



EMIMEO : E(rasmus) Mundus on Innovative Microwave Electronics and Optics Master

Foundations of Electromagnetic Wave Propagation – 2nd part

Contributors:

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UNIVERSITÀ
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Foundations of electromagnetic wave propagation

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Chapters:

0. Microwave domain
1. S-parameters and transmission line
 - a. Microwave signals - time and frequency domains
 - b. Description of microwave devices by scattering parameters
 - c. Exercises on the parameters S
 - d. Description of microwave devices by chain matrix
2. Theory of transmission lines
3. Smith Chart and impedance matching
 - a. Introduction, uses and principles
 - b. Movement along the line
 - c. Different methods for impedance matching
 - d. Matching by a stub
 - e. Matching by double stubs

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Chapters:

4. Antennas

- a. Reminder of fundamental concepts
- b. Solutions of Maxwell's equations
- c. The elementary electric dipole
- d. Characteristics of antennas
- e. Wired antennas
- f. Links between antennas
- g. Radar Cross Section
- h. Telecommunications' equations
- i. Antenna arrays
- j. Radiant aperture antennas
- k. Reflector Antennas
- l. Printed antennas
- m. UWB Antennas

Chapters:

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0. Microwave domain

1. Context of RF and microwave communications

- **Radio Frequencies** : basis of Wireless communications (unilateral: FM, DVB-T*, GPS, ...; bilateral: 2-5G , WIFI, Bluetooth, ...)

The near present: **IoT**** (5G, ...), **SmartAg** (cashless payment, ticketing, access control, photo activation & social media, Loyalty & gamification, management panel : wearable RFID) and **Smart Cities Applications** (energy, health care, water and waste management)

All this thanks to the use of EM fields and very high frequency signals:

- **EM radiation** family :

Consisting of a **magnetic** and **electric fields** that propagate as a wave

* DVB-T : Digital Video Broadcasting – Terrestrial

** Internet of Things : 30 billion connected objects by 2020, 75 billion by 2025

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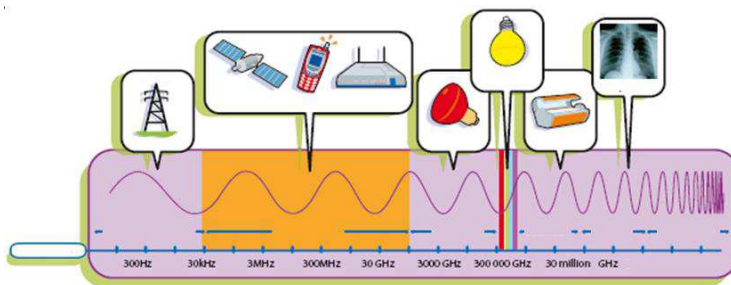
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0. Microwave domain

2. Spectrum of RF and microwave communications

Definition

Microwaves:



Frequency space between ‘short’ radio waves and infrared in its broadest definition

Centimeter and millimeter wavelengths (100 cm to 1 mm, 300 MHz to 300 GHz) in a more restricted definition

Frequency range from to in use

What does not change with the frequency level : physics, the law of electromagnetism (Maxwell)

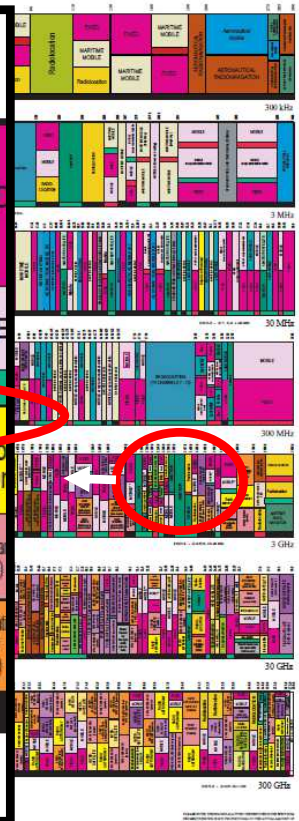
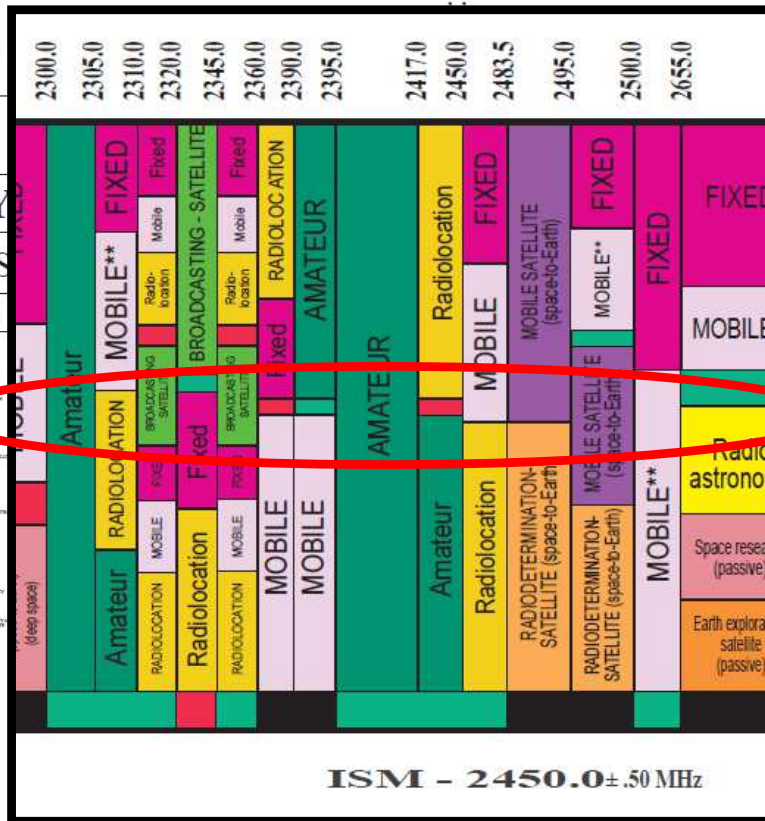
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0. Microwave domain

UNITED STATES FREQUENCY ALLOCATIONS THE RADIO SPECTRUM



5. Spectrum of RF and microwave communications

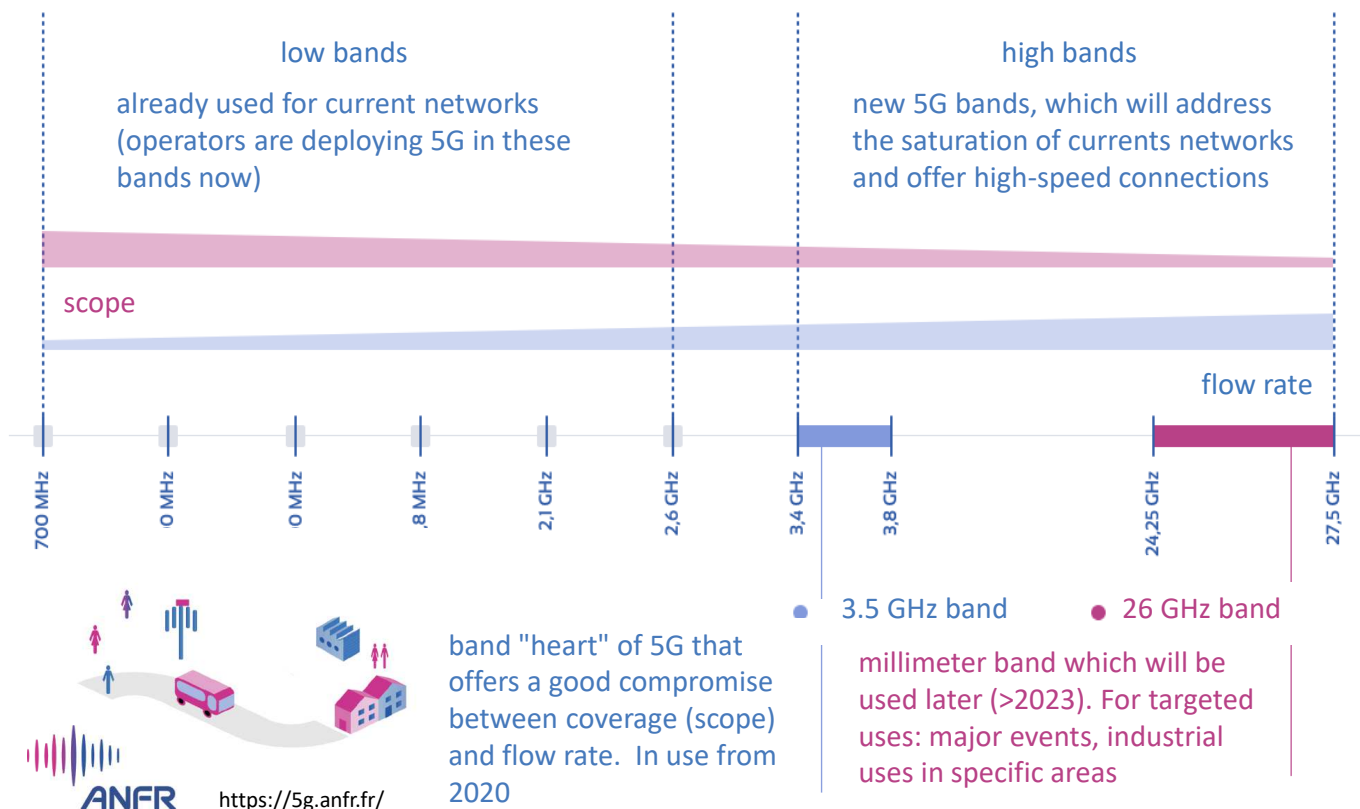
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0. Microwave domain

6. example of 5G frequency bands



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0. Microwave domain

7. Some specific tools for microwave communications

Some specific concepts and tools for RF and Microwave communications

Spectrum Analyzers (Signal Analyzers)

Dynamic Signal Analyzers, Materials Measurement

Vector Signal Analyzer

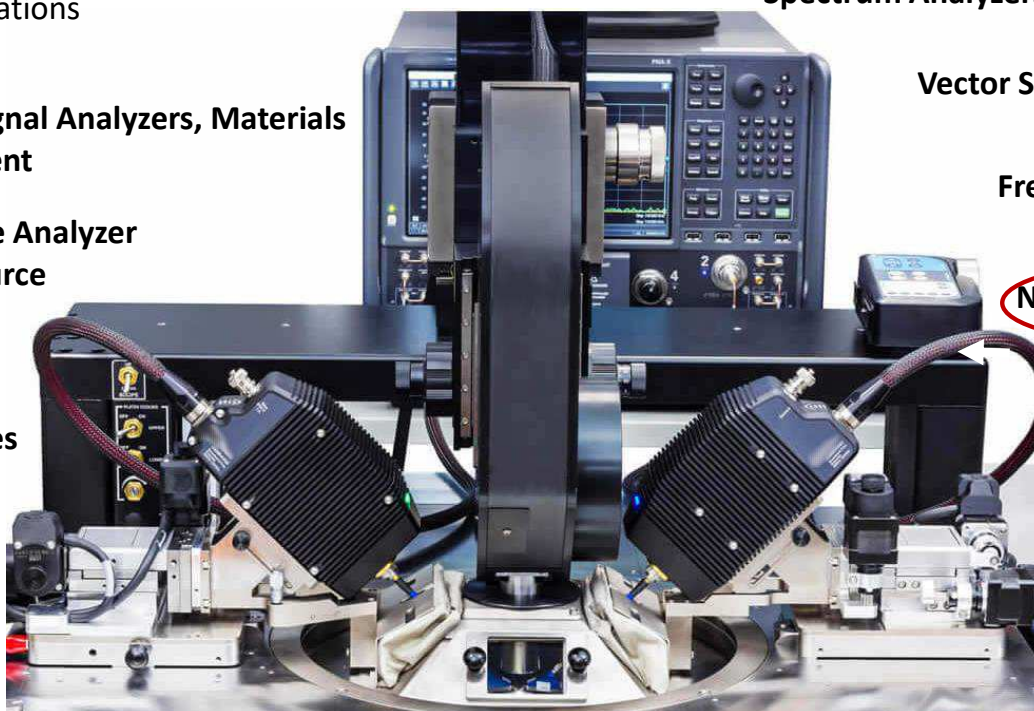
Frequency Counter

Noise Figure Analyzer & Noise Source

Network Analyzers

Oscilloscopes

Power Meter & Power Sensor



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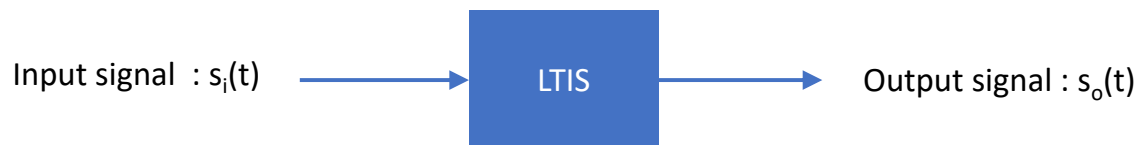
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Characterization of Linear Time Invariant System (LTIS) or Device Under Test (DUT)



- **Linear** : signal $x_1(t)$ or $x_2(t)$ at the input produce $y_1(t)$ or $y_2(t)$ at the output

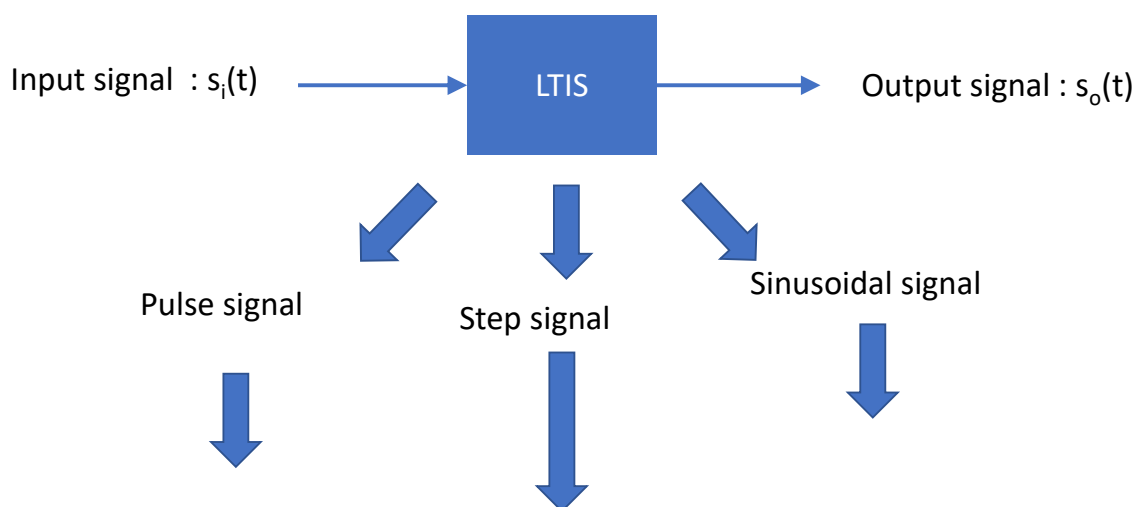
then, the signalat the input produce at the output

- **Time Invariant** : signal $x_1(t)$ at the input produce $y_1(t)$ at the output

then at the input produce at the output

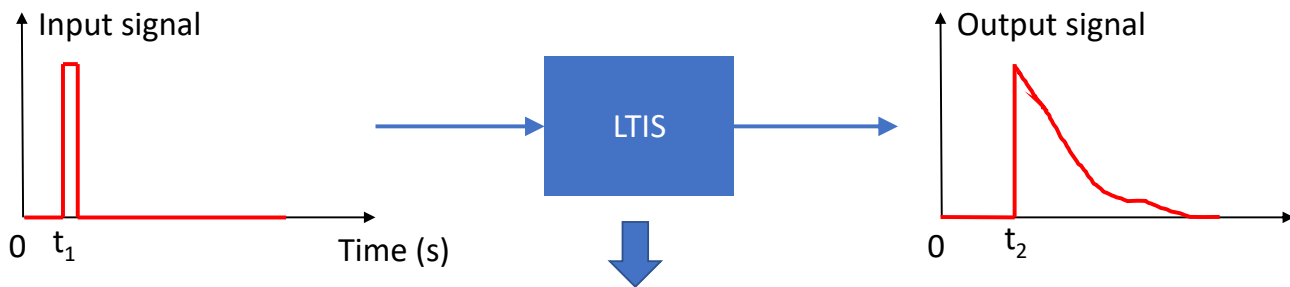


Characterization of Linear Time Invariant System (LTIS) or Device Under Test (DUT)





Characterization of Linear Time Invariant System (LTIS)

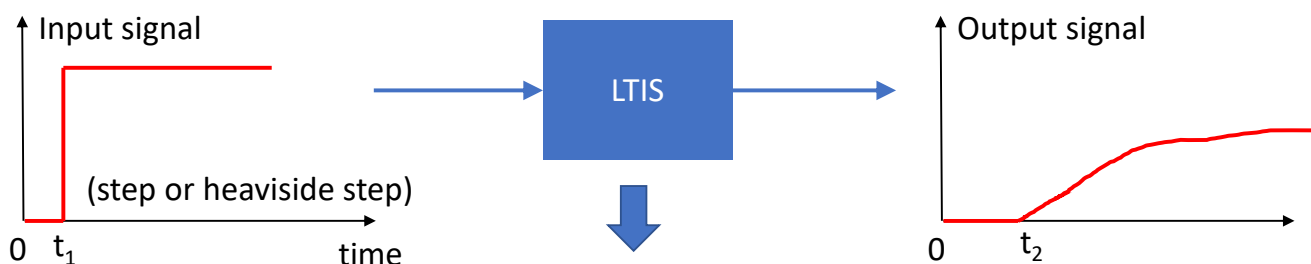


Impulse response

-
-
- Difficult generation of an ultra-short pulse of high amplitude
-



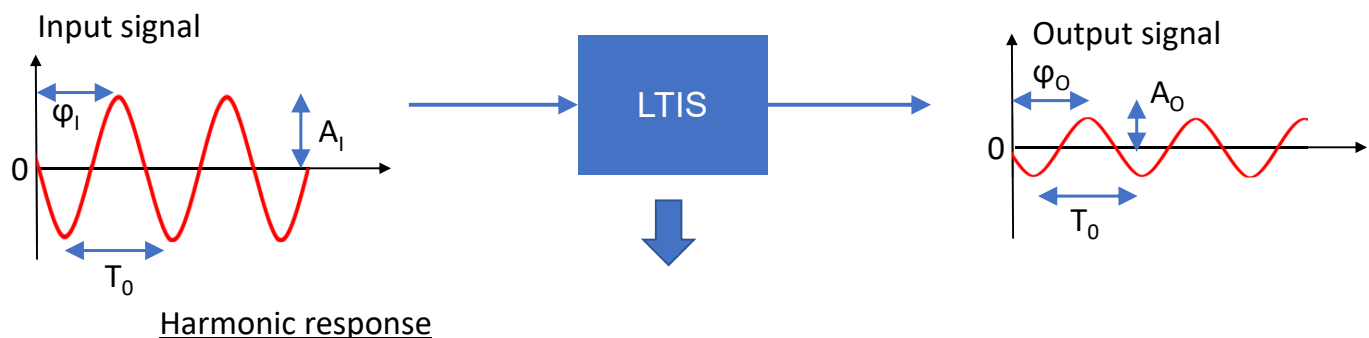
Characterization of Linear Time Invariant System (LTIS)



Step response

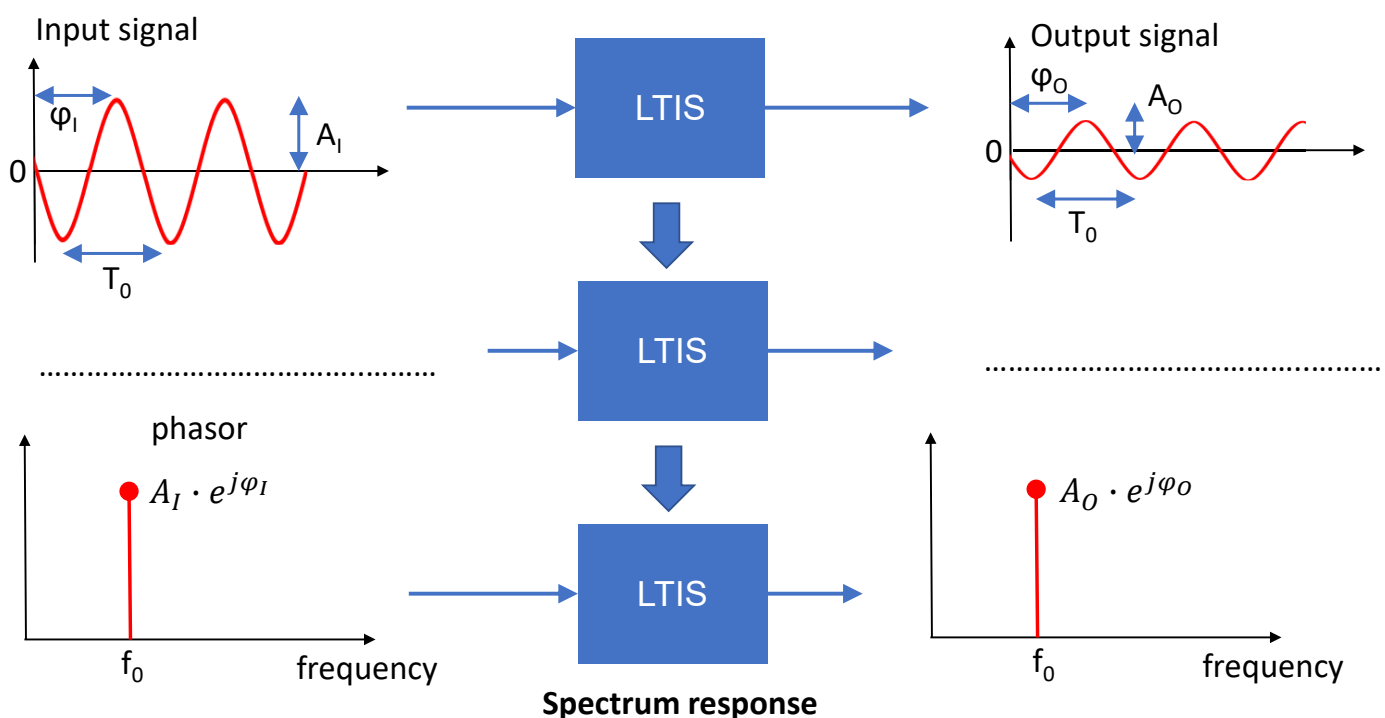
-
- Measurement of LTIS establishment time
- Generation of a Heaviside step with a very short rise time
-

Characterization of Linear Time Invariant System (LTIS)



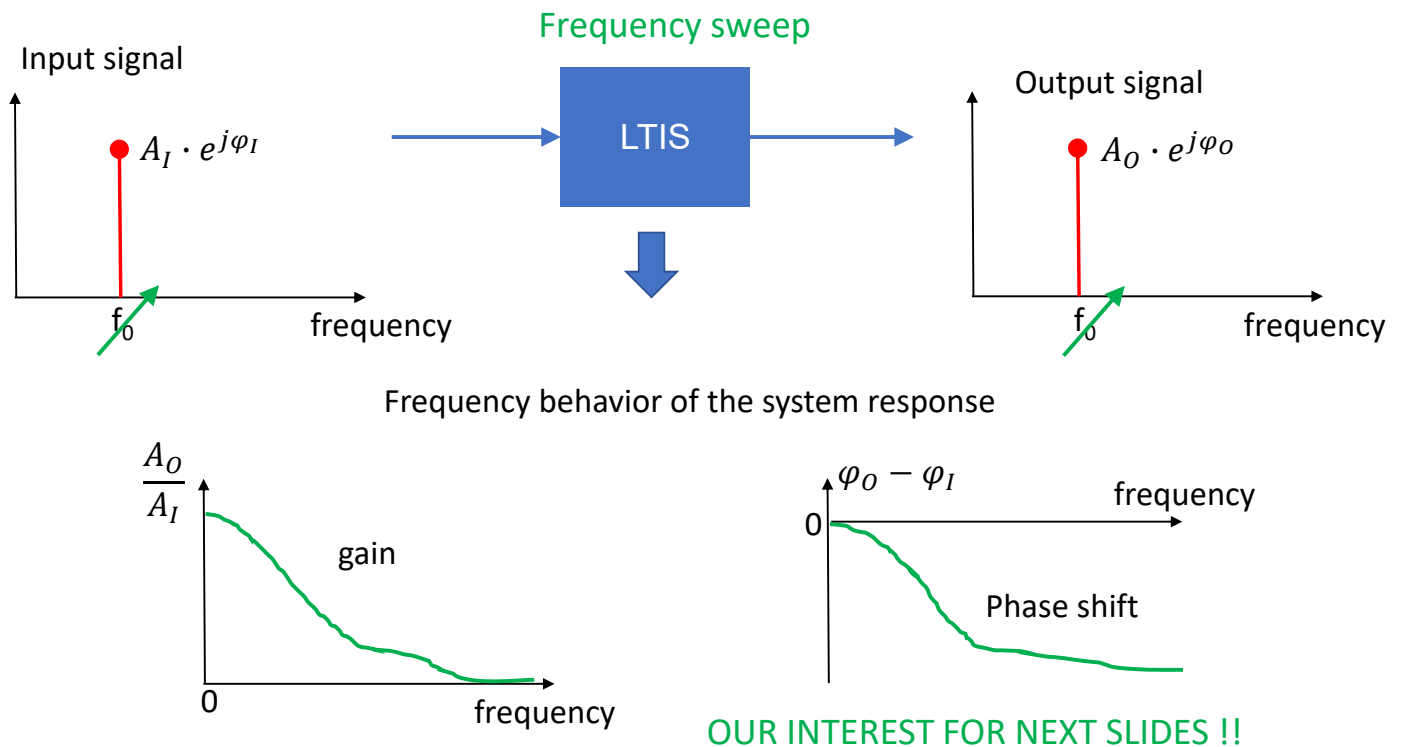
-
-
- Easy generation of a sinusoidal signal LF up to THz
- LTIS \rightarrow differential equations \rightarrow no deformation of the sinusoidal shape
-

Characterization of Linear Time Invariant System (LTIS)



1. S-parameters and transmission line

7. Microwave signals - time and frequency domains



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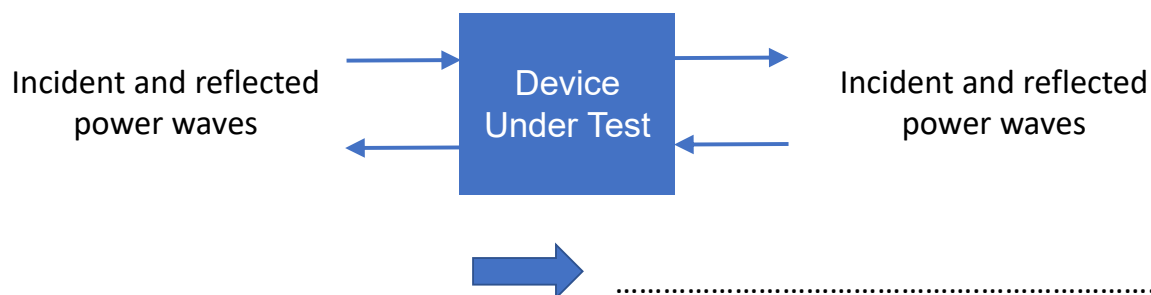
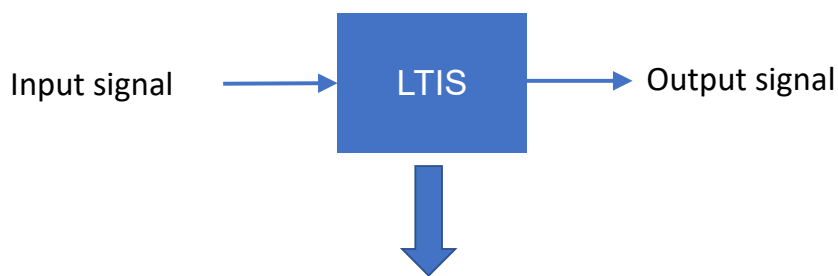
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1. S-parameters and transmission line

1. Description of microwave devices by scattering parameters



[1] David M. Pozar, Microwave Engineering, Third Edition, John Wiley & Sons Inc.; (ISBN 0-471-17096-8)

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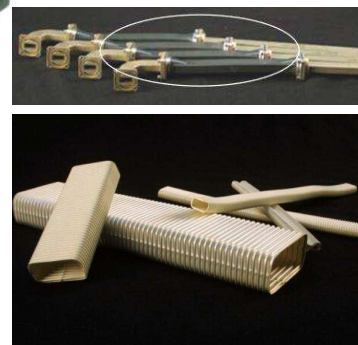
1. S-parameters and transmission line

2. Description of microwave devices by scattering parameters



Example : Rectangular waveguides

Only currents on conductor



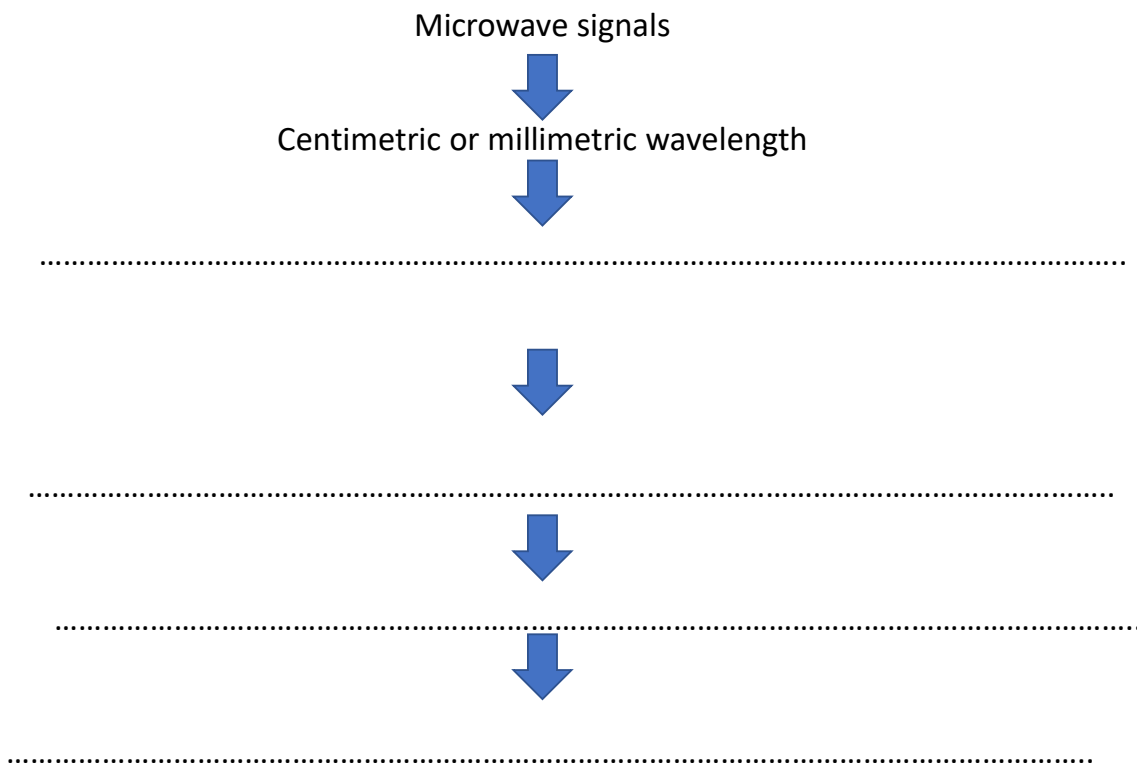
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1. S-parameters and transmission line

2. Description of microwave devices by scattering parameters



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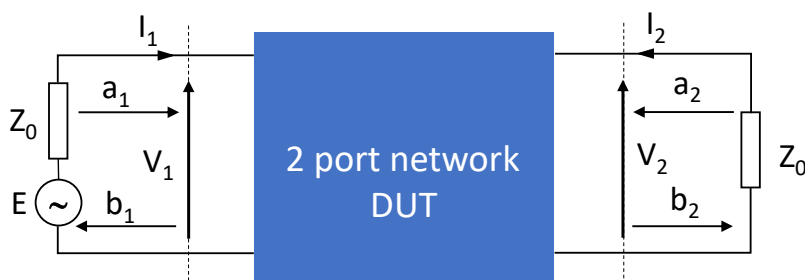
1. S-parameters and transmission line

3. Description of microwave devices by scattering parameters



Most RF/microwave components can be represented by a two-port network [2] :

For example, the expression of v_1 is :



For example, the expression of v_1 is : $v_1(t) = |V_1|\cos(\omega t + \phi) = \text{Re}(|V_1|e^{j(\omega t + \phi)}) = \text{Re}(V_1 e^{j\omega t})$

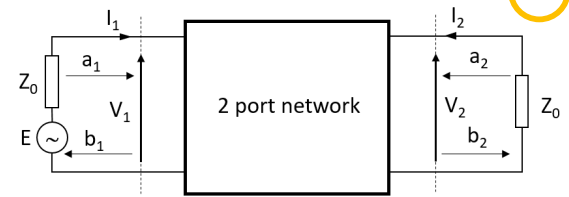
The wave variables a_1, a_2 (incident waves) and b_1, b_2 (reflected wave) are introduced.

[1] David M. Pozar, Microwave Engineering, Third Edition, John Wiley & Sons Inc.; (ISBN 0-471-17096-8)

1. S-parameters and transmission line

4. Description of microwave devices by scattering parameters

The relationships between the wave variables and the voltage and current variables are defined as :



$$\begin{aligned} \dots\dots\dots (1) \quad a_n &= \frac{1}{2} \left(\frac{V_n}{\sqrt{Z_0}} + \sqrt{Z_0} I_n \right) \quad \text{with } n = 1 \text{ and } 2 \\ \dots\dots\dots b_n &= \frac{1}{2} \left(\frac{V_n}{\sqrt{Z_0}} - \sqrt{Z_0} I_n \right) \quad \text{and } Z_0 \text{ the reference impedance} \end{aligned}$$

with a_n and b_n in, so the incident and reflected power can be expressed at the port n :

Usually, at microwave frequencies, $Z_0 = 50 \, \Omega$

[2] Jia-Sheng Hong, M. J. Lancaster, Microstrip Filters for RF/Microwave Applications, John Wiley & Sons Inc.(ISBN: 0-471-38877-7)

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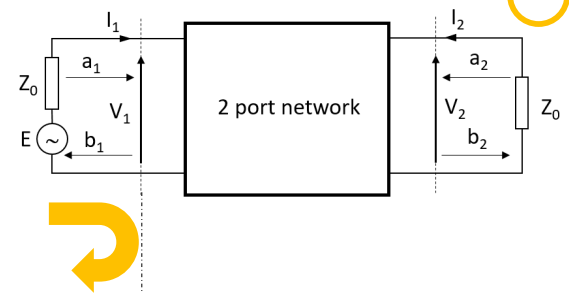
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1. S-parameters and transmission line

5. Description of microwave devices by scattering parameters

The relationships between the incident and reflected waves and the S parameters are :



$$S_{11} = \frac{b_1}{a_1} \text{ with } a_2 = 0$$

..... is the ratio between the reflected and the incident wave that is the definition of a

This coefficient must be minimize to promote the transmission of the power through the quadripole

The port 2 must be connected to the reference impedance Z_0 for $a_2 = 0$

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1. S-parameters and transmission line

6. Description of microwave devices by scattering parameters

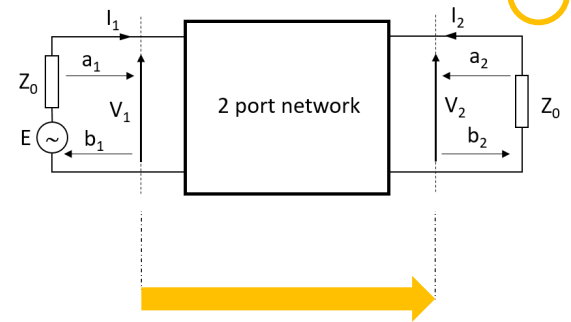
$$b_1 = S_{11} \cdot a_1 + S_{12} \cdot a_2$$

$$b_2 = S_{21} \cdot a_1 + S_{22} \cdot a_2$$

$$S_{21} = \frac{b_2}{a_1} \text{ with } a_2 = 0$$

..... is the ratio between the transmitted (port #2) and the incident (port #1) wave that is the definition of a between the port #1 to the port #2. This coefficient must be maximize the power through the quadripole.

The port #2 must be connected to the reference impedance Z_0 for $a_2 = 0$ (no incident wave on the port #2)



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1. S-parameters and transmission line

7. Description of microwave devices by scattering parameters

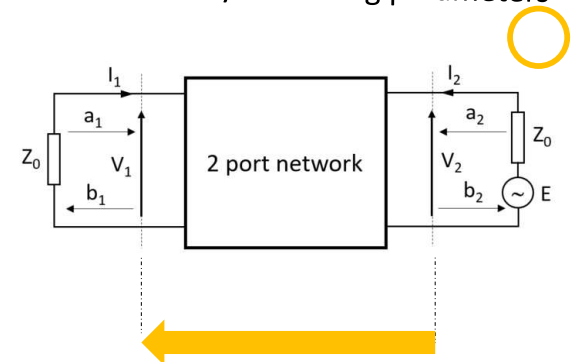
$$b_1 = S_{11} \cdot a_1 + S_{12} \cdot a_2$$

$$b_2 = S_{21} \cdot a_1 + S_{22} \cdot a_2$$

$$S_{12} = \frac{b_1}{a_2} \text{ with } a_1 = 0$$

..... is the ratio between the transmitted (port #1) and the incident (port #2) wave that is the definition of a between the port #2 to the port #1. This coefficient must be maximize the power through the quadripole.

The port #1 must be connected to the reference impedance Z_0 for $a_1 = 0$ (no incident wave on the port #1)



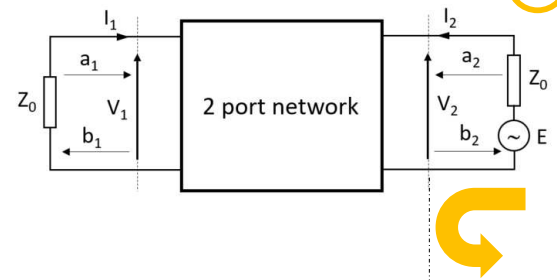
1. S-parameters and transmission line

8. Description of microwave devices by scattering parameters

$$b_1 = S_{11} \cdot a_1 + S_{12} \cdot a_2$$

$$b_2 = S_{21} \cdot a_1 + S_{22} \cdot a_2$$

$$S_{22} = \frac{b_2}{a_2} \text{ with } a_1 = 0$$



..... is the ratio between the reflected and the incident wave (on port #2) that is the definition of a

This coefficient must be minimize the reflected power of the quadripole at port #2.

The port #1 must be connected to the reference impedance Z_0 for $a_1 = 0$ (no incident wave on the port #1)

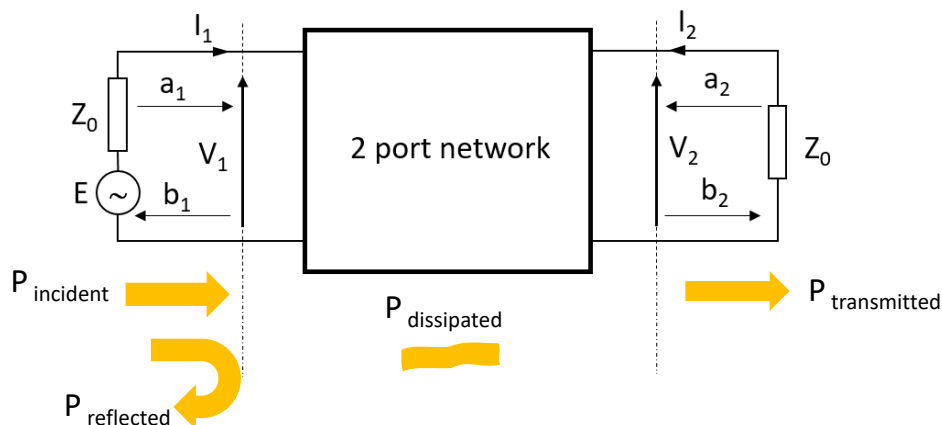
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1. S-parameters and transmission line

9. Description of microwave devices by scattering parameters



$$\Rightarrow 1 = \frac{P_{\text{reflected}}}{P_{\text{incident}}} + \frac{P_{\text{dissipated}}}{P_{\text{incident}}} + \frac{P_{\text{transmitted}}}{P_{\text{incident}}}$$

1. S-parameters and transmission line

10. Description of microwave devices by scattering parameters

$$1 = \frac{P_{\text{reflected}}}{P_{\text{incident}}} + \frac{P_{\text{dissipated}}}{P_{\text{incident}}} + \frac{P_{\text{transmitted}}}{P_{\text{incident}}}$$

with $P_{\text{incident}} = \frac{1}{2} |a_1|^2$

$$P_{\text{reflected}} = \frac{1}{2} |b_1|^2$$

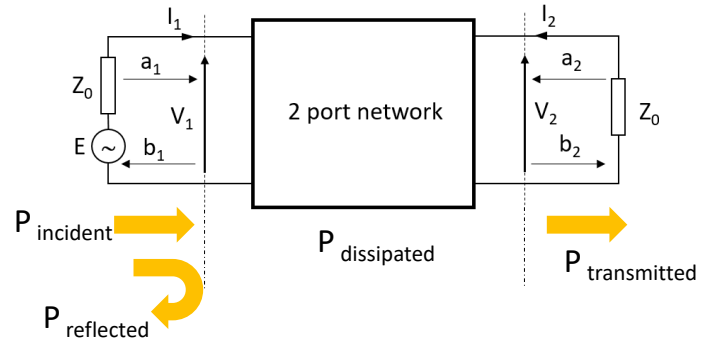
$$P_{\text{transmitted}} = \frac{1}{2} |b_2|^2$$

$$\Rightarrow 1 = \frac{|b_1|^2}{|a_1|^2} + \frac{P_{\text{dissipated}}}{P_{\text{incident}}} + \frac{|b_2|^2}{|a_1|^2}$$

$$\Rightarrow 1 = |S_{11}|^2 + \frac{P_{\text{dissipated}}}{P_{\text{incident}}} + |S_{21}|^2$$

For Loss-Less quadripole : $P_{\text{dissipated}} = 0$

$$\Rightarrow 1 = |S_{11}|^2 + |S_{21}|^2$$



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1. S-parameters and transmission line

11. Description of microwave devices by scattering parameters

Each term depends on the frequency:

$$\begin{pmatrix} b_1(f) \\ b_2(f) \end{pmatrix} = \begin{bmatrix} S_{11}(f) & S_{12}(f) \\ S_{21}(f) & S_{22}(f) \end{bmatrix} \begin{pmatrix} a_1(f) \\ a_2(f) \end{pmatrix}$$

\Rightarrow Frequency representation

\Rightarrow Harmonic response with the frequency sweep

If $S_{21} = S_{12}$ whatever f , then the DUT is reciprocal

If $S_{11} = S_{22} \quad \forall f$, the quadripole is symmetrical

Ideality (lossless) : $[S]^t [S]^* = [1]$ and $S_{11} S_{12}^* + S_{12} S_{22}^* = 0 \Rightarrow \Phi_{12} = \frac{\Phi_{11} + \Phi_{22}}{2} + \frac{\pi}{2}$

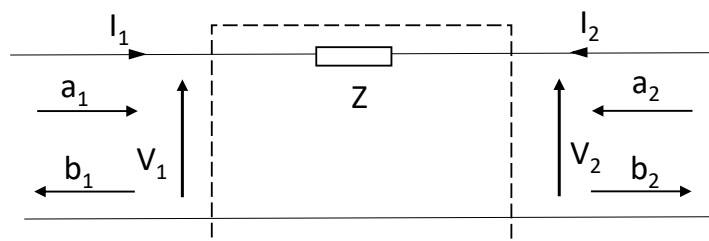
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1. S-parameters and transmission line

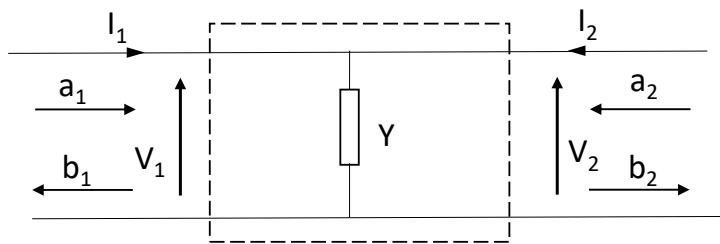
12. S matrix of a series impedance

Exercise #1 : S matrix of a serial impedance



From Kirchoff's and Ohm's laws and the expressions (1) of slide 1-4, give the S matrix of the serial impedance Z

Exercise #2 : S matrix of a shunt admittance



as previously, demonstrate that the S matrix for a shunt admittance could be written as:

$$[S] = \begin{bmatrix} -\frac{y_n}{y_n + 2} & \frac{2}{y_n + 2} \\ \frac{2}{y_n + 2} & -\frac{y_n}{y_n + 2} \end{bmatrix} \quad \text{where } y_n = \frac{Y}{Y_0} \text{ and } Y_0 = \frac{1}{Z_0}$$

References:

- [1] David M. Pozar, Microwave Engineering, Third Edition, John Wiley & Sons Inc.; (ISBN 0-471-17096-8)
- [2] Jia-Sheng Hong, M. J. Lancaster, Microstrip Filters for RF/Microwave Applications, John Wiley & Sons Inc. (ISBN: 0-471-38877-7)
- [3] G. Ghione, M. Pirola, Microwave Electronics, Cambridge University Press (ISBN 978-1-107-17027-8)
- [4] Richard Collier, Transmission Lines, Cambridge University Press (ISBN 978-1-107-02600-1)
- [5] V. Teppati, A. Ferrero, M. Sayed, Modern RF and Microwave Measurement Techniques, Cambridge University Press (ISBN 978-1-107-03641-3)
- [6] Y. Kusama and R. Isozaki, "Compact and Broadband Microstrip Band-Stop Filters with Single Rectangular Stubs", Applied Sciences, vol. 9, n0 248, 2019,