

Fundamentals on coherent optics:

linear propagation in optical waveguides

exercice 2 correction

1: region Z_{ext} = optical cladding ; region Z_{in} = core

$$2: NA = (n_1^2 - n_2^2)^{1/2} = (1.463^2 - 1.458^2)^{1/2} = 0.12$$

3: the volume of silica is not changed:

\Rightarrow volume of the preform V_p = Volume of the fiber V_f

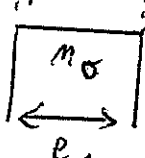
$$\Rightarrow \frac{\pi D_p^2}{4} L_p = \frac{\pi D_f^2}{4} L_f \quad (D \rightarrow \text{Diameter}; \text{index } p \rightarrow \text{preform})$$

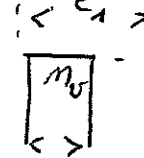
$L \rightarrow \text{length}; \text{index } f \rightarrow \text{fiber}$

$$\Rightarrow L_f = L_p \left(\frac{D_p}{D_f} \right)^2 = 0.5 \left(\frac{3 \cdot 10^{-2}}{125 \cdot 10^{-6}} \right)^2 = 28800 \text{ m} = 28.8 \text{ km}$$

$$4/ a) \Delta = \frac{NA^2}{2n_1^2} = \frac{0.12^2}{2 \times 1.463^2} \sim 3.4 \cdot 10^{-3} < 10^{-2}$$

The weak guidance approximation applies \rightarrow LP (= linearly polarized) modes can be considered. In a LP mode at given time and place (t and z fixed), the polarization remains linear (= in a given direction) in all the cross section.

b)  $\delta\varphi_1 = \frac{2\pi}{\lambda_T} n_0 e_1$

c)  $\delta\varphi_2 = \frac{2\pi}{\lambda_T} [n_0 e_2 + 1 \cdot (e_1 - e_2)]$

$$d) \Delta\varphi = \delta\varphi_1 - \delta\varphi_2 = \frac{2\pi}{\lambda_T} [n_0 e_1 - n_0 e_2 - (e_1 - e_2)] = \frac{2\pi}{\lambda_T} (n_0 - 1)(e_1 - e_2) = \frac{2\pi}{\lambda_T} (n_0 - 1) \Delta e$$

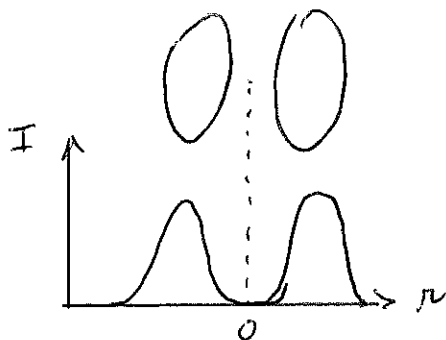
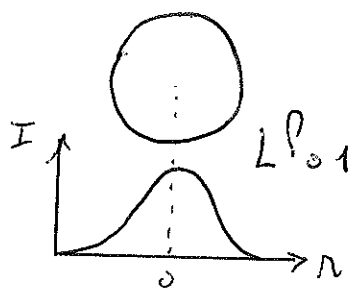
$$5/ a) \frac{d\Delta\varphi}{d\lambda} = \frac{-2\pi}{\lambda^2} (n_0 - 1) \Delta e \Big|_{\lambda=\lambda_T} \Rightarrow d\lambda = \frac{-d\lambda_T^2}{2\pi (n_0 - 1) \Delta e} d\Delta\varphi$$

$$b) \Delta\lambda = \frac{d\lambda_T^2}{2\pi (n_0 - 1) \Delta e} \times 2\pi = \frac{d\lambda_T^2}{(n_0 - 1) \Delta e}$$

$$c) \Delta e = e_1 - e_2 = 0.5 \text{ mm} \quad n_0 = 1.5 \quad \lambda_{T1} = 1.1 \mu\text{m}$$

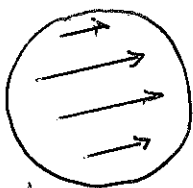
$$\Delta\lambda = \frac{(1.1 \cdot 10^{-6})^2}{(1.5 - 1) \times 0.5 \cdot 10^{-3}} = 4.8 \cdot 10^{-9} \text{ m} = 4.8 \text{ nm}$$

6/a) The fiber is able to guide only two modes. They are the modes with the lowest cutoff spatial frequency, i.e. $LP_{0,1}$ mode ($V_c = 0$) and $LP_{1,1}$ mode ($V_c = 2.405$), (see the dispersion curves, with $B = 0$ and the table of zeros of J_ν Bessel functions).

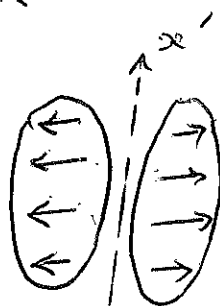


b) Generally speaking, the direction of the polarization of the field is the same all over the cross-section of the mode, at a given z , at a given time. This direction depends on the polarization of the input beam and on the birefringence of the fiber. Let us assume that it is \longleftrightarrow :

$LP_{0,1}$ mode :



; $LP_{1,1}$ mode

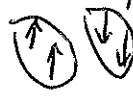


Let us note that the direction x' of the black line of the $LP_{1,1}$ mode depends on the field distribution Ψ_e of the exciting beam. It is the one for which the normalized integral overlap

$$\alpha^2 = \frac{|\iint \Psi_e LP_{1,1} dS|^2}{\iint |\Psi_e|^2 dS \iint |LP_{1,1}|^2 dS}$$

is maximum
(see Philippe DiBari lessons).

\Rightarrow there is no relation between the direction of the black line and the direction of the polarization (direction of the electric field) :

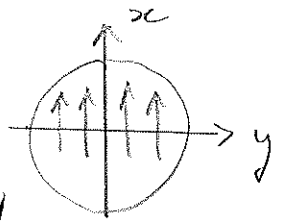


is possible !

7/ $\Delta\phi_1 = 2m\pi \rightarrow$ no additional phase shift
between the upper and the lower parts of
the beam after crossing the plates

\Rightarrow the exciting beam (after the plates) is an even beam

The LP_{01} mode (which is even $\uparrow\uparrow\uparrow$) can be excited



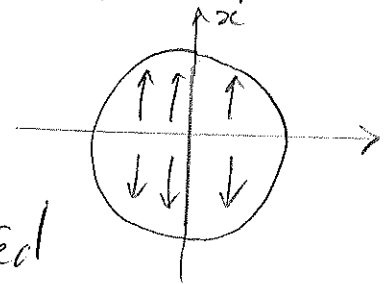
The LP_{11} mode (which is odd $\uparrow\downarrow$ or $\begin{pmatrix} \uparrow \\ \downarrow \end{pmatrix}$)

is not excited at all $\Rightarrow \alpha^2|_{LP_{11} \text{ mode}} = 0$

8/ wavelength shift $1102.4 - 1100 = 2.4 \text{ nm} = \frac{4.8}{2} \text{ nm}$
 $= \frac{1}{2} (\Delta\lambda \text{ of question 5c})$

\Rightarrow the phase difference between the upper part and the lower part
of the beam, after the plates is $\Delta\phi_2 = \Delta\phi_1 \pm \pi = (2m \pm 1)\pi$

\rightarrow The exciting beam (after the plates) is odd



The LP_{11} mode $\begin{pmatrix} \uparrow\uparrow \\ \downarrow\downarrow \end{pmatrix}$ will be excited

The LP_{01} mode (which is even $\uparrow\uparrow\uparrow$) is not excited at all

$\Rightarrow \alpha^2|_{LP_{01} \text{ mode}} = 0$

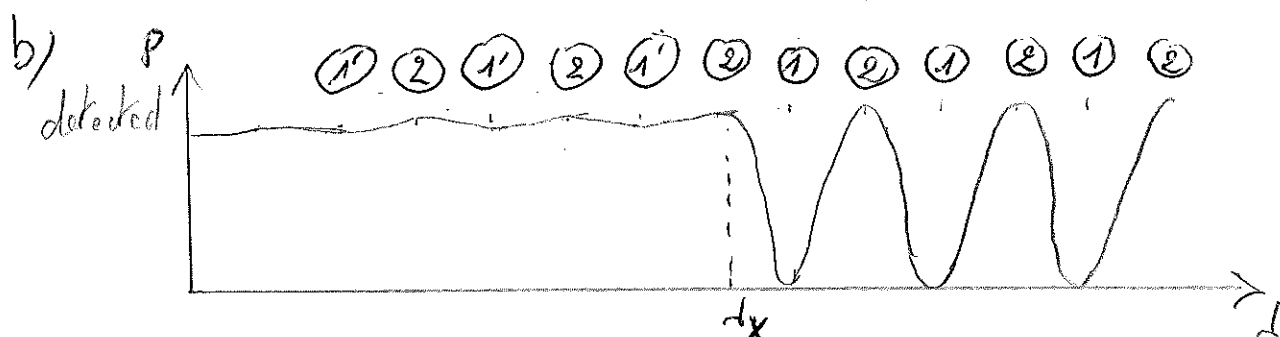


9/a) beyond a certain wavelength, the LP_{11} mode is no more guided

thus, when $\Delta\phi = (2m' + 1)\pi$ LP_{01} not excited
 LP_{11} mode excited but not guided } no power detected at the fiber output (1)

when $\Delta\phi = 2m'\pi$ LP_{01} excited (and always guided)
 LP_{11} not excited } power detected (2)

(1) and (2) : fluctuations of the detected power when λ is swept



(2) = LP_{01} excited and guided

(1') = LP_{11} excited and guided

(1) = LP_{11} excited but not guided ($P_{\text{detected}} \sim 0$)

λ_c is the wavelength corresponding to the cutoff wavelength λ_c of the LP_{11} mode

$\rightarrow \lambda_c = \lambda_c$: the device allows measuring the cutoff wavelength of the LP_{11} mode \rightarrow limit of the single mode region

in other words: below λ_c , the LP_{01} and LP_{11} modes are excited alternately when λ is swept and, as they are both guided, $P(\lambda)$ is relatively stable

Above λ_c , the LP_{01} and LP_{11} modes are excited alternately when λ is swept and, as LP_{01} mode is guided but not the LP_{11} mode, $P(\lambda)$ deeply fluctuates.

10/ a $d_c / \lambda_{P_{11}} = 1240 \text{ nm}$

@ d_c : $V = 2.405$

5/5

$$\frac{2\pi}{d_c} a NA = 2.405 \Rightarrow a = \frac{2.405 d_c}{2\pi NA} = \frac{2.405 \times 1240}{2\pi \times 0.12} = 396 \mu\text{m} \approx 4 \mu\text{m}$$

b) $V = \frac{2\pi}{d_{T_3}} a NA = \frac{2\pi}{0.633} \times 4 \times 0.12 \approx 4.75$

On the set of dispersion curves we can see that $V > V_c$ for the modes LP_{01} , LP_{11} , LP_{21} , and LP_{02} . Among these modes:

c) the lowest order mode n_L is the LP_{01} mode (highest B)
the highest order mode n_H is the LP_{02} mode (lowest B)

For $V = 4.75$ we can read on the normalized dispersion curves:

$$B(LP_{01}) \approx 0.82$$

$$\text{and } B(LP_{02}) \approx 0.13$$

$$B = \frac{\beta^2 - k_0^2 n_2^2}{k_0^2 \underbrace{(n_1^2 - n_2^2)}_{NA^2}}$$

$$\text{with } \beta = k_0 n_e \Rightarrow B = \frac{n_e^2 - n_2^2}{NA^2}$$

$$\Rightarrow n_e = (B NA^2 + n_2^2)^{1/2}$$

calculations: $n_e(LP_{01}) = (0.82 \times 0.12^2 + 1.458^2)^{1/2} = 1.462$

$$n_e(LP_{02}) = (0.13 \times 0.12^2 + 1.458^2)^{1/2} = 1.486$$

d) $v_g = \frac{c}{n_e}$

$$v_g(n_L) = v_g(LP_{01}) = \frac{c}{n_e(LP_{01})} = \frac{3 \times 10^8}{1.462} \approx 2.052 \times 10^8 \text{ m/s}$$

$$v_g(n_H) = v_g(LP_{02}) = \frac{c}{n_e(LP_{02})} = \frac{3 \times 10^8}{1.486} \approx 2.057 \times 10^8 \text{ m/s}$$