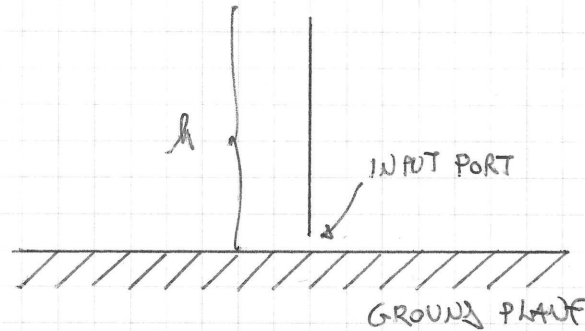


## PROBLEM P6

WE CONSIDER A WHIP ANTENNA MOUNTED ON A GROUND PLANE: IT IS A MONOPOLE  
THE WIRE (WHIP) HAS A RADIUS  $a = 1,5 \text{ mm}$  AND IT IS MADE OF STAINLESS  
STEEL WHOSE CONDUCTIVITY IS  $\sigma = 2 \times 10^6 \text{ } \Omega^{-1} \text{ m}^{-1}$



THE WHIP LENGTH IS  $h = 0,8 \text{ m}$  AND THE WORKING FREQUENCY IS  $f = 1 \text{ MHz}$

1) BY ASSUMING A UNIFORM CURRENT FIND THE INPUT IMPEDANCE

UNDER THE PREVIOUS HYPOTHESES THE ANTENNA IS EQUIVALENT TO "HALF IDEAL DIPOLE"

RADIATION RESISTANCE 
$$R_R = \frac{1}{2} 80 \pi^2 \left( \frac{2h}{\lambda} \right)^2 = 160 \pi^2 \left( \frac{h}{\lambda} \right)^2$$

$$\lambda = \frac{c}{f} = \frac{3 \cdot 10^8}{10^6} = 300 \quad (\text{THE WAVELENGTH IS MUCH LARGER THAN } h)$$

$$R_R = 160 \pi^2 \left( \frac{0,8}{300} \right)^2 = 0,0112 \text{ } \Omega = 11,2 \text{ m}\Omega$$

DISSIPATION (OR OHMIC) RESISTANCE 
$$R_d = \frac{h}{2\pi a \delta} \cdot \frac{1}{\sigma}$$

WHERE  $\delta$  IS THE SKIN DEPTH 
$$\delta = \frac{1}{\sqrt{\pi \mu f \sigma}} = 3,56 \cdot 10^{-5} \text{ m} = 0,356 \text{ mm}$$

$$R_d = \frac{0,8}{2\pi \cdot 1,5 \cdot 10^{-3} \cdot 3,56 \cdot 10^{-5}} \cdot \frac{1}{2 \cdot 10^6} = 0,1192 \text{ } \Omega = 119,2 \text{ m}\Omega$$

THE REACTIVE PART OF INPUT IMPEDANCE IS 
$$X_A = \frac{1}{2} \left\{ - \frac{120}{\pi \frac{2h}{\lambda}} \left[ \ln \left( \frac{2h}{2a} \right) - 1 \right] \right\}$$

$$X_A = -\frac{30}{\pi \frac{h}{\lambda}} \left[ \ln\left(\frac{h}{a}\right) - 1 \right] = -18905 \Omega$$

THE TOTAL INPUT IMPEDANCE IS  $Z_A = R_R + R_D + jX_A = 0,1309 - j18905 \Omega$

IT IS DIFFICULT TO IMPEDANCE MATCH THIS ANTENNA DUE TO THE SMALL INPUT RESISTANCE AND TO THE VERY LARGE CAPACITIVE REACTANCE. MOREOVER, THE RADIATION

EFFICIENCY IS VERY SMALL  $e_R = \frac{R_R}{R_R + R_D} = \frac{0,0112}{0,0112 + 0,1192} = 0,0859 \approx 8,6\%$

2) BY ASSUMING A LINEARLY VARYING CURRENT DISTRIBUTION, FIND THE INPUT IMPEDANCE  
WE OBSERVE THAT THE ANTENNA IS EQUIVALENT TO "HALF SHORT DIPOLE" (HAVING A TRIANGULAR CURRENT DISTRIBUTION)

$$\text{RADIATION RESISTANCE } R_R = \frac{1}{2} 20 \pi^2 \left( \frac{2h}{\lambda} \right)^2 = 40 \pi^2 \left( \frac{h}{\lambda} \right)^2 = 0,0028 \Omega = 2,8 \text{ m}\Omega$$

$$\text{DISSIPATION RESISTANCE } R_D = \frac{1}{2} \frac{1}{3} \frac{2h}{2\pi a \delta} \frac{1}{\sigma} = \frac{1}{3} \frac{h}{2\pi a \delta} \frac{1}{\sigma} = 0,0397 \Omega = 39,7 \text{ m}\Omega$$

$$\text{THE REACTIVE PART OF INPUT IMPEDANCE IS } X_A = -\frac{30}{\pi \frac{h}{\lambda}} \left[ \ln\left(\frac{h}{a}\right) - 1 \right]$$

$$X_A = -18905 \Omega$$

$$\text{THE TOTAL INPUT IMPEDANCE IS } Z_A = R_R + R_D + jX_A = 0,0425 - j18905 \Omega$$

$$\text{AND THE RADIATION EFFICIENCY IS } e_R = \frac{R_R}{R_R + R_D} = \frac{0,0028}{0,0028 + 0,0397} = 0,0659 \approx 6,6\%$$