



EMIMEO : E(rasmus) Mundus on Innovative Microwave Electronics and Optics Master

Foundations of Electromagnetic Wave Propagation – 2nd part

Contributors:

Olivier Tantot
Guillaume Neveux
Serge Verdeyme



UNIVERSITÀ
DEGLI STUDI
DI BRESCIA



Foundations of electromagnetic wave propagation

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Chapters:

0. Microwave domain
1. S-parameters and transmission line
 - a. Microwave signals - time and frequency domains
 - b. Description of microwave devices by scattering parameters
 - c. Exercices on the parameters S
 - d. Description of microwave devices by chain matrix
2. Theory of transmission lines
3. Smith Chart and impedance matching
 - a. Introduction, uses and principles
 - b. Movement along the line
 - c. Different methods for impedance matching
 - d. Matching by a stub
 - e. Matching by double stubs

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2. Transmission line

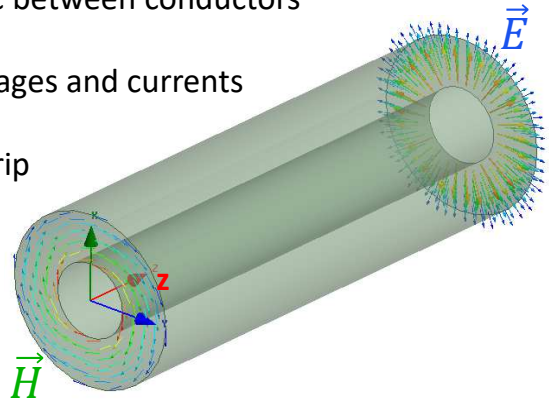
1. Theory of lines



Main goal : to study the propagation lines « TEM lines »

TEM lines (Transverse Electric and Magnetic):

- Electric and magnetic fields : contained in the plane which is perpendicular to the conductor (no longitudinal component of the field, $H_z = 0$, $E_z = 0$)
-:
depends on the dimensions and of the dielectric between conductors
- Allows to determine along the conductors, voltages and currents
- applications : coaxial lines, bifilar lines, microstrip or coplanar line and stripline



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2. Transmission line

2. Theory of lines - model



Modelization method ^[1]:

- Application of the "voltage-current" concept
- TEM line assimilated to a circuit of elements in networks
 - length L
 - powered by a HF generator with internal impedance Z_G at one end
 - Closed by a termination (load impedance) Z_R at the other end

Transmission line schematic:

[1] David M. Pozar, Microwave Engineering, Third Edition, John Wiley & Sons Inc.

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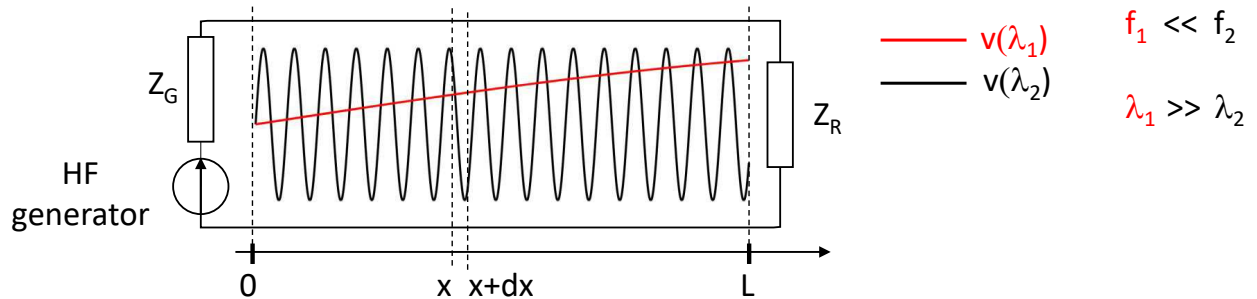
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2. Transmission line

3. Theory of lines - model

Modelization method:

Transmission line diagram:



in HF, $L \gg \lambda$ (wavelength $\lambda = c/f$)

-
- LF case ($L \ll \lambda$) is different: quasi-stationary state approximation is applied

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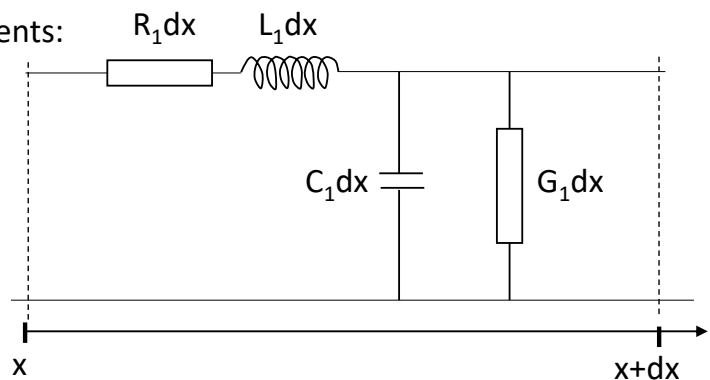
2. Transmission line

4. Theory of lines - model

Modelization method:

- TEM line assimilated to a circuit of elements in networks:

Decomposition of the line in identical elements:



- of a length $dx \ll \lambda$
- quadripoles with localized constants:
 R_1, L_1, G_1, C_1 of the line
- allows to model the voltage-current wave variations in space and time along the line

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2. Transmission line

5. Theory of lines - model

Modelization method:

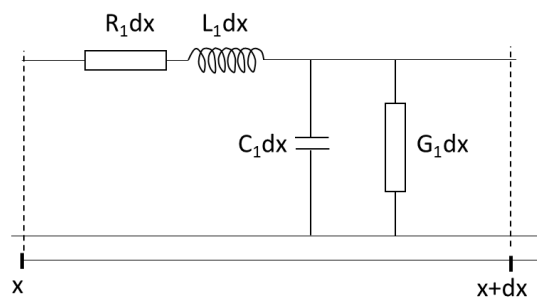
- TEM line assimilated to a circuit of elements in networks: R_1, L_1, G_1, C_1

R_1 : (Ω/m)

L_1 : (H/m)

C_1 :
..... (F/m)

G_1 :
..... (S/m)



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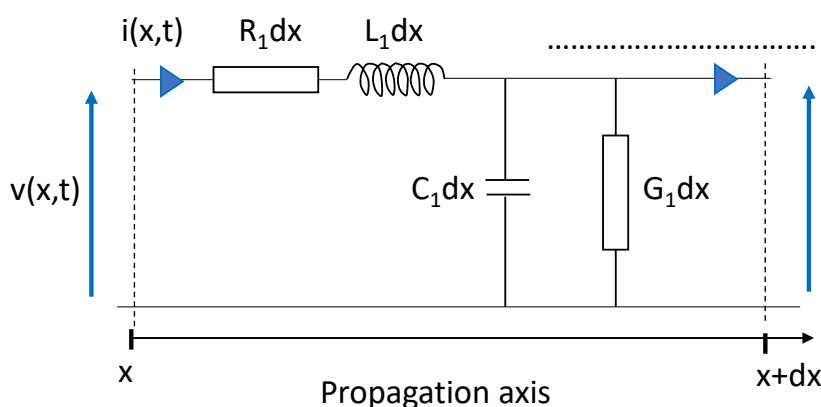
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2. Transmission line

6. Theory of lines - model

General case : lines with losses

- study of the element included between x and $x+dx$



Propagation effect neglected $dt = 0$ for $dx \ll \lambda$

From Kirchoff's laws (law of meshes and knots), we obtain [1]:

$$-L_1 C_1 \frac{\partial^2 v}{\partial t^2} + \frac{\partial^2 v}{\partial x^2} = (R_1 C_1 + G_1 L_1) \frac{\partial v}{\partial t} + R_1 C_1 v \quad -L_1 C_1 \frac{\partial^2 i}{\partial t^2} + \frac{\partial^2 i}{\partial x^2} = (R_1 C_1 + G_1 L_1) \frac{\partial i}{\partial t} + R_1 C_1 i$$

Telegraphers' equations

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2. Transmission line

7. Theory of lines - model

In the sinusoidal regime, we use the complex notation to :

- dissociate the temporal contribution from the geometrical one
- Solve the propagation equations

$$v(x, t) = R_e \left(\underline{v}(x, t) \right) = V(x) \cos(\omega t + \varphi_v(x))$$

$$i(x, t) = R_e \left(\underline{i}(x, t) \right) = I(x) \cos(\omega t + \varphi_i(x))$$

with $\underline{v}(x, t) = \underline{V}(x) e^{j\omega t}$ and

$\underline{i}(x, t) = \underline{I}(x) e^{j\omega t}$ and

$V(x)$ and $I(x)$ which are the real magnitudes (modulus) of v and i
 $\varphi_v(x)$ and $\varphi_i(x)$ which are the phases of v and i

2. Transmission line

8. Theory of lines – voltage and current propagation equations

$$-L_1 C_1 \frac{\partial^2 v}{\partial t^2} + \frac{\partial^2 v}{\partial x^2} = (R_1 C_1 + G_1 L_1) \frac{\partial v}{\partial t} + R_1 C_1 v$$

$$-L_1 C_1 \frac{\partial^2 i}{\partial t^2} + \frac{\partial^2 i}{\partial x^2} = (R_1 C_1 + G_1 L_1) \frac{\partial i}{\partial t} + R_1 C_1 i$$

The equations of the telegraphers in sinusoidal regime become:

$$\frac{\partial^2 \underline{V}(x)}{\partial x^2} = (R_1 + jL_1\omega)(G_1 + jC_1\omega)\underline{V}(x) \text{ and } \frac{\partial^2 \underline{I}(x)}{\partial x^2} = (R_1 + jL_1\omega)(G_1 + jC_1\omega)\underline{I}(x)$$

we set that

The equations become:

and

.....

Equations for voltage and current propagation along the line

2. Transmission line

9. Theory of lines – secondary parameters



Equations for voltage and current propagation along the line

$$\frac{\partial^2 \underline{V}(x)}{\partial x^2} = \gamma^2 \underline{V}(x) \quad \text{and} \quad \frac{\partial^2 \underline{I}(x)}{\partial x^2} = \gamma^2 \underline{I}(x)$$

Linear propagation constant, of the line

$$\gamma = \sqrt{(R_1 + jL_1\omega)(G_1 + jC_1\omega)}$$

The solutions of the two propagation equations are:

.....

and

.....

2. Transmission line

10. Theory of lines – secondary parameters



The current can also be expressed from the voltage:

$$\underline{I}(x) = \frac{V_i}{Z_c} e^{-\gamma x} - \frac{V_r}{Z_c} e^{\gamma x}$$

We then deduce the following relations:

$$\frac{V_i}{I_i} = -\frac{V_r}{I_r} = Z_c$$

with

.....

where Z_c is the characteristic impedance of the
2nd of the line

2. Transmission line

11. Theory of lines - superposition of two waves

Evidence of the superposition of two waves:

we set:

$$\gamma = \sqrt{(R_1 + j\omega L_1)(G_1 + jC_1\omega)} = \alpha + j\beta$$

α : linear attenuation coefficient
 β : linear coefficient of phase shift
 positive constants (physically)

Let's write again $\underline{v}(x,t)$:

$$\underline{v}(x, t) = \underline{V}(x)e^{j\omega t}$$

let's have: $\underline{v}(x, t) = \underline{V}_i e^{-\gamma x} e^{j\omega t} + \underline{V}_r e^{+\gamma x} e^{j\omega t}$

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2. Transmission line

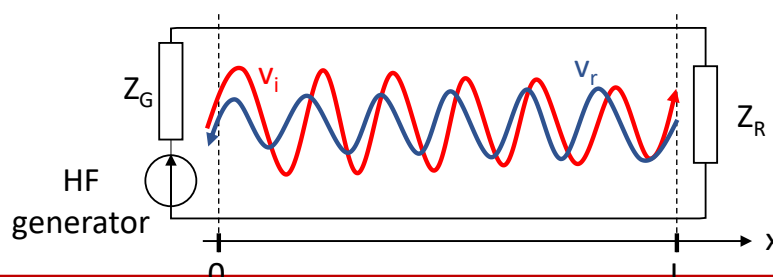
12. Theory of lines - superposition of two waves

Evidence of the superposition of two waves:

Taking into account the linear coefficients α and β , we obtain:

α is positive or null and $x >$

$$\underline{v}(x, t) = \underbrace{V_i e^{-\alpha x} e^{j(-\beta x + \omega t + \varphi_i)}}_{\text{incident wave}} + \underbrace{V_r e^{+\alpha x} e^{j(\beta x + \omega t + \varphi_r)}}_{\text{reflected wave}}$$



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2. Transmission line

13. Theory of lines - wave characteristics

Wave characteristics:

Consider the incident wave: $\underline{v}_i(x, t) = V_i e^{-\alpha x} e^{j(\omega t - \beta x + \varphi_i)}$

In real instantaneous real expression $v_i(x, t) = V_i e^{-\alpha x} \cos(\omega t - \beta x + \varphi_i)$
Note the double space-time periodicity

At a point on the line, the voltage is a sinusoidal function of periodicity in time:

$$T = \frac{2\pi}{\omega} \quad \text{x fixed, TEMPORAL PERIOD}$$

At a given time, the voltage is a sinusoidal function of x of periodicity in space:

$$\lambda = \frac{2\pi}{\beta} \quad \text{t fixed, SPATIAL PERIOD}$$

2. Transmission line

14. Theory of lines - wave characteristics

Wave characteristics:

Phase velocity is defined as the speed at which the wave moves at constant phase:

Given the phase: $\Phi = \omega t - \beta x + \varphi_i$

Its total differential is written (for constant phase) $d\Phi = \omega dt - \beta dx = 0$

then : $\omega dt = \beta dx$ therefore: $v_\varphi = \frac{\omega}{\beta} = \frac{dx}{dt}$ **PHASE VELOCITY**

Remark :

- the study of the reflected wave leads to the same results
- V_i and V_r are called AMORTED PROGRESSIVE WAVES

.....

2. Transmission line

15. Theory of lines - wave characteristics

Paramètre de propagation

$$\gamma = \alpha + j\beta$$

➤ Particular case : line without loss (LWL), then $R_1 = 0$ and $G_1 = 0$

$$\gamma = \sqrt{(j\omega L_1)(jC_1\omega)} = j\omega\sqrt{L_1 C_1} = \alpha + j\beta$$

so : $\beta = \omega\sqrt{L_1 C_1}$ $\alpha = 0$ **Wave propagation without attenuation**

and : $v = \frac{1}{\sqrt{L_1 C_1}}$

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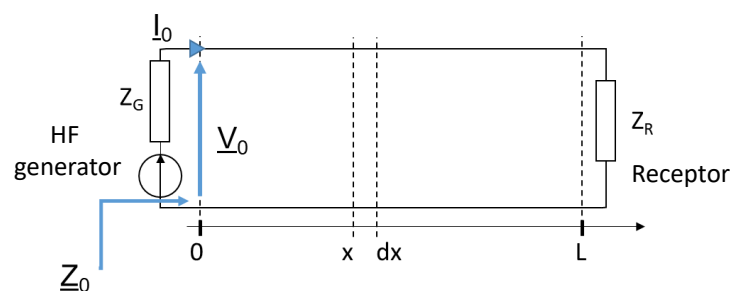
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2. Transmission line

16. Theory of lines - voltage current and impedance along a line

Voltage and current along the line (with losses)

from the previous equations



$$\underline{V}(x) = \underline{V}_0 \cosh \gamma x - \underline{Z}_C \underline{I}_0 \sinh \gamma x$$

$$\underline{I}(x) = -\frac{\underline{V}_0}{\underline{Z}_C} \sinh \gamma x + \underline{I}_0 \cosh \gamma x$$

$$\underline{Z}(x) = \frac{\underline{V}(x)}{\underline{I}(x)} = \underline{Z}_C \frac{\underline{Z}_0 - \underline{Z}_C \tanh \gamma x}{\underline{Z}_C - \underline{Z}_0 \tanh \gamma x}$$

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2. Transmission line

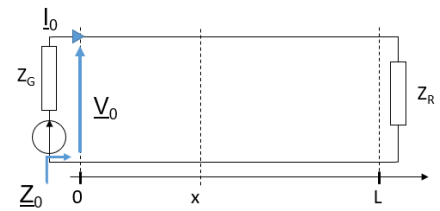
17. Theory of lines - voltage current and impedance along a line

Particular case: line without losses (LWL), $\alpha = 0$ and $\gamma = j\beta$

$$\underline{V}(x) = \underline{V}_0 \cos \beta x - j \underline{Z}_C \underline{I}_0 \sin \beta x$$

$$\underline{I}(x) = -j \frac{\underline{V}_0}{\underline{Z}_C} \sin \beta x + \underline{I}_0 \cos \beta x$$

$$\underline{Z}(x) = \underline{Z}_C \frac{\underline{Z}_0 - j \underline{Z}_C \operatorname{tg} \beta x}{\underline{Z}_C - j \underline{Z}_0 \operatorname{tg} \beta x}$$



with:

$$\begin{aligned} \operatorname{ch} \gamma x &= \operatorname{ch} j \beta x = \cos \beta x \\ \operatorname{sh} \gamma x &= \operatorname{sh} j \beta x = j \sin \beta x \\ \operatorname{th} \gamma x &= \operatorname{th} j \beta x = j \operatorname{tg} \beta x \end{aligned}$$

2. Transmission line

18. Theory of lines - voltage current and impedance along a line

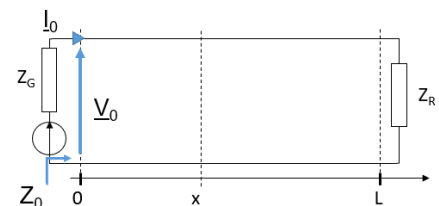
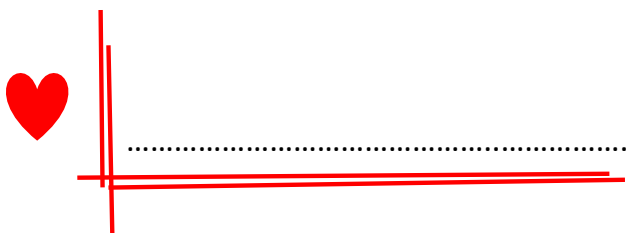


Input impedance ($x=0$) of the line as a function of the load impedance $Z(x=L)=Z_R$

from :

$$\underline{Z}_R = \underline{Z}(x = L) = \underline{Z}_C \frac{\underline{Z}_0 - \underline{Z}_C \operatorname{th} \gamma L}{\underline{Z}_C - \underline{Z}_0 \operatorname{th} \gamma L}$$

We deduce the input impedance of the line:



2. Transmission line

19. Theory of lines - line ended by Z_C

Line terminated by $\underline{Z}_R = \underline{Z}_C$

we write: $\underline{Z}_0 = \underline{Z}_C \frac{\underline{Z}_C + \underline{Z}_C \tanh \gamma L}{\underline{Z}_C + \underline{Z}_C \tanh \gamma L}$ then: $\underline{Z}_0 = \underline{Z}_C$

Everything happens as if the generator was directly closed on \underline{Z}_C

Using the expression for $\underline{Z}(x)$, on obtient :

$\underline{Z}(x) = \underline{Z}_C$



At any point on the line, the impedance is equal to \underline{Z}_C

2. Transmission line

20. Theory of lines - line ended by Z_C

Line terminated by $\underline{Z}_R = \underline{Z}_C$

with : $\underline{V}(x) = \underline{V}_0 e^{-\gamma x}$
 $\underline{I}(x) = \underline{I}_0 e^{-\gamma x}$



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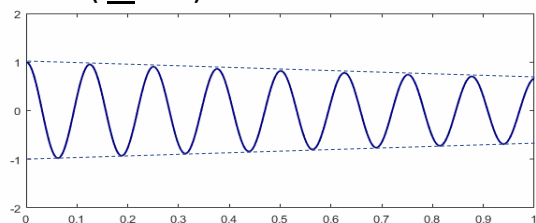
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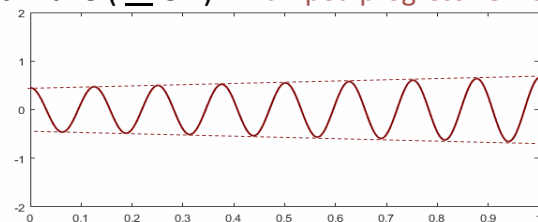
21. Theory of lines - line ended by Zc

General case

Incident wave ($\underline{V}_i.e^{-\gamma x}$) : Damped progressive wave

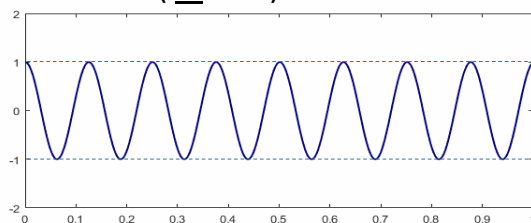


Reflected wave ($\underline{V}_r.e^{\gamma x}$) : Damped progressive wave

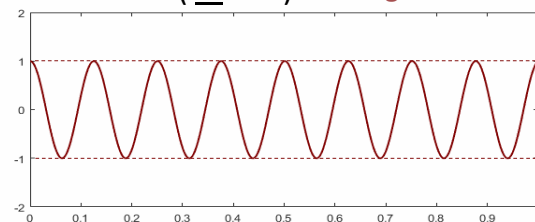


Case of the line without losses

Incident wave ($\underline{V}_i.e^{-j\beta x}$) : Progressive wave



Reflected wave ($\underline{V}_r.e^{j\beta x}$) : Progressive wave



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