

# Wireless Systems Lab

## Exercise Two: A Small Wideband Microstrip-fed Monopole Antenna

Andrew Simon Wilson

7th July, 2022



UNIVERSITÀ  
DEGLI STUDI  
DI BRESCIA

EMIMEO Programme

Module Coordinator: Prof. Daniele Modotto

# Author Details

## Andrew Simon Wilson, BEng

Post-graduate Masters Student, Erasmus Mundus JMD - EMIMEO Programme

@ andrew.s.wilson@protonmail.com     andrew-simon-wilson     AS-Wilson     +44 7930 560 383

# Contents

1	Design and Simulation Set-up	2
1.1	Assumptions and Any Parameters Not Given in the Paper . . . . .	2
1.2	Design and Simulation Set-up and Initial Results . . . . .	3
2	Final Results and Discussion	4

# 1 Design and Simulation Set-up

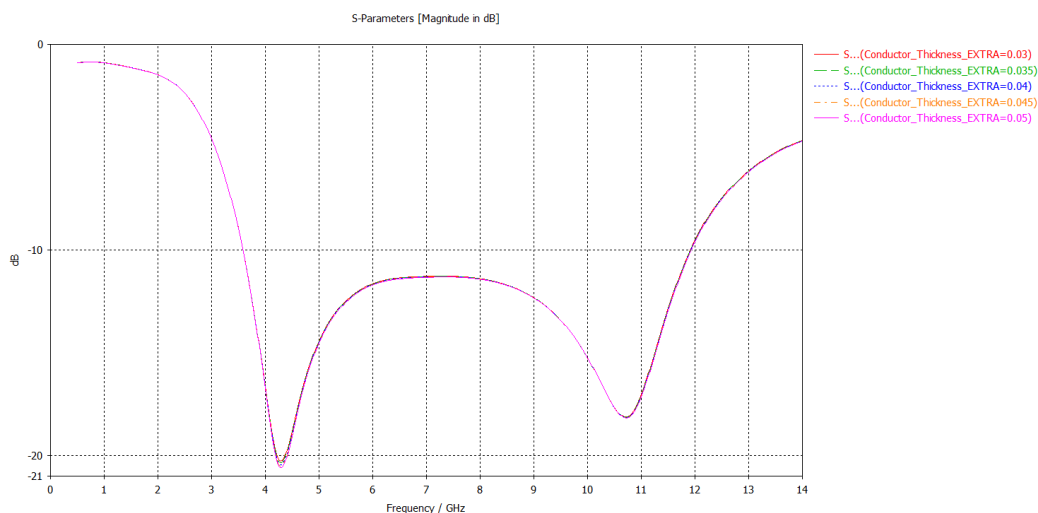
As the title states I was given paper number 5, A Small Wideband Microstrip-fed Monopole Antenna.

## 1.1 Assumptions and Any Parameters Not Given in the Paper

The main assumptions I have made when making the design (as the values are not given in the paper) are regarding the electric conductor; it's thickness and the material used.

I have decided upon copper with a thickness of  $50\mu\text{m}$ , this is based on the fact that if one was designing a PCB with a patch antenna such as this I am almost certain that for cost reasons standard materials and design would be used; meaning conductors such as gold would not be used (and furthermore, PEC not being a real material could not be used).

The thickness would have to be within the standard range provided by a PCB manufacturer and thus I choose to use the specifications of a manufacturer I have used before [1],  $50\mu\text{m}$  is at the thicker end of their specifications. I ran a parameter sweep, shown below in Figure 1, to prove that material thickness changes of this size ( $\mu\text{ms}$ ) cause negligible difference, at least when it comes to return loss.

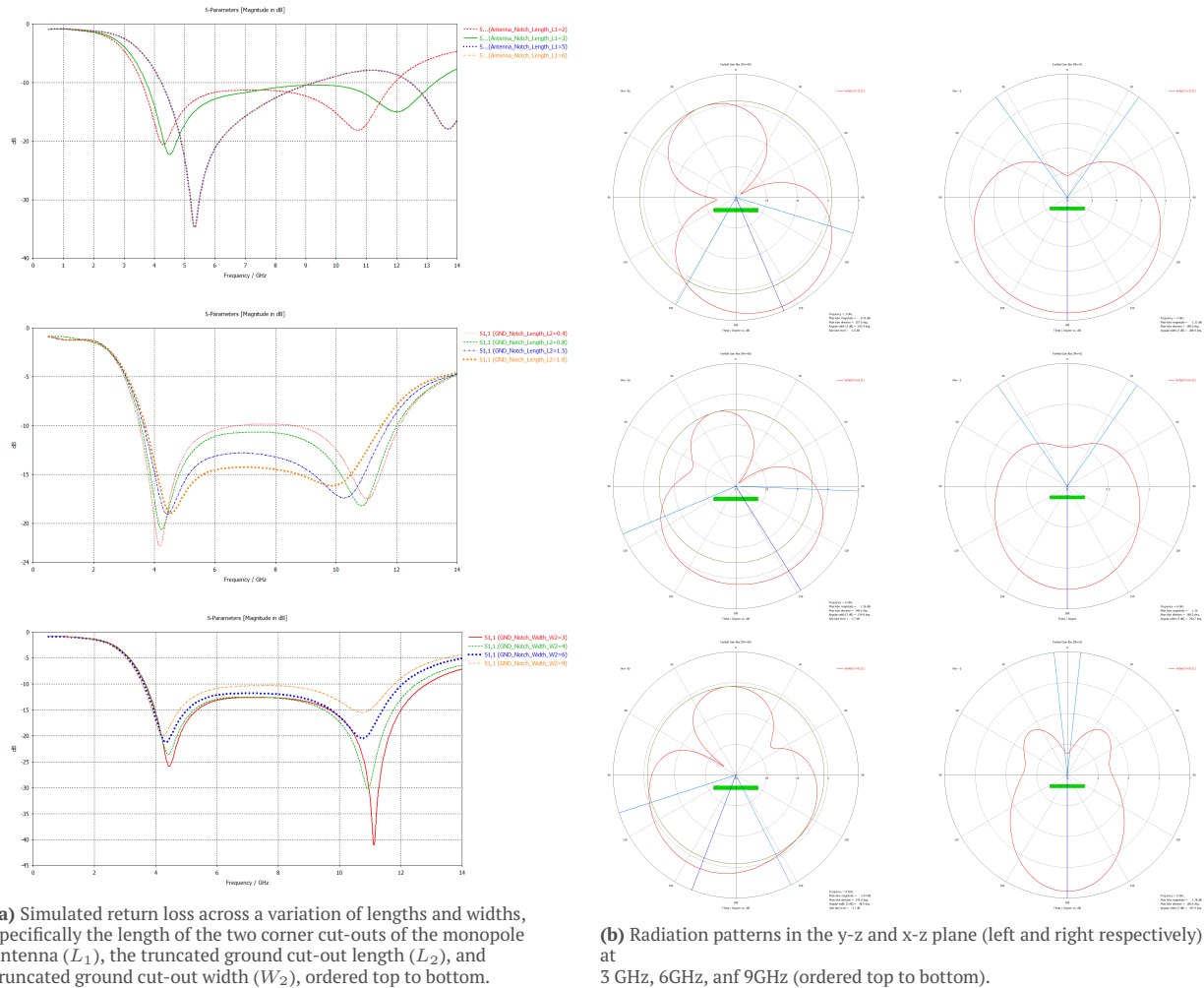


**Figure 1:**  $S_{11}$  Parameters as material thickness is changed.

Other than what is listed above, I tried to follow the paper as closely as possible, even going as far as to alter CST's default value for the relative dielectric constant of FR-4 from 4.3 (CST's default) to 4.4 (what the paper lists as the dielectric constant for FR-4).

## 1.2 Design and Simulation Set-up and Initial Results

The first step I carried out for the design was to design the structure of the monopole device as per the paper and then set up the excitation port, and various field, current, etc. monitors for the antenna. I recreated all of the graphs (that can be recreated by CST) shown in the the original paper, these are labelled Figures 2 through 6 in the original document, you can see them below in Figure 2:



**Figure 2:** A recreation of the graphs found in the paper.

The results obtained by CST when following the design specifications laid out in the paper are significantly different to that of the paper, so I strived to obtain a more accurate facsimile. I thought the most likely cause for the disparity could be that the port impedance was not actually  $50\mu$ , so I ran a significant number of parameter sweeps on the width of the feeder micro-strip. The results from this simulation is shown below in Figure 3. None of these results completely match that shown in the paper, and I ran many other simulations on a plethora of dimension parameters in an attempt to recreate the results of the paper, however there is not enough room in this report to present all of those attempts. In the next Section I present the results of my selected optimised values.

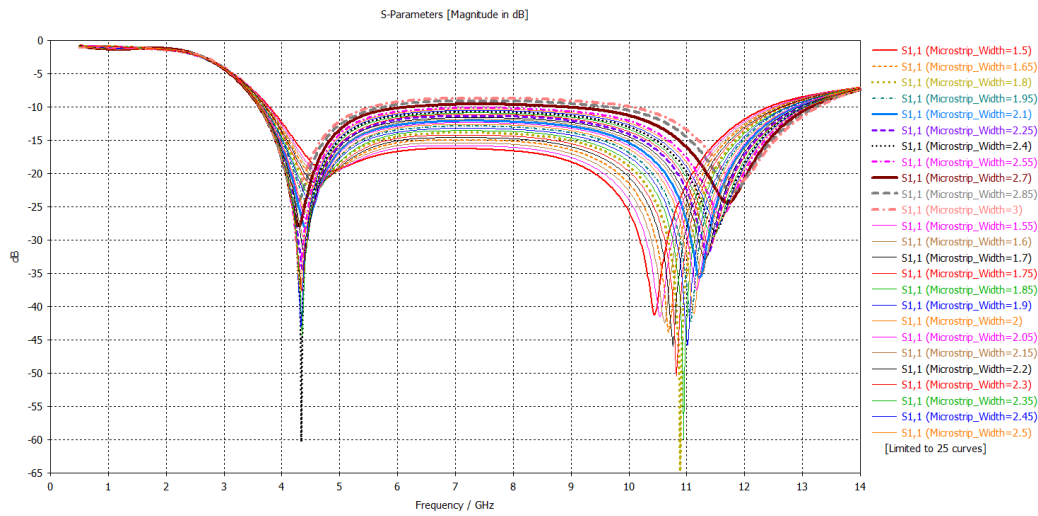


Figure 3:  $S_{11}$  Parameters as the feeding micro-strip width is changed.

## 2 Final Results and Discussion

The final results are obtained from a set of dimensions I chose in order to try to strike a balance between minimal average return loss and as wide an operating bandwidth as possible. The final dimensions I chose are:  $W_2 = 3mm$  and Microstrip Width = 1.9mm, compared to  $W_2 = 7mm$  and Microstrip Width = 2mm used in the paper. The resulting return loss graph from my chosen dimensions is shown below in Figure 4. These display a good bandwidth ( 3.7GHz to 12.5GHz) and a very good average return loss across the bandwidth, there is enough of a tolerance that a manufactured version of the antenna should be able to realistically operate across the bandwidth. These results, again, obviously do not perfectly replicate the paper but are close enough and are a result from enough simulation on part to make it as close as possible to the paper.

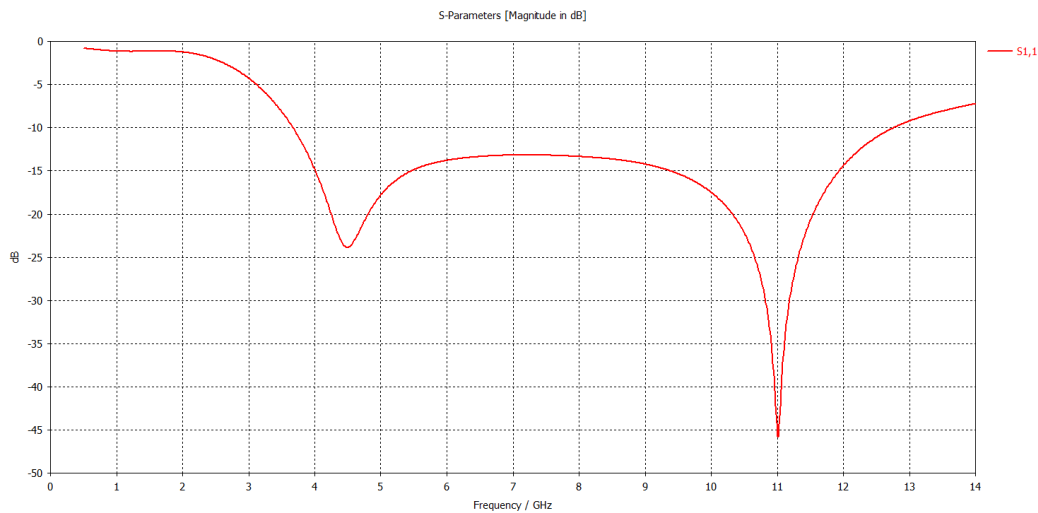
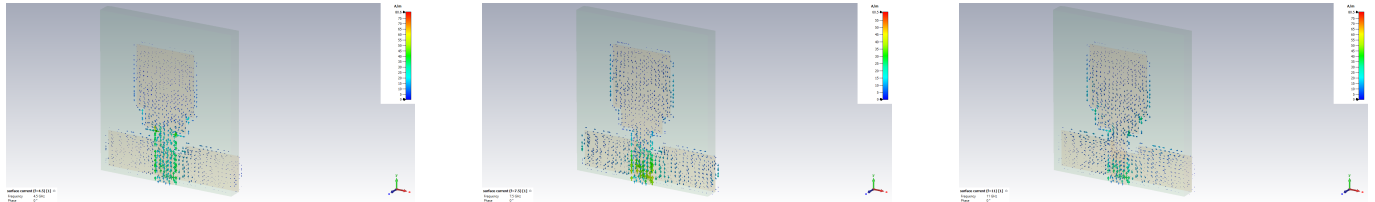


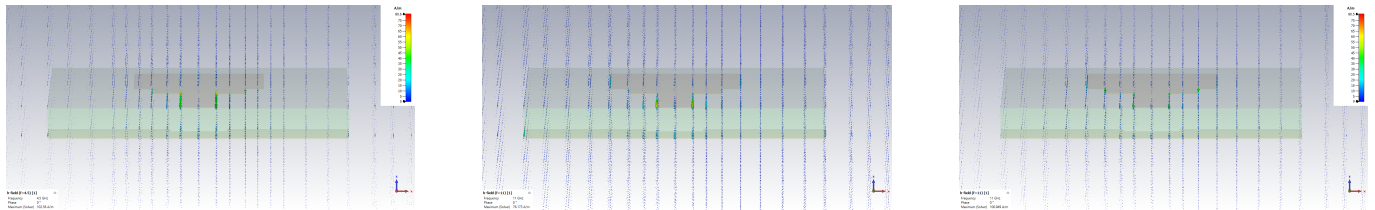
Figure 4:  $S_{11}$  Parameters of the optimised antenna

Looking at the current density distribution of the antenna at its resonant frequencies, and its central frequency (4.5GHz, 11GHz, and 7.5GHz respectively) shows that the current at the resonant frequencies and across the bandwidth is concentrated through the micro-strip after which it dissipates, which is to be expected considering that it should be radiating out from the rest of the antenna. A 3D representation of the current density is shown in Figure 5.

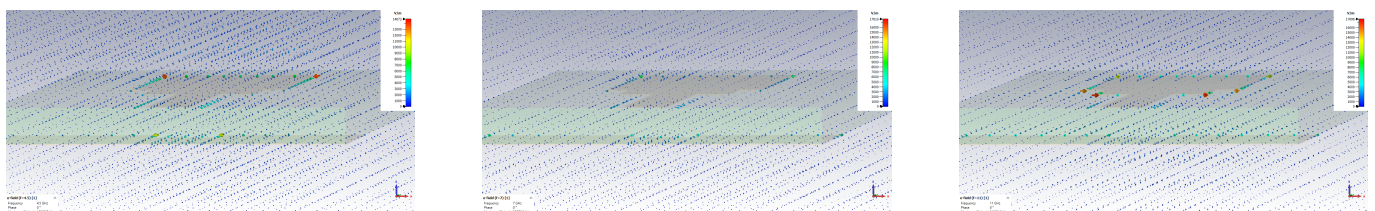


**Figure 5:** 3D images of the current density at 4.5GHz, 7.5GHz, & 11GHz

The magnetic and electric fields of the antenna at its resonant frequencies, and its central frequency (4.5GHz, 11GHz, and 7.5GHz respectively) also show an expected story, the magnetic field circles around the antenna's y-axis and the electric field is flowing towards the ground plane in a fashion very similar to that of a micro-strip transmission line. The fields also help to explain the far-field results shown later, the far-field is heavily directional, concentrating towards the ground plane with low gain in a lot of other directions. Figures 6 and 7 display the magnetic and electric fields respectively.

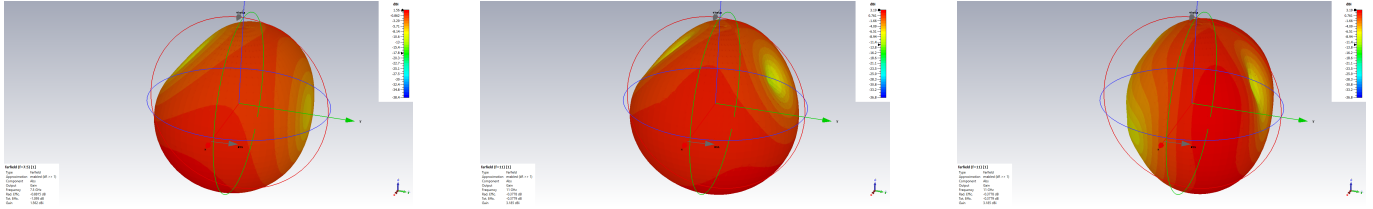


**Figure 6:** 3D images of the magnetic field at 4.5GHz, 7.5GHz, & 11GHz



**Figure 7:** 3D images of the electric field at 4.5GHz, 7GHz, & 11GHz

The far-field radiation pattern of the antenna at the relevant frequencies (4.5GHz, 7.5GHz, and 11GHz) displays that the resulting antenna does not have a very similar radiation pattern to that of a monopole antenna, it is not as directional as a traditional monopole, the pattern is somewhat similar to a torus shape but not much. At the resonant frequency of 11GHz the torus shape is particularly prominent.



**Figure 8:** The far-field radiation of the antenna at 4.5GHz, 7.5GHz, & 11GHz

## References

- [1] A. Wilson. (2022, Jun.) Beta layout pcb specifications. Beta Layout. (accessed: 12.06.2022). [Online]. Available: <https://us.beta-layout.com/pcb/technology/specifications/>