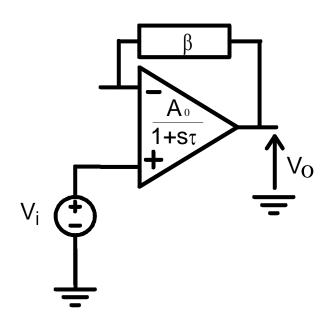
Operational amplifier: small signals behavior



$$G_{loop}(s) = -\beta \cdot A(s)$$

$$V_{O} T(s) = \frac{V_{o}(s)}{V_{i}(s)} = \frac{A(s)}{1 + \beta \cdot A(s)}$$

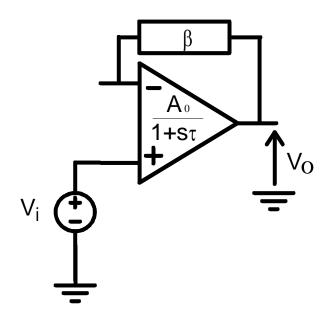
$$T(s) = \frac{A_o}{1+s\tau} \cdot \frac{1}{1+\beta \cdot \frac{A_o}{1+s\tau}} = \frac{A_o}{1+\beta A_o + s\tau}$$

$$T(s) = \frac{A_0}{1 + \beta A_0} \cdot \frac{1}{1 + s \cdot \frac{\tau}{1 + \beta A_0}} = \frac{A'_0}{1 + s \tau'} \qquad A'_0 \cdot \frac{1}{\tau'} = A_0 \cdot \frac{1}{\tau}$$

the gain-bandwidth product is a constant



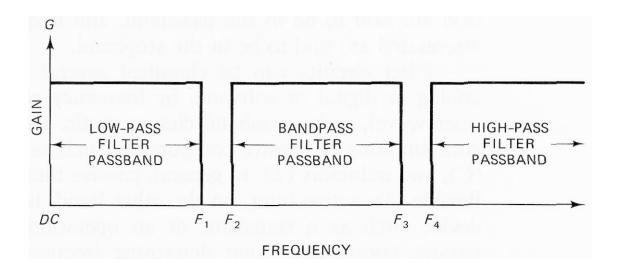
Operational amplifier: selecting the right one

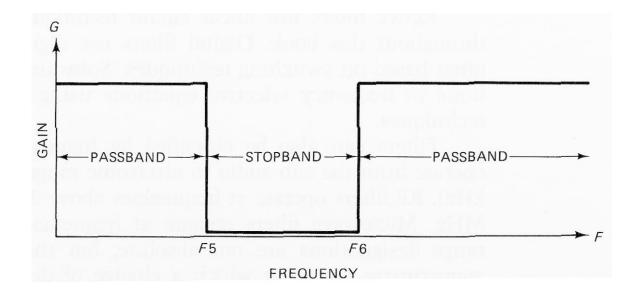


$$A_0' \cdot \frac{1}{\tau'} = A_0 \cdot \frac{1}{\tau}$$



Ideal linear filters



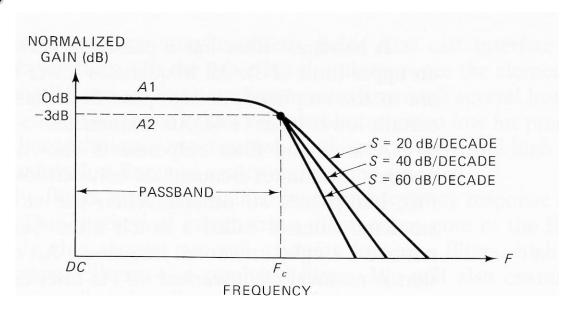


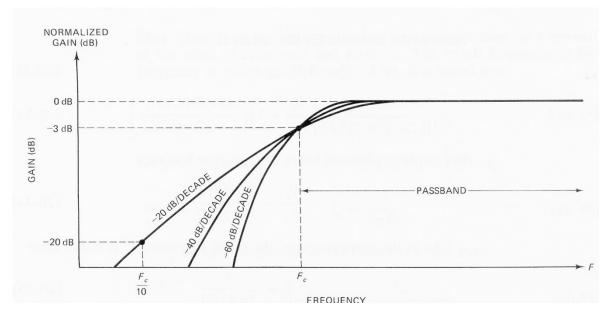


Butterworth filters

□low-pass

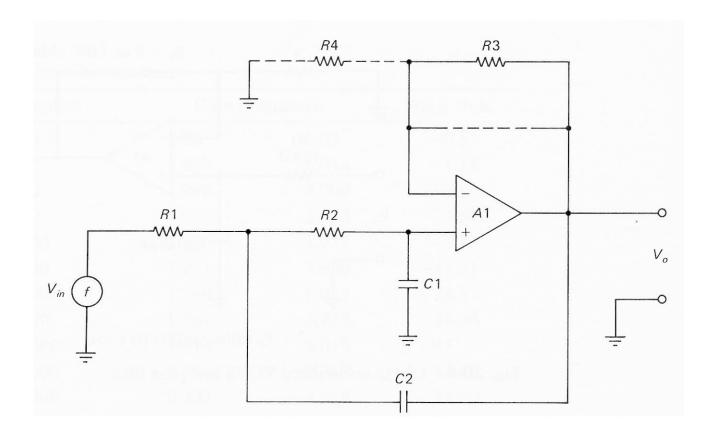








Example of second order LP filter





Example of second order HP filter

