



# Digital Modulation and Channel Coding

Review – Analogue Signal Modulation

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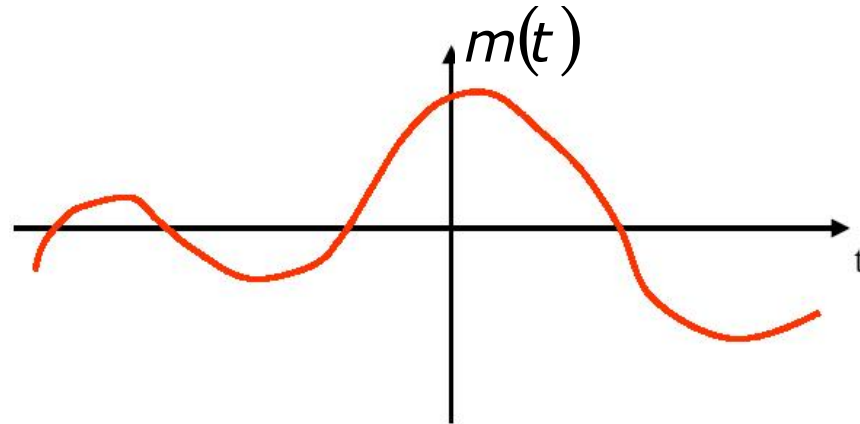
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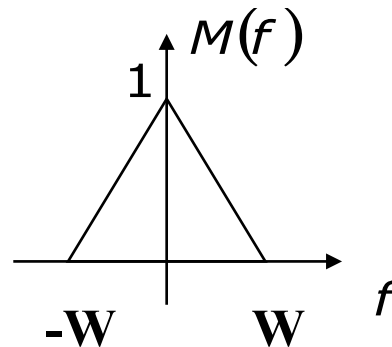
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# Analogue signal modulation

- Problem: we need to send the signal  $m(t)$  from TX to RX



- Spectrum in bandbase (band  $W$ ) generally low-pass type



# Modulation with one carrier

- **Amplitude modulation (AM)**

- translation of the signal spectrum

- linear

- **Angle modulation (PHASE/FREQUENCY)**

- changes the argument of the carrier

- not linear

- **Application**

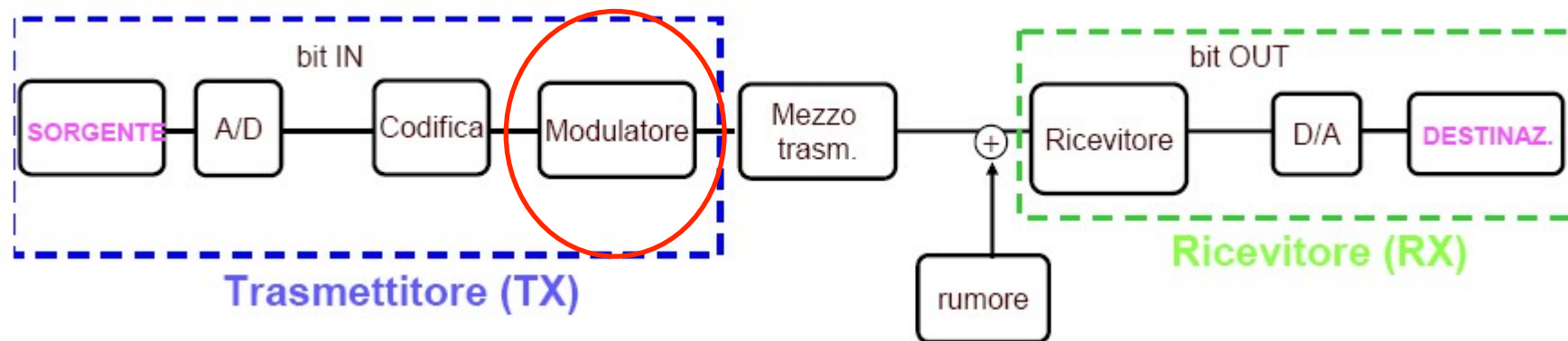
- radio AM, FM

- TV

- traditional telephony

# Modulation

- Signal modulation: turns the baseband bandwidth signal into a passband bandwidth signal, so the signal will be transmitted in a more easy way (it uses in an efficient way the frequency characteristics of the channel)



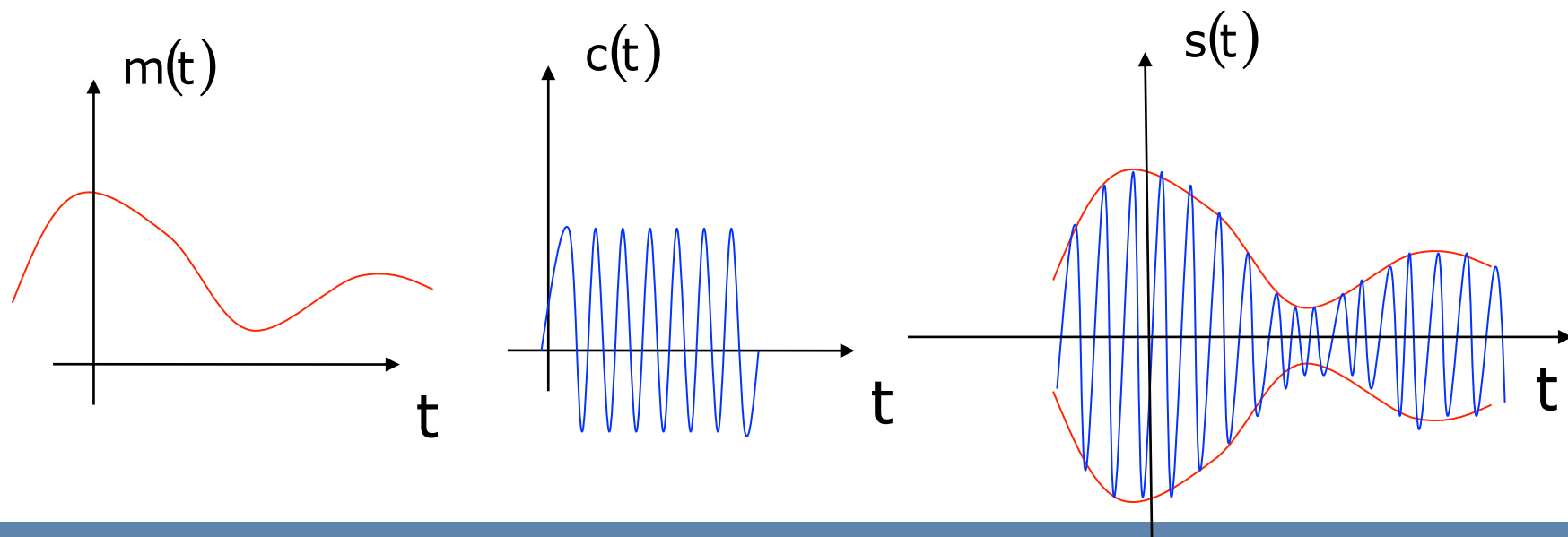
# Amplitude Modulation AM

- Amplitude Modulation - AM

INFORMATION:  $m(t)$  is the “message” that must be sent

CARRIER:  $c(t) = A_c \cos(2 \pi f_c t)$

MODULATED signal:  $s(t)$  is the signal that “travels” on the channel



# AM with transmitted carrier (1)

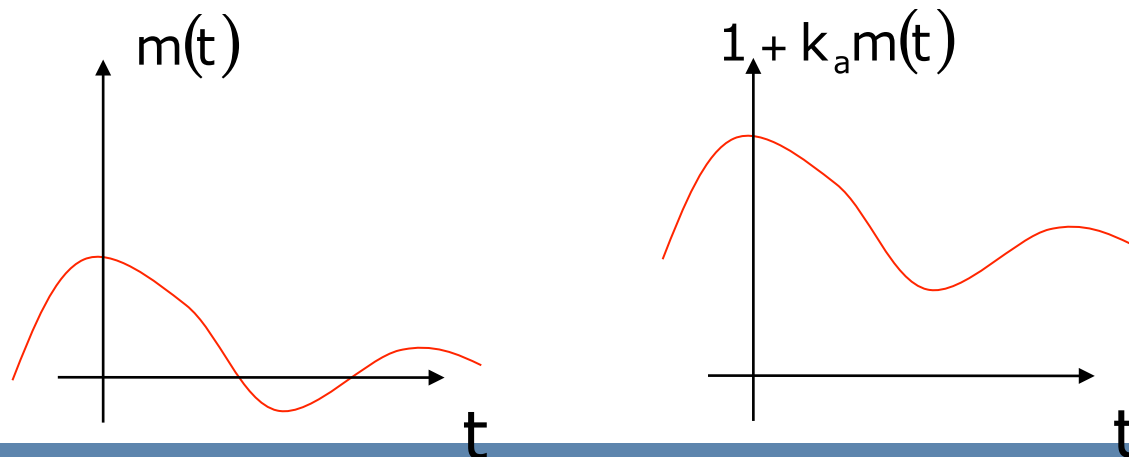
- Amplitude modulation with transmitted carrier (Classic Amplitude Modulation)

INFORMATION:  $m(t)$  is the “message” that must be sent

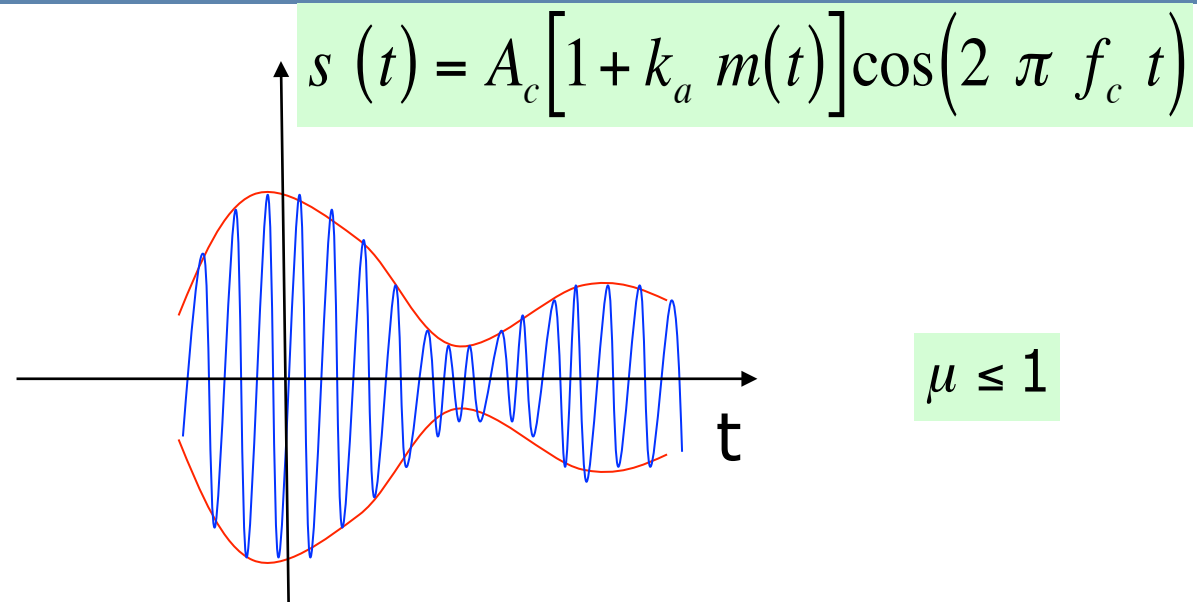
CARRIER:  $c(t) = A_c \cos(2 \pi f_c t)$

MODULATED signal:  $s(t)$  is the signal that “travels” on the channel

$$s(t) = A_c [1 + k_a m(t)] \cos(2 \pi f_c t)$$



# AM with transmitted carrier (2)



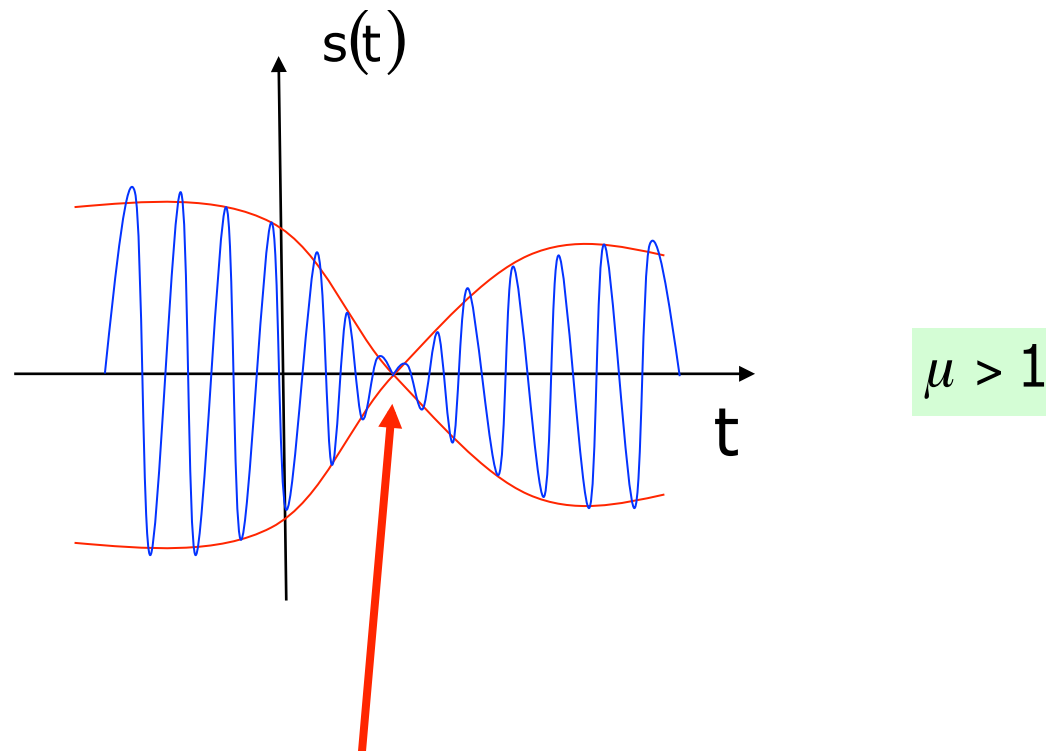
- The functioning limit is given from the index of the modulation.

$$\mu = |k_a m(t)|_{\max}, \quad 0 \leq \mu \leq 1$$

- N.B. The envelope doesn't cross zero!

# Over-modulation

- In the case that the modulation index is bigger than 1 we are in presence of over-modulation



- N.B. There is a phase inversion in the point where the function crosses zero!

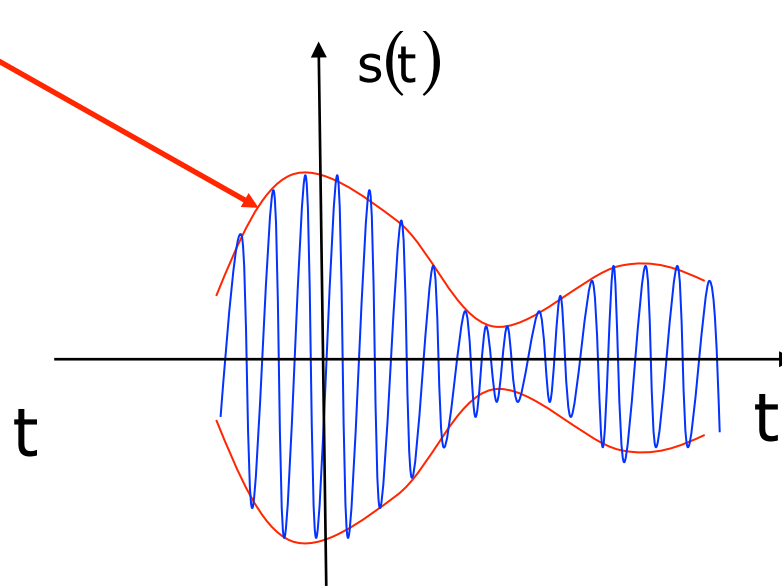


# Amplitude Modulation

- Another condition: the carrier frequency must be much bigger than the maximum frequency of the “information”:

$$f_c \gg W$$

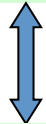
- Under these conditions, the amplitude of  $m(t)$  modules the instant amplitude of the carrier  $c(t)$ : The information is hidden in the envelope of the modulated signal  $s(t)$



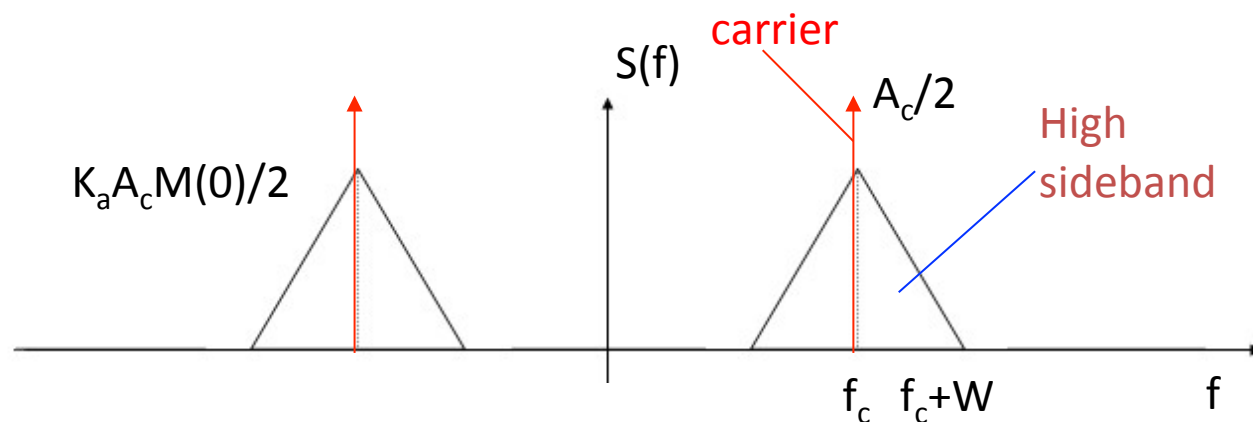
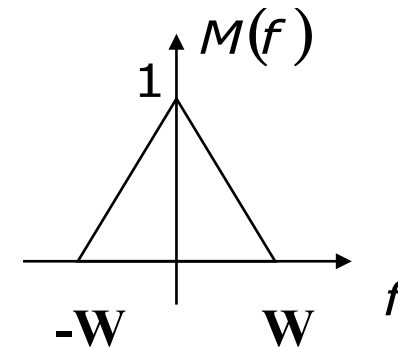
# AM Signal's spectrum (1)

- AM Spectral characteristic

$$s(t) = A_c [1 + k_a m(t)] \cos(2\pi f_c t)$$



$$S(f) = \frac{A_c}{2} [\delta(f - f_c) + \delta(f + f_c)] + \frac{A_c k_a}{2} [M(f - f_c) + M(f + f_c)]$$



# AM signal spectrum (2)

- AM Spectral characteristic

It's a simple translation of the signal's spectrum around the frequency of the carrier!!

- Bandwidth

$$B_T = 2W$$

- It's a LINEAR modulation
- It is DISTORTED from NON-LINEAR systems!!

It's easy to recovery (demodulate) the original signal

→ demodulation = envelope detector

# Bandwidth and power efficiency

- The efficiency of the bandwidth in the AM is equal to

$$\eta_B = \frac{W}{2W} = \frac{1}{2}$$

- The power efficiency is

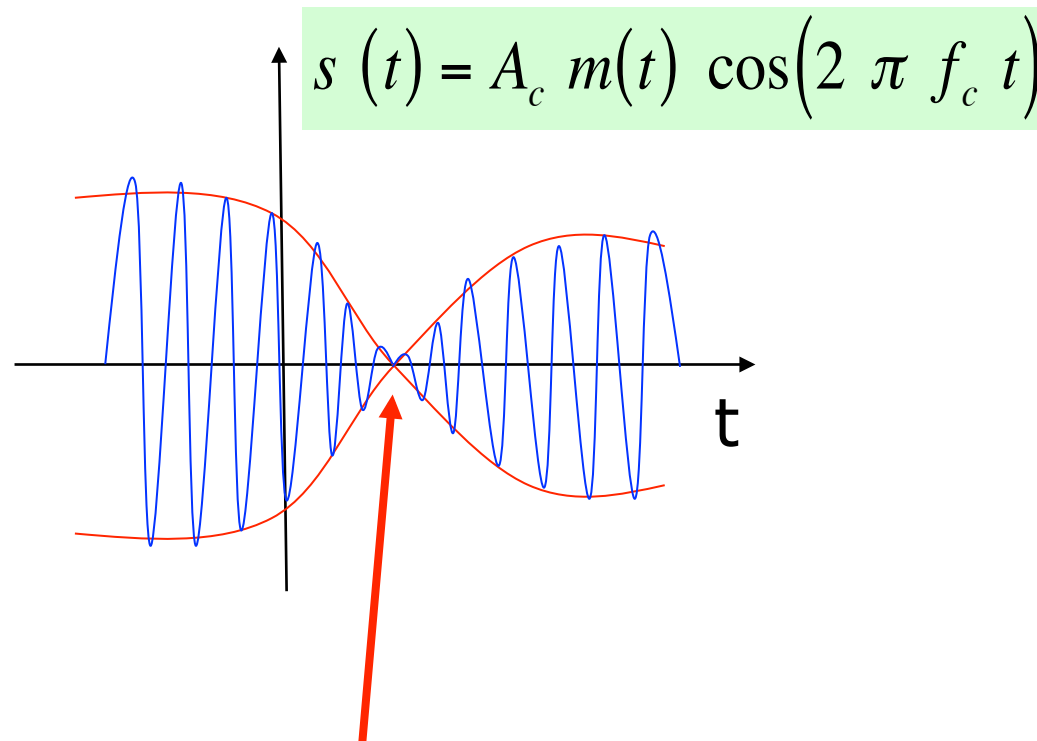
$$\eta_P = \frac{P_s}{P_s + P_c}$$

N.B. The transmitted carrier WASTES POWER!  $\rightarrow$  double-sideband suppressed-carrier transmission

# AM with Suppressed Carrier (1)

- Modulation DSB-SC (Double Side Band Suppressed Carrier)

Called “AM with Suppressed Carrier”

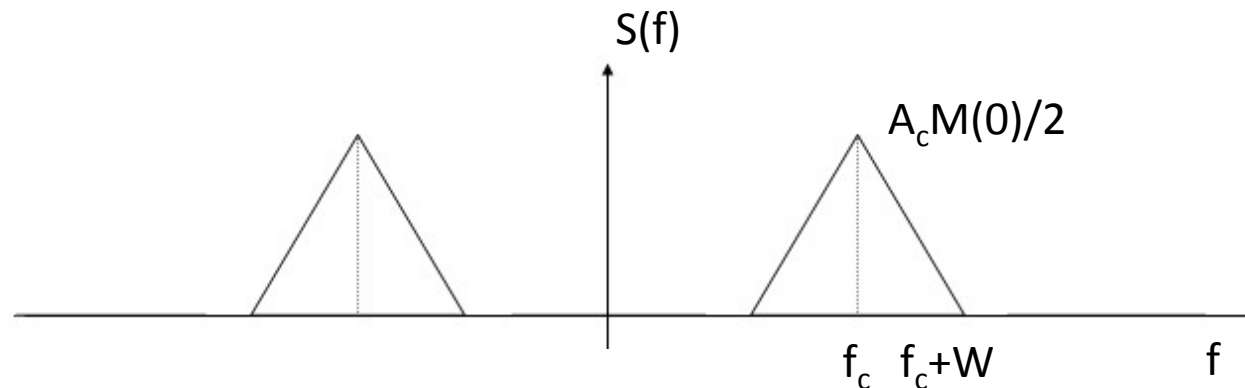


- There is a phase inversion in the point where the function crosses zero!

# AM with Suppressed Carrier (2)

- It's more difficult to recover (demodulate) the original signal
- It uses less power than the system with TRANSMITTED CARRIER
- The bandwidth is the same as before  $B_T=2W$ , in fact the spectrum is

$$s(t) = A_c m(t) \cos(2\pi f_c t) \longleftrightarrow S(f) = \frac{A_c}{2} [M(f - f_c) + M(f + f_c)]$$



# AM with Suppressed Carrier (3)

- The efficiency of the bandwidth in the AM with suppressed carrier is equal to

$$\eta_B = \frac{W}{2W} = \frac{1}{2}$$

- The power efficiency is

$$\eta_P = 1$$

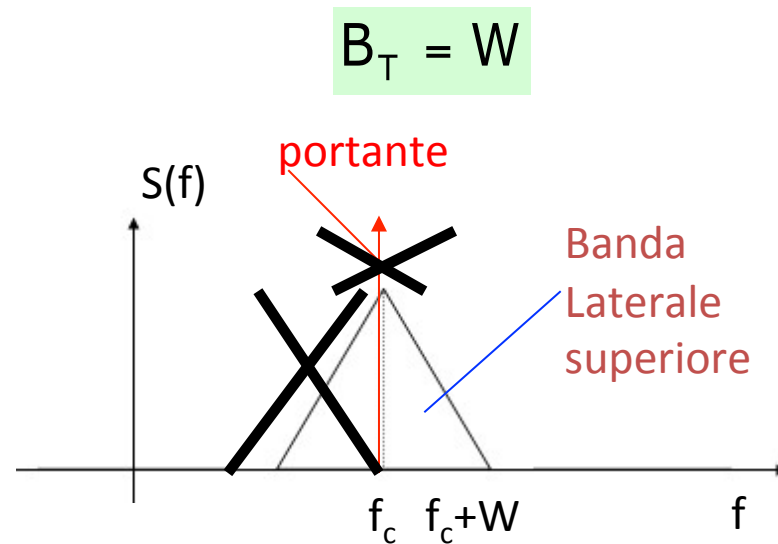
- For recovering the signal without transmitting the carrier we will need, at the demodulator, a sinusoid with the same frequency and phase of the carrier
- This system is called SYNCHRONOUS (expensive synchronization circuits based on PLL at the demodulator)

# AM with Unique SideBand

- There are some techniques of modulation that remove also ONE sideband of the two  
→ used of the spectrum band is reduced!

- AM with Suppressed Side Band (SSB)

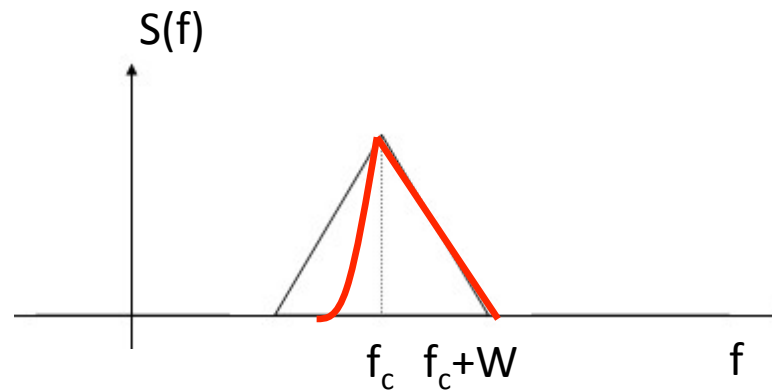
- Bandwidth





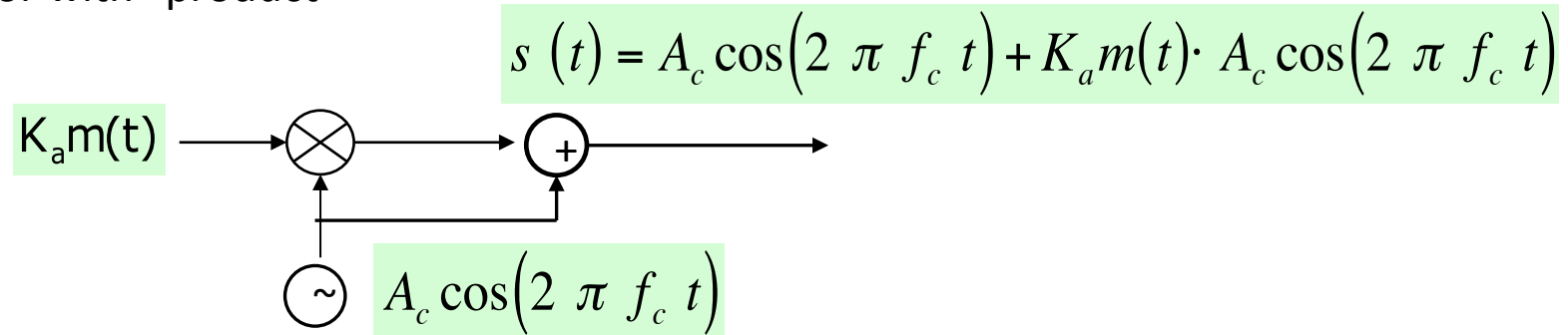
# Sideband partially suppressed

- It could be really difficult delete completely the sideband
- There are some modulation techniques that partially suppress the sideband
- Amplitude modulation with Vestigial Side Band (VSB)

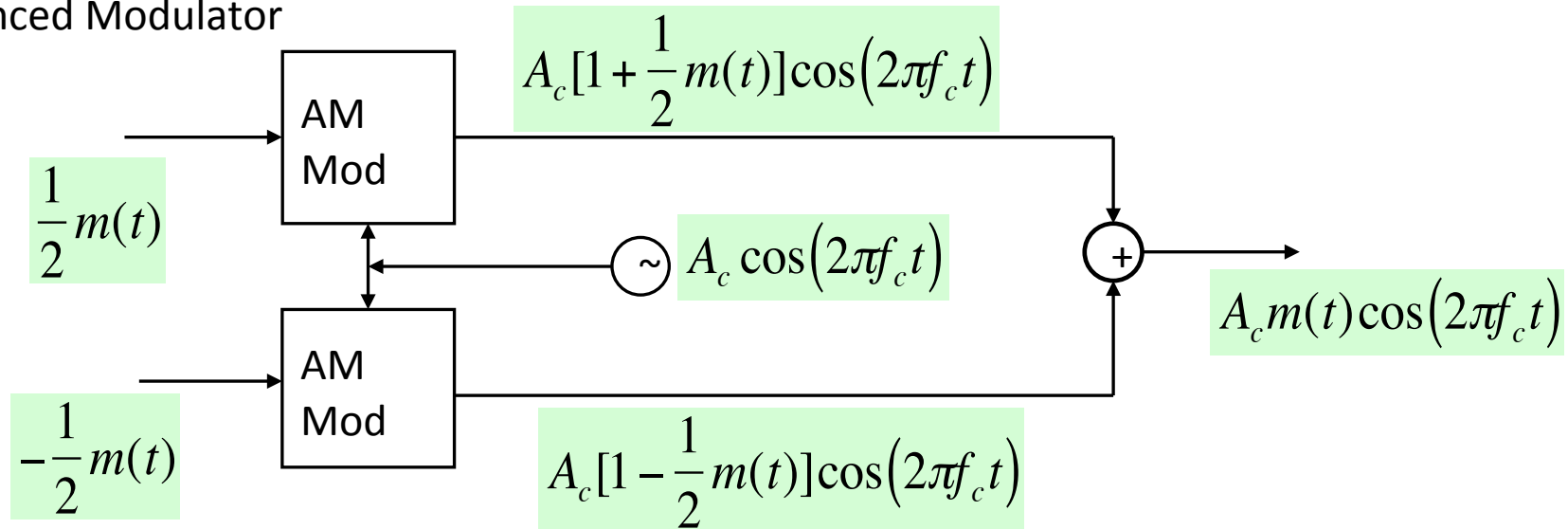


# Modulator (1)

- Modulator with “product”



- Balanced Modulator



# Modulator (2)

- **Kind of modulator:**

- Variable Transconductance

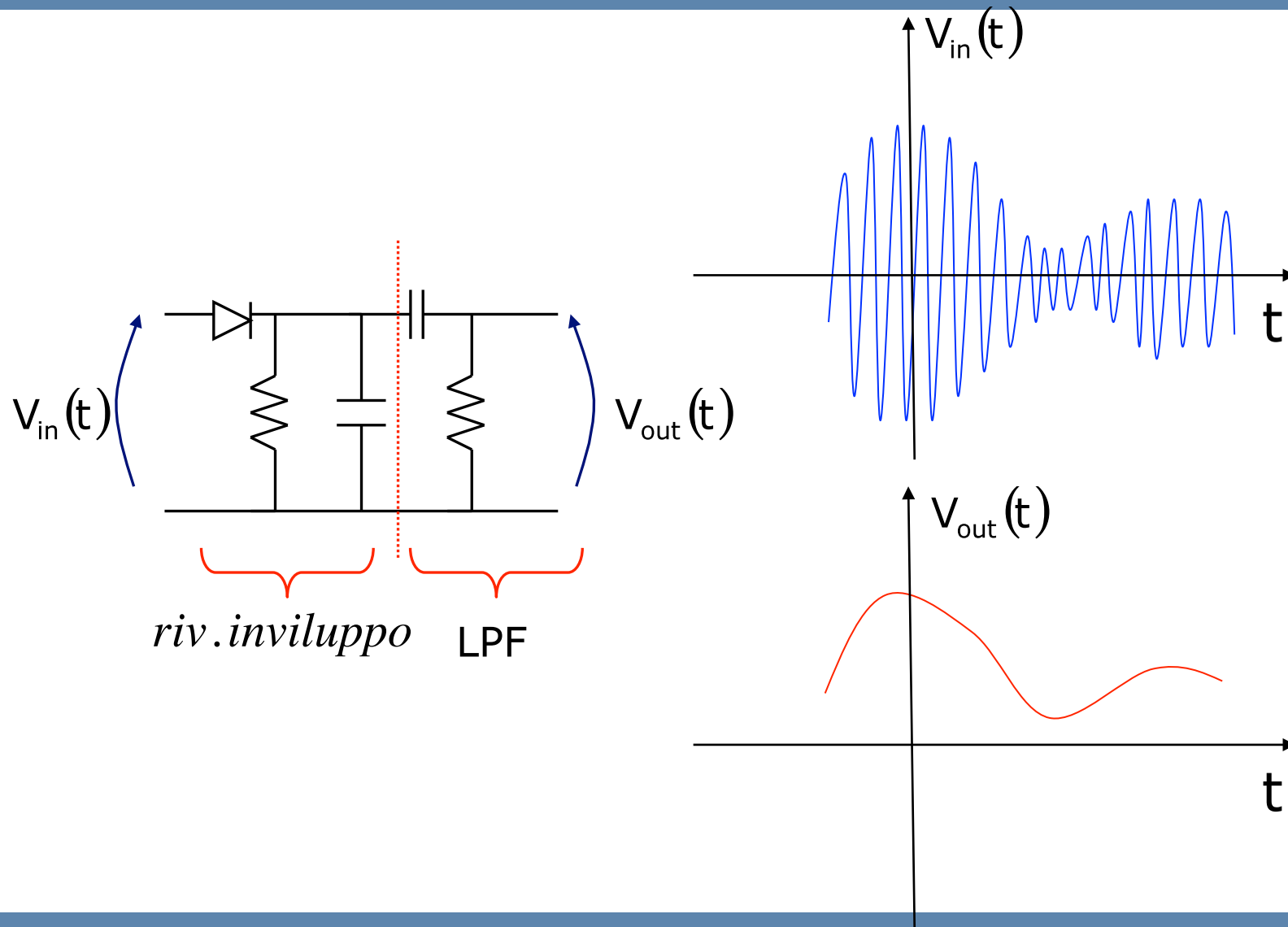
- Quadratic Modulator (Square law)

- Switching Modulator

# “Envelope” Demodulator (1)

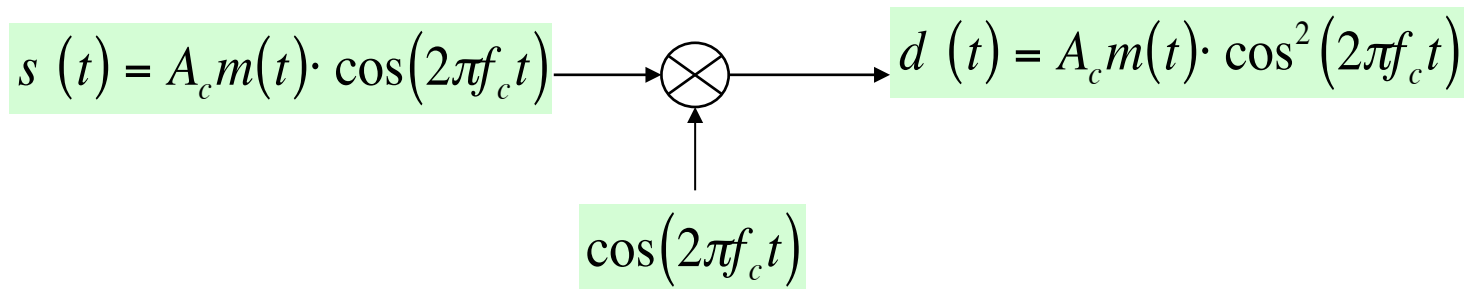
- Demodulation: it is the operation that allows for recovering  $m(t)$  from  $s(t)$
- In the case of amplitude modulation with transmitted carrier, we can obtain the “information” with a very simply demodulator, called “envelope” demodulator
- This demodulator is composed from a peak detector that discovers the envelope of the modulated signal.
- In the case of small modulation index ( $\mu \ll 1$ ) the performance are really good.

# “Envelope” Demodulator (2)



# Synchronous Demodulator (1)

- In the case of amplitude modulation with suppressed carrier, we can obtain the “information” with a synchronous demodulator.
- The modulated signal is multiplied with a co-sinusoidal at the same frequency and phase of the carrier

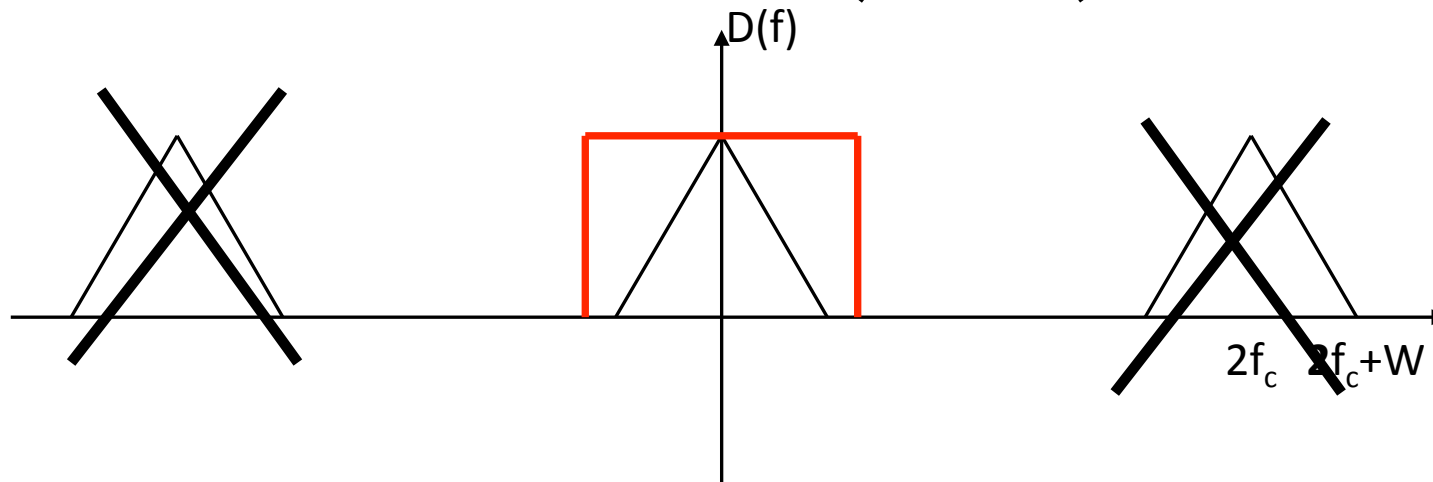


- Since  $\cos^2(\alpha) = \frac{(1 + \cos(2\alpha))}{2}$  we have  $d(t) = \frac{A_c}{2} m(t) \cdot (1 + \cos(2 \cdot 2\pi f_c t))$

# Synchronous Demodulator (2)

- Signal spectrum  $d(t)$

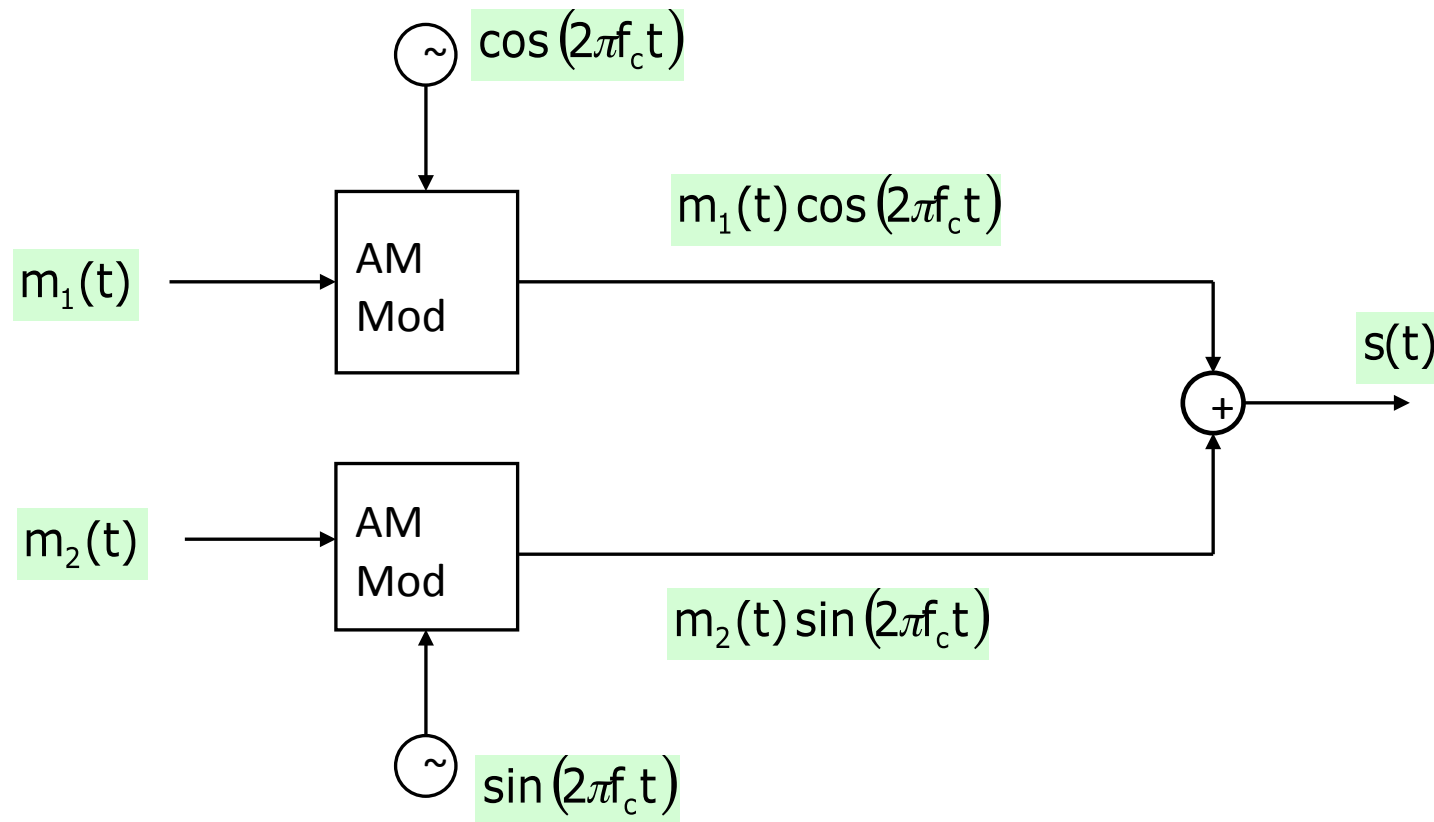
$$d(t) = \frac{A_c}{2} m(t) \cdot \left( 1 + \cos(2 \cdot 2\pi f_c t) \right)$$



- The signal can be obtained by filtering the signal with a simple low pass filter
- **N.B. I MUST know the characteristics of the carrier!!!**

# Quadrature Amplitude Modulation (QAM)

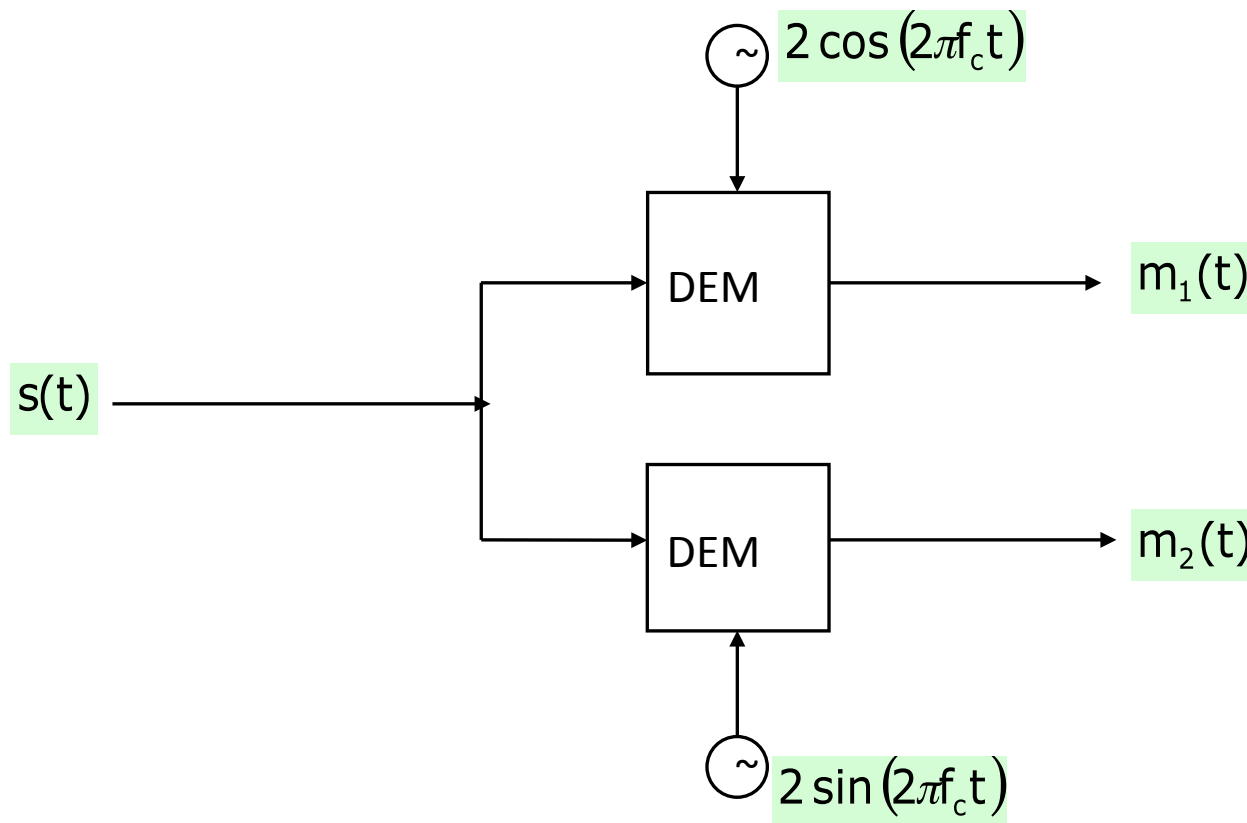
- The modulator simultaneously modules two signals  $m_1(t)$  and  $m_2(t)$  with two carries with a phase difference of  $\pi/2$





# QAM Demodulator (1)

- The demodulator simultaneously demodulates  $s(t)$  with two carries with a phase difference of  $\pi/2$



# Demodulator QAM (2)

- It's extremely important the SYNCRONISM, otherwise the two signal  $m_1(t)$  and  $m_2(t)$  will mix together.
- The sinusoidal signals must have not only the same FREQUENCY but also the same PHASE!!
- With these technique we have  $B_T = W$  like in the case of SSB
- In the case of SSB we CAN'T send two signals with the quadrature technique because the signal SSB occupies already both the orthogonal carriers

# Angular Modulation

- Angular Modulation

$$s(t) = A_c \cos(2\pi f_0 t + \varphi(t))$$

Where  $\varphi(t)$  is the “information” that we must transmit

- PHASE modulation

$$\varphi(t) = k_p \cdot m(t)$$

- FREQUENCY modulation

$$\varphi(t) = \int_{-\infty}^t k_F \cdot m(t') dt'$$

# Frequency Modulation FM

- Frequency Modulation (FM)

$$s_{FM}(t) = A_c \cos(\vartheta_i(t))$$

where  $\vartheta_i(t)$  is the instantaneous phase

- The instantaneous frequency of the FM signal changes in function of  $m(t)$

$$f_i(t) = f_c + k_F m(t)$$

where the instantaneous frequency is defined as the derivative of the instantaneous phase

$$f_i(t) = \frac{1}{2\pi} \frac{d\vartheta_i(t)}{dt}$$

# FM signal

- The instantaneous phase becomes

$$\vartheta_i(t) = 2\pi f_c t + 2\pi k_F \int_0^t m(\tau) d\tau$$

- So the FM signal is given by

$$s_{FM}(t) = A_c \cos\left(2\pi f_c t + 2\pi k_F \int_0^t m(\tau) d\tau\right)$$

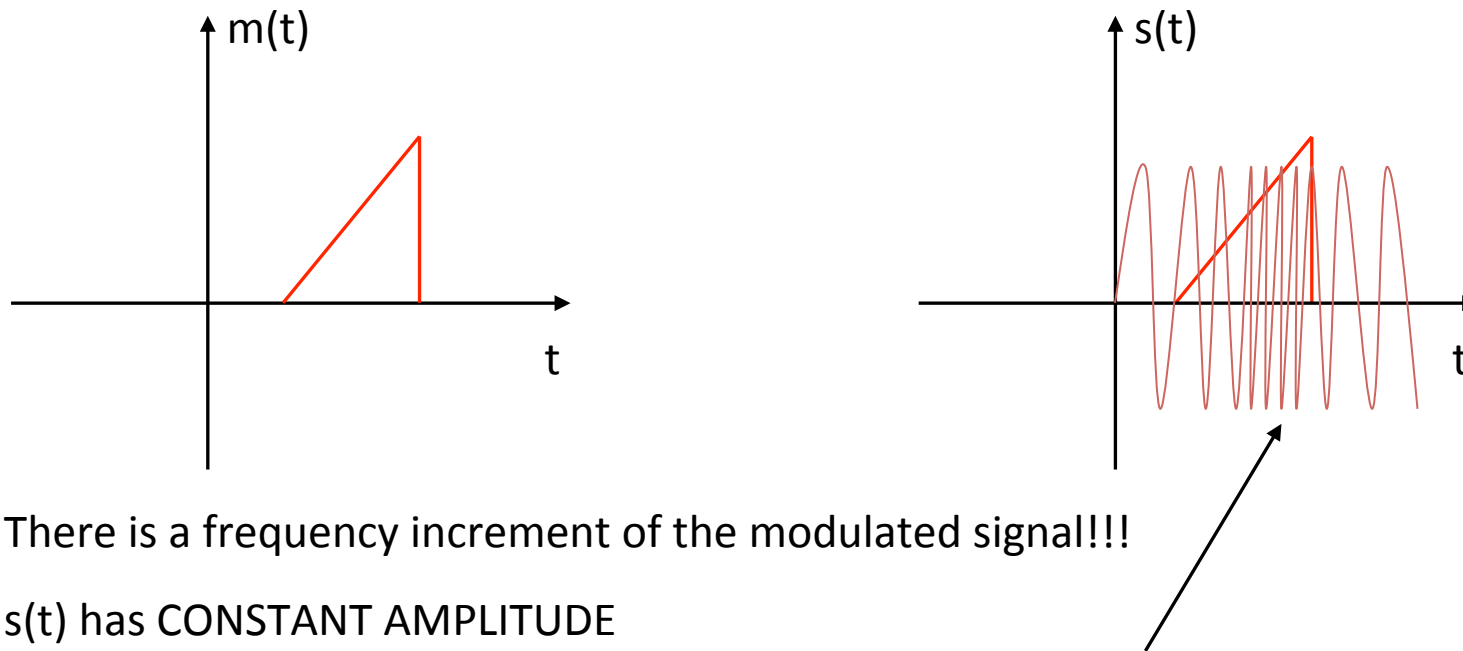
- The frequency deviation  $\Delta f$  is

$$\Delta f = \left|k_F m(t)\right|_{\max}$$

# Example

- The instantaneous frequency of the FM signal changes in function of  $m(t)$

$$f_i(t) = f_c + k_F m(t)$$



- There is a frequency increment of the modulated signal!!!
- $s(t)$  has CONSTANT AMPLITUDE

→ FM is ROBUST against NOT-LINEARITY!!!

# FM: single tone

- Particular case: single tone

$$m(t) = A_m \cos(2\pi f_m t)$$

- The FM signal becomes

$$s_{FM}(t) = A_c \cos\left(2\pi f_c t + \frac{k_f A_m}{f_m} \sin(2\pi f_m t)\right)$$

namely

$$s_{FM}(t) = A_c \cos\left(2\pi f_c t + \frac{\Delta f}{f_m} \sin(2\pi f_m t)\right), \quad \text{dove } \frac{\Delta f}{f_m} = \beta$$

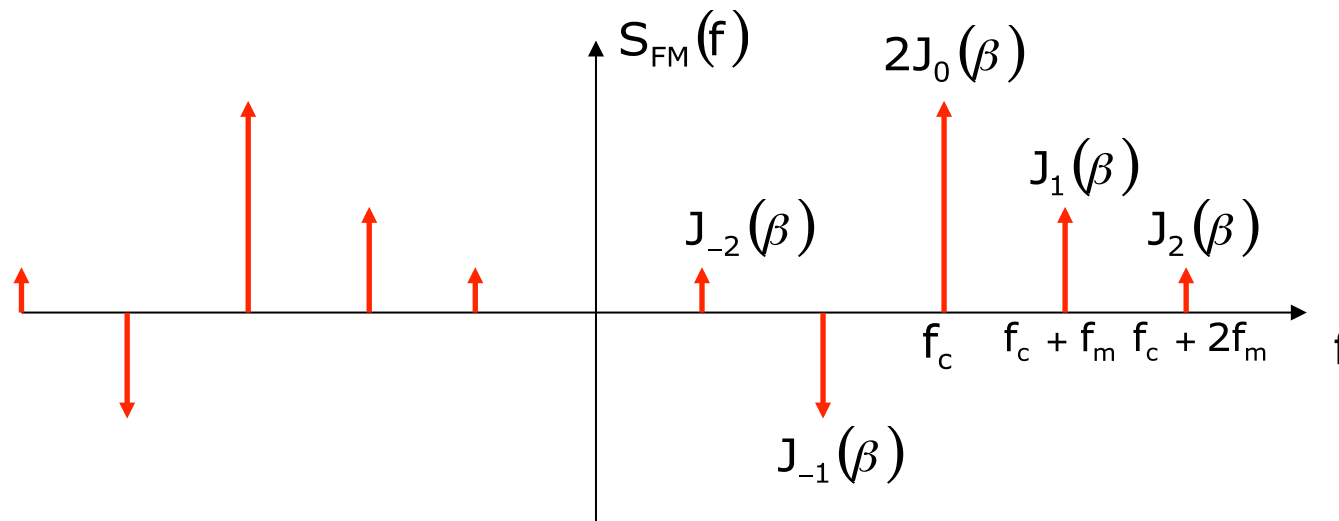
$\beta$  is the maximum frequency deviation

# FM signal's spectrum

- Ideally the spectrum has infinite band

$$S_{FM}(f) = \frac{A_c}{2} \sum_{n=-\infty}^{+\infty} J_n(\beta) \left[ \delta(f - f_c - nf_m) + \delta(f + f_c + nf_m) \right]$$

where  $J_n(\beta)$  are the Bessel's functions, that decrease very fast at the increasing of 'n' (even functions for even n, odd for odd n)





# Occupied band (1)

- In general the signal's band modulated with angular modulation is bigger than in the case of amplitude modulation.
- An approximated formula that returns the bandwidth is the Carson's formula:

$$B_T = 2f_{\max} + 2\Delta f$$

where  $\Delta f$  is the maximum frequency deviation and  $f_{\max}$  is the maximum frequency of the "information"

- The angular modulation needs more bandwidth than amplitude one, but has a better response to **noise** and at the **non-linearity** in the transmission channel.

# Occupied band (2)

- In the case  $\beta \ll 1$  (narrow band)

$$B_T = 2f_m$$

If the signal isn't at single frequency

$$B_T = 2f_{\max}$$

- In the case  $\beta \gg 1$  (strong amplitude deviation)

$$B_T = 2\Delta f$$

- Bandwidth (worst case): CARSON's approximation

$$B_T = 2f_{\max} + 2\Delta f$$

- In the case of single tone the Carson's bandwidth is equal to:

$$B_T = 2f_m + 2\Delta f$$

# FM Modulator

- VCO

Oscillator controlled in voltage



- VCO issues:

Stability in frequency

→ Usually the VCO is controlled/implemented with a feedback loop

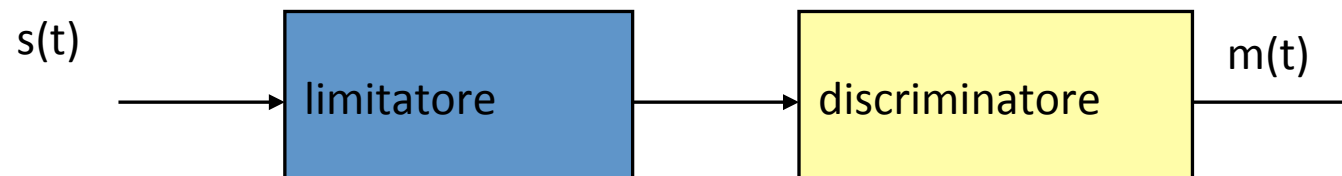
# FM De-modulator

- It's a kind of inverse VCO made of

- clipping stage

- frequency discriminator

always in series

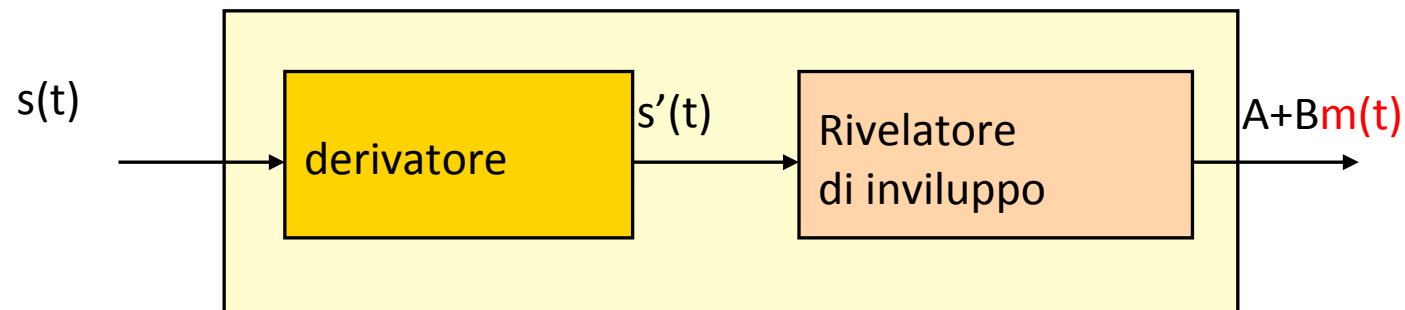


Limit control:

- it's necessary to make the amplitude of the FM signal constant (clipping)

# Frequency discriminator (1)

- The discriminator is made of
  - derivator
  - envelope detector
- always in series



# Frequency discriminator (2)

- Now the FM signal is equal

$$s(t) = A_c \cos\left(2\pi f_c t + 2\pi k_F \int_0^t m(\tau) d\tau\right)$$

- At the output of the derivator

$$s'(t) = -A_c \sin\left(2\pi f_c t + 2\pi k_F \int_0^t m(\tau) d\tau\right) \cdot [2\pi f_c t + 2\pi K_F m(t)]$$

- The calculation of the complex envelope of  $s'(t)$  return the signal

$$A_c \cdot [2\pi f_c t + 2\pi K_F m(t)] = A + B m(t)$$

And we recovered the information  $m(t)$ !

# Comparison between modulations (1)

## ▪ AMPLITUDE MODULATION (AM)

### - classic AM (with transmitted carrier)

→ Envelope Demodulator (simple)

→  $B_T = 2W$

→ Waste of carrier's power

→ Sensible to the NON-linearity

→ Use: AM radio

### - DSB-SC (Double SideBand Suppressed Carrier transmission)

→ Synchronous Demodulation

→  $B_T = 2W$ , but I can implement the QAM

→ Sensitive to the NON-linearity

# Comparison between modulations (2)

- SSB (AM with Suppressed Side Band )

- Filter is difficult to assemble

- $B_T = W$ , it ISN'T possible use the QAM

- **FREQUENCY MODULATION**

- FM advantage

- Robust against the NON-linearity and to the NOISE

- Not too difficult to implement

- Particularly indicated when we have LITTLE power

- (saturation amplifier)

$$B_T = 2f_{\max} + 2\Delta f$$

- FM disadvantage

- Huge use of the bandwidth!!!



# Use of the analogue modulations (1)

- AM

- Radio Broadcasting

- SSB

- TV signal distribution

- Telephone channels on coaxial cable (FDM)

- QAM

- Numeric Transmission

# Use of the analogue modulations (2)

## - FM

- Radio Stereo
- Transmission by SATELLITE and RADIO BRIDGE
- Contribution in the TV signal
- Optic and magnetic recording
- Audio for TV
- ...
- SPACE transmissions
- Radio mobile Transmissions

## - PM

- Numeric Transmission