rightarrow$  INTRINSIC PROPERTY OF THE RESONATOR



can be in series or parallel

we can define the EXTERNAL Q

$$Q_E = \begin{cases} \frac{\omega_0 L}{R_L} & \text{SERIES} \\ \frac{R_L}{\omega_0 L} & \text{PARALLEL} \end{cases}$$

The LOADED Q FACTOR IS THEN :

$$1/Q_L = 1/Q_E + 1/Q$$

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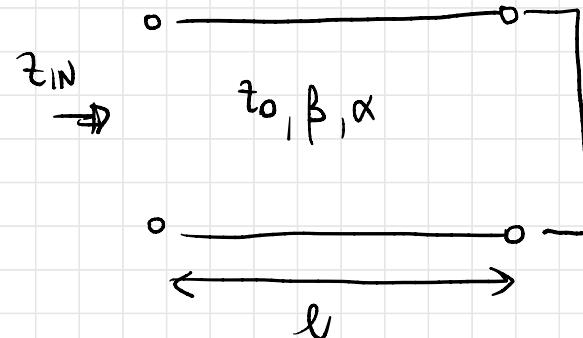
# TRANSMISSION LINE RESONATORS

- Short-circuit  $\lambda/2$  line

At  $\omega = \omega_0$

$$l = \frac{\lambda}{2}$$

$$\lambda = \frac{2\pi}{\beta}$$



$$z_{IN} = z_0 \tanh(\alpha + j\beta) l = z_0 \frac{\tanh \alpha l + j \tanh \beta l}{1 + j \tanh \alpha l \tanh \beta l}$$

If we assume to have small losses  $\alpha l \ll 1 \Rightarrow \underline{\alpha l \approx \tanh \alpha l}$

If we let  $\omega = \omega_0 + \Delta\omega$  ( $\Delta\omega$  very small)

for a TEM line

$$\beta l = \frac{\omega l}{V_p} = \frac{\omega_0 l}{V_p} + \frac{\Delta\omega l}{V_p}$$

we also know  $l = \frac{\lambda}{2} = \frac{\pi}{\beta}$  ( $\omega = \omega_0$ )

so we can write

$$\beta l = \pi + \frac{\Delta\omega l}{V_p} = \pi + \frac{\Delta\omega \pi}{\omega_0}$$

it follows that

$$\underline{\tan \phi} = \tan \left( \pi + \frac{\Delta \omega \pi}{\omega_0} \right) = \tan \frac{\Delta \omega \pi}{\omega_0} \approx \frac{\Delta \omega \pi}{\omega_0}$$

Replacing in the expression of the input impedance:

$$Z_{IN} = Z_0 \frac{\tan \alpha l + j \tan \phi}{1 + j \tan \phi \tan \alpha l} \approx$$

$$\approx Z_0 \frac{\alpha l + j \left( \frac{\Delta \omega \pi}{\omega_0} \right)}{1 + j \alpha l \left( \underbrace{\frac{\Delta \omega \pi}{\omega_0}}_{\frac{\Delta \omega \alpha l}{\omega_0} \ll 1} \right)}$$

The input impedance is in the form of :

$$Z_{IN} = R + 2jL\Delta\omega$$

↳ Impedance of an RLC resonant circuit

$$R = Z_0 \alpha L$$

$$L = \frac{Z_0 \pi}{2\omega_0}$$

At resonance  $\omega_0 = \frac{1}{\sqrt{LC}} \Rightarrow C = \frac{1}{\omega_0^2 L}$

The  $\frac{\lambda}{2}$  short-circuited TL resonates at  $\Delta\omega=0$  ( $\ell=\frac{\lambda}{2}$ )  
circuit resonates for

$$\Rightarrow Z_{IN} = R + Z_0 \alpha \ell$$

$$\ell = n \frac{\lambda}{2}$$

$$n = 1, 2, 3, \dots$$

## Quality factor

$$Q = \frac{w_0 L}{R} = \frac{\pi}{2\alpha e} = \frac{f}{2\alpha}$$

$f_l = \pi$  at  
the first  
resonance

- Short-circuited  $\frac{\lambda}{4}$  line

$$Z_{IN} = Z_0 \tanh(\alpha + j\beta)e =$$

$$Z_0 \frac{\tanh \alpha e + j \tanh \beta e}{1 + j \tanh \beta e \tanh \alpha e}$$

Multiply  $Z_{IN}$  by  $-j \cot \beta l$

$$Z_{IN} = Z_0 \frac{1 - j \tan \alpha l \cot \beta l}{\tan \alpha l - j \cot \beta l}$$

If  $l = \frac{\lambda}{4}$  at  $\omega = \omega_0$  and we let  $\omega \approx \omega_0 + \Delta\omega$  then

for a TEM line:

$$\beta l = \frac{\omega_0 l}{k_p} + \frac{\Delta\omega l}{k_p} = \frac{\pi}{2} + \frac{\pi \Delta\omega}{2\omega_0}$$

$$\text{so that } \cot \beta l = \cot \left( \frac{\pi}{2} + \frac{\pi \Delta\omega}{2\omega_0} \right) = -\tan \frac{\pi \Delta\omega}{2\omega_0} \approx$$

$$\approx -\frac{\pi \Delta\omega}{2\omega_0}$$

We are also assuming small losses  $\alpha L \approx \text{constant}$

We can write

$$Z_{IN} = Z_0 \frac{1 + j\alpha L \frac{\pi \Delta w}{2w_0}}{\alpha L + j\pi \frac{\Delta w}{2w_0}} \underset{\ll 1}{\sim} \frac{Z_0}{\alpha L + j\pi \frac{\Delta w}{2w_0}}$$

This type of impedance is typical of parallel RLC circuits

$$Z_{IN} = \frac{1}{\frac{L}{R} + 2j\Delta w C}$$

$$R = Z_0 / \alpha L$$

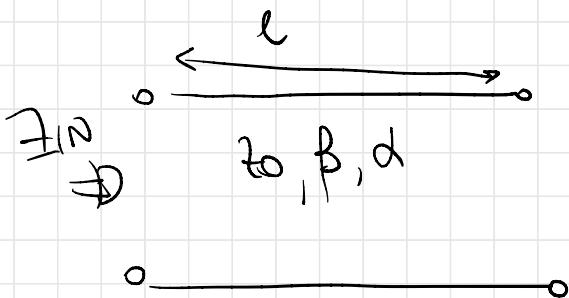
$$C = \frac{\pi}{4w_0 Z_0}$$

The value of inductance can be calculated as  $L = \frac{1}{w_0^2 C}$

The Quality factor :

$$Q = \omega_0 R C = \frac{\pi}{4\alpha l} = \frac{\beta}{2\alpha}$$

• Open-circuited  $\lambda/2$  line



$$\begin{aligned} Z_{IN} &= z_0 \coth(\alpha + j\beta)l = \\ &= z_0 \frac{1 + j \tan \alpha l \tanh \beta l}{\tanh \alpha l + j \tan \beta l} \end{aligned}$$

We assume  $l = \frac{\lambda}{2}$  and  $\omega = \omega_0 + \Delta\omega \Rightarrow \beta l = \pi + \pi \frac{\Delta\omega}{\omega_0} \Rightarrow \tan \beta l \approx \pi \frac{\Delta\omega}{\omega_0}$   
 $\Delta l \approx \tan \alpha l$  it follows:

$$Z_{IN} = \frac{Z_0}{\alpha L + j \left( \frac{\Delta W \pi}{W_0} \right)}$$

$$R = \frac{Z_0}{\alpha e}$$

$$C = \frac{\pi}{2W_0 Z_0}$$

$$L = \frac{1}{W_0^2 C} = \frac{2W_0 Z_0}{\pi W_0^2} = \frac{2Z_0}{\pi W_0}$$

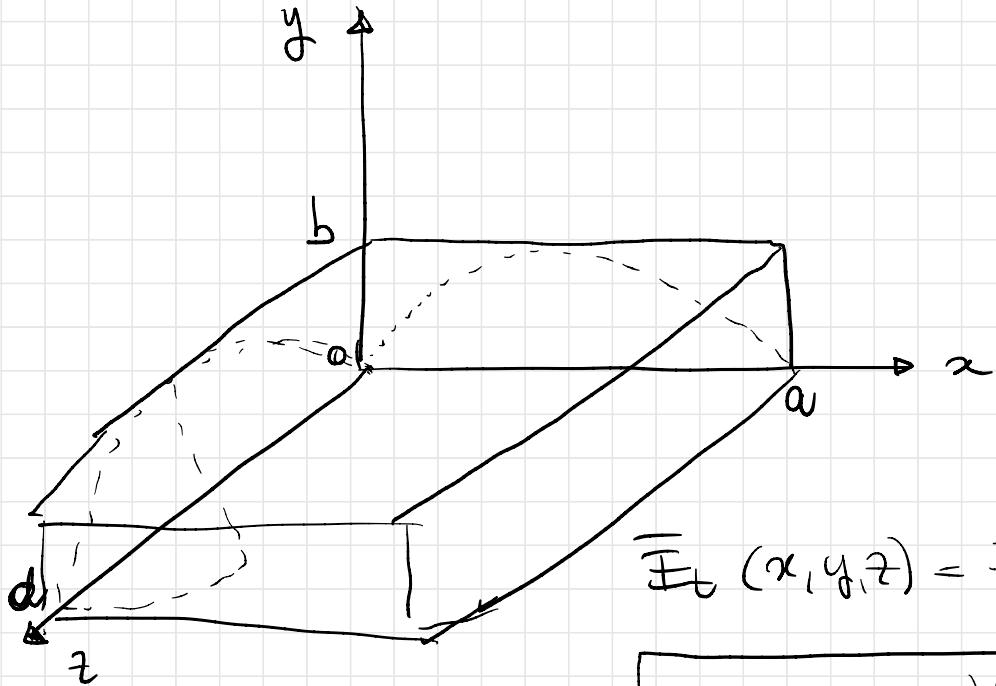
Quality Factor Q:

$$Q = \omega_0 R C = \frac{\pi}{2\alpha e} = \frac{\beta}{2\alpha}$$

$\ell = \frac{\pi}{\beta}$  at  
resonance

## RECTANGULAR WAVEGUIDE CAVITIES

Resonant frequencies are found assuming WG is lossless.



$$\bar{E}_t(x, y, z) = \bar{e}(x, y) [A^+ e^{-j\beta_{mn}z} + \Delta e^{j\beta_{mn}z}]$$

$$\beta_{mn} = \sqrt{k^2 - \left(\frac{m\pi}{a}\right)^2 - \left(\frac{n\pi}{b}\right)^2}$$

$$k = \omega \sqrt{\mu \epsilon}$$

By imposing that  $\bar{E}_t = 0$  at  $z=0 \Rightarrow A^+ = -A^-$

At  $z=d$  we have

$$\bar{E}_t(x, y, d) = -\bar{e}(x, y) A^+ z_j \sin \beta_{mn} d = 0$$



$$\beta_{mn} d = l\pi$$

$$l = 1, 2, 3, \dots$$



The waveguide  
version of the  $\frac{\lambda}{2}$  TL/SC

The resonant wave number  $k_{mn} = \sqrt{\left(\frac{m\pi}{a}\right)^2 + \left(\frac{n\pi}{b}\right)^2 + \left(\frac{lk}{d}\right)^2}$

The resonant frequencies for TE<sub>mne</sub> or TM<sub>mne</sub> modes are:

$$f_{mne} = \frac{CK_{mne}}{2\pi\sqrt{\mu_r\varepsilon_r}} = \frac{C}{2\pi\sqrt{\mu_r\varepsilon_r}} \sqrt{\left(\frac{mn}{a}\right)^2 + \left(\frac{n\pi}{b}\right)^2 + \left(\frac{l\pi}{d}\right)^2}$$

If b < a < d  $\rightarrow$  THE DOMINANT MODE IS TE<sub>101</sub> for TE  
TM<sub>110</sub> for TM

Quality factor of TE<sub>101</sub> mode

The stored electric energy is:  $W_0 = \frac{\varepsilon}{4} \int_V E_y E_y^* dV = \frac{\varepsilon abd}{16} E_0^2$

The stored magnetic energy is:

$$W_m = \frac{\mu}{4} \int_V (H_x H_x^* + H_z H_z^*) dV = \frac{\mu abd}{16} \frac{E_0^2}{Z_{TE}^2} \left( \frac{1}{Z_{TE}^2} + \frac{\pi^2}{k^2 \eta^2 a^2} \right)$$

$$Z_{TE} = \frac{k_m}{\beta}$$

$$\beta = \sqrt{1 - \frac{\pi^2}{a^2}}$$

$$W_m = \frac{\mu abd}{16} \frac{E_0^2}{Z_{TE}^2} \left( \frac{\beta^2}{k^2 \eta^2} + \frac{\pi^2}{k^2 \eta^2 a^2} \right) =$$

$$\frac{\mu abd}{16} \frac{E_0^2}{Z_{TE}^2} \left( \frac{k^2 - \frac{\pi^2}{a^2} + \frac{\pi^2}{a^2}}{k^2 \eta^2} \right) = \frac{\mu abd}{16} \frac{E_0^2}{\eta^2} = \frac{abd E_0^2 \epsilon}{16 \mu \epsilon} = W_E$$

For small losses in the conducting walls we get:

$$P_0 = \frac{R_s}{2} \int_{\text{walls}} |H_t|^2 dS$$

$$R_s = \sqrt{\frac{\omega \mu_0}{26}}$$

$$H_x^2 + H_z^2$$

$$\boxed{P_C = \frac{R_s \pi^2 \lambda^2}{8 \eta^2} \left( \frac{l^2 ab}{d^2} + \frac{bd}{a^2} + \frac{l^2 a}{2d} + \frac{d}{2a} \right)}$$

$$\text{Then: } Q_C = \frac{2 \omega_0 W_e}{P_C}$$

The power lost in the dielectric ( $\sigma = \omega \epsilon'' = \omega \epsilon_0 \epsilon_{\text{tan}\delta}$ )

$$P_d = \frac{1}{2} \int_V \mathbf{J} \cdot \mathbf{E}^* dV = \frac{\omega \epsilon''}{2} \int_V |\mathbf{E}|^2 dV =$$

$$= \frac{abd \omega \epsilon'' |E_0|^2}{8}$$

then

$$Q_d = \frac{2\omega W_e}{P_d} = \frac{\epsilon'}{\epsilon''} = \frac{1}{\tan\delta}$$

The total power loss is  $P_{\text{loss}} = P_c + P_d$  and the quality factor is

$$Q = \left( \frac{1}{Q_c} + \frac{1}{Q_d} \right)^{-1}$$