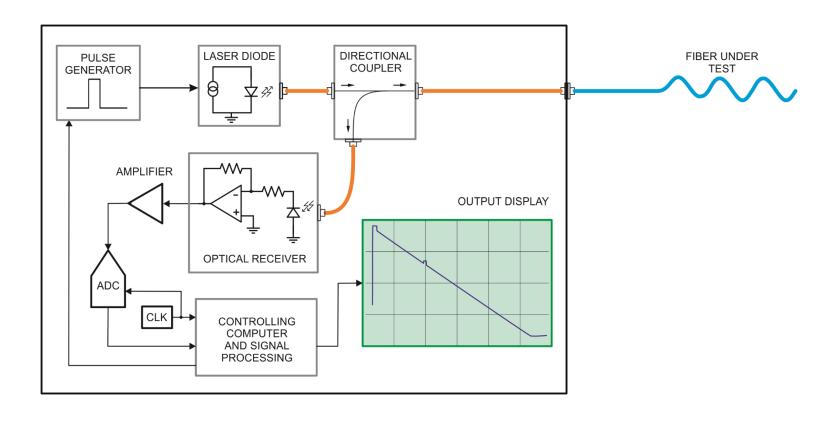
Monitoring of loss in installed fiber links

- ☐ the total loss of the fiber link determines the quality of the transmission system
- □ fiber loss and attenuation are subject to environmental influences, mainly:
 - humidity
 - temperature
 - physical stress
- □ a non-destructive method for measuring the loss is required
- □ the Optical Time Domain Reflectometer (OTDR) is the right solution for monitoring installed optical fibers



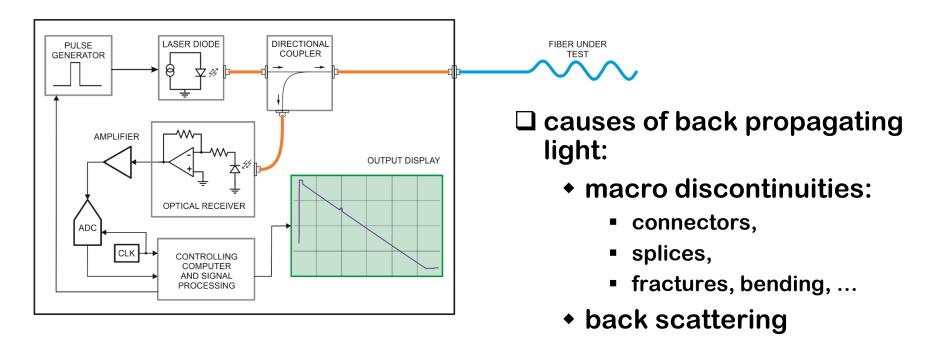
OTDR: principle of operation

- ☐ a short duration pulse is launched into the fiber
- □ the power of the light coming back to the fiber input end is recorded as a function of delay from pulse launch





OTDR: principle of operation



- ☐ scattering:
 - linear:
 Rayleigh, it is due to density fluctuations in the fiber, inhomogeneities
 - nonlinear:
 Brillouin, due to acoustic waves inside the fiber Raman, due to molecular vibrations



absorbance

Backscattering analysis

 \square given P_0 the optical power entering the fiber, the power at a distance z is:

$$P(z) = P_0 \cdot e^{-\alpha z}$$

where α is the attenuation coefficient (km^{-1})

 \square expressing the attenuation in dB/km:

$$\alpha_{dB/km} = 10 \log_{10} \left(\frac{P_0}{P(z)} \right) \frac{1}{z} = 10 \frac{1}{z} \log_{10} (e^{\alpha z}) = 10 \frac{1}{z} \ln(e^{\alpha z}) \frac{1}{\ln(10)} = \frac{10\alpha}{\ln(10)} \approx 4.34\alpha$$



- ☐ in a good modern fiber, the scattering loss is predominant
- \square we can assume $\alpha_S \cong \frac{1}{\lambda^4}$

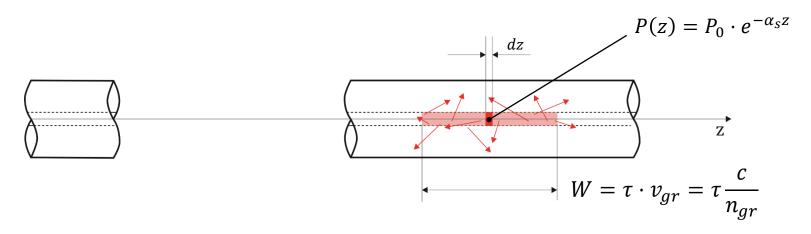


- □ due to scattering, the pulse propagation is affected by losses both in forward and in backward direction
 □ the further, the discontinuity from the input fiber end, the lower the
- ☐ the further the discontinuity from the input fiber end, the lower the power reaching back the photo-sensor

☐ at a given delay from the pulse launching what is the level of the power measured by the photodetector?



Backscattering analysis



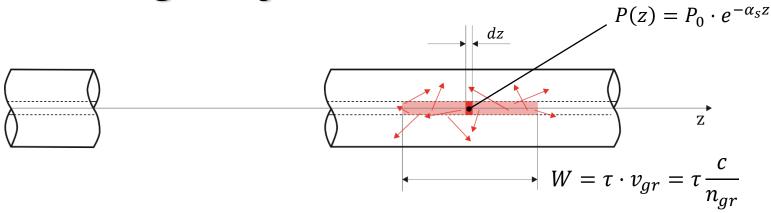
- τ is the temporal duration of the pulse, v_{gr} is the group velocity and n_{gr} is the group refractive index of the glass
- \Box the optical power dP_s scattered by an infinitesimal length of fiber dz is equal to the power lost in that fiber length:

$$dP_S = P(z) - P(z + dz) = -P'(z)dz = \alpha_S \cdot P_0 \cdot e^{-\alpha_S z}dz = \alpha_S \cdot P(z)dz$$

 $lue{}$ only a small fraction dp_s of dP_s will be coupled backward in the fiber and guided towards the fiber input, that is toward the photodetector



Backscattering analysis



☐ the fraction of the optical power scattered that returns to the photo-sensor is:

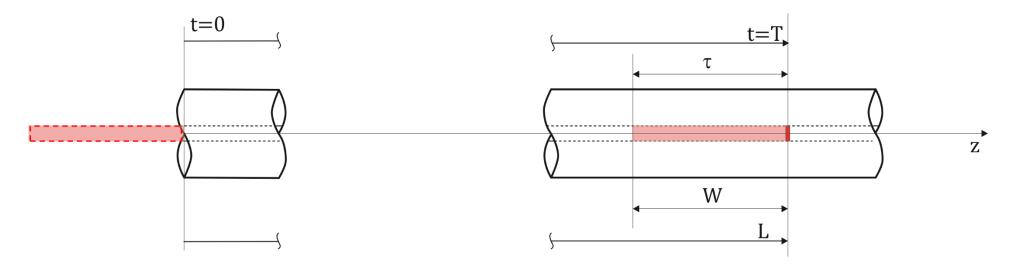
$$dp_S = S \cdot dP_S = S \cdot \alpha_S \cdot P(z) \cdot dz$$
 $\alpha_S \cong \frac{1}{\lambda^4}$

 \Box where S, representing the fraction of the light scattered in all directions that is captured by the fiber core and guided back, is given by:

$$S = \left(\frac{NA}{n_0}\right)^2 \cdot \frac{1}{m}$$

lacktriangled where NA is the numerical aperture of the fiber, n_0 is the refractive index at center of the fiber core, and m is a correcting parameter depending on the refractive index profile of the fiber

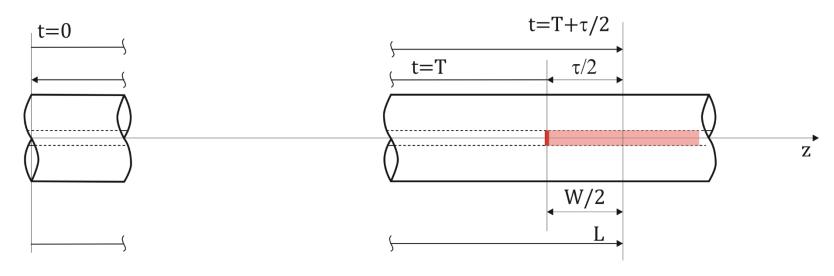




☐ the light scattered at the leading-edge position of the travelling pulse reaches the photo-detector after the round-trip time equal to:

$$T_{forward} + T_{backward} = 2T$$



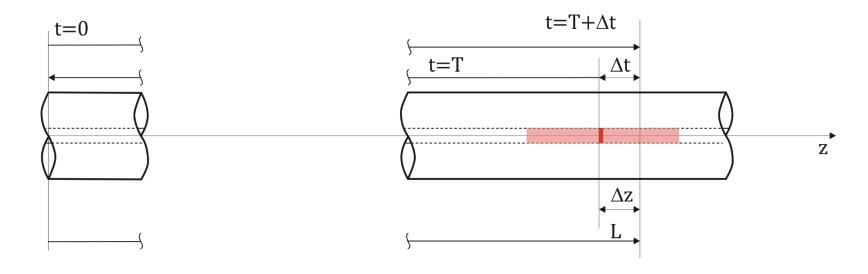


- \Box after a further delay of $\tau/2$ the trailing edge is at L-W/2
- ☐ the light scattered by this trailing edge will reach the photo-detector at

the time
$$T + \frac{\tau}{2}$$
 (forward trip) + $T - \frac{\tau}{2}$ (backwardtrip) = $2T$

 \Box exactly together with the light scattered by the leading edge at time T



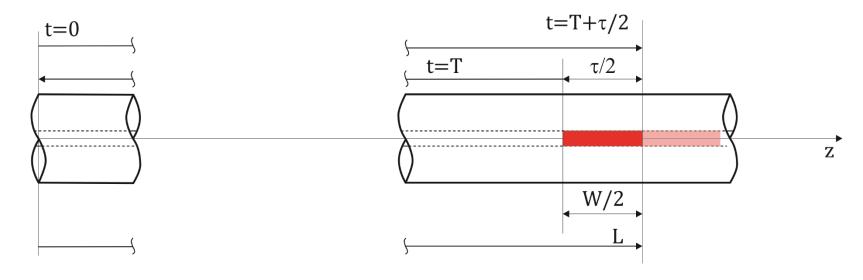


 \Box for any time delay $\Delta t \leq \tau/2$, the light scattered at position

 $L - \Delta z = L - \Delta t \cdot v_{gr}$ takes the same time 2T to reach the photo-detector



 \Box the light collected at the photo-detector at time 2T is, therefore, the integral of the light scattered by the fiber section located from z = L - W/2 to z = L (W is the pulse width)



$$P_{s}(L) = \int_{L-W/2}^{L} \underbrace{e^{-\alpha z}}_{\substack{loss in \\ return \\ trip}} dp_{s} = \int_{L-W/2}^{L} S \cdot \alpha_{s} \cdot (P_{0} \cdot e^{-\alpha z}) \cdot e^{-\alpha z} dz = \frac{S\alpha_{s}P_{0}}{2\alpha} \cdot e^{-2\alpha L}(e^{\alpha W} - 1)$$

for $L \ge W/2$



☐ for short pulses the losses inside the piece of fiber illuminated by the pulse can be neglected, we can assume:

$$P_{s}(L) = \underbrace{P_{0} \cdot e^{-\alpha L} \cdot W/_{2} \cdot S \cdot \alpha_{s}}_{\text{scattered power at position L}} \cdot e^{-\alpha L} = P_{0} \cdot k \cdot W \cdot e^{-2\alpha L}$$

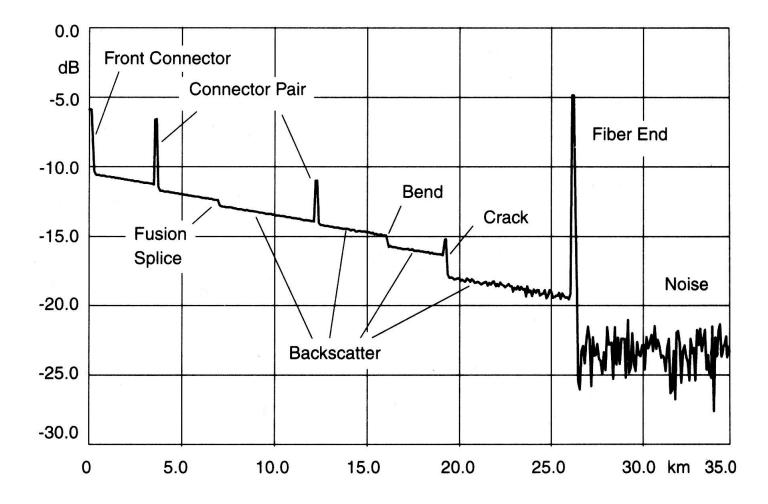
$$coupled backward$$

 \Box we define the backscatter factor as $\sigma = 10 \log \frac{P_0}{P_s(0)} = -10 \log (k \cdot W)$

it can be measured, given W, it is a parameter characterizing the fiber



OTDR: measurement example

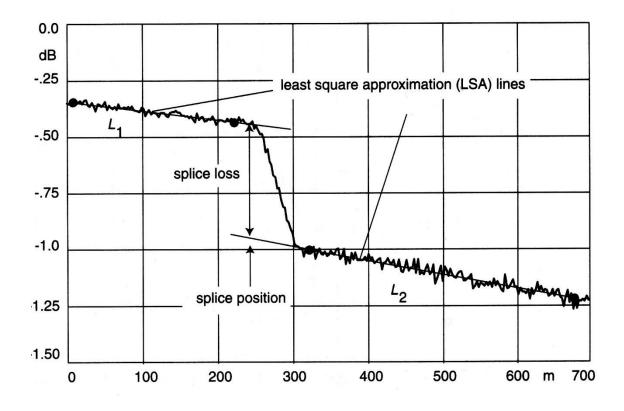




☐ the pulse propagation is affected by losses both in forward and in backward direction ☐ the further the discontinuity from the input fiber end, the lower the power reaching back the photo-sensor ☐ the OTDR works in the time-domain the time-to-distance conversion is based on the knowledge of the light propagation velocity for the round-trip time we can assume: 10 μs/Km ☐ the distance uncertainty is mainly defined by the uncertainty of the refraction index of the fiber ☐ a dual wavelength is usually available: 1310 and 1550 nm **U** typical pulse duration from 5 ns to 10 μS ☐ the signal to noise ratio of the measurement is improved by averaging the acquisition over a great number of pulses



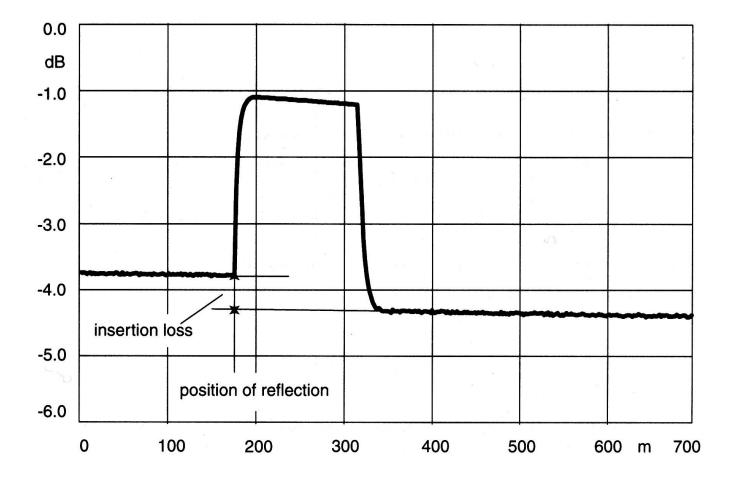
Splicer loss measurement



□the OTDR provides both the splicer loss and the splicer location

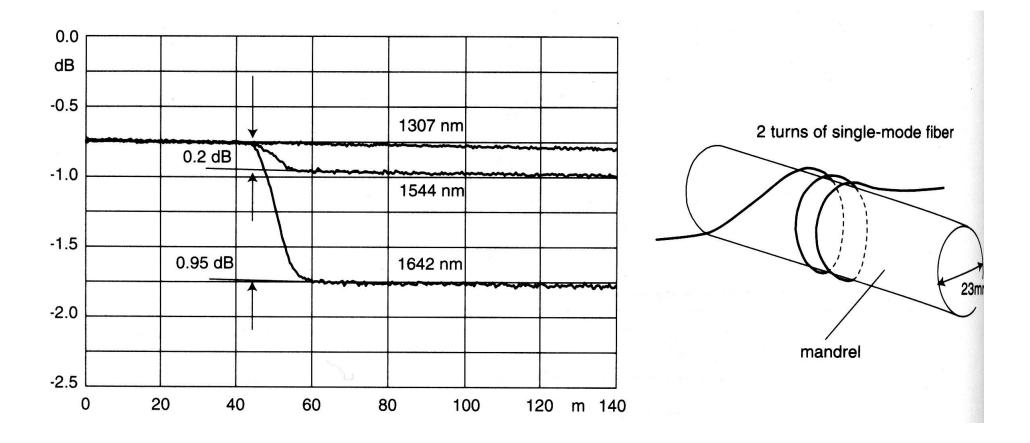


Measurement of a connector insertion loss



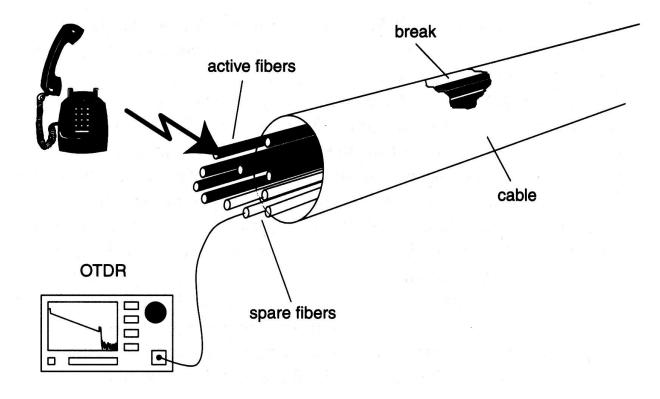


Bending losses





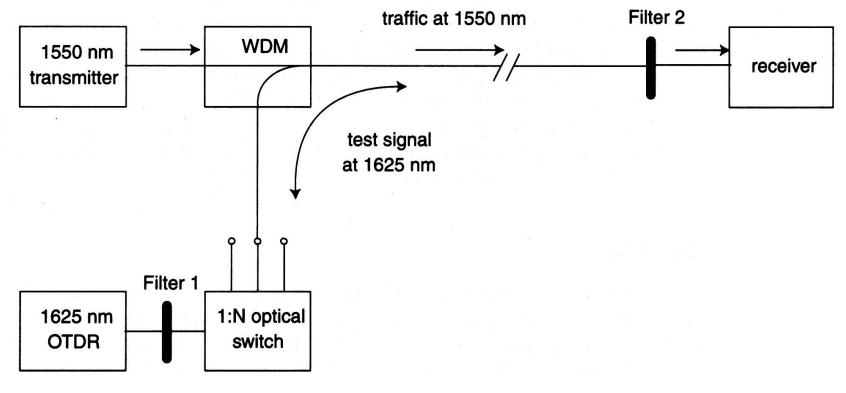
Dark fiber testing



- □the measurement is carried out on spare fibers
- □the hypothesis is that the eventual cable brake damages all fibers of the cable



Active fiber testing



- ☐ the optical filters play a very important role:
 - f1 to guarantee that the OTDR measurement is not influenced by the data traffic
 - f2 to avoid that the OTDR pulses interfere with the data traffic at the digital link receiver