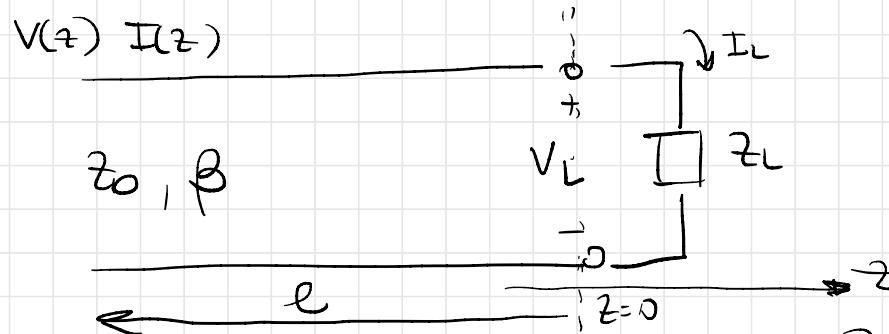


# MICROWAVE ENGINEERING

Lecture 8:

Terminated  
Transmission  
lines

## TERMINATED LOSSLESS TRANSMISSION LINE



If the line is terminated on a load  $z_L \neq z_0 \Rightarrow$  The ratio  $\frac{V}{I}$  at the load is  $\Gamma$

A reflected wave is generated



at the load  
is  $\Gamma$

$$\left\{ \begin{array}{l} V(z) = V_0^+ e^{-j\beta z} + V_0^- e^{j\beta z} \\ I(z) = \frac{V_0^+}{Z_0} e^{-j\beta z} - \frac{V_0^-}{Z_0} e^{j\beta z} \end{array} \right.$$

At the load ( $z=0$ )  $\frac{V(0)}{I(0)} = Z_L$

It follows:

$$Z_L = \frac{V_0^+ + V_0^-}{V_0^+ - V_0^-} \cdot Z_0 \Rightarrow V_0^- = \frac{Z_L - Z_0}{Z_L + Z_0} V_0^+$$

VOLTAGE REFLECTION COEFFICIENT  $\Gamma$  ( $z=0$ )

$$\boxed{\Gamma = \frac{V_0^-}{V_0^+} = \frac{Z_L - Z_0}{Z_L + Z_0}}$$

So we can re-write:

$$V(z) = V_0 + [e^{-j\beta z} + \Gamma e^{j\beta z}]$$

$$I(z) = \frac{V_0}{Z_0} [e^{-j\beta z} - \Gamma e^{j\beta z}]$$

|| Standing waves  
= superposition  
of FW and  
BW waves

If the LOAD IS MATCHED to the line, i.e.,  $Z_L = Z_0$

$$\boxed{\Gamma = 0}$$

Time averaged power flow at a generic point ( $z$ ) :-

$$P_{av} = \frac{1}{2} \operatorname{Re} [V(z) I(z)^*] =$$

$$= \frac{1}{2} \frac{|V_o^+|^2}{Z_0} \operatorname{Re} \left\{ 1 - \Gamma^* e^{-2j\beta z} + \Gamma e^{2j\beta z} - |\Gamma|^2 \right\}$$

~~~~~  
purely imaginary terms

$$P_{AV} = \frac{1}{2} \frac{|V_o^+|^2}{Z_0} [1 - |\Gamma|^2]$$

NOTE 1  $P_{AV}$  IS CONSTANT ALONG THE LINE

NOTE 2 Max power transfer occurs for  $\Gamma = 0$   
No power is delivered if  $\Gamma = 1$

The power that is NOT DELIVERED TO THE LOAD is called  
RETURN LOSS (RL) =  $-20 \log |\Gamma| \text{ dB}$

If  $\Gamma = 0 \rightarrow RL = \infty \text{ dB}$

$\Gamma = 1 \rightarrow RL = 0 \text{ dB}$

If  $\Gamma = 0 \quad |V(z)| = V_0^+ \rightarrow \text{constant along the line}$

If  $\Gamma \neq 0$  we have a standing wave

$$|V(z)| = V_0^+ \left| 1 + \Gamma e^{2j\beta z} \right| = |V_0^+| \left| 1 + \Gamma e^{-2j\beta z} \right| =$$
$$= |V_0^+| \left| 1 + |\Gamma| e^{j(\theta - 2\beta z)} \right|$$

$\nearrow z = -l$   
 $\searrow \text{distance from the load}$

$$\Gamma = |\Gamma| e^{j\phi}$$

The voltage oscillates between

$$V_{\max} = |V_0^+| (1 + |\Gamma|)$$

$$V_{\min} = |V_0^+| (1 - |\Gamma|)$$

A measure of the mismatch on the line is the

$$\text{STANDING WAVE RATIO (SWR)} = \frac{V_{\max}}{V_{\min}} = \frac{1+|\Gamma|}{1-|\Gamma|}$$

The distance between two voltage maxima or minima is:

$$\text{imposing } 2\pi \ell = 2\pi$$

$$\ell = \frac{2\pi}{2B} = \frac{\pi \lambda}{2\pi} = \frac{\lambda}{2}$$

The distance between a maximum and a minimum by inspection

$$2\pi d = \pi$$

At any point on the line we can calculate the reflection coefficient at  $z = -l$

$$\Gamma(-l) = \frac{V_0^- e^{-j\beta l}}{V_0^+ e^{j\beta l}} = \Gamma(0) e^{-2j\beta l} = \frac{Z_L - Z_0}{Z_L + Z_0} e^{-2j\beta l}$$

We can also calculate the impedance at any point on the line:

$$Z_{IN} = Z(-l) = \frac{V(-l)}{I(-l)} = \frac{V_0^+ [e^{j\beta l} + \Gamma e^{-j\beta l}]}{V_0^+ [e^{j\beta l} - \Gamma e^{-j\beta l}]} \quad Z_0 =$$

$$= Z_0 \frac{1 + \Gamma e^{-2j\beta l}}{1 - \Gamma e^{-2j\beta l}}$$

knowing  
 $\Gamma = \frac{z_L - z_0}{z_L + z_0}$

we replace  $\Gamma$   
 $\rightarrow$

$$Z_{IN} = z_0 \frac{(z_L + z_0) e^{j\beta L} + (z_L - z_0) e^{-j\beta L}}{(z_L + z_0) e^{j\beta L} - (z_L - z_0) e^{-j\beta L}}$$

$$= z_0 \frac{z_L \cos\beta L + j z_0 \sin\beta L}{z_0 \cos\beta L + j z_L \sin\beta L}$$

=

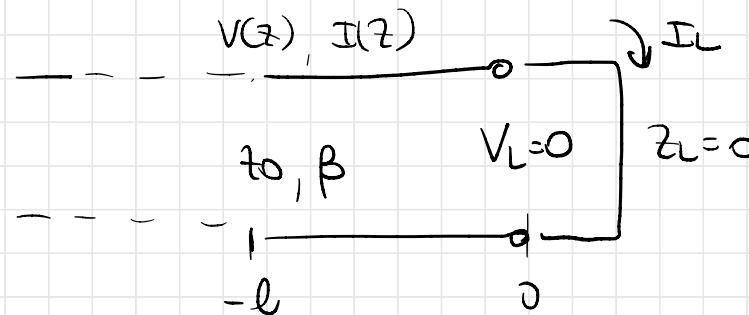
$$= \boxed{z_0 \frac{z_L + j z_0 \tan\beta L}{z_0 + j z_L \tan\beta L}}$$

TRANSMISSION LINE  
IMPEDANCE

## SPECIAL CASES

$$\textcircled{1} \quad z_L = 0$$

SHORT  
CIRCUIT  
TERMINATION

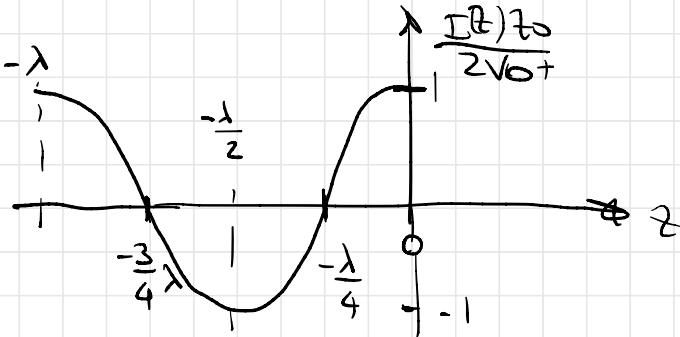
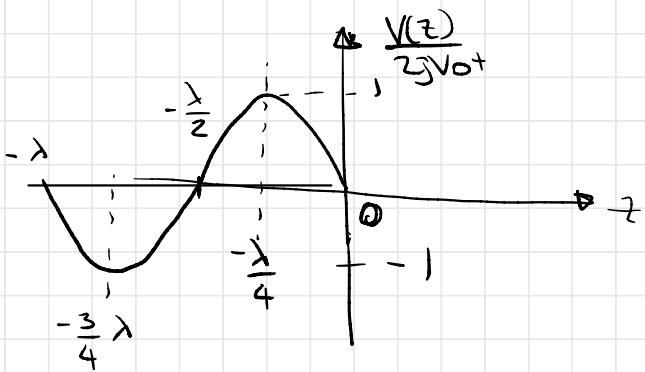


$$\Gamma = \frac{z_L - z_0}{z_L + z_0} = -1$$

$$\text{SWR} = \frac{1 + \Gamma}{1 - \Gamma} = \infty$$

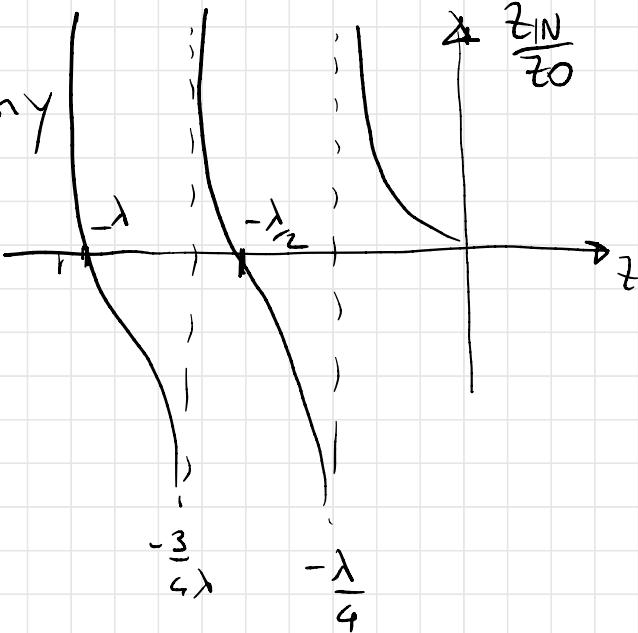
$$V(z) = V_0^+ [e^{-j\beta z} - e^{j\beta z}] = -2jV_0^+ \sin\beta z$$

$$I(z) = \frac{V_0^+}{z_0} [e^{-j\beta z} + e^{j\beta z}] = 2\frac{V_0^+}{z_0} \cos\beta z$$



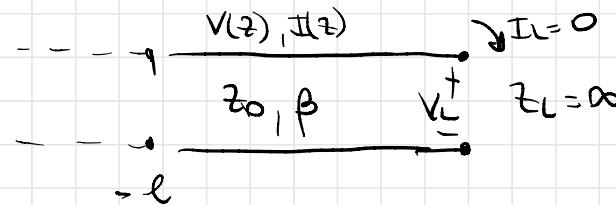
$$z_{IN} = jz_0 \tan \beta L$$

$\leftarrow$  purely imaginary



$$\textcircled{2} \quad \boxed{z_L = \infty}$$

OPEN CIRCUIT  
TERMINATION

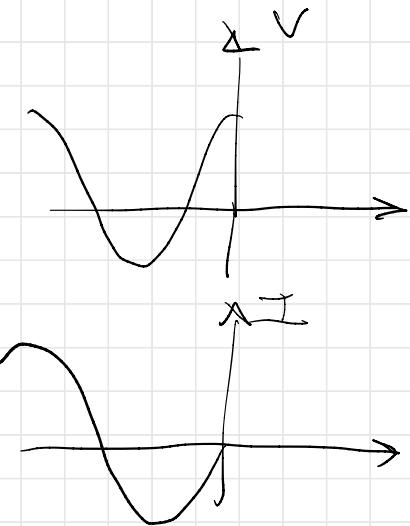


$$\Gamma = \frac{z_L - z_0}{z_L + z_0} = \frac{1 - \frac{z_0}{z_L}}{1 + \frac{z_0}{z_L}} = 1$$

$$\text{SWR} = \frac{1 + |\Gamma|}{1 - |\Gamma|} = \infty$$

$$V(z) = V_0^+ \left[ e^{-j\beta z} + e^{j\beta z} \right] = 2V_0 \cos \beta z$$

$$I(z) = \frac{V_0^+}{z_0} \left[ e^{-j\beta z} - e^{j\beta z} \right] = -\frac{2j}{z_0} V_0^+ \sin \beta z$$



$$Z_N = -j Z_0 \cot \beta l \quad \leftarrow \text{purely imaginary}$$

$$\boxed{③ \quad l = \frac{\lambda}{2}}$$

$$\beta l = \frac{2\pi}{\lambda} \cdot \frac{\lambda}{2} = \pi \Rightarrow \tan \beta l = \tan \pi = 0 \Rightarrow \boxed{Z_{IN} = Z_L}$$

$$\boxed{④ \quad l = \frac{\lambda}{4}}$$

$$\beta l = \frac{2\pi}{\lambda} - \frac{\lambda}{4} = \frac{\pi}{2} \Rightarrow \tan \beta l = \tan \frac{\pi}{2} = \infty$$

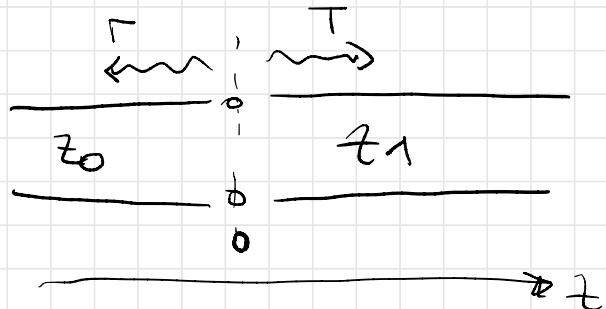
$$\underline{Z_{IN} = Z_0 \frac{Z_L + j Z_0 \tan \beta l}{Z_0 + j Z_L \tan \beta l}} = Z_0 \frac{\cancel{Z_L} + j Z_0 \cancel{\tan \beta l}}{\cancel{Z_0} + j \cancel{Z_L} \cancel{\tan \beta l}} = \frac{Z_0^2}{Z_L}$$

$$\boxed{Z_{IN} = \frac{Z_0^2}{Z_L}}$$

## QUARTER WAVE TRANSFORMER

### ⑤ JUNCTION BETWEEN TWO LINES

$$\Gamma = \frac{Z_1 - Z_0}{Z_1 + Z_0}$$



How do we calculate the portion of wave that is transmitted

$$\text{for } z < 0 \quad V(z) = V_0^+ (e^{-j\beta z} + \Gamma e^{j\beta z})$$

$$\text{for } z > 0 \quad V(z) = V_0^+ T e^{-j\beta z}$$

At  $z=0$

$$T = 1 + \Gamma = 1 + \frac{Z_1 - Z_0}{Z_1 + Z_0} \leq \frac{2Z_1}{Z_1 + Z_0}$$

## INSERTION LOSS

$$IL = -20 \log_{10} |T| \text{ dB}$$