

$$(x+y)^2 = x^2 + y^2 + 2xy$$

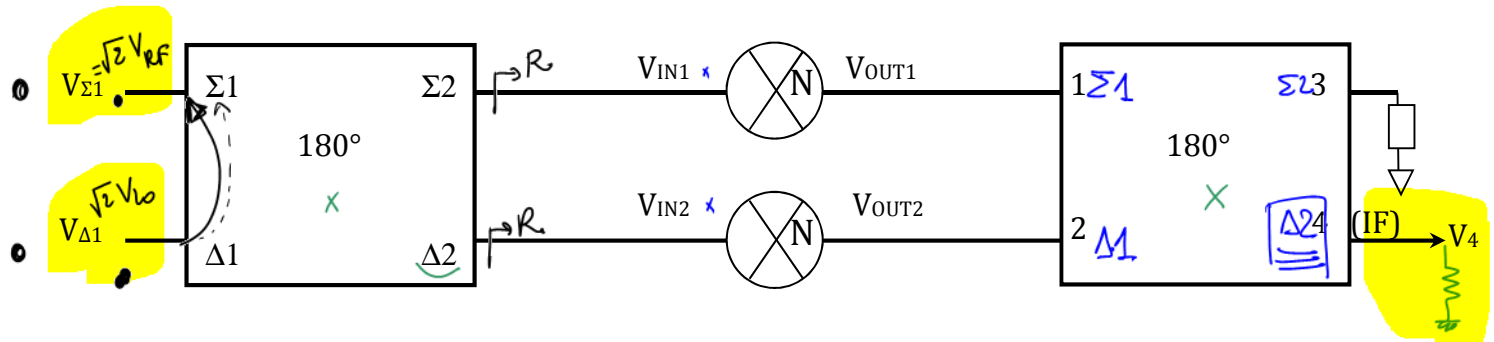
$$(x-y)^2 = x^2 + y^2 - 2xy$$

## Tutorial (Balanced Mixer SBM)

- The mixer is based on a **nonlinear device N** characterized with the following 3<sup>rd</sup> order transfer function :

$$V_{OUT} = a \cdot V_{IN}^2 - b \cdot V_{IN}^3 \quad \text{where (a and b) are constants}$$

- The following block diagram represents a **single balanced mixer SBM** consisting of two 180°-couplers and two identical mixers N.



- 1) In the studied case, the input voltages are  $V_{\Sigma 1} = (\sqrt{2} \cdot V_{RF})$  and  $V_{\Delta 1} = (\sqrt{2} \cdot V_{LO})$ .

Therefore, express the input control voltages  $V_{IN1}$  and  $V_{IN2}$  of N as a function of  $V_{LO}$  and  $V_{RF}$ .

$$V_{IN1} = \frac{1}{\sqrt{2}} (V_{\Sigma 1} + V_{\Delta 1}) = \frac{1}{\sqrt{2}} (\sqrt{2} V_{RF} + \sqrt{2} V_{LO}) = V_{RF} + V_{LO}$$

$$V_{IN2} = \frac{1}{\sqrt{2}} (V_{\Sigma 1} - V_{\Delta 1}) = \frac{1}{\sqrt{2}} (\sqrt{2} V_{RF} - \sqrt{2} V_{LO}) = V_{RF} - V_{LO}$$

- 2) Deduce the expressions of output voltages ( $V_{OUT1}$ ,  $V_{OUT2}$ ) as a function of  $V_{LO}$  and  $V_{RF}$ .

$$V_{OUT1} = a (V_{RF} + V_{LO})^2 - b (V_{RF} + V_{LO})^3$$

$$V_{OUT2} = a (V_{RF} - V_{LO})^2 - b (V_{RF} - V_{LO})^3$$

- 3) The SBM down-converter is designed at an IF angular frequency  $\omega_{IF} = \omega_{LO} - \omega_{RF}$ .

What should be the type ( $\Sigma$  or  $\Delta$ ) of port 4 in the output coupler?

$\Delta$  port  $\rightarrow$  I want  $V_{LO} \times V_{RF}$  at the output  $\rightarrow$  only  $(V_{RF} + V_{LO})^2 - (V_{RF} - V_{LO})^2 \Rightarrow$

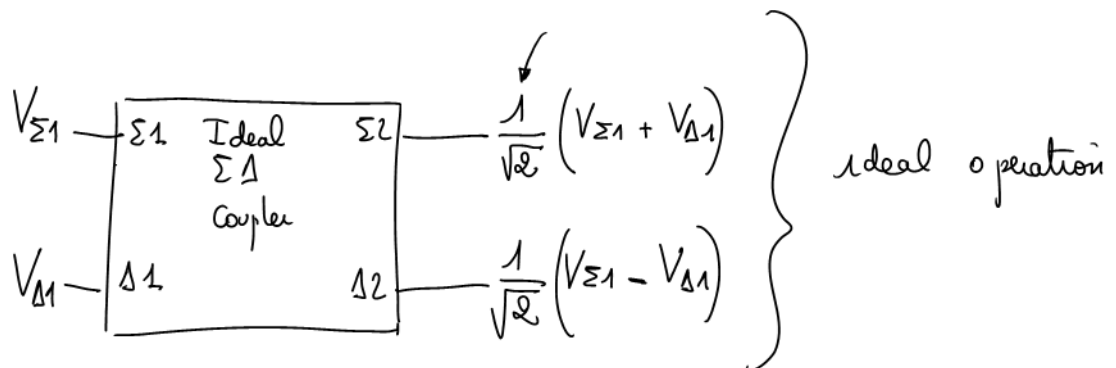
- 4) Given that  $V_{LO} = V_0 \cos(\omega_{LO} t)$  and  $V_{RF} = V_1 \cos(\omega_{RF} t)$ , express the output voltage spectrum  $V_4$  of the SBM as a function of  $V_0$  and  $V_1$ . What are the remaining frequencies at the IF output port of the SBM?

- 5) What are the advantages of this SBM configuration (LO input at  $\Delta$  port)?

- 6) Express the voltage conversion gain  $G_{CV}$  of the SBM. What is the power conversion gain  $G_{CP}$  if all 180° couplers are matched to 50Ω?

LO - RF isolation of SBM = LO - RF isolation of input coupler  
LO - IF isolation

- 7) What are the values of LO-to-RF and LO-to-IF isolations?



$$\begin{aligned} (x+y)^2 &= x^2 + y^2 + 2xy \\ (x-y)^2 &= x^2 + y^2 - 2xy \end{aligned}$$

$\downarrow$   
 $4xy$

$$\begin{aligned} (x+y)^3 &= x^3 + y^3 + 3x^2y + 3xy^2 \\ (x-y)^3 &= x^3 - y^3 - 3x^2y + 3xy^2 \end{aligned}$$

$\downarrow$   
 $2y^3 + 6x^2y$

$$\begin{aligned} \cos^2(x) &= \frac{1}{2} + \frac{1}{2} \cos(2x) \\ \cos^3(x) &= \frac{3}{4} \cos(x) + \frac{1}{4} \cos(3x) \end{aligned}$$

$$\begin{aligned} \cos^3(x) &= \cos^2(x) \cos(x) \\ &= \frac{1}{2} \cos(x) + \frac{1}{2} \cos(2x) \cos(x) \\ &= \frac{1}{2} \cos(x) + \frac{1}{4} \cos(3x) + \frac{1}{4} \cos(x) \end{aligned}$$

$$\begin{aligned} V_4 &= \frac{1}{\sqrt{2}} (V_{out1} - V_{out2}) = \frac{1}{\sqrt{2}} \left[ a(V_{RF} + V_{LO})^2 - b(V_{RF} + V_{LO})^3 - a(V_{RF} - V_{LO})^2 + b(V_{RF} - V_{LO})^3 \right] \\ &= \frac{1}{\sqrt{2}} \left[ \textcircled{A} 4aV_{RF}V_{LO} - \textcircled{B} 2bV_{LO}^3 - \textcircled{C} 6bV_{RF}^2V_{LO} \right] \end{aligned}$$

$\omega_{IF} \propto \omega_{\Sigma}$        $\omega_{LO}$        $2\omega_{RF} \pm \omega_{LO}$

$$\begin{aligned} V_{RF} &= V_1 \cos(\omega_{RF}t) \\ V_{LO} &= V_0 \cos(\omega_{LO}t) \\ \omega_{IF} &= \omega_{LO} - \omega_{RF} \\ \omega_{\Sigma} &= \omega_{LO} + \omega_{RF} \\ \omega_1 &= 2\omega_{RF} + \omega_{LO} \\ \omega_2 &= 2\omega_{RF} - \omega_{LO} \end{aligned}$$

Ⓐ term

$$4aV_{RF}V_{LO} = 2aV_0V_1 [\cos(\omega_{IF}t) + \cos(\omega_{\Sigma}t)]$$

Ⓑ term

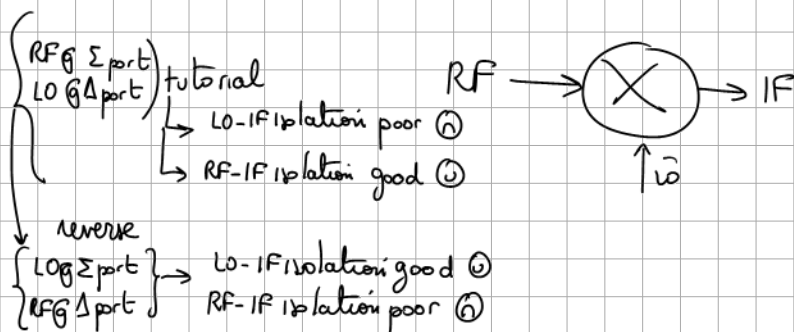
$$-2bV_{LO}^3 = -\frac{1}{2}bV_0^3 [3\cos(\omega_{LO}t) + \cos(3\omega_{LO}t)]$$

Ⓒ term

$$\begin{aligned} -6bV_{RF}^2V_{LO} &= -6bV_1^2V_0 \left[ \frac{1}{2} + \frac{j}{2} \cos(2\omega_{RF}t) \right] [\cos(\omega_{LO}t)] \\ &= -3bV_1^2V_0 \cos(\omega_{LO}t) - \frac{3}{2}bV_1^2V_0 [\cos(\omega_1t) + \cos(\omega_2t)] \end{aligned}$$

$$V_4 = \frac{1}{\sqrt{2}} (\textcircled{A} + \textcircled{B} + \textcircled{C})$$

$\downarrow$   
 $\omega_{IF} \propto \omega_{\Sigma}$        $3\omega_{LO}$        $\omega_{LO}$        $\omega_1, \omega_2$



- ① LO  $\rightarrow$  RF
  - ② LO  $\rightarrow$  IF (not good)
  - ③ RF  $\rightarrow$  IF (down) or IF  $\rightarrow$  RF (up)
- good
- if inputs are reversed (good)

$$\begin{aligned} \text{LO-IF isolation}_{dB} &= 10 \log \left( \frac{P_{LO \text{ port}}(\omega_{LO})}{P_{IF \text{ port}}(\omega_{LO})} \right) = 10 \log \left( \frac{\frac{1}{2} \frac{|V_{\Delta 1}(\omega_{LO})|^2}{50\Omega}}{\frac{1}{2} \frac{|V_4(\omega_{LO})|^2}{R_L}} \right) \\ &= 10 \log \left( \frac{\frac{1}{2} \frac{1}{50} (\sqrt{2}V_0)^2}{\frac{1}{2} \frac{1}{R_L} \left[ \frac{1}{\sqrt{2}} \left( -\frac{3}{2}bV_0^3 - 3bV_1^2V_0 \right) \right]^2} \right) = 10 \log \left( \frac{\frac{1}{50} \times 2}{\frac{1}{R_L} \frac{9}{2} b^2 \left( \frac{1}{2}V_0^2 + V_1^2 \right)^2} \right) \end{aligned}$$

$$G_{CV} = \frac{V_{OUT}(\omega_{OUT})}{V_{IN}(\omega_{IN})} = \frac{V_4(\omega_{IF})}{V_{\Sigma 1}(\omega_{RF})} = \frac{\frac{1}{\sqrt{2}} \cancel{2} a V_0 \cancel{V_1}}{\sqrt{2} \times \cancel{V_1}} = a V_0$$

$$G_{CP} = \frac{P_{OUT}(\omega_{OUT})}{P_{IN}(\omega_{IN})} = \frac{\frac{1}{2} \frac{|V_4(\omega_{IF})|^2}{R_L}}{\frac{1}{2} \frac{|V_{\Sigma 1}(\omega_{RF})|^2}{S_0}} = \frac{\frac{1}{2 R_L} \times \left( \frac{1}{\sqrt{2}} \cancel{2} a V_0 \cancel{V_1} \right)^2}{\frac{1}{2} \frac{(\sqrt{2} V_1)^2}{S_0}}$$

$$= \frac{S_0}{R_L} a^2 V_0^2$$